



Research article

Integrated design workflow and a new tool for urban rainwater management

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ARTICLE INFO

Article history:

Received 24 July 2015

Received in revised form

11 April 2016

Accepted 28 April 2016

Keywords:

Decision-making tool

Rainwater management

Stormwater runoff

LID

Integrated design

Bioretention

ABSTRACT

Low Impact Development (LID) practices provide more sustainable solutions than traditional piping and storm ponds in stormwater management. However, architects are not equipped with the knowledge to perform runoff calculations at early design stage. In response to this dilemma, we have developed an open-source stormwater runoff evaluation and management tool, Rainwater+. It is seamlessly integrated into computer-aided design (CAD) software to receive instant estimate on the stormwater runoff volume of architecture and landscape designs. Designers can thereby develop appropriate rainwater management strategies based on local precipitation data, specific standards, site conditions and economic considerations. We employed Rainwater+ to conduct two case studies illustrating the importance of considering stormwater runoff in the early design stage. The first case study showed that integrating rainwater management into design modeling is critical for determining LID practice at any specific site. The second case study demonstrated the need of visualizing runoff flow direction in assisting the placement of LID practices at proper locations when the terrain is of great complexity.

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1. Introduction

With the rapid progress of urbanization, environmental deterioration and ecological destruction in urban areas are becoming the bottleneck of sustainable urban growth (Cohen, 2006; Grimmond, 2007; Hubacek et al., 2009; Tong et al., 2015, 2016a, 2016b). The increased impervious surfaces associated with city development have consistently shown to result in degraded aquatic ecosystems (Carter and Jackson, 2007; Hsieh and Davis, 2005; Lee and Bang, 2000; Miltner et al., 2004). The replacement of vegetated areas that provide rainwater interception and storage often results in an increase in the rate and volume of stormwater runoff (Kim et al., 2003; Mansell, 2003; Whitford et al., 2001). The subsequent urban flooding with increased frequency and severity is exacerbated by the climate change, which causes amplified magnitude of rainfall intensity in some parts of the world (Dore, 2005; Villarreal et al., 2004). The resultant urban flooding causes exceptionally severe damage where massive, rapid urbanization is occurring due to poorly engineered infrastructure (Huong and Pathirana, 2011; Liu, 2009; Wang, 2001). To address this urgent

concern, it is crucial for architects and landscape designers to have a greater understanding and modeling capability of stormwater runoff to face the increasing risks in the future.

In regard to strategies for reducing high runoff and harvesting of rainwater as an alternative water supply source, the conventional strategy—using piping to partially offset the environmental damage of impervious surfaces—is becoming obsolete because of its limited effect on drainage capacity and pollution control, as well as the high costs and disturbance to local neighborhoods (EPA, 2000). As a result, Low Impact Development (LID) practices have been suggested as a viable solution (Burns et al., 2012; Chang, 2010; Dietz, 2007; Maniquiz-Redillas and Kim, 2016; Qin et al., 2013; Tong et al., 2016c). LID practices increase sustainability by using porous pavement, bioretention, green roofs, rainwater harvesting and other strategies that manage rainwater as close to its source as possible. In particular, bioretention is effective in retaining large volumes of runoff. As well, porous pavement is effective in infiltrating stormwater runoff (Niu et al., 2015), and green roofs can retain a large percentage of rainfall in a variety of climates (Dietz, 2007). These approaches increase groundwater replenishment, rainwater reuse, and on-site water balance, while mitigating downstream flooding (Pyke et al., 2011).

In the U.S., the rainwater runoff of a development project is

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calculated by hydrology engineers who are usually engaged during the design development phase or perhaps even later. In addition, for the sizing of conventional runoff management such as retention ponds or drainage pipes, hydrology engineers could conduct the task with little participation by the architectural team. Unfortunately, overlooking the site hydrology in the early design stage can lead to many challenges when incorporating LID strategies. This is because many LID practices must be integrated with other design elements or, to some extent, are parts of the design itself. Architects and landscape designers must be able to develop preliminary on-site stormwater management strategies in harmony with early architectural, structural and landscape design. Addressing the problem later in the process may limit one's options for selection, location or sizing of systems. Moreover, since local regulations, environmental standards such as LEED (USGBC, 2013) and design best practices increasingly mandate rainwater management targets, project teams need to consider runoff issues as an integrated part of the early design to guarantee the fulfillment of their goals. The team should be able to conduct quick compliance checks, and if the design falls short, adjust their strategies accordingly.

