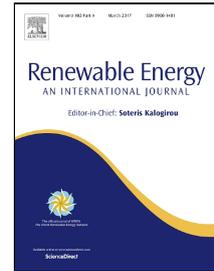


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Co-firing combustion characteristics of different ages of *bambusa balcooa* relative to a high ash coal

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- Combustion of different ages of bamboo, coal and their blends was studied using TGA.
- Bamboo properties were enhanced by thermal treatment
- Raw bamboo has the highest fuel reactivity and lowest ignition temperature
- DTG curves indicate that Bamboo-biochar improves the reactivity of blends
- All samples tested exhibit lower burnout temperatures compared to coal

1 CO-FIRING COMBUSTION CHARACTERISTICS OF DIFFERENT AGES OF *BAMBUSA*  
2 *BALCOOA* RELATIVE TO A HIGH ASH COAL

3  
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12  
13  
14 Abstract

15 *Bambusa balcooa* samples of 1, 3 and 4 years old were subjected to torrefaction at 250 °C  
16 and 280 °C, and low temperature carbonization at 350 °C and 400 °C to establish their  
17 combustion, co-combustion and physicochemical properties. The combustibility of these raw  
18 and thermally treated bamboo materials was studied using thermogravimetric analysis  
19 (TGA).

20 The nitrogen content of the raw bamboo samples decreased with the plant's age and there  
21 was no correlation between the volatile matter content of the bamboo and the age of the  
22 samples. The calorific values (CV) for the raw bamboo samples ranging from 17 MJ/kg to 18  
23 MJ/kg, while the torrefied and carbonized samples exhibited CVs ranging from 25 MJ/kg to  
24 28 MJ/kg and 28 MJ/kg to 30 MJ/kg, respectively. The torrefied 4 year old sample has the  
25 highest mass and energy yield, whereas the carbonized 3 year old had the highest values.  
26 Both the raw and thermally treated bamboo had higher reactivities and lower ignition  
27 temperatures than the coal. The carbonized 4 year old bamboo is found to be more  
28 compatible to coal in terms of its combustion characteristic. Therefore, it's likely to be the  
29 preferred alternative source of fuel for co-firing with coal.

30  
31 Keywords: Bamboo, Carbonisation, Combustion, Torrefaction, Reactivity.

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## 37 1. Introduction

38 South Africa is economically vulnerable to climate change because its economy is powered  
39 by electricity generated from coal fired power stations. There is a need to reduce the over  
40 reliance on fossil fuel energy not only because of greenhouse gas emissions but also to ensure  
41 energy security. Biomass “bamboo” has received significant attention with a positive  
42 prospect as a future energy source due to its fast growth rate, considerable strength and mass,  
43 low ash content and its ability to attain full maturity within five years, and as a carbon neutral  
44 renewable resource [1-4]. Studies have shown that biomass, along with solid waste can be  
45 converted into energy either by combustion, liquefaction or through gasification [5, 6]. In  
46 addition, recent investigations have also shown that biomass can be co-fired with coal in  
47 existing power plant with very little modifications [5, 7]. Co-firing biomass with coal shows a  
48 potential for reducing CO<sub>2</sub> and NO<sub>x</sub> emission among other benefits. Even though bamboo has  
49 been used as an alternative fuel source, it must be noted that, like other woody biomass  
50 materials, this too has its drawbacks in its natural state. This includes poor physicochemical  
51 properties, high volatile matter contents and low energy densities.

52

53 Previous research has shown that these drawbacks can be addressed by thermal pre-treatment  
54 of the biomass by two mild pyrolysis processes, i.e. torrefaction and low temperature  
55 carbonization. [2, 7, 8-13]. The application of these techniques has a major influence on the  
56 chemical and physical properties of raw biomass. During these pre-treatment processes,  
57 biomass molecules are restructured, leading to losses in the hydrogen and oxygen content of  
58 biomass along with the decomposition of its cellulose and lignin functional groups.  
59 Ultimately, this biomass is converted into a densified solid with improved grindability and  
60 non-polar unsaturated products [12, 14, 15]. Bergman *et al* [9] stated that pre-treated biomass  
61 has energy densities similar to that of coal which could render it more suitable for co-firing.  
62 A study conducted by Rousset *et al* [2] found that, at torrefaction temperatures between 250  
63 °C and 280 °C, hemicellulose and cellulose decomposes, yielding a biomass char that  
64 possesses a higher carbon content. Park *et al* [12] investigated the effect of thermal treatment  
65 on various biomasses and found that at carbonisation temperatures between 400 °C and 500  
66 °C, the resulting char product has improved fuel properties such as higher fixed carbon, lower  
67 volatile matter and increased calorific value.

68

69 The species of bamboo utilized in this investigation is *Bambusa balcooa*, which was acquired  
70 from the Western Cape region of South Africa. *Bambusa balcooa* is known as a clumping

71 bamboo and occurs as a naturalized species of bamboo in South Africa. It has a very thick  
72 wall culms, height within 15-20 m, and an internode of about 20-45 cm. Altogether, these are  
73 characteristic of species with a high yield biomass (tonne/ hectare/ yr). Hence, according to  
74 the report by Poppens et al [16] a well managed bamboo plantation may yield over 30  
75 (t/ha/yr) dry matter biomass depending on the species. The use of bamboo for re-greening  
76 and rehabilitation of abandoned mined sites is due to its physicochemical and biological  
77 properties. The concept of bamboo cultivation can provide clean, efficient and economical  
78 alternative fuel source with sustainable community benefits. If grown successfully, a large  
79 number of abandoned mined sites such as asbestos, gold tailing dumps and coal mines, could  
80 be rehabilitated and promote job creation.

81  
82 A detailed comparison of the physicochemical properties of some species of bamboo at  
83 different ages was conducted by Scurlock *et al* [17]. This author found that there was no  
84 correlation between the volatile matter, ash content, fixed carbon content and the age of the  
85 bamboo species utilized. All samples, regardless of their ages were found to have similar  
86 higher heating values, total carbon and hydrogen content. However, in this study, the  
87 characteristic combustion and co-combustion behavioural characteristics of bamboo  
88 "*Bambusa balcooa*" of different ages (1, 3 and 4) year were found to differ. The main  
89 objectives of this study were to quantify the differences in properties and behavioural  
90 characteristics between raw bamboo of different ages and thermally treated bamboo, as well  
91 as to compare their combustion features to coal along with their co-firing potential with  
92 coal.

93  
94 The combustibility of these raw and thermally treated bamboo species, along with coal were  
95 investigated using thermogravimetric analysis. During the combustion and the co-combustion  
96 tests, the parameters measured included initiation devolatilisation temperature ( $IT_{VM}$ ), peak  
97 temperature (PT) and burnout temperature (BT) based on the burning profiles generated from  
98 the differential thermogravimetric analysis (DTG).

