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# External stability and $H_\infty$ control of switching systems with delay and impulse

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## Abstract

In this paper, we investigate the external stability and  $H_\infty$  control of switching systems with time-varying delay and impulse. First of all, a modified two-direction inequality (relation) between the switching numbers and the maximum, minimum dwell time is proposed. This new inequality is applied to proving the external stability of switching systems with delay and impulse consisting of subsystems with Hurwitz stable matrices of internal dynamics. By using this new inequality, a normal  $L_2$  norm constraint is derived rather than weighted  $L_2$  norm constraint. In addition, by a realizable switching law, the obtained result is extended to the switching systems comprised of subsystems with both Hurwitz stable and unstable matrices of internal dynamics. The results are finally applied to  $H_\infty$  control and illustrated by a numerical example.

**Keywords:** External stability;  $H_\infty$  control; Switching systems; Impulse; Maximum (minimum) dwell time

## 1 Introduction

External stability (ES) is defined as a property of control systems: every  $L_2$  input generates an  $L_2$  zero-state output [1–4], which plays an essential role in system analysis. As one type of systems, switching systems (SSs), consisting of a family of subsystems, and a switching rule that orchestrates the switching between them [5–8], have been an important framework in the area of input–output analysis. In practice, effects of time delay [9, 10] and impulse [11, 12] are usually inevitable. Therefore, there are lots of results on system and input–output analysis of delayed SSs [11–21]. For example of a discrete-time framework, the problem of robust exponential  $H_\infty$  filtering for switched fuzzy delayed systems was investigated in [15]; for example of a continuous-time framework, in [11], fault-tolerant synchronization for SSs with delay and impulse was considered.

In the field of ES,  $H_\infty$  control,  $H_\infty$  model reduction,  $L_2$ -gain analysis and disturbance attenuation for the SSs, how to obtain the  $L_2$  norm bound constraint is a critical part of our study. Owing to the essence of SSs and average dwell time (DT) scheme, the concept of weighted  $L_2$  norm bound constraint, instead of the normal  $L_2$  norm bound constraint, has been proposed [16, 17, 22]. However, this weighted concept changes the original physical meaning of  $L_2$ . Recently, some researchers tried to remove this label “weighted”, see

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[18] in 2012, [23] in 2016 and [19] in 2017. However, there are still some doubtful problems. Specifically, Liu and Yuan adopted a normal  $L_2$  relation between input and output in [18] but where the average DT could not be substituted into the integral in (36); In [23], Eq. (21) could not be directly derived because  $\Psi(s)$  could not be guaranteed greater than zero; Syed Ali et al. employed the square of  $L_2$  norm, see (6) in [19], but it is questionable for the cancelation of  $e^{\alpha(T-s)}$  on both sides of the inequality right below (57). Very recently, a two-direction inequality ( $\frac{t-\tau}{T_{\max}} \leq N_\sigma(t, \tau) \leq \frac{t-\tau}{T_{\min}}$ ) between the switching numbers and the maximum, minimum DT was proposed in [11] such that the label “weighted” can be removed properly. Furthermore, an improved two-direction inequality ( $\frac{t-\tau}{T_{\max}} - 1 \leq N_\sigma(t, \tau) \leq \frac{t-\tau}{T_{\min}} + 1$ ) was provided in [24, 25]. But this improved inequality is still not precise enough. A more accurate two-direction inequality ( $\max\{\frac{t-\tau}{T_{\max}} - 1, 0\} \leq N_\sigma(t, \tau) \leq \frac{t-\tau}{T_{\min}} + 1$ ) was given in [21]. To the best of our knowledge, this more accurate two-direction inequality has not been used to study the ES and  $H_\infty$  control of SSs with delay and impulse.

In order to study the ES of SSs comprised of subsystems with both Hurwitz stable and unstable matrices, a suitable switching law is necessary. There are a few results that have been reported in [22, 25–29]. Some state-dependent switching laws were proposed in [27, 28], while some time-dependent switching laws were presented [22, 25, 26, 29]. The authors of [29] applied fast switching and slow switching, respectively, to unstable and stable subsystems. In [26], the precondition  $\inf_{t \geq t_0} [\frac{T^-(t)}{T^+(t)}] \geq -\frac{\beta}{\alpha}$  was given to guarantee that  $-\gamma t = T^-(t)\alpha + T^+(t)\beta < 0$  holds. But this precondition cannot make sure that  $-\gamma t = T^-(t)\alpha + T^+(t)\beta$  holds or that  $T^-(t)\alpha + T^+(t)\beta$  is a linear function as desired. Only  $T^-(t)\alpha + T^+(t)\beta < 0$  can be deduced there. Another resolution was proposed in [22], a new separation of switching instants was arranged in advance. By a given parameter  $c_* > 0$  without a specified sequence of time instants, the switching law in [25] is easier and clearer to implement than the one in [22]. This makes it worth to study how to adopt the switching law in [25] to investigate the ES and  $H_\infty$  control of SSs with delay and impulse.

Motivated by the above discussion, the problem of ES and  $H_\infty$  control of SSs with delay and impulse is investigated in this paper. The main contribution of the paper is as follows. First, a two-direction inequality (relation) between the switching numbers and the maximum, minimum DT is used such that the label “weighted” can be removed properly and the normal  $L_2$  norm constraint is derived. Second, a suitable switching law is adopted to deal with the SSs with both Hurwitz stable and unstable subsystems. Third, we take the overlooked case  $0 < \mu < 1$  into consideration (in almost all mentioned results above the range of  $\mu$  is only larger or equal to 1), i.e. the range of switching parameters  $\mu$  is extended to the set of all positive real numbers. Fourth, the non-weighted  $H_\infty$  control [30–32] of switching control systems with delay and impulse is established, in which the matrices of internal dynamics of the controlled system are not necessarily all Hurwitz as usual. Finally, the effectiveness of the results is illustrated by a numerical example.

## 2 Problem statement and preliminaries

Let  $\mathbb{R}^n$  denote the  $n$ -dimensional real Euclidean space. For  $x \in \mathbb{R}^n$ ,  $\|x\|$  denotes the Euclidean norm of  $x$ . We use the notation  $L_2([0, \infty), \mathbb{R}^n)$  to denote the class of square integrable functions from  $[0, \infty)$  to  $\mathbb{R}^n$ , i.e. for each  $x \in L_2([0, \infty), \mathbb{R}^n)$ , the  $L_2$  norm of  $x$  is  $\|x\|_{L_2} = (\int_0^\infty \|x(t)\|^2 dt)^{\frac{1}{2}} < \infty$ . Define  $x_t(s) = x(t+s)$ ,  $-d \leq s \leq 0$ , and  $\|x_t\|_d = \sup_{-d \leq s \leq 0} \|x(t+s)\|$ . The notation  $P > 0$  indicates that matrix  $P$  is positive definite.  $\lambda_{\max}(P)$  ( $\lambda_{\min}(P)$ ) denotes the maximum (minimum) eigenvalue of matrix  $P$ .  $\alpha_-$  means such a positive number that the inequality  $A_i^T P_i + P_i A_i + \alpha_- P_i < 0$  holds where  $A_i$  is Hurwitz stable,

while  $\alpha_+$  means such a positive number that  $A_i^T P_i + P_i A_i - \alpha_+ P_i < 0$  holds where  $A_i$  is not Hurwitz stable.

Consider the following switching control system with delay and impulse:

$$\begin{aligned} \dot{x}(t) &= A_{\sigma(t)}x(t) + A_{d\sigma(t)}x(t - \tau(t)) + B_{\sigma(t)}u(t), \quad t \in [t_{k-1}, t_k), \\ \Delta x &= x(t_k) - x(t_k^-) = I_{\sigma(t_k^-)}x(t_k^-), \quad t = t_k, \\ y(t) &= C_{\sigma(t)}x(t) + C_{d\sigma(t)}x(t - \tau(t)) + E_{\sigma(t)}u(t), \\ x_{t_0} &= x(t_0 + \theta) = \phi(\theta), \quad \theta \in [-d, 0], \end{aligned} \tag{1}$$

where  $x(t) \in \mathbb{R}^n$ ,  $u(t) \in \mathbb{R}^m$  and  $y(t) \in \mathbb{R}^p$  represent the state vector, external input vector and output vector, respectively.  $A_{\sigma(t)}$ ,  $A_{d\sigma(t)}$ ,  $B_{\sigma(t)}$ ,  $C_{\sigma(t)}$ ,  $C_{d\sigma(t)}$ ,  $E_{\sigma(t)}$  and  $I_{\sigma(t)}$  are constant matrices with appropriate dimensions, where  $\sigma(t)$  is the switching signal, which takes values from  $\mathcal{P} = \{1, 2, \dots\}$  and  $\sigma(t) = i \in \mathcal{P}$  means the subsystem  $i$  is active at  $t$ . The switching time instants  $t_k$  ( $k = 1, 2, \dots$ ) satisfy  $0 \leq t_0 < t_1 < t_2 < \dots < t_k < \dots$ ,  $\lim_{k \rightarrow \infty} t_k = \infty$ . The initial function  $\phi(\theta)$  is piecewise continuous on  $[-d, 0]$ . The delay function  $\tau(t)$  is differentiable and satisfies  $0 \leq \tau(t) \leq d$ ,  $\dot{\tau}(t) \leq \rho < 1$ .

*Remark 2.1* Here  $\dot{x}$  is considered as the right derivative of  $x$  based on two considerations. On the one hand, the derivative at  $t_0$  is taken to be a right derivative, since  $\phi(\theta)$  may not admit a left derivative at  $t_0$  or this left derivative even exists but may not equal the right hand function. To be consistent with the derivative at  $t_0$ ,  $\dot{x}(t_k)$  needs to be the notation of the right derivative at  $t_k$ . On the other hand, at  $t_k$ , the subsystem  $\sigma(t_k) = \sigma(t_k^+)$  is already active, i.e.  $\dot{x}(t) = A_{\sigma(t_k^+)}x(t) + A_{d\sigma(t_k^+)}x(t - \tau(t)) + B_{\sigma(t_k^+)}u(t)$ . It follows that  $\dot{x}(t_k)$  also denotes the right derivative at  $t_k$ .

*Remark 2.2* The solution  $x(t)$  is right continuous at  $t_k$ , i.e.  $x(t_k^+) = x(t_k)$ , since  $\dot{x}(t_k)$  represents the right derivative at  $t_k$  and the right derivative is defined based on right continuity.