To address the issues discussed earlier in the paper, there is a need for developing a stormwater runoff model that provides quantitative visualization and estimation that incorporates site geometries. There are only few models in the market for stormwater runoff calculation that can benefit landscape design. The most advanced tool is EPA's Storm Water Management Model (SWMM) (Huber et al., 2005). It is a rainfall-runoff simulation model that predicts runoff quantity and quality from primarily urban areas. It is not friendly to landscape designers for the following reasons. First, the model does not support direct import of complex computer-aided design (CAD) geometries. Second, the model simplifies terrain to two dimensions, which does not indicate runoff flow directions. HydroCAD is another application developed by HydroCAD Software Solutions, LLC (Koo, 1989). Its function is limited to water conveyance and pond design (including storage chamber), and this model has no capacity for other runoff management practices such as green roofs, permeable pavement or rainwater harvesting. The model presented in the paper is the first one to our knowledge that offers 1) graphical visualization of buildings and landscape; 2) prediction of runoff flow directions; and 3) user-friendly interface for architect and landscape designers. With these tailored features, Rainwater+ is an intuitive tool for runoff evaluation and management that can enable designers to integrate rainwater considerations into their design workflow.

In Table 1, four softwares listed are positioned to solve different problems although they all belong to the general category of "stormwater runoff estimation". SWMM and HydroCAD are comprehensive packages with dynamic modeling capacity for peak flow and water quality prediction, whereas the National Stormwater Calculator (NSC) and Rainwater+ only concern about runoff volume. The former two can be used for water conveyance (e.g. pipe design) in the Construction Documents phase, while the latter two, used in the Schematic Design phase, can provide general reference for the compliance of the "runoff management"

requirements in the vast majority of sustainable rating systems or state codes. Unlike SWMM and HydroCAD whose target users are civil engineers and researchers, Rainwater+ and NSC are tools tailored for "less-professional" users such as architects and landscape designers. Their user interfaces are designed to be much simpler. In contrast with NSC, Rainwater+ provides features (system sizing and flow visualization) that can greatly assist the LID design process. In addition, the integration of Rainwater+ into CAD platform (e.g., Rhino) allows the possibility to accommodate the need of frequent design changes in the early design stage while achieving the same accuracy of calculation. The streamlined process of Rainwater+ eliminates the uncertainties associated with re-drawing and simplifying geometries in other platforms for runoff calculation.

This paper is organized as follows: We start with a detailed description of our numerical model, Rainwater+. Next, we share two case studies that employed the Rainwater+ software to illustrate the importance of considering stormwater runoff in the early design stage. Finally, we provide design recommendations based on the results of our analysis.

2. Model description

Rainwater+ presented in this paper is an intuitive and interactive tool for the use in the early design process, which was designed to better serve architects, landscape designers and ultimately the hydrological engineers who work with them. Rainwater+ is an open source model available for download from the website, www.rainwaterplus.com.

Rainwater+ is built upon the software platforms Rhinoceros and Grasshopper, developed by Robert McNeel & Associates. Rhinoceros is one of the fastest-growing, three-dimensional modeling tools for architects and landscape designers. As many designers are already familiar with Rhinoceros, Rainwater+ allows them to consider stormwater runoff based on existing geometries without interrupting their workflow by having to engage a separate tool. Rainwater+ is developed with Grasshopper, a graphical programming platform integrated with Rhinoceros's 3D modeling tools. The general workflow of Rainwater+ is displayed in Fig. 2. Using this platform, Rainwater+ is able to provide instant feedback based on CAD models throughout the entire design process. Rainwater+ is positioned to address rainwater management issues of site less than 1 km² – the relatively small and integrated drainage basins in highly developed urban regions that are vulnerable to severe urban flood risks (Lee and Heaney, 2003; Dietz and Clausen, 2008).