99

100

## 101 2. Experimental

### 102 2.1. Materials

103 Samples of "*Bambusa balcooa*" of different ages and high ash coal were utilized in this  
104 investigation. The three different ages of bamboo were 1 year, 3 years and 4 years old, all

105 sourced from the Western Cape, South Africa. These were used as the raw biomass materials.  
106 The stem, known as the culm, was blended from the top, middle and bottom, as well as the  
107 underground root, also known as rhizomes. The bamboo samples were then cut into blocks of  
108 approximately 25 X 25 X 10 mm in size to generate feed for the thermal treatment  
109 investigation. The coal used for the co-firing was sourced from the Free State, South Africa.  
110 This high ash coal was pulverized to 100% passing a 212  $\mu\text{m}$  screen in a pulveriser for  
111 preparation and use in the tests, both alone and with bamboo samples.

112  
113

## 114 2.2. *Thermal treatment*

115 The thermal treatment processes conducted on the raw *Bambusa balcooa* utilized in this  
116 investigation were known as torrefaction and low temperature carbonization. Torrefaction is  
117 a slight pyrolysis process carried out within the range of 200  $^{\circ}\text{C}$  to 300  $^{\circ}\text{C}$  under an inert  
118 environment, with the aim to produce a densified and carbon rich solid. The raw 1, 3 and 4  
119 years bamboo were torrefied at 250  $^{\circ}\text{C}$  and 280  $^{\circ}\text{C}$ . The raw samples were further subjected  
120 to thermal treatment at 350  $^{\circ}\text{C}$  and 380  $^{\circ}\text{C}$  using low temperature carbonization process. The  
121 process was conducted at a higher temperature compared to torrefaction, and in an oxygen  
122 free environment. The thermal processes were carried out in a gas tight laboratory scale  
123 heated electric muffle furnace embedded with a glass tube reactor at a constant heating rate of  
124 3  $^{\circ}\text{C}/\text{min}$  under argon gas at 0.5 l/min. Approximately 600 g of the respective raw bamboo  
125 samples was charged into the glass tube reactor and heated to the set temperature, and held  
126 for 40 minutes. After the treatment time, the samples were removed and covered with a  
127 container to prevent oxidation, and thereafter milled to -212  $\mu\text{m}$  size fraction. Several blends  
128 of coal and bamboo were then prepared from the raw samples, torrefied (T250  $^{\circ}\text{C}$  and T280  
129  $^{\circ}\text{C}$ ) and low-carbonized (C350  $^{\circ}\text{C}$  and C 380  $^{\circ}\text{C}$ ), and adding at 10%, 30%, 50% and 75% of  
130 coal by weight for the investigation.

131  
132

## 133 2.3. *Thermo-gravimetric analysis*

134 The combustion behaviour of the raw and the thermally treated bamboo samples as well as  
135 when blended with coal in different proportions (25, 50 and 75% bamboo, the difference  
136 being coal), was studied using thermogravimetric analysis. The combustion tests were  
137 conducted in a Leco 701 thermogravimetric analyser (TGA), under an oxidising atmosphere  
138 using air. Approximately 100 mg of each sample (100% passing a 212  $\mu\text{m}$  screen), of raw

139 bamboo biomass, coal, pre-treated bamboo and all the different bamboo/coal blends, was  
140 used for the experiment. The differential thermogravimetric (DTG) curves, i.e. combustion  
141 profiles were obtained at a constant heating rate of 10°C/min, from 25°C to 850°C and held  
142 until there is constancy in weight loss. The differential thermogravimetric curves (DTG)  
143 indicating the rate of weight loss (%/min) with increasing temperature were used to directly  
144 evaluate the combustion properties including initiation devolatilisation temperature ( $IT_{VM}$ ),  
145 peak temperature (PT) and burnout temperature (BT). The reactivity ( $R_m$ ) of the combusting  
146 material was quantified using the same expression as that used by Bada *et al* [3] and is  
147 presented in Equation 1 below:

148  
149

$$150 \quad R_m = \frac{100 \times DTG_{max}}{PT} \quad (1)$$

151

152 Where  $DTG_{max}$  is the maximum weight loss rate (%/min) and PT is the corresponding peak  
153 temperature.

154

155

#### 156 2.4. Fuel characterization, mass and energy yield

157 The proximate and the calorific value of the coal, raw and thermally treated bamboo samples  
158 were evaluated. The proximate analysis was conducted in accordance with the ASTM D-  
159 5142, utilizing approximately 1 g of each sample (coal and bamboo sample) in a TGA 701  
160 Leco instrument. The calorific value was determined using a Leco AC500 bomb calorimeter  
161 in accordance with ASTM D5865-04. The system uses an electronic thermometer with an  
162 accuracy of 0.0001 °C to measure the temperature every six seconds, with the results obtained  
163 within 4.5 to 7.5 minutes. The raw bamboo samples were further characterized for their  
164 elemental constituents using a LECO CHN 628 with add on 628 S module, in accordance  
165 with the ASTM D3176-89.

166

167 The impact of the thermal treatment on mass and energy yield was also evaluated. The mass  
168 yield ( $\eta_M$ ) and energy yield ( $\eta_E$ ) obtained at different pre-treatment temperature were  
169 calculated using Equations 2 and 3, reported by Bada *et al* [3] and Park *et al* [11].

170

$$\eta_M = \left( \frac{M_t}{M_o} \right) \text{ dry basis} \quad (2)$$

172

$$\eta_E = \eta_M \left( \frac{GCV_t}{GCV_u} \right) \text{ dry basis} \quad (3)$$

174

175 Where  $M_o$  and  $M_t$  are the initial biomass mass and final mass of the biomass after thermal  
 176 treatment, respectively. The  $GCV_o$  and  $GCV_t$  are the initial biomass gross calorific values and  
 177 final biomass gross calorific values after heat treated, respectively.

178

179

### 180 3. Results and discussions

#### 181 3.1. Fuel characteristics of coal and bamboo samples.

182 The results of the ultimate and the proximate analyses for all the samples tested are presented  
 183 in Table 1. The proximate and the ultimate analysis of the raw bamboo samples showed that  
 184 the three raw fuels have a low ash content and an insignificant amount of sulphur. The  
 185 nitrogen content in the raw bamboo samples was also low, suggesting that  $\text{NO}_x$  emissions  
 186 might be minimized during the co-combustion of the fuel compared with coal as the  
 187 percentage ratio of the biomass increases in the blend. These characteristics are seen in most  
 188 commercial co-fired power plant and are essential for clean coal combustion conditions  
 189 [5,18]. There was little difference observed from the proximate results of the three raw  
 190 bamboo samples in terms of moisture content, fixed carbon and volatile matter, these ranged  
 191 from 7.01 to 8.09 %, 18.03 to 19.25 % and 79.20 to 81.04%, respectively. The nitrogen  
 192 content of the bamboo samples decreased with the age of the harvested plant, while there was  
 193 no correlation between the total carbon content of the bamboo and the age of the samples.  
 194 Similarly, there was no correlation between volatile matter and the age of the samples.