**Definition 2.1** ([1]) The  $L_2$  gain of an externally stable system is

$$\gamma = \sup_{u \in L_2, u \neq \theta} \frac{\|y\|_{L_2}}{\|u\|_{L_2}}.$$

(Here  $\theta$  indicates the zero function.) The  $L_2$  gain is the maximum ratio of  $\|y\|_{L_2} / \|u\|_{L_2}$ .

**Lemma 2.1** ([21]) For any  $t \geq \tau \geq t_0$ ,  $N_\sigma(t, \tau)$  denote the number of discontinuities of region over  $(\tau, t)$ , i.e., the number of region switching over  $(\tau, t)$ ,

$$\max \left\{ \frac{t - \tau}{T_{\max}} - 1, 0 \right\} \leq N_\sigma(t, \tau) \leq \frac{t - \tau}{T_{\min}} + 1, \tag{2}$$

where  $T_{\max} = \sup_{k=1,2,\dots} (t_k - t_{k-1})$ ,  $T_{\min} = \inf_{k=1,2,\dots} (t_k - t_{k-1})$  are the maximum and minimum DT of system (1).

### 3 Main results

At the beginning of this section, the ES of SSSs with delay and impulse consisting of subsystems with Hurwitz  $A_i$ 's is proved. Then the obtained result is extended to the ES of SSSs,

in which not all subsystems are Hurwitz stable, by employing a switching law. In obtained results, the normal  $L_2$  norm constraint, rather than a weighted  $L_2$  norm constraint, is derived by using the new proposed relation (2). Finally, the derived results of ES is applied to  $H_\infty$  control.

### 3.1 External stability

In this subsection, by using Eq. (2), the ES of SSs with delay and impulse consisting of subsystems that are all Hurwitz stable, and subsystems that are not all Hurwitz stable, is proved, respectively.

#### 3.1.1 All subsystems are Hurwitz stable

**Theorem 3.1** *Given scalars  $\alpha > 0, \mu > 0$  and the numbers of any two consecutive subsystems  $i, j \in \mathcal{P}$  ( $\sigma$  switches from  $j$  to  $i$ ), the system (1) is externally stable with a  $L_2$  gain  $\gamma$ , if there exist  $n \times n$  positive definite matrices  $P_i, Q_i, P_j, Q_j$  such that*

$$\begin{bmatrix} A_i^T P_i + P_i A_i + \alpha P_i + Q_i & P_i A_{di} & P_i B_i & C_i^T \\ * & -(1 - \rho)e^{-\alpha d} Q_i & 0 & C_{di}^T \\ * & * & -F_\mu^2 I & E_i^T \\ * & * & * & -I \end{bmatrix} < 0, \tag{3}$$

$$\begin{bmatrix} \mu P_j & (I + I_j)^T P_i \\ * & P_i \end{bmatrix} \geq 0, \quad Q_i \leq \mu Q_j, \tag{4}$$

and

$$\alpha > \frac{\ln \mu}{T_{\min}}, \tag{5}$$

where  $F_\mu = \frac{\gamma}{\mu} \sqrt{\frac{\alpha - \ln \mu / T_{\min}}{\alpha - \ln \mu / T_{\max}}}$  if  $\mu > 1$ ;  $F_\mu = \gamma$  if  $\mu = 1$ ;  $F_\mu = \gamma \mu \sqrt{\frac{\alpha - \ln \mu / T_{\max}}{\alpha - \ln \mu / T_{\min}}}$  if  $0 < \mu < 1$ .

*Proof* Consider the following Lyapunov functional candidate:

$$V_{\sigma(t)}(t, x_t) = V_{1\sigma(t)}(t, x_t) + V_{2\sigma(t)}(t, x_t), \tag{6}$$

where  $V_{1\sigma(t)}(t, x_t) = x^T(t) P_{\sigma(t)} x(t)$  and  $V_{2\sigma(t)}(t, x_t) = \int_{t-\tau(t)}^t x^T(s) e^{\alpha(s-t)} Q_{\sigma(t)} x(s) ds$ . For simplicity, we shall use  $V_{\sigma(t)}(t)$  to denote  $V_{\sigma(t)}(t, x_t)$ .

Suppose  $\sigma(t) = i$  for  $t \in [t_{k-1}, t_k)$ , then the derivatives of  $V_{1\sigma(t)}(t)$  and  $V_{2\sigma(t)}(t)$  are

$$\begin{aligned} \dot{V}_{1\sigma(t)}(t) &= \dot{V}_{1i}(t) \\ &= \dot{x}^T(t) P_i x(t) + x^T(t) P_i \dot{x}(t) \\ &= [A_i x(t) + A_{di} x(t - \tau(t)) + B_i u(t)]^T P_i x(t) \\ &\quad + x^T(t) P_i [A_i x(t) + A_{di} x(t - \tau(t)) + B_i u(t)] \\ &= x^T(t) (A_i^T P_i + P_i A_i) x(t) + x^T(t - \tau(t)) A_{di}^T P_i x(t) \\ &\quad + x^T(t) P_i A_{di} x(t - \tau(t)) + u^T(t) B_i^T P_i x(t) + x^T(t) P_i B_i u(t) \end{aligned} \tag{7}$$

and

$$\begin{aligned}
 \dot{V}_{2\sigma}(t) &= \dot{V}_{2i}(t) \\
 &= -\alpha \int_{t-\tau(t)}^t x^T(s)e^{\alpha(s-t)} Q_i x(s) ds + x^T(t) Q_i x(t) \\
 &\quad - [1 - \dot{\tau}(t)] e^{-\alpha\tau(t)} x^T(t - \tau(t)) Q_i x(t - \tau(t)) \\
 &\leq -\alpha V_{2i}(t) + x^T(t) Q_i x(t) - (1 - \rho) e^{-\alpha d} x^T(t - \tau(t)) Q_i x(t - \tau(t)),
 \end{aligned} \tag{8}$$

respectively.

Denote  $\Delta(t) = y^T(t)y(t) - F_\mu^2 u^T(t)u(t)$ . Then we get

$$\begin{aligned}
 &\dot{V}_i(t) + \alpha V_i(t) + \Delta(t) \\
 &\leq x^T(t)(A_i^T P_i + P_i A_i)x(t) + x^T(t - \tau(t))A_{di}^T P_i x(t) + x^T(t)P_i A_{di}x(t - \tau(t)) \\
 &\quad + u^T(t)B_i^T P_i x(t) + x^T(t)P_i B_i u(t) - \alpha V_{2i}(t) + x^T(t)Q_i x(t) \\
 &\quad - (1 - \rho)e^{-\alpha d} x^T(t - \tau(t))Q_i x(t - \tau(t)) + \alpha x^T(t)P_i x(t) + \alpha V_{2i}(t) \\
 &\quad + x^T(t)C_i^T C_i x(t) + x^T(t)C_{di}^T C_{di}x(t - \tau(t)) + x^T(t)C_i^T E_i u(t) \\
 &\quad + x^T(t - \tau(t))C_{di}^T C_{di}x(t) + x^T(t - \tau(t))C_{di}^T C_{di}x(t - \tau(t)) \\
 &\quad + x^T(t - \tau(t))C_{di}^T E_i u(t) + u^T(t)E_i^T C_i x(t) + u^T(t)E_i^T C_{di}x(t - \tau(t)) \\
 &\quad + u^T(t)E_i^T E_i u(t) - F_\mu^2 u^T(t)u(t) \\
 &= \eta^T(t) \begin{bmatrix} (1, 1) & P_i A_{di} + C_i^T C_{di} & P_i B_i + C_i^T E_i \\ * & -(1 - \rho)e^{-\alpha d} Q_i + C_{di}^T C_{di} & C_{di}^T E_i \\ * & * & E_i^T E_i - F_\mu^2 I \end{bmatrix} \eta(t),
 \end{aligned}$$

where  $\eta(t) = [x^T(t), x^T(t - \tau(t)), u^T(t)]^T$  and  $(1, 1) = A_i^T P_i + P_i A_i + \alpha P_i + Q_i + C_i^T C_i$ .

From (3), by using the Schur complement [33], we obtain

$$\begin{aligned}
 &\begin{bmatrix} A_i^T P_i + P_i A_i + \alpha P_i + Q_i & P_i A_{di} & P_i B_i \\ * & -(1 - \rho)e^{-\alpha d} Q_i & 0 \\ * & * & -F_\mu^2 I \end{bmatrix} - \begin{bmatrix} C_i^T \\ C_{di}^T \\ E_i^T \end{bmatrix} (-I)^{-1} \begin{bmatrix} C_i & C_{di} & E_i \end{bmatrix} \\
 &= \begin{bmatrix} (1, 1) & P_i A_{di} + C_i^T C_{di} & P_i B_i + C_i^T E_i \\ * & -(1 - \rho)e^{-\alpha d} Q_i + C_{di}^T C_{di} & C_{di}^T E_i \\ * & * & E_i^T E_i - F_\mu^2 I \end{bmatrix} < 0.
 \end{aligned}$$

Therefore, we can deduce that

$$\dot{V}_i(t) + \alpha V_i(t) + \Delta(t) \leq 0. \tag{9}$$

Thus, integrating the inequality (9) from  $t_{k-1}$  to  $t$ ,  $t \in [t_{k-1}, t_k)$ , produces

$$V_i(t) \leq V_i(t_{k-1})e^{-\alpha(t-t_{k-1})} - \int_{t_{k-1}}^t \Delta(s)e^{-\alpha(t-s)} ds. \tag{10}$$

Since  $\sigma$  switches from  $j$  to  $i$ ,  $\sigma(t_{k-1}^-) = j$  and  $\sigma(t_{k-1}^+) = \sigma(t_{k-1}) = i$ . Now we consider the change of  $V_{\sigma(t)}(t)$  at  $t = t_{k-1}$  as follows. Firstly,

$$\begin{aligned} &V_{1\sigma(t_{k-1}^+)}(t_{k-1}^+) - \mu V_{1\sigma(t_{k-1}^-)}(t_{k-1}^-) \\ &= V_{1i}(t_{k-1}^+) - \mu V_{1j}(t_{k-1}^-) \\ &= x^T(t_{k-1}^+)P_i x(t_{k-1}^+) - \mu x^T(t_{k-1}^-)P_j x(t_{k-1}^-) \\ &= x^T(t_{k-1}^-)[(I + I_j)^T P_i(I + I_j) - \mu p_j]x(t_{k-1}^-). \end{aligned}$$