2.1. Model features

Rainwater+ can be used for design evaluation, decision-making, compliance checking, and rough cost estimation. It is comprised of four major process components that will be discussed in greater detail: 1) a built-in precipitation database; 2) a terrain analysis tool; 3) a runoff volume calculator; and 4) a library of LID practices and sizing components. The interface integrates directly with the

Table 1
A comparison of four stormwater runoff estimation softwares in terms of their features and target users.

Tool	Runoff volume estimation	Flow rate estimation	Water quality prediction	LID design	System sizing	Graphic inter-connection	Flow visualization	Targeted user
SWMM	✓	✓	✓	✓	✓	Limited	N/A	Civil engineers, Scientific researchers
HydroCAD	✓	✓	Limited	Limited	Limited	Limited	N/A	Civil engineers
National Stormwater Calculator (NSC)	✓	N/A	N/A	✓	N/A	N/A	N/A	Developer, Landscape architects, Urban planners, Homeowner
Rainwater+	✓	N/A	N/A	✓	✓	✓	✓	Architects, Landscape architects

designer's model in Rhinoceros (Fig. 1). All components, except the terrain analysis tool, will also function with a two-dimensional drawing as well as a 3D model.

2.1.1. Precipitation database

Rainwater+ contains a library of multiple types of precipitation data input. Rainwater+ currently includes a library of percentile data input (85th, 90th and 95th percentile rainfall event data for 16 major cities in the United States), as well as recurrence interval data inputs (once in 1, 2, 5, 10, 25, 50 or 100 year rainfall events for 13 major cities in the United States). The precipitation data are from the National Oceanic and Atmospheric Administration's (NOAA) Precipitation Frequency Data Server (PFDS).

2.1.2. Terrain analysis tool

The terrain analysis function in Rainwater+ interprets a three-dimensional site plan to visualize the site's hydrological flow conditions. This is realized by an iterative algorithm. A grid of nodes is projected onto the terrain surface. For each of the nodes, the algorithm locates the lowest node in elevation at one step size away from the previous node. The node then moves to the new location, and the process repeats. The density of the grid and the step size can be adjusted by the user. This feature allows users to visualize surface flow, which helps designers re-grade the site, if necessary, and place runoff mitigation systems, such as bioretention, in the most appropriate locations.

2.1.3. Library of LID practices and sizing components

Rainwater+ can evaluate the effects of various rainwater management strategies. The current LID library includes bioretention systems, subsurface infiltration systems, permeable pavements, green roofs and rain harvest cisterns. The model first evaluates the runoff volume of the current conditions before LID treatment. In the LID design phase, Rainwater+ helps designers determine the coverage area and storage capacity of the bioretention system or subsurface infiltration system based on site topology and runoff reduction targets. The model is coded to automatically update the runoff volume in real time whenever there are changes in location,

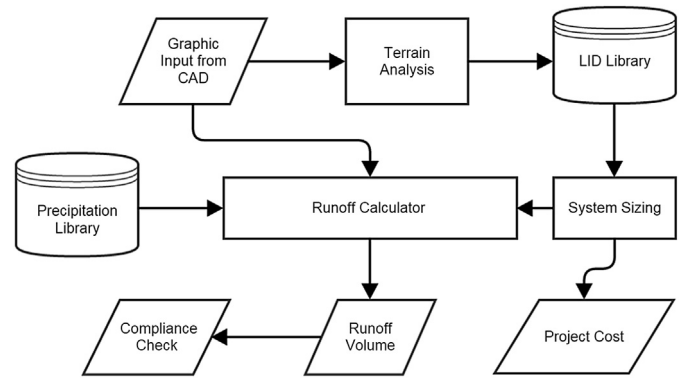


Fig. 2. Workflow of Rainwater+.

size or designed retention depth of the geometry, which provides convenience, particularly in the early design stage.