195

196 After torrefaction and low temperature carbonization treatment the fixed carbon and calorific  
 197 values of all samples were observed to increase (see Table 1) while moisture and volatile  
 198 matter content were reduced. Also in Table 1 fixed carbon for the 4 year old bamboo is  
 199 shown to be more than triple its content from 19.25% to 63.64% after torrefaction at 280°C,  
 200 and that increased further to 76.6% after treatment in the low carbonization temperature of  
 201 400°C. A similar result was observed in a study by Park et al [12] who found the fixed carbon

202 content of a woody biomass to be more than tripled after torrefaction at 275°C. In terms of  
203 the sample's age and the effect of heat treatment, the older bamboo is observed to have a  
204 higher fixed carbon content at all treatment temperatures, with the exception of torrefaction  
205 at 280°C, where a slightly higher fixed carbon content was observed for a 3 year old bamboo  
206 sample. In conclusion, it has been shown that the 4 year old bamboo carbonized at 400°C has  
207 the highest fixed carbon content of all the samples heat treated.

208  
209

210 Table 1: Fuel properties of raw and thermally treated bamboo.

211

212 The volatile matter content of the bamboo samples decreased with an increase in treatment  
213 temperature, irrespective of the age of the bamboo, as seen in Table 1 above. The volatile  
214 matter contents of 3 year and 4 year old bamboo samples decreased to about half when  
215 torrefied at 250°C, i.e. from 79% to 39% and 79% to 37% on a dry basis, respectively. The  
216 degree to which the bamboo samples tested in this study devolatilized was found to be more  
217 pronounced than samples reported by other authors using biomass materials such as *Bambusa*  
218 *vulgaris*, pine chips, logging residue chips, willow, eucalyptus and woody biomass [2, 11-  
219 13]. The ash content was also seen to increase as the treatment temperature increases. The  
220 raw and the thermally treated 1 year old bamboo had the lowest ash content (0.93-3.65%) at  
221 all treatment temperatures.

222

223 Table 2: Mass and Energy yield of thermally treated bamboo

224

225

226 The calorific value (CV) of the raw bamboo samples was found to be between 17.10 and  
227 18.53 MJ/kg as shown in Table 2 above. Bada *et al* [3] reported similar results on the raw  
228 *Bambusa multiplex*. The CV of all raw bamboo samples (1, 3 and 4 year old) increased by at  
229 least 40% after being torrefied at 250°C and increased even further at higher thermal  
230 treatment temperatures. The CV value of the 4 year old bamboo increased from 17.63 MJ/kg  
231 to 26.38 MJ/kg and 30.24 MJ/kg after torrefied at 280°C and carbonized at 400°C,  
232 respectively. Similar results were reported by Phanphanich and Mani [11], Ibrahim *et al*  
233 [12] and Bada *et al* [3] on logging residue chips, Eucalyptus and *Bambusa multiplex*,  
234 respectively.

235

236 In terms of mass yields, the torrefied products in this study were found to have the highest  
237 mass yields of 51%, 40% and 39% for the 4, 3 and 1 year old bamboo samples relative to the  
238 carbonized products which exhibited lower mass yields as seen in Table 2. Ibrahim *et al* [13]  
239 obtained a higher mass yield of 68.76% on willow torrefied at 270 °C for 30 min. The lower  
240 mass yields noted in this study might be as a result of the impact of torrefaction (280 °C) on  
241 bamboo, which is similar to the results obtained by Rodrigues and Rousset [19]. In the case  
242 of carbonization, similar mass yield (32.8%) obtained by Park *et al* [12] on woody biomass at  
243 350°C for 30 min was obtained. The energy yield was found to be consistently higher at  
244 torrefaction temperatures for all bamboo samples. The 4 year old bamboo sample had the  
245 highest energy yield of 74% and 68% after torrefied treatment at 250°C and 280°C, compared  
246 to other samples as shown in Table 2 above.

247  
248

### 249 3.2. Combustion of coal, raw and thermally treated bamboo

250 Figure 1 below shows that the combustion of the raw bamboo samples occurs in stages.  
251 The first stage of the combustion profiles represents the initial weight loss which occurred as  
252 a result of the moisture being driven off (25 °C to 140 °C), this was seen in all the  
253 thermographs (Figures 1-8). After the moisture loss, a downward trend or negative deflection  
254 (weight gain) was observed due to the oxidation of the organic matter within the samples. As  
255 the curve rises above the zero line of the x-axis, the devolatilization stage begun and this  
256 point is known as the volatile matter initiation temperature ( $IT_{vm}$ ). The  $IT_{vm}$  occurred within  
257 the temperature of (142°C to 200 °C) for the bamboo samples and above 230 °C for the coal,  
258 thereafter, complete char combustion above 400 °C for all samples (Figures 1-8). This is  
259 similar to the three distinctive stages observed by Bada *et al* [3] from the combustion of  
260 *Bambusa multiplex*. The combustion of the raw bamboo is rapid and occurs at lower  
261 temperatures when compared to that of coal. This is evident from the peak and burnout  
262 temperatures range of 224-250 °C and 460-475 °C for the three different bamboo ages in  
263 Figure 1. The coal is shown to have a peak combustion temperature of 406 °C and a burnout  
264 temperature of at least 90 °C higher than that of the raw bamboo. This difference is expected  
265 because coal has a higher fixed carbon content than all the raw bamboo samples.

266  
267

268 Figure 1: DTG curves for coal and all the raw bamboo samples.

269

270 It may be noted in Figure 2a below that the maximum weight loss rate (%/min), i.e.  $DTG_{max}$ ,  
271 of the raw 1 year old bamboo decreased by almost 60% after torrefied at 250 °C and it  
272 decreased even further at higher treatment temperatures as shown in the same Figure. The 3  
273 and 4 year old bamboo samples also show similar trends as seen in Figure 2b and 2c. The  
274 decrease in volatile matter contents of the thermally treated samples and the consequent  
275 increase in their fixed carbon contents is considered to be responsible for the changes in their  
276 burning profiles, all of which brings the combustion profiles of the bamboo samples closer to  
277 that of coal.

278

279 The respective combustion profiles of the 1 year old bamboo samples treated at different  
280 temperatures show two distinctive peaks. The same number of peaks is noted for the 3 year  
281 old samples, although the low carbonized bamboo at 400 °C was less pronounced. These  
282 results are identical to the observation made by Park et al [12] on the combustion profile of  
283 low temperature carbonized woody biomass. The PT and BT of the torrefied and carbonized  
284 bamboo samples are also observed to increase as the thermal treatment temperature increases.  
285 Bada et al [3] reported a similar observation on *Bambusa multiplex*. The 4 year old low  
286 carbonized bamboo at 400 °C has only one peak with a similar combustion profile to coal.  
287 This sample also has the highest burnout temperature compared to other bamboo samples,  
288 signifying a coal like nature. The major difference to coal, however, is that all bamboo  
289 samples devolatilise and ignite at lower temperatures compared to coal. In general, it would  
290 appear that the burnout temperatures of the raw and the thermally treated bamboo samples are  
291 influenced by the increase in fixed carbon content.