Using the Schur complement again, it follows from the first inequality in (4) that  $(I + I_j)^T P_i(I + I_j) - \mu p_j \leq 0$  such that  $V_{1i}(t_{k-1}) = V_{1i}(t_{k-1}^+) \leq \mu V_{1j}(t_{k-1}^-)$ . Secondly,

$$\begin{aligned} &V_{2\sigma(t_{k-1}^+)}(t_{k-1}^+) - \mu V_{2\sigma(t_{k-1}^-)}(t_{k-1}^-) \\ &= V_{2i}(t_{k-1}^+) - \mu V_{2j}(t_{k-1}^-) \\ &= \int_{t_{k-1}^+ - \tau(t_{k-1}^+)}^{t_{k-1}^+} x^T(s)e^{\alpha(s-t_{k-1}^+)} Q_{\sigma(t_{k-1}^+)} x(s) ds \\ &\quad - \int_{t_{k-1}^- - \tau(t_{k-1}^-)}^{t_{k-1}^-} x^T(s)e^{\alpha(s-t_{k-1}^-)} \mu Q_{\sigma(t_{k-1}^-)} x(s) ds \\ &= \int_{t_{k-1} - \tau(t_{k-1})}^{t_{k-1}} x^T(s)e^{\alpha(s-t_{k-1})} Q_i x(s) ds \\ &\quad - \int_{t_{k-1} - \tau(t_{k-1})}^{t_{k-1}} x^T(s)e^{\alpha(s-t_{k-1})} \mu Q_j x(s) ds \\ &= \int_{t_{k-1} - \tau(t_{k-1})}^{t_{k-1}} x^T(s)e^{\alpha(s-t_{k-1})} (Q_i - \mu Q_j) x(s) ds. \end{aligned}$$

The second inequality in (4) and the calculation above together imply that  $V_{2i}(t_{k-1}) = V_{2i}(t_{k-1}^+) \leq \mu V_{2j}(t_{k-1}^-)$ . Thus, one has

$$V_i(t_{k-1}) \leq \mu V_j(t_{k-1}^-). \tag{11}$$

Using the technique in (2.7) of [22], it follows from (10) and (11) that

$$\begin{aligned} V_i(t) &\leq \mu V_j(t_{k-1}^-) e^{-\alpha(t-t_{k-1})} - \int_{t_{k-1}}^t \Delta(s) e^{-\alpha(t-s)} ds \\ &\leq \mu \left[ V_j(t_{k-2}) e^{-\alpha(t_{k-1}-t_{k-2})} - \int_{t_{k-2}}^{t_{k-1}} \Delta(s) e^{-\alpha(t_{k-1}-s)} ds \right] \\ &\quad \times e^{-\alpha(t-t_{k-1})} - \int_{t_{k-1}}^t \Delta(s) e^{-\alpha(t-s)} ds \\ &\leq \dots \\ &= \mu^{N_{\sigma}(t,t_0)} V_{\sigma(t_0)}(t_0) e^{-\alpha(t-t_0)} - \mu^{N_{\sigma}(t,t_0)} \int_{t_0}^{t_1} \Delta(s) e^{-\alpha(t-s)} ds \\ &\quad - \mu^{N_{\sigma}(t,t_1)} \int_{t_1}^{t_2} \Delta(s) e^{-\alpha(t-s)} ds - \dots - \mu^{N_{\sigma}(t,t_{k-1})} \int_{t_{k-1}}^t \Delta(s) e^{-\alpha(t-s)} ds \end{aligned} \tag{12}$$

$$\begin{aligned}
 &= V_{\sigma(t_0)}(t_0)e^{-\alpha(t-t_0)+N_{\sigma}(t,t_0)\ln\mu} - \int_{t_0}^{t_1} \Delta(s)e^{-\alpha(t-s)+N_{\sigma}(t,s)\ln\mu} ds \\
 &\quad - \int_{t_1}^{t_2} \Delta(s)e^{-\alpha(t-s)+N_{\sigma}(t,s)\ln\mu} ds - \dots - \int_{t_{k-1}}^t \Delta(s)e^{-\alpha(t-s)+N_{\sigma}(t,s)\ln\mu} ds \\
 &\leq V_{\sigma(t_0)}(t_0)e^{-\alpha(t-t_0)+N_{\sigma}(t,t_0)\ln\mu} - \int_{t_0}^t \Delta(s)e^{-\alpha(t-s)+N_{\sigma}(t,s)\ln\mu} ds.
 \end{aligned}$$

Under the zero initial condition, we acquire

$$\int_{t_0}^t \Delta(s)e^{-\alpha(t-s)+N_{\sigma}(t,s)\ln\mu} ds \leq -V_i(t) \leq 0. \tag{13}$$

That is,

$$\begin{aligned}
 &\int_{t_0}^t y^T(s)y(s)e^{-\alpha(t-s)+N_{\sigma}(t,s)\ln\mu} ds \\
 &\leq F_{\mu}^2 \int_{t_0}^t u^T(s)u(s)e^{-\alpha(t-s)+N_{\sigma}(t,s)\ln\mu} ds.
 \end{aligned} \tag{14}$$

To obtain the ES, we discuss (14) in three cases, that is,  $\mu > 1$ ,  $\mu = 1$  and  $0 < \mu < 1$ . For the case of  $\mu > 1$  ( $\ln\mu > 0$ ). It follows from (2) that  $\frac{\ln\mu}{T_{\max}}(t-s) - \ln\mu \leq N_{\sigma}(t,s)\ln\mu \leq \frac{\ln\mu}{T_{\min}}(t-s) + \ln\mu$ . Then inequality (14) can be rearranged as follows:

$$\begin{aligned}
 &\frac{1}{\mu} \int_{t_0}^t y^T(s)y(s)e^{-(\alpha-\frac{\ln\mu}{T_{\max}})(t-s)} ds \\
 &\leq \mu F_{\mu}^2 \int_{t_0}^t u^T(s)u(s)e^{-(\alpha-\frac{\ln\mu}{T_{\min}})(t-s)} ds,
 \end{aligned} \tag{15}$$

where  $\alpha - \frac{\ln\mu}{T_{\max}} > 0$  and  $\alpha - \frac{\ln\mu}{T_{\min}} > 0$  due to (5) and  $\alpha > 0$ .

Integrating both sides of (15) from  $t = t_0$  to  $\infty$  and interchanging the order of integrals lead to

$$\int_{t_0}^{\infty} \int_{t_0}^t y^T(s)y(s)e^{-(\alpha-\frac{\ln\mu}{T_{\max}})(t-s)} ds dt \tag{16}$$

$$\begin{aligned}
 &\leq \mu^2 F_{\mu}^2 \int_{t_0}^{\infty} \int_{t_0}^t u^T(s)u(s)e^{-(\alpha-\frac{\ln\mu}{T_{\min}})(t-s)} ds dt, \\
 &\int_{t_0}^{\infty} y^T(s)y(s)e^{-(\alpha-\frac{\ln\mu}{T_{\max}})(-s)} \int_s^{\infty} e^{-(\alpha-\frac{\ln\mu}{T_{\max}})t} dt ds \\
 &\leq \mu^2 F_{\mu}^2 \int_{t_0}^{\infty} u^T(s)u(s)e^{-(\alpha-\frac{\ln\mu}{T_{\min}})(-s)} \int_s^{\infty} e^{-(\alpha-\frac{\ln\mu}{T_{\min}})t} dt ds.
 \end{aligned} \tag{17}$$

By substituting  $F_{\mu} = \frac{\gamma}{\mu} \sqrt{\frac{\alpha-\ln\mu/T_{\min}}{\alpha-\ln\mu/T_{\max}}}$  into (17), we obtain

$$\int_{t_0}^{\infty} y^T(s)y(s) ds \leq \gamma^2 \int_{t_0}^{\infty} u^T(s)u(s) ds. \tag{18}$$

The remaining arguments for the other two cases,  $\mu = 1$  and  $0 < \mu < 1$ , are analogous to the above analysis and will not be reproduced here. Consider  $u(s) = 0$ , for  $s \in [0, t_0]$ , then

we have

$$\int_0^\infty y^T(s)y(s) ds \leq \gamma^2 \int_0^\infty u^T(s)u(s) ds, \tag{19}$$

which implies that the system (1) is externally stable with a  $L_2$  gain  $\gamma$ . □

*Remark 3.1* The switching parameter  $0 < \mu < 1$  was usually overlooked, as mentioned also in [11]. Only  $\mu \geq 1$  was considered in [16–18, 22] and in [19] that was  $\eta \geq 1$ . If the sets of those matrices (such as  $P_i, Q_i$  in this work) were finite, as assumed in [16–19, 22], it would be not easy to consider this overlooked case. However, in [11, 25] and this work, the switching index set, see  $\mathcal{P}$  below (1), is not restricted to be finite such that the just mentioned sets of matrices can be infinite. Moreover, in conditions like  $Q_i \leq \mu Q_j$ ,  $i$  and  $j$  are only any two consecutive ( $j$  is just after  $i$ ) rather than two arbitrary indices as in [16–19, 22]. These together make the case  $0 < \mu < 1$  feasible, i.e. the range of  $\mu$  can be all positive real numbers.

*Remark 3.2* It follows from (12) and Theorem 3.1, the zero-input state  $\|x(t)\| \leq K_\mu \|x_{t_0}\|_d e^{-\alpha_\mu(t-t_0)}$ , where  $K_\mu = \sqrt{\frac{\mu[\lambda_{\max}(P_{\sigma(t_0)})+d\lambda_{\max}(Q_{\sigma(t_0)})]}{\inf_{i \in \mathcal{P}}(\lambda_{\min}(P_i))}}$ ,  $\alpha_\mu = \frac{1}{2}(\alpha - \frac{\ln \mu}{T_{\min}})$  if  $\mu > 1$ ;  $K_\mu = \sqrt{\frac{\lambda_{\max}(P_{\sigma(t_0)})+d\lambda_{\max}(Q_{\sigma(t_0)})}{\inf_{i \in \mathcal{P}}(\lambda_{\min}(P_i))}}$ ,  $\alpha_\mu = \frac{1}{2}\alpha$  if  $\mu = 1$ ;  $K_\mu = \sqrt{\frac{\lambda_{\max}(P_{\sigma(t_0)})+d\lambda_{\max}(Q_{\sigma(t_0)})}{\mu \inf_{i \in \mathcal{P}}(\lambda_{\min}(P_i))}}$ ,  $\alpha_\mu = \frac{1}{2}(\alpha - \frac{\ln \mu}{T_{\max}})$  if  $0 < \mu < 1$ .