2.2. Calculation method

In order to calculate runoff depth, the Natural Resource Conservation Service (NRCS) Curve Number method (Cronshey, 1986; Durran and Dietrich, 2003; USDA, 1985), developed by the U.S. Department of Agriculture (DOA), was selected for Rainwater+ among several available runoff calculating methods. This method was chosen because of its relatively complete database, as well as the fact that it has been widely used for decades (Chung et al., 2010; Tsihrintzis and Hamid, 1997). This method is shown as Eqs. (1)–(3).

$$P_e = \frac{(P - I_a)^2}{(P - I_a) + S} \quad (1)$$

where:

P_e = depth of effective precipitation (runoff)
 P = total rainfall depth in storm event

The user interface of Rainwater+ is divided into several sections:

- Runoff Volume:** Unit: Gallon, Value: 0. Annual Runoff Volume (only for Annual Data input): 0.
- Estimated Cost:** Low: 0, High: 0.
- Percentile Data (for LEED):** St. Louis, 95th, 1.7.
- Recurrence Interval Data (Duration = 1 hour):** Charlotte, 5 years, 2.03.
- Designated Data:** Precipitation Depth (in): 1.52.
- Annual Data:** Table with columns for precipitation depth (in) and frequency (per year).
- Hydrologic Soil Group:** C.
- Basic Geometries:** Roof, Impervious paving, Lawn, Paved: open ditches, Poor - grass cover <50%.
- Bioretention \$:** Bioretention, Depth (in): 6.0.
- Subsurface Infiltration System \$:** InfiltrationSystem, Storage Depth (ft): 1.3.
- Permeable Pavement \$\$:** Porous Paving, Retention Depth (in): 0.2.
- Greenroof \$\$\$:** Greenroof, Retention Depth (in): 2.0.
- Rain Harvest Cistern \$\$\$:** No data was, Volume (1,000-Gallon): 0.
- Site Hydraulic Tool:** Terrain, Grid density: 29, 28, Step size: 30.0.

Fig. 1. User interface of Rainwater+.

I_a = equivalent depth of initial abstractions
 S = maximum possible water retention

Data analyzed by the NRCS indicated that on average, $I_a = 0.2S$, thus the equation above becomes

$$P_e = \frac{(P - 0.2S)^2}{P + 0.8S} \tag{2}$$

The maximum possible retention S is related to the curve number (CN):

$$S = \frac{1000}{CN} - 10 \tag{3}$$

where: CN = runoff curve number.

The curve number used in Rainwater+ and shown in Table 2 is from Urban Hydrology for Small Watersheds TR-55 by the U.S. DOA (Cronshey et al., 1985). In the Rainwater+ calculation, the curve number is automatically read from the table based on the land cover condition of each surface and user-specified soil type. Detailed land cover conditions are assigned to geometries (individual, group or layer) in the designer's model, which enables Rainwater+ to read geometry data from Rhinoceros.

Soils in the United States have been classified by the NRCS into four hydrologic groups: A, B, C and D, as shown in Table 3. Group A soils have high infiltration rates. These soil types are available for selection by the user in Rainwater+. Hydrologic soil groups for locations in the United States can be found on NRCS's SOILS website (soils.usda.gov).

As described above, the user's decision on the location of LID features is assisted by the terrain analysis tool, which will illustrate the flow and its convergence within the site boundary. The user's decision on the size of LID features is reached by adjusting the area and depth (or volume for cistern) of each feature to achieve the aimed runoff volume of the site. Table 4 lists the constraints of retention capacity of each LID feature adopted in Rainwater+ according to common engineering practice and the manufacturer's catalog. These constraints are included in the Rainwater+ to prevent unrealistic system sizing during the design process. However, users are able to override these settings with custom values if necessary.

3. Case studies

Two case studies are presented in this study to demonstrate the application of Rainwater+ on real sites and the importance of

Table 2
Land cover description and curve number.