292

293

294 Figure 2: DTG curves for thermally treated bamboo and coal (a:1yr; b:3yr and c:4yr)

295

296

297 According to both Table 2 and Figure 2 above, the reactivity of the raw bamboo samples may  
298 be seen to be 4 times faster than that of coal. This is considered to be related to the higher  
299 volatile matter content, lower fixed carbon and the lower mass density of the raw bamboo  
300 relative to coal. This finding is in agreement with that achieved by Kastanaki and Vamvuka  
301 [20] when studying the reactivity of coal, olive and kernel char. The reactivities of the  
302 thermally treated bamboo samples T250, T280, C350 and C400 were also found to be higher  
303 than that of coal, but were lower than that of the raw bamboo sample. In summary, raw

304 bamboo samples ignite easily at low temperatures and are more reactive than the thermally  
305 treated bamboo samples and the coal used in this study. In terms of reactivity, 1 year old raw  
306 bamboo is the fastest burning fuel than all other fuels tested.

307

### 308 3.3. *Co-combustion profiles of raw bamboo and coal*

309 Raw bamboo (1, 3 and 4 year old) and coal were co-combusted in a TGA furnace. The blends  
310 studied were composed as follows: (i) 75% raw bamboo + 25% coal, (ii) 50% raw bamboo +  
311 50% coal and (iii) 25% raw bamboo + 75% coal, for each respective age of the bamboo. The  
312 co-combustion profiles of 1 year, 3 year and 4 year old raw bamboo with coal are presented  
313 in Figure 3a, b and c, respectively.

314

315

316 Figure 3: DTG curves of co-combustion of raw bamboo/coal (3a:1yr; 3b:3yr and 3c:4yr)

317

318

319 It may be noted that for the blends of raw bamboo (1, 3 and 4 year old) and coal, the  
320 maximum rate of mass loss ( $DTG_{max}$ ) decreased significantly with the decrease in the  
321 proportional weight percentage of bamboo in the bamboo/coal blend (Figure 3a, b and c).  
322 This is considered to be due to the decrease in volatile matter and low density materials in the  
323 blend. In contrast, as the weight percentage of the coal in the blend increases, the DTG  
324 profiles were seen to move away from that of the raw bamboo and closer to the coal's  
325 profile. A blend containing (25% raw bamboo + 75% coal) was found to have the highest  
326 burnout temperatures compared to other blends seen in Figures 3a, 3b and 3c. The blends  
327 containing (75% raw bamboo + 25% coal) may be seen to have similar burning profiles to  
328 that of the raw bamboo combusted alone, and similar high combustion reactivities. It must  
329 also be noted that the peak temperature of all blends occurred in the lower temperature region  
330 compared to that of coal. Coal is shown to have similar reactivity to samples with (25% raw  
331 bamboo + 75% coal).

332

333

### 334 3.4. *Co-combustion profiles of the thermally treated 1 year old bamboo and coal*

335 Torrefied and low temperature carbonized 1 year old bamboo samples were blended with  
336 coal at different weight ratios and co-fired. As seen in figure 4a below, the profiles of all  
337 blends of 1 year old T250 and coal are similar, but coal alone exhibits a burning profile

338 different from the other fuels. The 1 year old T250 and its respective coal blends show two  
339 different peaks, which are probably due to the release of the large amount of volatiles in the  
340 first peak and carbon-rich lignin combustion in the second peak. This trend was also observed  
341 in the profiles of the 1 year old T280, C350 and C400 blended with coal (Figures 4b-4d). The  
342 burning profile of (75% T250 + 25% coal) sample closely matches that of 100% T250 alone  
343 (Figure 4a), with both thermographs having a peak temperature of about 193°C and a burnout  
344 temperature of about 491°C. In Figure 4b, 4c and 4d, the blends of (75% + 25% coal) were  
345 seen to be far higher in reactivity compared to other thermally treated samples. These  
346 samples are seen to possess higher volatile matter content compared to other samples with an  
347 increased carbon content, thereby reduced reactivity. In addition, these blends (75% + 25%  
348 coal) burnout temperatures also occurred within the low temperature zone similar to the 1  
349 year 100% (T280, C350 and C400) samples. The (25% C400 + 75% coal) blends in Figure  
350 4d was seen with a DTG profile closest to that of coal. A similar observation was made by  
351 Bada *et al* [21] on the co-firing of thermally treated *Bambusa balcooa* at 400 °C with high  
352 ash coal, and the thermograph obtained shows a close co-combustion compatibility with coal.  
353 Furthermore, the reactivity of all the samples in the Figures was observed to decrease as the  
354 coal proportion in the blend increases, hence this leads to a higher burnout temperature for all  
355 the (25% bamboo + 75% coal) samples than that of coal.

356

357

358 Figure 4: DTG curves of co-fired thermal treated 1year old bamboo/coal (4a; 4b; 4c and 4d)

359

360

### 361 3.5. *Co-combustion profiles of the thermally treated 3 year old bamboo and coal*

362 The co-combustion profiles of the torrefied 3 year old bamboo samples T250 and T280 with  
363 coal are shown in Figures 5a and 5b, respectively. In Figure 5a, it can be seen that all blends  
364 of T250 with coal have a similar burning profiles and lower peak compared to that of a 100%  
365 T250 sample. As the percentage coal in the blend increases, the profiles are seen to move  
366 closer to that of coal. The blend of (75% T280 + 25% coal) in Figure 5b was seen with the  
367 highest peak, followed by that of (50% T280 + 50% coal). In all 3 year bamboo fuels co-fired  
368 with coal, the blends containing (75% bamboo + 25% coal) were seen to have maximum  
369 weight loss rate (%/min) DTG profiles closest to that of the respective 100% bamboo sample  
370 fired solely.

371

372 Figure 5a & 5b: DTG curves for co-combustion of 3 year T250 & T280/coal

373

374 Figure 6a & 6b: DTG curves for co-combustion of 3 year C350 & C400/coal

375

376 From Figure 6b above, the 3 year old bamboo sample (25% C400 + 75% coal) showed a  
377 single peak combustion profile and a relatively similar burning profile to coal, suggesting  
378 coal-like burning characteristics. The same observation was made by Park *et al* [12] on  
379 blends of thermally treated woody biomass and coal. All samples co-fired with coal in the  
380 proportion of (25% bamboo + 75% coal) were seen to ignite at the high temperature region  
381 with higher burnout temperatures compared to the other blends. In respect to reactivity, all  
382 samples (Figures 5a, 5b, 6a & 6b) co-fired with coal in the proportions of (75% bamboo +  
383 25% coal) were seen to ignite at low temperatures. In all co-firing tests conducted, bamboo  
384 appears to aid in the ignition of coal at lower temperatures.