### 3.1.2 Not all subsystems are Hurwitz stable

In the following, we consider to investigate the ES of SSs consisting of subsystems that are not all Hurwitz stable.

For a subsystem  $A_i$  (Hurwitz stable), similar to (6)–(10),  $A_{di}, B_i, C_i, D_i$  on  $[t_{k-1}, t_k)$ , replacing  $\alpha$  with  $\alpha_-$  under the condition (3), then, for  $t \in [t_{k-1}, t_k)$ , we can derive that

$$V_i(t) \leq V_i(t_{k-1})e^{-\alpha_-(t-t_{k-1})} - \int_{t_{k-1}}^t \Delta(s)e^{-\alpha_-(t-s)} ds. \tag{20}$$

For a subsystem  $A_i$  (not Hurwitz), there always exist  $P_i > 0$  and  $\alpha_+ > 0$  (as long as  $\alpha_+$  is large enough), such that  $A_i^T P_i + P_i A_i - \alpha_+ P_i < 0$ . If the condition

$$\begin{bmatrix} A_i^T P_i + P_i A_i - \alpha_+ P_i + Q_i & P_i A_{di} & P_i B_i & C_i^T \\ * & -(1-\rho)e^{-\alpha d} Q_i & 0 & C_{di}^T \\ * & * & -F_\mu^2 I & E_i^T \\ * & * & * & -I \end{bmatrix} < 0 \tag{21}$$

holds, we can deduce that

$$\dot{V}_i(t) + \alpha V_{2i}(t) - \alpha_+ V_{1i}(t) + \Delta(t) \leq 0, \tag{22}$$

then

$$\dot{V}_i(t) - \alpha_+ V_i(t) + \Delta(t) \leq 0. \tag{23}$$

Therefore, the following inequality holds:

$$V_i(t) \leq V_i(t_{k-1})e^{\alpha_+(t-t_{k-1})} - \int_{t_{k-1}}^t \Delta(s)e^{\alpha_+(t-s)} ds. \tag{24}$$

Under the inequality in (4), using the same arguments as in (12), (13) and (14), from  $t_0$  to  $t$ ,  $t \in [t_{k-1}, t_k)$ , we can get

$$V_i(t) \leq V_{\sigma(t_0)}(t_0)e^{\alpha_+T_+(t,t_0)-\alpha_-T_-(t,t_0)+N_{\sigma}(t,t_0)\ln \mu} - \int_{t_0}^t \Delta(s)e^{\alpha_+T_+(t,s)-\alpha_-T_-(t,s)+N_{\sigma}(t,s)\ln \mu} ds, \tag{25}$$

And then

$$\int_{t_0}^t y^T(s)y(s)e^{\alpha_+T_+(t,s)-\alpha_-T_-(t,s)+N_{\sigma}(t,s)\ln \mu} ds \leq F_{\mu}^{-2} \int_{t_0}^t u^T(s)u(s)e^{\alpha_+T_+(t,s)-\alpha_-T_-(t,s)+N_{\sigma}(t,s)\ln \mu} ds, \tag{26}$$

where  $T_+(t, \tau)$ ,  $T_-(t, \tau)$  denote the total active time of those subsystems with Hurwitz  $A_i^T$ s, not Hurwitz  $A_i^T$ s over  $(\tau, t)$ , respectively.

Taking the case  $\mu > 1$  as an example, the exponential index on the left side of (26):  $\alpha_+T_+(t, s) - \alpha_-T_-(t, s) + N_{\sigma}(t, s)\ln \mu$  may be reduced to be  $-(\alpha_- - \frac{\ln \mu}{T_{\max}})(t - s)$ , while the same index on the right side of (26) may not be immediately increased to be in the form:  $-\lambda(t - s)$ ,  $\lambda > 0$ . Now, we choose a scalar  $\alpha_* \in (0, \alpha_-)$  arbitrarily and propose the following switching law.

**Switching Law 3.1** ([25]) *Given a sequence of time instants  $t_1 < t_2 < \dots < t_k < \dots$ ,  $\lim_{k \rightarrow \infty} t_k = \infty$ , where  $t_k, k = 1, 2, \dots$ , is the switching instant and  $t_1 > t_0$ , such that, for given scalars  $\alpha_+ > 0, \alpha_- > 0, 0 < \alpha_* < \alpha_-$  and  $c_* > 0$ , the inequality  $\alpha_+T_+(t, \tau) - \alpha_-T_-(t, \tau) \leq c_* - \alpha_*(t - \tau)$  holds, for any  $t \geq \tau \geq t_0$ .*

**Theorem 3.2** *Given scalars  $\alpha > 0, 0 < \alpha_- < \alpha, \alpha_+ > 0, c_* > 0, \mu > 0$  and the numbers of any two consecutive subsystems  $i, j \in \mathcal{P}$  ( $\sigma$  switches from  $j$  to  $i$ ), the system (1), under Switching Law 3.1, is externally stable with a  $L_2$  gain  $\gamma$ , if there exist real  $n \times n$  positive definite matrices  $P_i, Q_i, P_j, Q_j$  such that, for each subsystem ( $A_i$  is Hurwitz),*

$$\begin{bmatrix} A_i^T P_i + P_i A_i + \alpha_- P_i + Q_i & P_i A_{di} & P_i B_i & C_i^T \\ * & -(1 - \rho)e^{-\alpha d} Q_i & 0 & C_{di}^T \\ * & * & -F_{\mu}^{-2} I & E_i^T \\ * & * & * & -I \end{bmatrix} < 0; \tag{27}$$

for each subsystem ( $A_i$  is not Hurwitz),

$$\begin{bmatrix} A_i^T P_i + P_i A_i - \alpha_+ P_i + Q_i & P_i A_{di} & P_i B_i & C_i^T \\ * & -(1 - \rho)e^{-\alpha d} Q_i & 0 & C_{di}^T \\ * & * & -F_{\mu}^{-2} I & E_i^T \\ * & * & * & -I \end{bmatrix} < 0, \tag{28}$$

$$\begin{bmatrix} \mu P_j & (I + I_j)^T P_i \\ * & P_i \end{bmatrix} \geq 0, \quad Q_i \leq \mu Q_j, \tag{29}$$

and

$$\alpha_* > \frac{\ln \mu}{T_{\min}}, \tag{30}$$

where  $F_\mu = \frac{\gamma}{\mu} \sqrt{\frac{\alpha_* - \ln \mu / T_{\min}}{e^{c_*} (\alpha_- - \ln \mu / T_{\max})}}$  if  $\mu > 1$ ;  $F_\mu = \gamma \sqrt{\frac{\alpha_*}{e^{c_*} \alpha_-}}$  if  $\mu = 1$ ;  $F_\mu = \gamma \mu \sqrt{\frac{\alpha_* - \ln \mu / T_{\max}}{e^{c_*} (\alpha_- - \ln \mu / T_{\min})}}$  if  $0 < \mu < 1$ .

*Proof* Under Switching Law 3.1, one has

$$e^{\alpha_+ T_+(t,s) - \alpha_- T_-(t,s)} \leq e^{c_* - \alpha_*(t-s)}. \tag{31}$$

To obtain the ES, we also investigate (26) in three cases, that is  $\mu > 1$ ,  $\mu = 1$  and  $0 < \mu < 1$ . For the case of  $\mu > 1$ . It follows from (2) that  $\frac{\ln \mu}{T_{\max}}(t-s) - \ln \mu \leq N_\sigma(t,s) \ln \mu \leq \frac{\ln \mu}{T_{\min}}(t-s) + \ln \mu$ . From (26), we obtain

$$\int_{t_0}^t y^T(s)y(s)e^{-\alpha_-(t-s) + N_\sigma(t,s) \ln \mu} ds \leq F_\mu^2 \int_{t_0}^t u^T(s)u(s)e^{-\alpha_*(t-s) + N_\sigma(t,s) \ln \mu} ds. \tag{32}$$

Then

$$\frac{1}{\mu} \int_{t_0}^t y^T(s)y(s)e^{-(\alpha_- - \frac{\ln \mu}{T_{\max}})(t-s)} ds \leq \mu F_\mu^2 \int_{t_0}^t u^T(s)u(s)e^{-(\alpha_* - \frac{\ln \mu}{T_{\min}})(t-s)} ds. \tag{33}$$

Using  $\alpha_* > \frac{\ln \mu}{T_{\min}}$  (then  $\alpha_* - \frac{\ln \mu}{T_{\min}} > 0$  and  $\alpha_- - \frac{\ln \mu}{T_{\max}} > 0$  due to  $\alpha_* < \alpha_-$ ) and selecting  $F_\mu = \frac{\gamma}{\mu} \sqrt{\frac{\alpha_* - \ln \mu / T_{\min}}{e^{c_*} (\alpha_- - \ln \mu / T_{\max})}}$ , then following a similar process to (16) to (19), we can conclude that the control system (1), under Switching Law 3.1 is externally stable with a  $L_2$  gain  $\gamma$ .  $\square$

*Remark 3.3* It follows from (25), Switching Law 3.1 and Theorem 3.2 that the state  $\|x(t)\| \leq \hat{K}_\mu \|x_{t_0}\|_d e^{-\hat{\alpha}_\mu(t-t_0)}$ , where  $\hat{K}_\mu = e^{\frac{c_*}{2}} \sqrt{\frac{\mu[\lambda_{\max}(P_\sigma(t_0)) + d\lambda_{\max}(Q_\sigma(t_0))]}{\inf_{i \in \mathcal{P}}(\lambda_{\min}(P_i))}}$ ,  $\hat{\alpha}_\mu = \frac{1}{2}(\alpha_* - \frac{\ln \mu}{T_{\min}})$  if  $\mu > 1$ ;  $\hat{K}_\mu = e^{\frac{c_*}{2}} \sqrt{\frac{\lambda_{\max}(P_\sigma(t_0)) + d\lambda_{\max}(Q_\sigma(t_0))}{\inf_{i \in \mathcal{P}}(\lambda_{\min}(P_i))}}$ ,  $\hat{\alpha}_\mu = \frac{1}{2}\alpha_*$  if  $\mu = 1$ ;  $\hat{K}_\mu = e^{\frac{c_*}{2}} \sqrt{\frac{\lambda_{\max}(P_\sigma(t_0)) + d\lambda_{\max}(Q_\sigma(t_0))}{\mu \inf_{i \in \mathcal{P}}(\lambda_{\min}(P_i))}}$ ,  $\hat{\alpha}_\mu = \frac{1}{2}(\alpha_* - \frac{\ln \mu}{T_{\max}})$  if  $0 < \mu < 1$ .