Cover description	Curve numbers for hydrologic soil group			
	A	B	C	D
Lawns	68	79	86	89
Poor condition (grass cover < 50%)				
Lawns	49	69	79	84
Fair condition (grass cover 50%–75%)				
Lawns	39	61	74	80
Good condition (grass cover > 75%)				
Roofs	98	98	98	98
Paved parking lots	98	98	98	98
Paved (curbs and sewers)	98	98	98	98
Paved (open ditches)	83	89	92	93
Gravel	76	85	89	91
Dirt	72	82	87	89
Newly graded areas	77	86	91	94

Table 3
Hydrologic soil group.

Type	Infiltration rate	Texture
A	0.76–1.14 cm/h	Sand and gravels
B	0.38–0.76 cm/h	Coarse to moderately fine
C	0.13–0.38 cm/h	Moderately fine to fine
D	<0.13 cm/h	Clays with high swelling, high water tables

considering stormwater runoff at the early design stage. Case 1 is a real university campus extension plan, and Case 2 is a new development of a R&D center. Our goal of using these two case studies is to prove the importance and feasibility of integrating rainwater management into the workflow of architects and landscape designers to maximize the site potential of runoff mitigation and rainwater harvesting, which also helps to meet the requirement in corresponding standards and codes such as LEED and state regulations.

The university campus in Case 1 (Fig. 3) is located in the Northeastern U.S. with a total area of approximately 72 ha. The development team aims to achieve LEED v4 credits by managing on site the 95th percentile rainfall. Given that the current site consists of a high percentage of previously developed, impervious surfaces, there is an opportunity to reduce the volume of stormwater discharge to the river adjacent to the campus and increase water conservation by rainwater harvesting. The site elevations from local government's GIS database show that overall the site is vastly flat, with very sparse contour lines ranging from 2.7 m to 5.8 m over several city blocks with no clear surface trend. Therefore we treated the terrain as two-dimensional in our model. The 95th percentile rainfall of 3.86 cm was selected from the built-in precipitation library of Rainwater+. Hydrologic soil group C was also assigned based on site condition.

The project in Case 2 is an R&D Center also located in the Northeastern U.S. with the site boundary of approximately 26 ha (Fig. 5). The 590 m × 440 m hilly terrain has a large variation in altitude. The greatest difference between the lowest and highest altitude is 50 m. The gross floor area of this development is 50,000 m², comprised of three major buildings on an elevated platform. One of the project's goals for reaching site sustainability is to manage on site the annual increase in runoff volume from the natural land cover condition to the post-developed condition. The average annual precipitation of the location is approximately 102 cm. On average, there are approximately 56 rainfall events with more than 0.25 cm in precipitation.

4. Results

4.1. Case 1: extension plan of a university campus

Through the preliminary site screening test using Rainwater+, the visualized results as shown in Fig. 3 suggest that building roof areas have the greatest runoff depth, followed by the paved roads and walkways. The red and orange colors of these areas illustrate that the largest portion of the 3.86 cm of rain falling on these surfaces will run off the site. In contrast, the lawn area in blue shows a partial infiltration capacity. Given the condition that the site is vastly flat, it is assumed that the runoff will be channeled to the designated treatment areas. Therefore, we can skip the Rainwater+ terrain analysis.

In order to better apply localized stormwater management practices, the proposed site has been divided into six sub-zones (Fig. 4a) on which the various rainwater management practices are tested with Rainwater+. For cost consideration, we selected bioretention practices first, because these systems generally have

Table 4
LID retention capacity constraints.