385

386

387 3.6. *Co-combustion profiles of the thermally treated 4 year old bamboo and coal*

388 The combustion profiles of the blends of torrefied 4 year old bamboo and coal are shown in  
389 Figures 7a and 7b, below. As is the case for the other blends of treated 1 year old and 3 year  
390 old bamboo samples, the DTG profile of the 4 year old sample with 75% coal (i.e. 25% T250  
391 + 75% coal) was the closest match to that of coal as seen in Figure 7a below. The same  
392 observation was made in Figure 7b for the blend of (25% T280 + 75% coal). In addition, as  
393 the weight percentage of coal increases in the blends, the initiation devolatilisation  
394 temperatures ( $IT_{vm}$ ) and burnout temperatures (BT) are seen to increase in all samples  
395 (Figures 7a & 7b). These observations can be attributed to the higher fixed carbon and lower  
396 volatile matter content of the bamboo and the coal in the blends. Bada *et al* [3] also reported  
397 the same observations for the co-combustion of torrefied *Bambusa multiplex* and coal.

398

399

400 Figure 7a & 7b: DTG curves for co-combustion of 4 year T250 & T280/coal

401

402 The respective maximum weight loss rate (%/min) DTG profiles in Figure 8a for the co-  
403 combustion of 4 year old C350 with coal shows a peak, which indicate volatile release at  
404 temperature between 200 °C and 220 °C for the 50% and 75% bamboo inclusion, but little if  
405 any in the 25% C350 + 75% coal sample below. These peaks signify the presence of some

406 volatile matter left in the blends after treatment at 350 °C. The near-single peak and the  
407 highest initiation devolatilisation temperature ( $IT_{VM}$ ) observed for the (25% C350 + 75%  
408 coal) blend indicate a combustion behaviour close to coal. Moreover, there is minimal  
409 difference in terms of BT between the profiles of all the blends in Figure 8a.

410

411 Figure 8a and 8b: DTG curves for co-combustion of 4 year C350 and C400/coal

412

413

414 Figure 8b above shows an illustration of the combustion of 100% carbonized 4 year old  
415 bamboo (C400) and its co-combustion with coal under different weight proportions. All  
416 samples in this Figure report a single peak, with PT, BT and combustion profiles closely  
417 similar to coal. The same observation was made by both Park *et al* [12] and Bada *et al* [21]  
418 on the co-combustion of low carbonized woody biomass and *Bambusa balcooa* with high ash  
419 coal, respectively. Only sample (75% C400 and 25% coal) presents a profile with an  
420 initiation devolatilisation temperature ( $IT_{vm}$ ) similar to that of the 100% C400 bamboo  
421 sample. From the observations made in all the burning profiles, it can be concluded that 4  
422 year old C400 bamboo material has combustion properties similar to coal and that it is  
423 therefore likely to be the most compatible fuel that could be co-fired with coal for power  
424 generation, especially in a pulverized fuel boiler. Furthermore, given that the blend with the  
425 highest proportion of C400 had better reactivity, it is possible that the bamboo blended with  
426 coal could improve the overall burning efficiency in a co-fired power station.

427

428

#### 429 4. Conclusions

430 Torrefication and carbonization were established as a suitable process to enhance the fuel  
431 properties of different ages of raw bamboo as a source for co-firing with coal. The calorific  
432 value of 1 year, 3 year and 4 year old bamboo plants was increased by low temperature  
433 carbonization from 18.53 MJ/kg to 28.54 MJ/kg for 1 year old bamboo, 17.10 MJ/kg to 30.17  
434 MJ/kg for 3 year old bamboo and 17.63 MJ/kg to 30.24 MJ/kg for 4 year old bamboo. The  
435 fixed carbon for all ages of bamboo was increased to over 66% (db) from low temperature  
436 carbonization, matching high quality coal. The *nitrogen content* of the bamboo samples was  
437 noted to decrease with the age of the harvested plant, but there was no correlation between  
438 the *total carbon content* of the bamboo and the age of the samples. The raw bamboo sample  
439 had the highest fuel reactivity and the lowest devolatilisation, peak and burnout temperatures

440 compared to all heat treated fuels. All the bamboo samples, raw and heat treated, were found  
441 to exhibit lower initiation ( $IT_{VM}$ ), peak and burnout temperatures compared to coal. Moreso,  
442 the DTG curves of the 4 year old carbonized samples (C400) closely matched that of coal.  
443 Hence, a *blend of carbonized 4 year old bamboo (C400) with coal* resulted in a DTG profile  
444 characterized by a single peak, and with the most compatible combustion characteristic with  
445 coal.

446

447

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453

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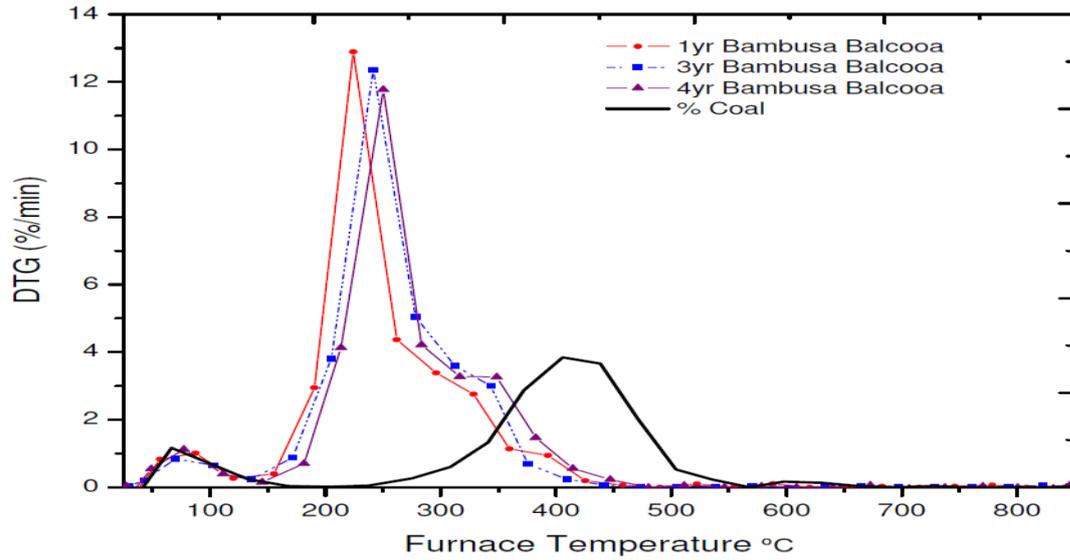


Figure 1: DTG curves for coal and all the raw bamboo samples.