In fact, for the case  $0 < \mu < 1$ , without Switching Law 3.1, we also have the following conclusion.

**Corollary 3.1** *Given scalars  $\alpha > 0, 0 < \alpha_- < \alpha, \alpha_+ > 0, 0 < \mu < 1$  and the numbers of any two consecutive subsystems  $i, j \in \mathcal{P}$  ( $\sigma$  switches from  $j$  to  $i$ ), the system (1) is externally stable with a  $L_2$  gain  $\gamma$ , if there exist real  $n \times n$  positive definite matrices  $P_i, Q_i, P_j, Q_j$  such that, for each subsystem ( $A_i$  is Hurwitz),*

$$\begin{bmatrix} A_i^T P_i + P_i A_i + \alpha_- P_i + Q_i & P_i A_{di} & P_i B_i & C_i^T \\ * & -(1-\rho)e^{-\alpha d} Q_i & 0 & C_{di}^T \\ * & * & -F_\mu^2 I & E_i^T \\ * & * & * & -I \end{bmatrix} < 0; \tag{34}$$

for each subsystem ( $A_i$  is not Hurwitz),

$$\begin{bmatrix} A_i^T P_i + P_i A_i - \alpha_+ P_i + Q_i & P_i A_{di} & P_i B_i & C_i^T \\ * & -(1 - \rho)e^{-\alpha d} Q_i & 0 & C_{di}^T \\ * & * & -F_\mu^2 I & E_i^T \\ * & * & * & -I \end{bmatrix} < 0, \tag{35}$$

$$\begin{bmatrix} \mu P_j & (I + I_j)^T P_i \\ * & P_i \end{bmatrix} \geq 0, \quad Q_i \leq \mu Q_j, \tag{36}$$

and

$$\alpha_+ < \frac{|\ln \mu|}{T_{\max}}, \tag{37}$$

where  $F_\mu = \gamma \mu \sqrt{\frac{-\alpha_+ + |\ln \mu|/T_{\max}}{\alpha_- + |\ln \mu|/T_{\min}}}$ .

*Proof* Taking a similar process to (20) to (26), we have

$$\begin{aligned} & \int_{t_0}^t y^T(s)y(s)e^{\alpha_+ T_+(t,s) - \alpha_- T_-(t,s) + N_\sigma(t,s) \ln \mu} ds \\ & \leq F_\mu^2 \int_{t_0}^t u^T(s)u(s)e^{\alpha_+ T_+(t,s) - \alpha_- T_-(t,s) + N_\sigma(t,s) \ln \mu} ds. \end{aligned} \tag{38}$$

Since  $\frac{t-s}{T_{\max}} - 1 \leq N_\sigma(t,s) \leq \frac{t-s}{T_{\min}} + 1$ ,  $\frac{-|\ln \mu|}{T_{\min}}(t-s) + \ln \mu \leq N_\sigma(t,s) \ln \mu \leq \frac{-|\ln \mu|}{T_{\max}}(t-s) - \ln \mu$ . Then

$$\begin{aligned} & \mu \int_{t_0}^t y^T(s)y(s)e^{-(\alpha_- + \frac{|\ln \mu|}{T_{\min}})(t-s)} ds \\ & \leq \frac{1}{\mu} F_\mu^2 \int_{t_0}^t u^T(s)u(s)e^{-(\alpha_+ + \frac{|\ln \mu|}{T_{\max}})(t-s)} ds. \end{aligned} \tag{39}$$

Suppose  $\alpha_+ < \frac{|\ln \mu|}{T_{\max}}$  and choose  $F_\mu = \gamma \mu \sqrt{\frac{-\alpha_+ + |\ln \mu|/T_{\max}}{\alpha_- + |\ln \mu|/T_{\min}}}$ . Then following a similar process to (16) to (19), we can prove that the control system (1), consisting of both subsystems with Hurwitz  $A_i$ 's and subsystems with  $A_i$ 's that are not Hurwitz, is externally stable with a  $L_2$  gain  $\gamma$ . □

*Remark 3.4* It follows from (25) and the Corollary 3.1 that, for the case  $0 < \mu < 1$ , we have the zero-input state

$$\|x(t)\| \leq \sqrt{\frac{\lambda_{\max}(P_\sigma(t_0)) + d\lambda_{\max}(Q_\sigma(t_0))}{\mu \inf_{i \in \mathcal{P}}(\lambda_{\min}(P_i))}} \|x_{t_0}\| e^{-\frac{1}{2}(-\alpha_+ + \frac{|\ln \mu|}{T_{\max}})(t-t_0)}.$$

*Remark 3.5* The Corollary 3.1 does not use Switching Law 3.1, the right side of inequality (38) is enlarged as  $F_\mu^2 \int_{t_0}^t u^T(s)u(s)e^{\alpha_+(t-s) + N_\sigma(t,s) \ln \mu} ds$  instead of  $F_\mu^2 \int_{t_0}^t u^T(s)u(s) \times$

$e^{-\alpha_+(t-s)+N_\sigma(t,s)\ln\mu} ds$ . As an additional condition,  $\alpha_+ < \frac{\ln\mu}{T_{\max}}$  is imposed. Therefore, Theorem 3.2 is less conservative.

*Remark 3.6* By employing the new proposed two-direction inequality (2), after the steps (15)–(19), (33) and (39), the normal  $L_2$  norm constraint instead of the weighted  $L_2$  norm constraint is obtained. However, only the weighted  $L_2$  norm constraint was derived in [16, 17, 22]. This can be easily seen in the proof steps (2.10)–(2.15) in [22], (33)–(34) in [16] and (49)–(50) in [17]. The “average dwell time” method is adopted in these references, that is, the one-direction inequality  $N_\sigma(0, \tau) \leq \frac{\tau}{\tau_a}$  is applied.

### 3.2 Application to $H_\infty$ control

In this section, we apply the derived results of ES to  $H_\infty$  control. The so-called  $H_\infty$  control is named from the  $H_\infty$  functions defined on the  $H_\infty$  (Hardy) space (see page 1 in [30]):  $H_\infty := \{F : C \rightarrow C \mid F \text{ is analytic, } \sup_{\operatorname{Re}(s)>0} |F(s)| < \infty\}$  equipped with the norm  $\|F\|_\infty := \sup_{\operatorname{Re}(s)>0} |F(s)|$ , for  $F \in H_\infty$ . As is well known (also see page 4 in [31]), transfer functions for finite dimensional linear control systems are rational functions with real coefficients. Thus, we may consider the subset of  $H_\infty$  consisting of real-rational functions:  $RH_\infty \subset H_\infty$ . In fact [31], a transfer function  $F(s) \in RH_\infty$  if and only if  $F$  is proper ( $\lim_{s \rightarrow \infty} F(s) < \infty$ ) and stable ( $F$  has no poles in the closed right half complex plane). In this case,  $\|F\|_\infty = \sup_{\omega \in \mathbb{R}} |F(j\omega)| = \sup_{u \in L_2, u \neq \theta} \|y\|_{L_2} / \|u\|_{L_2}$ , where  $u, y$  denote the input, output of the considered control system [1]. Therefore, the transfer function of a linear control system  $F(s)$  is a real-rational  $H_\infty$  function implies that the control system is externally stable, i.e. every  $L_2$  input only excites an  $L_2$  zero-state output. If the input is considered to be a disturbance, then ES measures the robustness of the zero-state output on the disturbance, i.e. it ensures that the zero-state output excited by the energy-bounded (because the square of the  $L_2$  norm of a signal can be considered as the energy content of the signal) disturbance will not blow up.

For linear control systems,  $H_\infty$  control is to find a control (consisting of measured variables) such that the norm of the transfer function from the disturbance (input)  $u_d$  to the output  $y$  (something we want to minimize)  $\|F_{d \rightarrow y}\|_\infty$  is minimized, i.e. the zero-state output excited by disturbance  $y_d$  is minimized [32]. For nonlinear control systems including the system considered in this paper, they do not have transfer functions as the linear ones do. However, the same name  $H_\infty$  control is employed for the following control objective: to find a control such that the controlled system is asymptotically stable when no disturbances are present, and moreover, has finite  $L_2$  gain from  $u_d$  to  $y$ , under the zero initial condition (is externally stable from  $u_d$  to  $y$ ), see page 6 in [31]. As we see above, for either linear or nonlinear control systems,  $H_\infty$  control has the same physical meaning: the  $H_\infty$  controller starts to stabilize the system after the energy-bounded disturbance has already decayed to zero, then maintains the stabilized system to be externally stable from the disturbance to the output such that effect of the disturbance on the output is attenuated during the steady period. This specializes the practical importance of  $H_\infty$  control in industry roared with noises. However, by the existing average dwell time approach, those results obtained for switched system are only on weak noise attenuation index of weighted form than cannot truly reflect the practical meaning of  $H_\infty$  problems [17].

In this section, by adopting maximum, minimum dwell time and the new proposed two-direction inequality (2), we state the details for the non-weighted  $H_\infty$  control of switching

control systems with delay and impulse. Consider (1) with both control input  $u_c$  and disturbance input  $u_d$  as follows:

$$\begin{aligned}
 \dot{x}(t) &= A_{\sigma(t)}x(t) + A_{d\sigma(t)}x(t - \tau(t)) + B_{\sigma(t)}(u_c(t) + u_d(t)), \quad t \in [t_{k-1}, t_k), \\
 \Delta x &= x(t_k) - x(t_k^-) = I_{\sigma(t_k^-)}x(t_k^-), \quad t = t_k, \\
 y(t) &= C_{\sigma(t)}x(t) + C_{d\sigma(t)}x(t - \tau(t)) + E_{\sigma(t)}(u_c(t) + u_d(t)), \\
 x_{t_0} &= x(t_0 + \theta) = \phi(\theta), \quad \theta \in [-d, 0].
 \end{aligned}
 \tag{40}$$

As just discussed, the control (input)  $u_c$  is comprised of measured variables. A special (and common) form is  $u_c = K_{\sigma(t)}x$  (state feedback), where  $K_{\sigma(t)}$  is the control gain to be designed and  $x$  is the state variable that is pre-assumed to be measurable (available). Generally,  $u_c$  may be also designed as a function of  $x_t$  (delayed state feedback),  $x(t_k^-)$  (impulsive state feedback) and  $y$  (output feedback) as needed, if they can be measured.