LID	Constraint
Bioretention	Preferred retention depth between 15 cm and 30 cm (max 38 cm)
Subsurface infiltration system	Equivalent retention depth between 30 cm and 135 cm
Permeable pavement	Max retention depth 7.5 cm
Green roof	Max retention depth 5 cm
Rain harvest cistern	Max retention volume 160 m ³

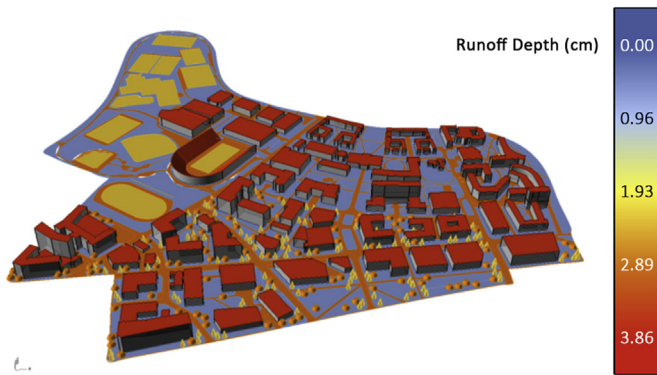


Fig. 3. Whole site runoff depth in 95th rainfall event before LID design.

the lowest cost per unit of stormwater treated (Dietz, 2007). If bioretention systems are not adequate for capturing the desired runoff volume, permeable pavement, cisterns and green roofs will be considered in the order based on relative costs. In most cases a combination of practices was selected as part of an integrated treatment system. We repeatedly adjusted the system size of these design combinations by trial-and-error and checked the runoff number until it reached zero. The campus plans before and after redesign are shown in Fig. 4.

The analysis from Rainwater+ suggests that proper LID design is able to offset the total 4542 m³ of runoff from the entire site in the 95th percentile rainfall event. At the subzone level of each individual land parcel, the combination of bioretention, subsurface infiltration system and porous pavement was sufficient to retain the 95th percentile rainfall on-site for a majority of the project zones. Other on-site low-impact stormwater management practices such as rain harvest tanks and green roofs were only needed in one zone with a high Floor Area Ratio (FAR) and percentage of impervious area.

The calculations performed by Rainwater+ for zone D in this case study are shown in Table 5 as an example. 516 m³ of rainwater will end up as runoff from this 21,329 m² site area in a 95th percentile rainfall event if no mitigation strategy is applied on-site. However, with properly designed 9677 m² of green roof with 2.3 cm water retention capacity, 3907 m² of porous paving with 5.1 cm retention capacity, 407 m² of bioretention area with 20.3 cm retention capacity, as well as two rainwater harvest cisterns of 83 m³ and 68 m³, theoretically the runoff volume can be entirely offset if the site drainage is appropriately designed.

4.2. Case 2: new development of an R&D center

The aim of this project is to earn LEED v4 credit that requires managing on site the annual increase in runoff volume from the

Table 5
Runoff calculations – zone D.

Project area D				
No LID				
	Area (m ²)	Runoff depth (cm)	Runoff (m ³)	
Roof	12,096	3.30	399	
Paved	3907	2.08	81	
Lawn	5326	0.68	36	
Total	21,329		516	
With LID Planning				
	Area (m ²)	Retention Capacity	Runoff Depth (cm)	Runoff (m ³)
Roof	2419		3.30	80
Green roof	9677	2.30 cm	1.56	152
Porous Paving	3907	5.10 cm	−1.24	−48
Lawn	4919		0.68	33
Bio-retention	407	20.30 cm	−16.44	−67
Cistern		83 m ³		−151
		68 m ³		
Total	21,329			−1