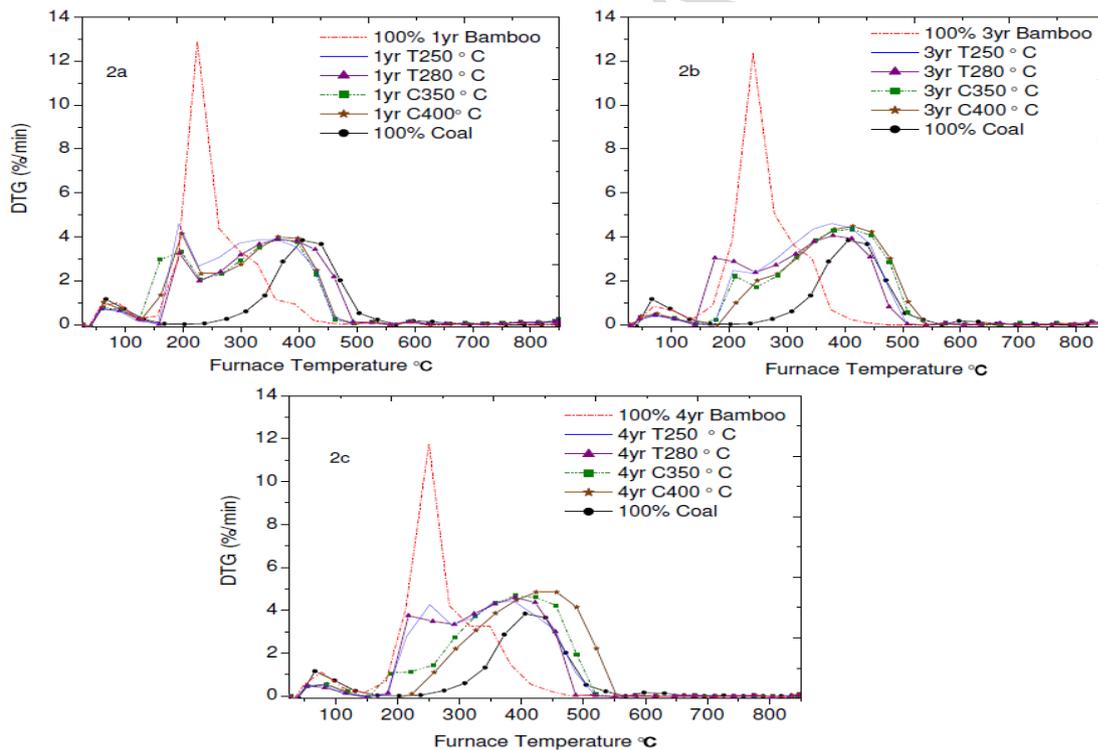


Figure 2: DTG curves for thermally treated bamboo and coal (a:1yr; b:3yr and c:4yr)

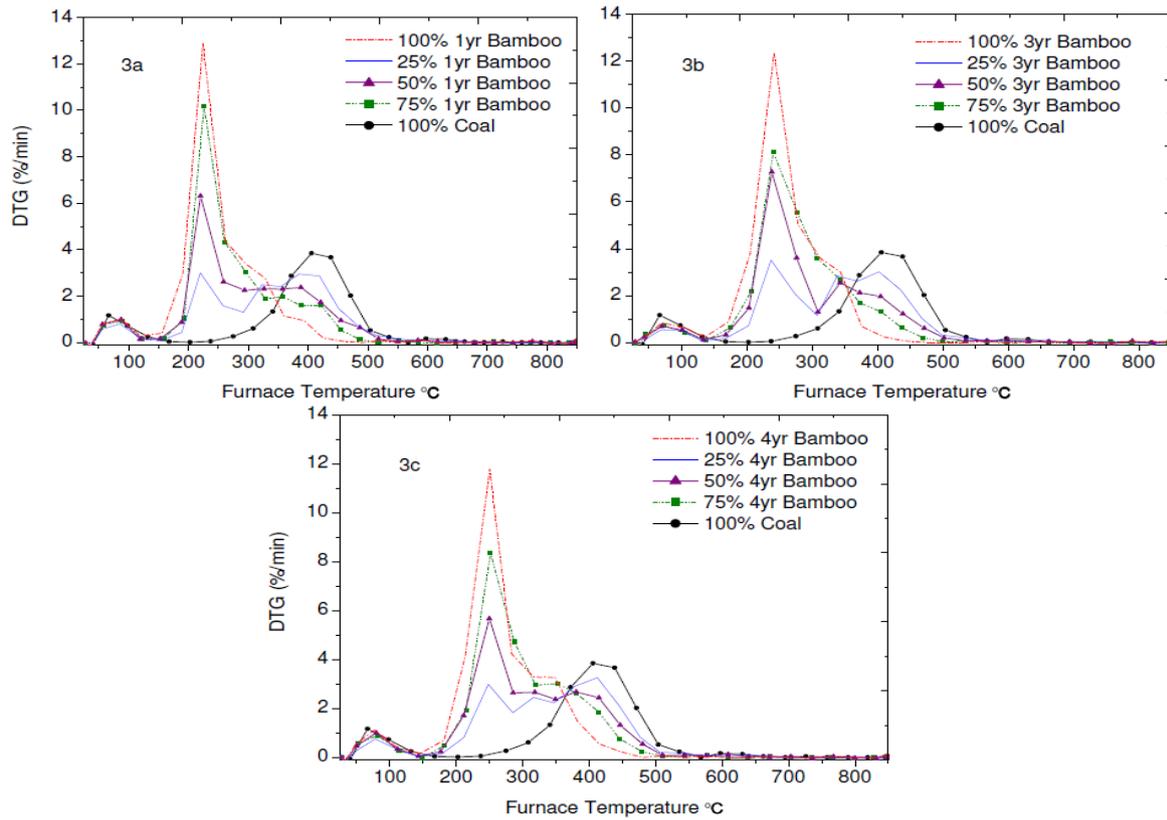


Figure 3: DTG curves of co-combustion of raw bamboo/coal (3a:1yr; 3b:3yr and 3c:4yr)