Controlled by  $u_c = K_{\sigma(t)}x$ , the system above can be rewritten as

$$\begin{aligned}
 \dot{x}(t) &= \bar{A}_{\sigma(t)}x(t) + A_{d\sigma(t)}x(t - \tau(t)) + B_{\sigma(t)}u_d(t), \quad t \in [t_{k-1}, t_k), \\
 \Delta x &= x(t_k) - x(t_k^-) = I_{\sigma(t_k^-)}x(t_k^-), \quad t = t_k, \\
 y(t) &= \bar{C}_{\sigma(t)}x(t) + C_{d\sigma(t)}x(t - \tau(t)) + E_{\sigma(t)}u_d(t), \\
 x_{t_0} &= x(t_0 + \theta) = \phi(\theta), \quad \theta \in [-d, 0],
 \end{aligned}
 \tag{41}$$

where  $\bar{A}_{\sigma(t)} = A_{\sigma(t)} + B_{\sigma(t)}K_{\sigma(t)}$  and  $\bar{C}_{\sigma(t)} = C_{\sigma(t)} + E_{\sigma(t)}K_{\sigma(t)}$ . The  $H_\infty$  control problem is to find  $K_{\sigma(t)}$  such that (41) is asymptotically stable when  $u_d = 0$ , and is externally stable from  $u_d$  to  $y$ , i.e.  $\|y(t)\|_{L_2} \leq \gamma^* \|u_d(t)\|_{L_2}$  for some prescribed constant  $\gamma^*$ , when  $\phi(\theta) = 0$ .

Comparing (41) with (1), it can be concluded that the objectives of  $H_\infty$  control are all achieved (since exponential stability implies asymptotic stability and the ES is already proven) in different cases if  $A_{\sigma(t)}, C_{\sigma(t)}$  are replaced by  $\bar{A}_{\sigma(t)}, \bar{C}_{\sigma(t)}$ , respectively, in the corresponding theorems. To avoid tediousness, we only state a theorem for the  $H_\infty$  control corresponding to Theorem 3.2. The result corresponding to Theorem 3.1 is left to the reader.

**Theorem 3.3** *Given scalars  $\alpha > 0, 0 < \alpha_- < \alpha, \alpha_+ > 0, c_* > 0, \mu > 0$  and the numbers of any two consecutive subsystems  $i, j \in \mathcal{P}$  ( $\sigma$  switches from  $j$  to  $i$ ), the  $H_\infty$  control problem of (40), under the switching law S3.1, is solved, if there exist real  $n \times n$  positive definite matrices  $P_i, Q_i, P_j, Q_j$  and appropriate dimensions matrices  $K_i, K_j$  such that, for each subsystem ( $\bar{A}_i$  is Hurwitz),*

$$\begin{bmatrix}
 \bar{A}_i^T P_i + P_i \bar{A}_i + \alpha_- P_i + Q_i & P_i A_{di} & P_i B_i & \bar{C}_i^T \\
 * & -(1 - \rho)e^{-\alpha d} Q_i & 0 & C_{di}^T \\
 * & * & -F_\mu^2 I & E_i^T \\
 * & * & * & -I
 \end{bmatrix} < 0;
 \tag{42}$$

for each subsystem ( $\bar{A}_i$  is not surely Hurwitz),

$$\begin{bmatrix} \bar{A}_i^T P_i + P_i \bar{A}_i - \alpha_+ P_i + Q_i & P_i A_{di} & P_i B_i & \bar{C}_i^T \\ * & -(1-\rho)e^{-\alpha d} Q_i & 0 & C_{di}^T \\ * & * & -F_\mu^2 I & E_i^T \\ * & * & * & -I \end{bmatrix} < 0, \tag{43}$$

$$\begin{bmatrix} \mu P_j & (I + I_j)^T P_i \\ * & P_i \end{bmatrix} \geq 0, \quad Q_i \leq \mu Q_j, \tag{44}$$

and

$$\alpha_* > \frac{\ln \mu}{T_{\min}}, \tag{45}$$

where  $F_\mu = \frac{\gamma^*}{\mu} \sqrt{\frac{\alpha_* - \ln \mu / T_{\min}}{e^{c_*} (\alpha_* - \ln \mu / T_{\max})}}$ , if  $\mu > 1$ ;  $F_\mu = \gamma^*$ , if  $\mu = 1$ ;  $F_\mu = \gamma^* \mu \sqrt{\frac{\alpha_* - \ln \mu / T_{\max}}{e^{c_*} (\alpha_* - \ln \mu / T_{\min})}}$ , if  $0 < \mu < 1$ .

**Remark 3.7** It follows from Remark 3.3, under the same conditions as in Theorem 3.3, the state  $\|x(t)\| \leq \tilde{K}_\mu \|x_{t_0}\|_d e^{-\tilde{\alpha}_\mu(t-t_0)}$ , where  $\tilde{K}_\mu = e^{\frac{c_*}{2}} \sqrt{\frac{\mu[\lambda_{\max}(P_\sigma(t_0)) + d\lambda_{\max}(Q_\sigma(t_0))]}{\inf_{i \in \mathcal{D}}(\lambda_{\min}(P_i))}}$ ,  $\tilde{\alpha}_\mu = \frac{1}{2}(\alpha_* - \frac{\ln \mu}{T_{\min}})$  if  $\mu > 1$ ;  $\tilde{K}_\mu = e^{\frac{c_*}{2}} \sqrt{\frac{\lambda_{\max}(P_\sigma(t_0)) + d\lambda_{\max}(Q_\sigma(t_0))}{\inf_{i \in \mathcal{D}}(\lambda_{\min}(P_i))}}$ ,  $\tilde{\alpha}_\mu = \frac{1}{2}\alpha_*$  if  $\mu = 1$ ;  $\tilde{K}_\mu = e^{\frac{c_*}{2}} \sqrt{\frac{\lambda_{\max}(P_\sigma(t_0)) + d\lambda_{\max}(Q_\sigma(t_0))}{\mu \inf_{i \in \mathcal{D}}(\lambda_{\min}(P_i))}}$ ,  $\tilde{\alpha}_\mu = \frac{1}{2}(\alpha_* - \frac{\ln \mu}{T_{\max}})$  if  $0 < \mu < 1$ .

**Remark 3.8** After substituting  $\bar{A}_i, \bar{C}_i$ , nonlinear terms like  $P_i B_i K_i$  and  $K_i^T B_i^T P_i$  appear in (42) and (43). We can first left and right multiply (42), (43) by  $\text{diag}(P_i^{-1}, I, I, I)$ . Then we apply the Schur complement and use  $-Q_i^{-1} \leq -2\epsilon_i I + \epsilon_i^2 Q_i, \epsilon_i > 0$  to derive the following linear matrix inequalities of  $P_i^{-1}, Q_i$  and  $Y_i$ :

$$\begin{bmatrix} (1, 1)_1 & A_{di} & B_i & P_i^{-1} C_i^T + Y_i^T E_i^T & P_i^{-1} \\ * & -(1-\rho)e^{-\alpha d} Q_i & 0 & C_{di}^T & 0 \\ * & * & -F_\mu^2 I & E_i^T & 0 \\ * & * & * & -I & 0 \\ * & * & * & * & -2\epsilon_i I + \epsilon_i^2 Q_i \end{bmatrix} < 0,$$

$$\begin{bmatrix} (1, 1)_2 & A_{di} & B_i & P_i^{-1} C_i^T + Y_i^T E_i^T & P_i^{-1} \\ * & -(1-\rho)e^{-\alpha d} Q_i & 0 & C_{di}^T & 0 \\ * & * & -F_\mu^2 I & E_i^T & 0 \\ * & * & * & -I & 0 \\ * & * & * & * & -2\epsilon_i I + \epsilon_i^2 Q_i \end{bmatrix} < 0,$$

where  $(1, 1)_1 = A_i P_i^{-1} + P_i^{-1} A_i^T + \alpha_- P_i^{-1} + B_i Y_i + Y_i^T B_i^T, (1, 1)_2 = A_i P_i^{-1} + P_i^{-1} A_i^T - \alpha_+ P_i^{-1} + B_i Y_i + Y_i^T B_i^T$  and  $Y_i = K_i P_i^{-1}$ , obeying (42), (43), respectively. It follows that  $K_i = Y_i P_i$ .

As for the first inequality in (44), we can first left and right multiply it by  $\text{diag}(P_i^{-1}, I)$ . Then left and right multiply it by  $\text{diag}(I, P_i^{-1})$  to derive an equivalent linear matrix inequality

ity as

$$\begin{bmatrix} \mu P_j^{-1} & P_j^{-1}(I + I_j)^T \\ * & P_i^{-1} \end{bmatrix} \geq 0.$$

Thus, all matrix inequalities in Theorem 3.3 are already transformed to linear matrix inequalities of  $P_i^{-1}$ ,  $Q_i$  and  $Y_i$  that can be solved by Matlab.

*Remark 3.9* It is arbitrary to pre-assume that a certain  $\bar{A}_i$  is Hurwitz or not surely Hurwitz, as long as feasible solutions for the inequalities can be found; see Example 4.1, where  $\bar{A}_1$  is pre-assumed to be Hurwitz.