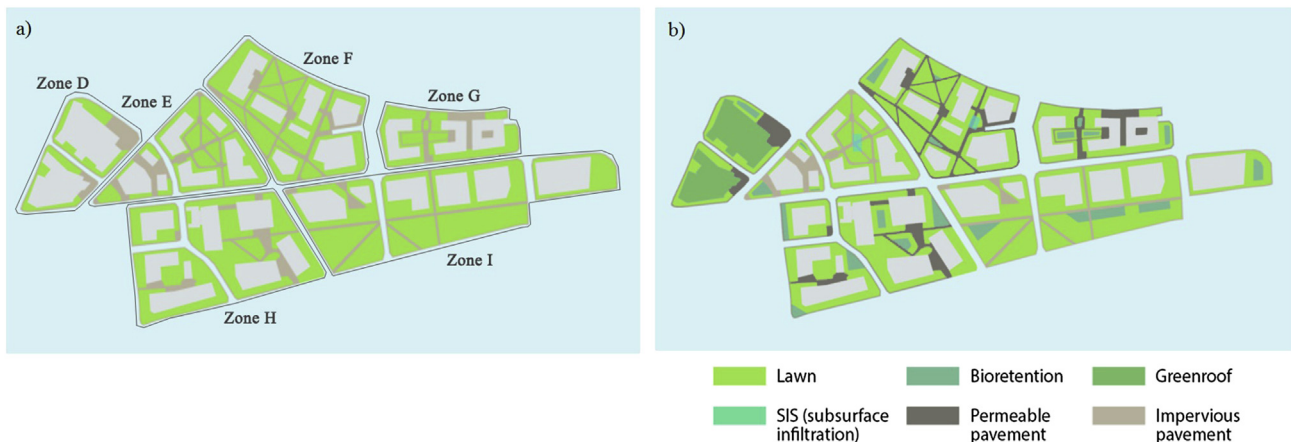


Fig. 4. Site plan without (a) and with LID design (b).

Table 6
Runoff calculations.

	Natural land cover condition	Design without LID	Design with LID		
	Runoff (m ³)	Runoff (m ³)	LID specification	Runoff (m ³)	Rainwater harvest (m ³)
From land	37,129	32,177	Three bioretention areas in total of 9994 m ² , with retention capacity of 15.2 cm	7229	
From roof		12,994	Two cisterns of 151 and 76 m ³	6781	6212
From pavement		14,279	5655 m ² of porous paving parking lot	5769	
Total	37,129	59,450		19,779	6212

natural land cover condition to the post-developed condition. According to the calculation of Rainwater+, the annual runoff volume of the natural land cover condition without building at this site is 37,129 m³ (Table 6). In the post-developed condition, the impervious surfaces of building and hard pavement reduce the infiltration capacity of the site and consequently result in an increased runoff volume of 59,450 m³, which is equivalent to a 60% increase. In this project, the selected LID practices are bioretention, permeable pavement and cisterns for rainwater harvest, decisions made after taking cost, site availability and water recycling into consideration.

Given the complexity of the terrain at the site, it is critical to consider the runoff flow directions for LID practices. With the aid of the terrain analysis tool in Rainwater+, the flow directions of the runoff can be easily visualized. As shown in Fig. 5b, the proposed bioretention area can be properly located and sized based on where the rainwater converges in the model. The sum of the three bioretention areas are 9994 m² with retention capacity of 15.2 cm. The rainwater harvest cisterns are sized with the corresponding component in Rainwater+ by accounting the runoff volume of each rainfall events within a year from the certain rooftop areas that use cisterns for collecting rainwater. Our analysis suggests that two cisterns of 151 m³ and 76 m³ are large enough to accommodate 80% of annual rainfall events in order to partially resolve the runoff issue from the rooftop, as well as be an alternative water source for toilet flushing and landscape irrigation. The 5655 m² pavement of the parking lot could be modified to pervious concrete to treat the runoff on-site. The combination of the above mentioned LID practices shows a potential capacity for reducing the annual runoff volume of the site to 19,779 m³, which is 53.3% of the natural land cover condition. In addition, theoretically a maximum amount of 6212 m³ of rainwater could be harvested from the rooftop by the use of cisterns.

5. Discussion and conclusion

A better understanding and assessment of rainwater runoff volume is of great importance for predicting risk and mitigating the damage of urban flooding, and consequently become a crucial issue

to be taken into consideration during the early design stage in order to deliver effective results of rainwater management in sustainable development.

The first case study illustrated the importance of integrating rainwater management into computer-aided design (CAD) software, e.g., Rhino, for the reason that visualizing specific site conditions is critical for choosing LID practice. Although there are a few design guidelines, such as cost-effective solutions that can be applied to most projects, the LID design should be considered on a case-by-case basis due to the unique site characteristics, such as the shape of the buildings, landscape, and the spatial relationship between buildings and landscape. The second case study demonstrated the important role of terrain analysis tools in the proper placement of LID practice by visualizing runoff flow direction at a site of complex terrain. The capability to size the rainwater harvest cistern also provides designers with great convenience for a quick estimation of rainwater collecting potential from the targeted roof area.