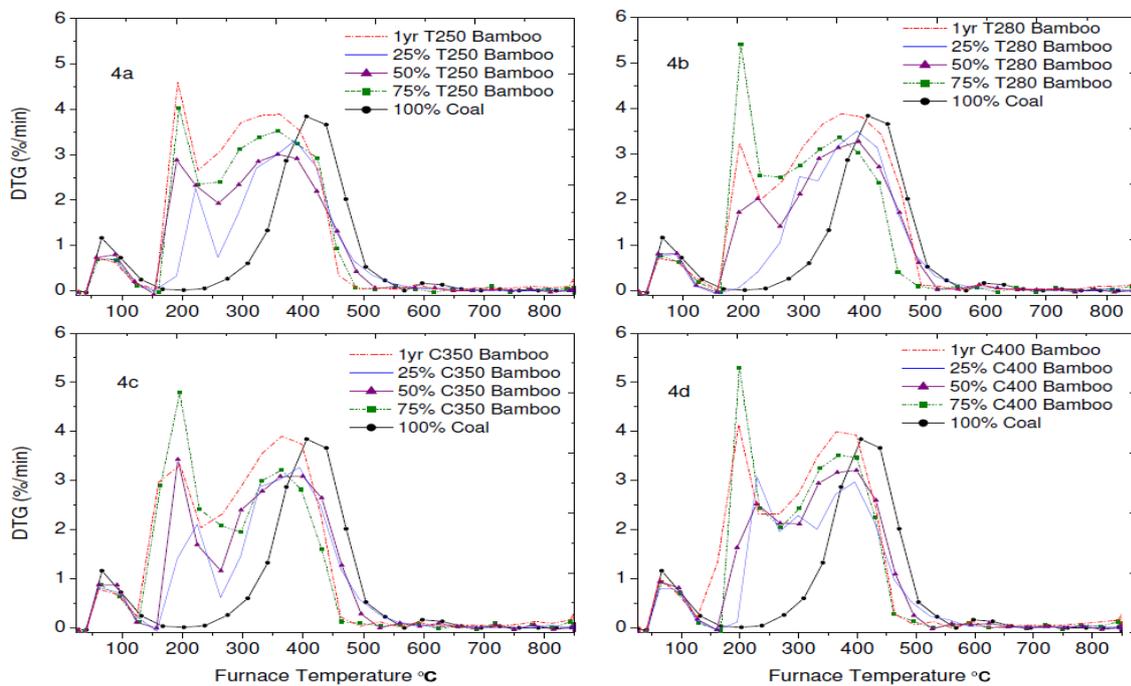


Figure 4: DTG curves of co-fired thermal treated 1year old bamboo/coal (4a; 4b; 4c and 4d)