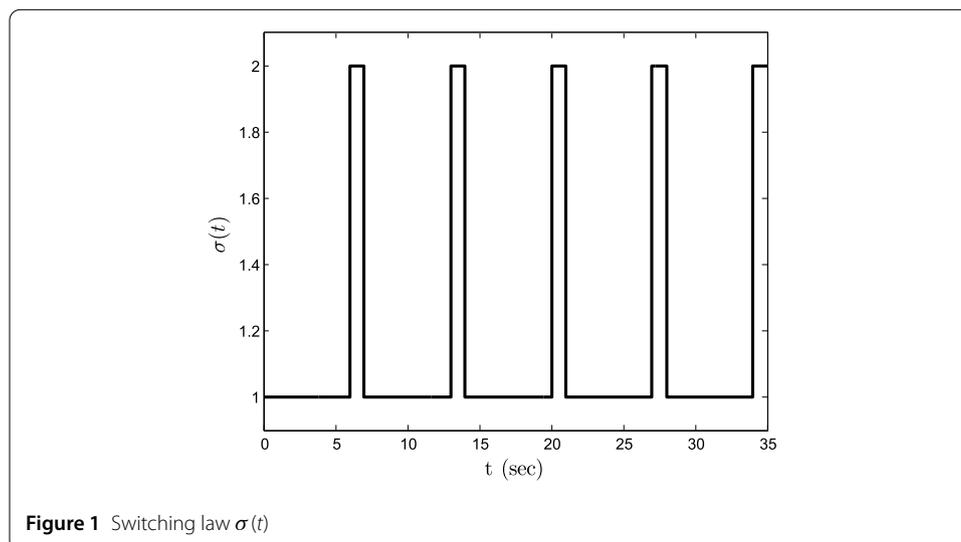
### 4 Illustrative example

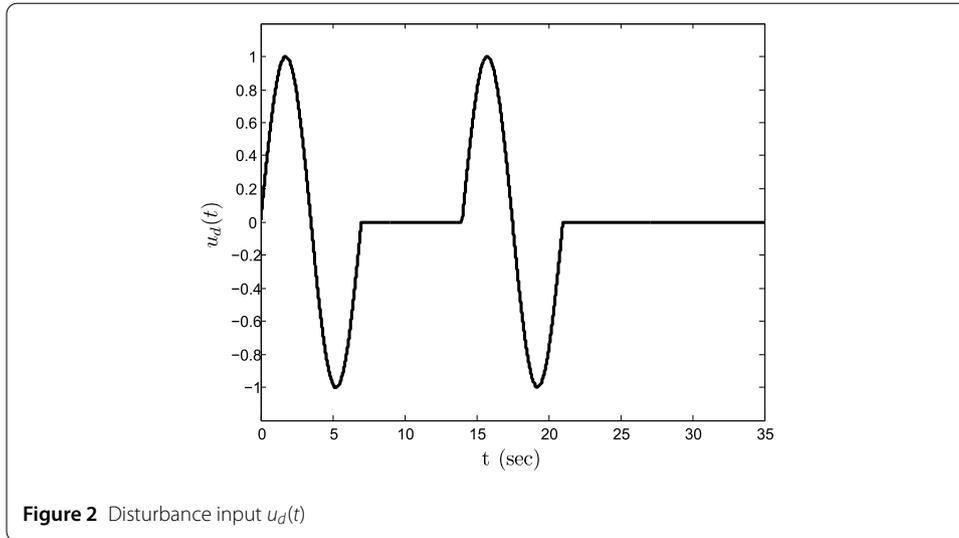
In this section, we provide an example of  $H_\infty$  control with numerical simulations to illustrate previous results.

*Example 4.1* Consider the switching control system with delay and impulse initialized as follows:

$$\begin{aligned} A_1 &= \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix}, & A_{d1} &= \begin{bmatrix} -0.1 & 0 \\ 0 & -0.1 \end{bmatrix}, & B_1 &= \begin{bmatrix} 0.1 \\ 0.1 \end{bmatrix}, & I_1 &= \begin{bmatrix} -0.1 & 0 \\ 0 & -0.1 \end{bmatrix}, \\ C_1 &= \begin{bmatrix} 0.1 & 0.1 \end{bmatrix}, & C_{d1} &= \begin{bmatrix} 0.1 & 0.1 \end{bmatrix}, & E_1 &= 0.1, \\ A_2 &= \begin{bmatrix} 0.5 & 0 \\ 0 & 0.5 \end{bmatrix}, & A_{d2} &= \begin{bmatrix} 0.05 & 0 \\ 0 & 0.05 \end{bmatrix}, & B_2 &= \begin{bmatrix} 0.1 \\ 0.1 \end{bmatrix}, & I_2 &= \begin{bmatrix} 0.05 & 0 \\ 0 & 0.05 \end{bmatrix}, \\ C_2 &= \begin{bmatrix} 0.1 & 0.1 \end{bmatrix}, & C_{d2} &= \begin{bmatrix} 0.1 & 0.1 \end{bmatrix}, & E_2 &= 0.1. \end{aligned}$$

Let  $\alpha_- = 1, \alpha_+ = 2, \alpha_* = 0.25 < \alpha_-$  and  $c_* = 2.25$ , then we can select the switching signal  $\sigma(t)$  satisfied Switching Law 3.1. From Remark 3.6 in [25], here we choose a simple switching law realization as shown in Fig. 1. The first active subsystem is a Hurwitz stable subsystem.





And the switching time is periodic. Let  $t_{2j} - t_{2j-1} = T_+ = 1$ ,  $t_{2j-1} - t_{2j-2} = T_- = 6$ ,  $j = 1, 2, \dots$ , then  $T_+ \leq c_*/(\alpha_+ + \alpha_*)$  and  $T_- \geq 2T_+(\alpha_+ + \alpha_*)/(\alpha_- - \alpha_*)$  are satisfied. Therefore,  $T_{\max} = T_- = 6$ ,  $T_{\min} = T_+ = 1$ . In fact, any switching signal can be selected as long as Switching Law 3.1 is satisfied.

Select the disturbance input  $u_d(t) = \sin(\frac{2\pi}{7}t)[H(t) - H(t - 7)] + \sin(\frac{2\pi}{7}(t - 14))[H(t - 14) - H(t - 21)] \in L_2[0, \infty)$  as shown in Fig. 2 and the initial condition  $\phi(\theta) = \phi(\theta_1, \theta_2) = [\theta_1 + 1, \theta_2 + 1]^T$ , where  $H(t)$  is the Heaviside step function. Given the delay function  $\tau(t) = 0.1 + 0.1 \sin t$ , then we can select  $d = 0.2$  and  $\rho = 0.1$  such that  $\tau(t) \leq d$ ,  $\dot{\tau}(t) \leq \rho < 1$  as required.

All other common parameters for three cases are given as  $\gamma^* = 1$ ,  $\alpha = 1.01(\alpha > \alpha_-)$ ,  $\epsilon_1 = 0.6$  and  $\epsilon_2 = 0.6$ .

Case 1:  $0 < \mu < 1$ . Select  $\mu = 0.98$ , then  $F^-_{\mu} = 0.1586$  and  $\alpha_* > \ln \mu / T_{\min} = -0.0202$ . In this case, we consider  $(A_1 + B_1K_j, A_{d1}, B_1, I_1, C_1 + E_1K_j, C_{d1}, E_1)$ ,  $j = 1, 3, 5, \dots, 9$  as the controlled subsystem  $j = 1, 3, 5, \dots, 9$ , and  $(A_2 + B_2K_i, A_{d2}, B_2, I_2, C_2 + E_2K_i, C_{d2}, E_2)$ ,  $j = 2, 4, 6, \dots, 10$ , as the controlled subsystem  $j = 2, 4, 6, \dots, 10$ . Note that in the switching signal, see Fig. 1, the lower ‘1’s represent 1, 3, 5, ..., 9 and the upper ‘2’s represent 2, 4, 6, ..., 10, from left to right. Employing the linear matrix inequality tool box of Matlab, we derive

$$\begin{aligned}
 P_1 &= \begin{bmatrix} 2.5714 & -1.2904 \\ -1.2904 & 2.5714 \end{bmatrix}, & Q_1 &= \begin{bmatrix} 2.0723 & -0.1300 \\ -0.1300 & 2.0723 \end{bmatrix}, \\
 P_2 &= \begin{bmatrix} 1.7038 & -0.8411 \\ -0.8411 & 1.7038 \end{bmatrix}, & Q_2 &= \begin{bmatrix} 1.0502 & -0.6317 \\ -0.6317 & 1.0502 \end{bmatrix}, \\
 P_3 &= \begin{bmatrix} 1.2712 & -0.5577 \\ -0.5577 & 1.2712 \end{bmatrix}, & Q_3 &= \begin{bmatrix} 0.8672 & -0.4842 \\ -0.4842 & 0.8672 \end{bmatrix}, \\
 P_4 &= \begin{bmatrix} 1.3189 & -0.5085 \\ -0.5085 & 1.3189 \end{bmatrix}, & Q_4 &= \begin{bmatrix} 0.7349 & -0.3881 \\ -0.3881 & 0.7349 \end{bmatrix}, \\
 P_5 &= \begin{bmatrix} 1.0562 & -0.3770 \\ -0.3770 & 1.0562 \end{bmatrix}, & Q_5 &= \begin{bmatrix} 0.6212 & -0.3020 \\ -0.3020 & 0.6212 \end{bmatrix},
 \end{aligned}$$

$$\begin{aligned}
 P_6 &= \begin{bmatrix} 1.1485 & -0.3693 \\ -0.3693 & 1.1485 \end{bmatrix}, & Q_6 &= \begin{bmatrix} 0.5253 & -0.2344 \\ -0.2344 & 0.5253 \end{bmatrix}, \\
 P_7 &= \begin{bmatrix} 0.9375 & -0.2832 \\ -0.2832 & 0.9375 \end{bmatrix}, & Q_7 &= \begin{bmatrix} 0.4342 & -0.1686 \\ -0.1686 & 0.4342 \end{bmatrix}, \\
 P_8 &= \begin{bmatrix} 1.0295 & -0.2778 \\ -0.2778 & 1.0295 \end{bmatrix}, & Q_8 &= \begin{bmatrix} 0.3507 & -0.1115 \\ -0.1115 & 0.3507 \end{bmatrix}, \\
 P_9 &= \begin{bmatrix} 0.8405 & -0.2137 \\ -0.2137 & 0.8405 \end{bmatrix}, & Q_9 &= \begin{bmatrix} 0.2616 & -0.0498 \\ -0.0498 & 0.2616 \end{bmatrix}, \\
 P_{10} &= \begin{bmatrix} 0.8597 & -0.1445 \\ -0.1445 & 0.8597 \end{bmatrix}, & Q_{10} &= \begin{bmatrix} 0.1602 & 0.0211 \\ 0.0211 & 0.1602 \end{bmatrix}, \\
 K_1 &= \begin{bmatrix} -13.5184 & -13.5184 \end{bmatrix}, & K_2 &= \begin{bmatrix} -2.4877 & -2.4877 \end{bmatrix}, \\
 K_3 &= \begin{bmatrix} -7.3631 & -7.3631 \end{bmatrix}, & K_4 &= \begin{bmatrix} -2.4773 & -2.4773 \end{bmatrix}, \\
 K_5 &= \begin{bmatrix} -6.9145 & -6.9145 \end{bmatrix}, & K_6 &= \begin{bmatrix} -2.4720 & -2.4720 \end{bmatrix}, \\
 K_7 &= \begin{bmatrix} -6.5315 & -6.5315 \end{bmatrix}, & K_8 &= \begin{bmatrix} -2.4724 & -2.4724 \end{bmatrix}, \\
 K_9 &= \begin{bmatrix} -6.0558 & -6.0558 \end{bmatrix}, & K_{10} &= \begin{bmatrix} -2.4844 & -2.4844 \end{bmatrix}.
 \end{aligned}$$

Then the conditions for this case in Theorem 3.3, where  $\bar{A}_1$  (or  $A_1 + B_1K_j$ ) is pre-assumed to be Hurwitz, are satisfied. From Remark 3.7,  $K_\mu = 8.1513$  and  $\alpha_\mu = 0.1267$ .