As discussed before, the runoff evaluation and management consists of a broad range of topics, including drainage and water quality control. Many of these works require specialized knowledge, therefore can hardly be done by people other than hydrological engineers. However, in response to the increased magnitude and frequency of stormwater runoff events, various green development certification programs encourage cost-effective LID strategies to manage the stormwater onsite. The first step to achieve this goal is to integrate LID design into site planning at early design stage and evaluate the runoff reduction potential by volume. Tools such as SWMM require specialized knowledge in hydrology. Typically, hydrological engineers are not involved in the early design stage, and it is often impractical to ask designers to use these complex tools. Facing this dilemma, the intent of developing Rainwater+ is to assist designers with less knowledge on hydrological processes to conduct runoff evaluation without much involvement of hydrological engineers. To achieve the goal, seamless integration with CAD, user-friendly interface, and well-documented case studies are designed. The usability of Rainwater+ by designers with little to none experience in hydrology is assured by the intuitive GUI and straightforward workflow. The

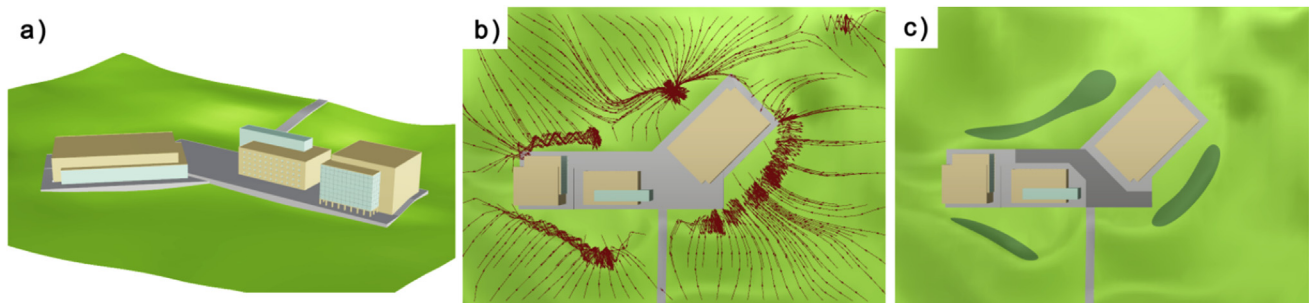


Fig. 5. a) Perspective view of the Case 2 design; b) Terrain analysis; c) Design with LID practices.

Rainwater+ has some limitations. Functions such as estimating runoff water quality and flow rate are not included in the model. However, they are not required in most municipal and state codes as well as LEED for rainwater management. In the [Supplementary Material](#), we compared five key steps in the workflow of Rainwater+ with SWMM, which shows the advantage of using Rainwater+ in the early design stage.

Rainwater management is no longer solely the engineer's responsibility in the new era of low-impact development. In fact, architects and landscape designers may be uniquely positioned to consider rainwater management strategies in the early design stage to avoid the lost rainwater management opportunities in the later phases as well as prevent construction confliction of building structure and LIDs. However, no tool currently exists to adequately support designers in integrating rainwater performance into their decision-making process. Considering this context, Rainwater+ is an intuitive tool for runoff evaluation and management that can enables designers to integrate rainwater considerations into their design workflow with tailored features such as ease of use, instant feedback of runoff volume, seamless graphic interconnection, straightforward system sizing, compliance checking, and visualization of rainwater surface flow.

Acknowledgement

We would like to thank Dr. Edward Eric Adams, Professor Joyce Klein Rosenthal, Nicole Holmes and Chelsea Christenson for their insightful comments and suggestions.

Appendix A. Supplementary data

Supplementary data related to this article can be found at <http://dx.doi.org/10.1016/j.jenvman.2016.04.059>.

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