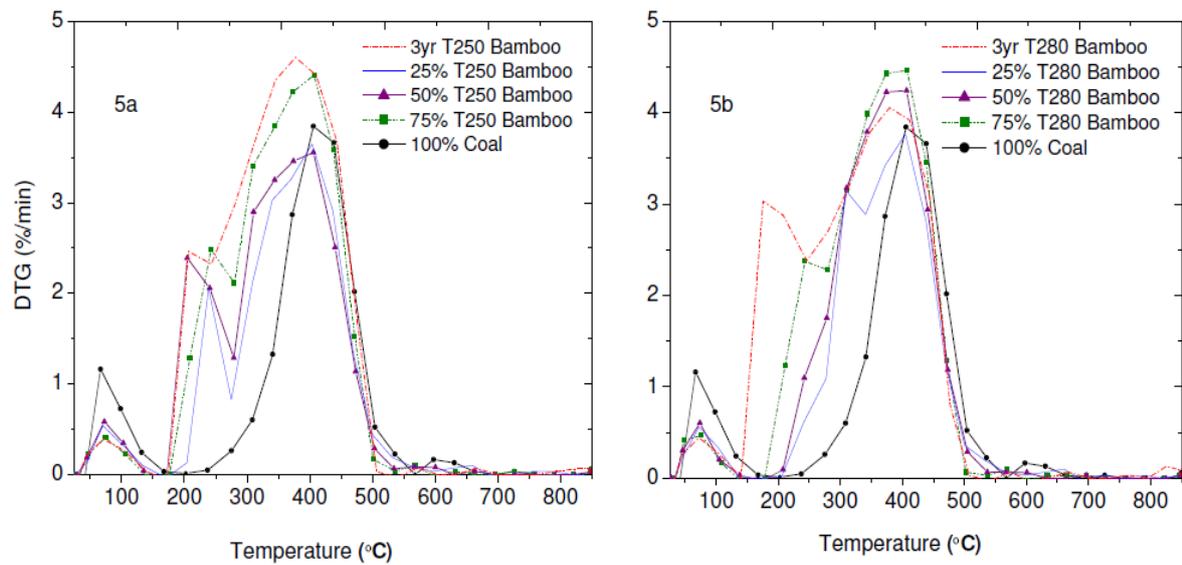


Figure 5a & 5b: DTG curves for co-combustion of 3 year T250 & T280/coal

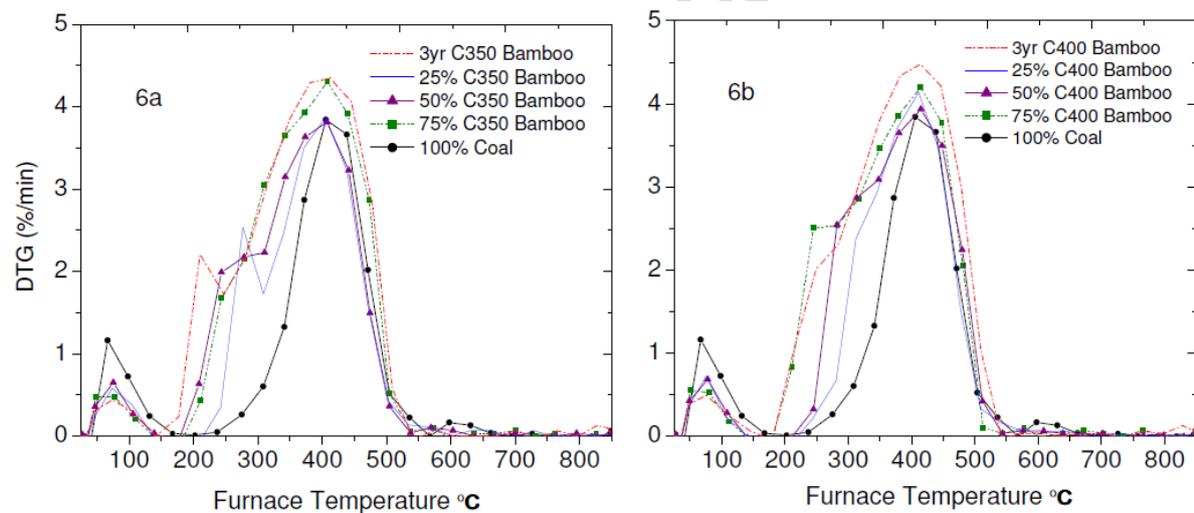


Figure 6a & 6b: DTG curves for co-combustion of 3 year C350 & C400/coal

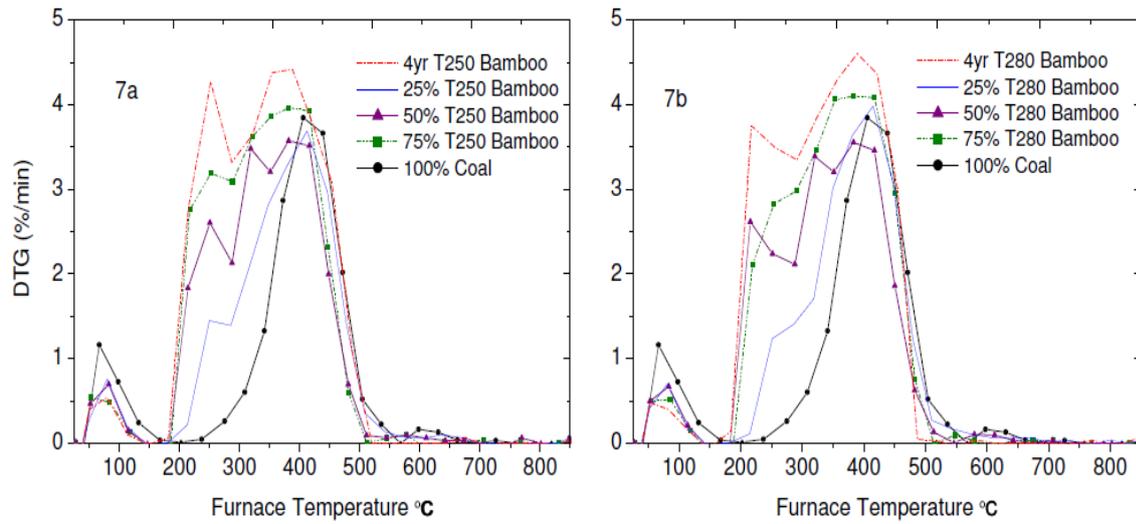


Figure 7a & 7b: DTG curves for co-combustion of 4 year T250 & T280/coal

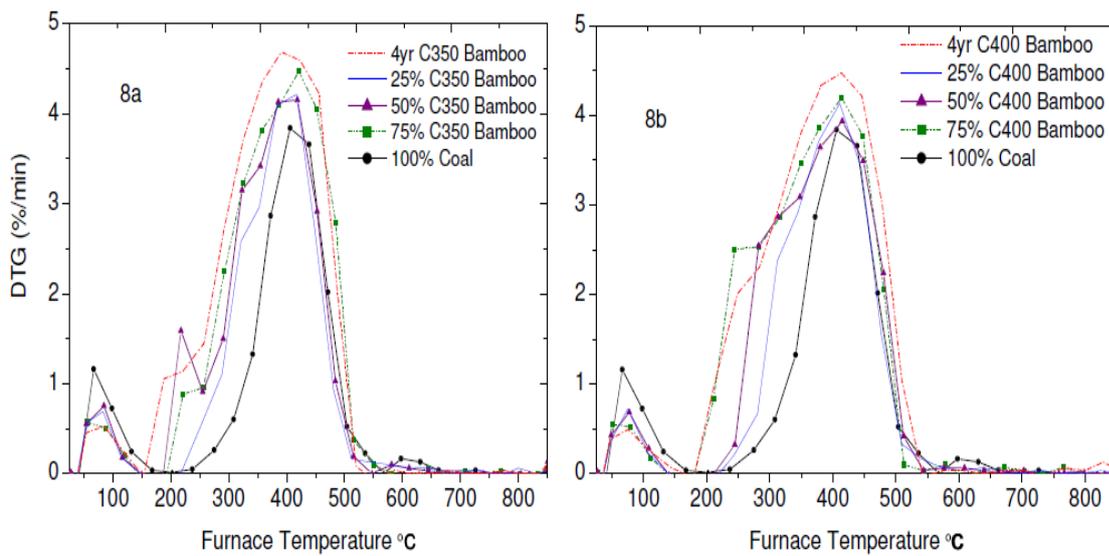


Figure 8a and 8b: DTG curves for co-combustion of 4 year C350 and C400/coal

Table 1: Fuel properties of raw and thermally treated bamboo.

<b>Sample ID</b>	Nitrogen	Total carbon	Hydrogen	Total sulphur	Oxygen		
1 year bamboo	0.88	44.91	6.17	0.07	39.14		
3 year bamboo	0.41	46.76	6.22	0.02	37.21		
4 year bamboo	0.32	46.52	6.26	0.03	37.37		
Coal	1.07	38.58	5.13	0.58	3.64		
	M (%)	FC (%)	VM (%)	Ash (%)	FC db.%	VM db.%	Ash db.%
<b>1 year bamboo</b>	7.97	16.59	74.58	0.86	18.03	81.04	0.93
1 year T250	1.26	45.58	50.72	2.44	46.16	51.36	2.47
1 year T280	0.92	50.21	46.41	2.47	50.67	46.84	2.49
1 year C350	2.52	66.91	27.02	3.56	68.64	27.72	3.65
1 year C400	1.99	68.55	26.88	2.58	69.94	27.43	2.63
<b>3 year bamboo</b>	7.01	16.97	73.64	2.37	18.25	79.20	2.55
3 year T250	3.05	52.32	38.33	6.30	53.97	39.54	6.50
3 year T280	3.18	64.60	25.10	7.13	66.71	25.92	7.36
3 year C350	3.30	66.34	22.13	8.25	68.60	22.88	8.53
3 year C400	4.14	68.46	18.90	8.50	71.42	19.72	8.87
<b>4 year bamboo</b>	8.09	17.69	72.81	1.41	19.25	79.22	1.53
4 year T250	1.41	57.76	37.25	3.59	58.58	37.78	3.64
4 year T280	1.62	62.61	31.63	4.15	63.64	32.15	4.21
4 year C350	2.07	71.62	21.62	4.69	73.14	22.08	4.78
4 year C400	2.62	74.59	17.75	5.04	76.60	18.23	5.18
Coal	6.28	29.64	19.36	44.72	31.63	20.66	47.72

M: Inherent Moisture; FC: Fixed carbon; VM: Volatile matter; and db: Dry basis and O: Oxygen by difference [100-(M+Ash+S+H+C+N)]

Table 2: Mass and Energy yield of thermally treated bamboo

Sample ID	Mass loss (%)	$\eta_M$	$\eta_E$	$R_m$ (%/min/K)	CV (MJ/Kg)
Raw 1 year	-	-	-	2.59	18.53
1 year T250	60.7	0.39	0.55	0.99	25.94
1 year T280	67.7	0.32	0.48	0.61	27.78
1 year C350	69.6	0.30	0.47	0.61	28.51
1 year C400	70.9	0.29	0.45	0.63	28.54
Raw 3 year	-	-	-	2.40	17.10
3 year T250	59.8	0.40	0.64	0.71	27.34
3 year T280	64.4	0.36	0.59	0.61	28.39
3 year C350	68.7	0.31	0.55	0.63	29.76
3 year C400	69.4	0.31	0.54	0.65	30.17
Raw 4 year	-	-	-	2.25	17.63
4 year T250	48.6	0.51	0.74	0.67	25.46
4 year T280	54.5	0.46	0.68	0.69	26.38
4 year C350	67.6	0.32	0.54	0.71	29.16
4 year C400	70.3	0.30	0.51	0.66	30.24
Coal	-	-	-	0.55	12.70

$n_M$ : Mass yield;  $n_E$ : Energy yield; CV: Calorific value;  $R_m$ : Reactivity