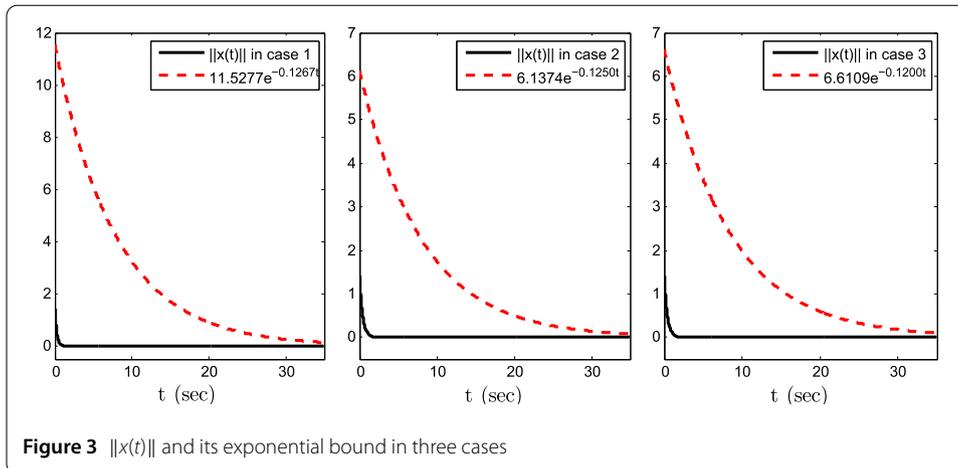
Case 2:  $\mu = 1$ . In this case,  $F_\mu = 0.1623$  and  $\alpha_* > \ln \mu / T_{\min} = 0$ . Using Matlab, we obtain

$$\begin{aligned}
 P_1 &= \begin{bmatrix} 0.9213 & -0.2664 \\ -0.2664 & 0.9213 \end{bmatrix}, & Q_1 &= \begin{bmatrix} 0.4469 & -0.3123 \\ -0.3123 & 0.4469 \end{bmatrix}, \\
 P_2 &= \begin{bmatrix} 1.0734 & -0.3074 \\ -0.3074 & 1.0734 \end{bmatrix}, & Q_2 &= \begin{bmatrix} 0.4469 & -0.1087 \\ -0.1087 & 0.4469 \end{bmatrix}, \\
 K_1 &= \begin{bmatrix} -6.7553 & -6.7553 \end{bmatrix}, & K_2 &= \begin{bmatrix} -2.4085 & -2.4085 \end{bmatrix}.
 \end{aligned}$$

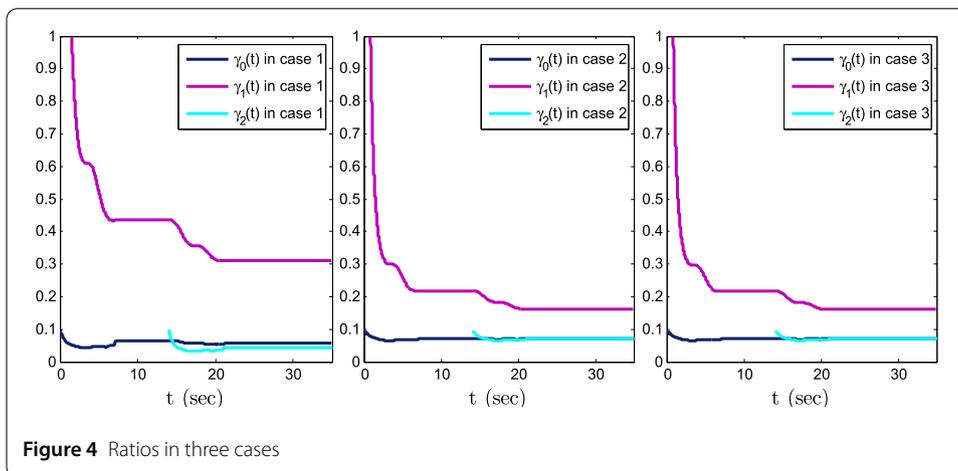
Thus, all conditions in Theorem 3.3 (where  $\bar{A}_1$  is pre-assumed to be Hurwitz) hold. It follows from Remark 3.7 that  $K_\mu = 4.3379$  and  $\alpha_\mu = 0.1250$ .

Case 3:  $\mu > 1$ . Select  $\mu = 1.01$ , then  $F_\mu = 0.1576$  and  $\alpha_* > \ln \mu / T_{\min} = 0.0100$ . By Matlab, we get

$$\begin{aligned}
 P_1 &= \begin{bmatrix} 1.0091 & -0.3389 \\ -0.3389 & 1.0091 \end{bmatrix}, & Q_1 &= \begin{bmatrix} 0.5889 & -0.3123 \\ -0.3123 & 0.5889 \end{bmatrix}, \\
 P_2 &= \begin{bmatrix} 1.1750 & -0.3900 \\ -0.3900 & 1.1750 \end{bmatrix}, & Q_2 &= \begin{bmatrix} 0.5889 & -0.3123 \\ -0.3123 & 0.5889 \end{bmatrix}, \\
 K_1 &= \begin{bmatrix} -6.7104 & -6.7104 \end{bmatrix}, & K_2 &= \begin{bmatrix} -2.4849 & -2.4849 \end{bmatrix}.
 \end{aligned}$$



**Figure 3**  $\|x(t)\|$  and its exponential bound in three cases

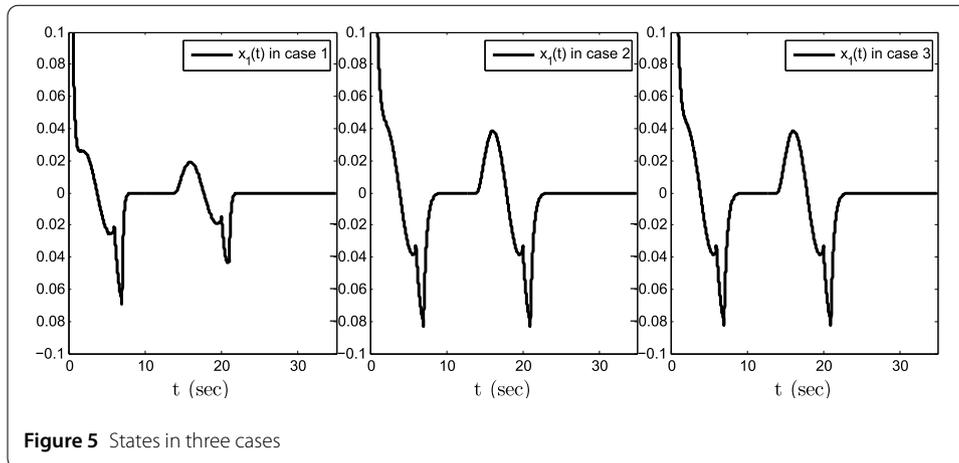


**Figure 4** Ratios in three cases

Therefore, conditions in Theorem 3.3 (where  $\bar{A}_1$  is pre-assumed to be Hurwitz) are all satisfied. According to Remark 3.7,  $K_\mu = 4.6746$  and  $\alpha_\mu = 0.1200$ .

As expected, the zero-input ( $u_d(t) \equiv 0$ ) states with the initial condition  $\phi(\theta)$  in these three cases are bounded by  $K_\mu \|x_{t_0}\|_d e^{-\alpha_\mu(t-t_0)}$ :  $11.5277e^{-0.1267t}$  (case 1),  $6.6109e^{-0.1200t}$  (case 2) and  $6.1347e^{-0.1250t}$  (case 3), see Fig. 3, respectively; and  $\gamma_0(t)$  defined as  $(\int_0^t y^2(s) ds / \int_0^t u_d^2(s) ds)^{\frac{1}{2}}$ , under the zero initial condition, for each case, is less than  $\gamma = 1$ ; see Fig. 4. Therefore, the  $H_\infty$  control goal has been achieved.

As introduced before, the  $H_\infty$  controller  $u_c = K_{\sigma(t)}x$  starts to stabilize the system (the state  $x_1$  with the initial condition  $\phi(\theta)$  completely equaling  $x_2$  in each case is almost stabilized between  $t = 7$  s and  $t = 14$  s, and after  $t = 21$  s, see Fig. 5) after the energy-bounded disturbance  $u_d$  has already decayed to zero (between  $t = 7$  s and  $t = 14$  s, and after  $t = 21$  s; see Fig. 2), then maintains the stabilized system to be externally stable from the disturbance to the output such that the effect of the disturbance on the output is attenuated during the steady period, see  $\gamma_2(t)$  of each case in Fig. 4, defined as  $(\int_{14}^t y^2(s) ds / \int_{14}^t u_d^2(s) ds)^{\frac{1}{2}}$  under the initial condition  $\phi(\theta)$ , which is less than  $\gamma^* = 1$  and is of almost the same form as  $\gamma_0(t)$ . However, before the system is stabilized for the first time, i.e. during the transient period, the ES cannot be ensured, see  $\gamma_1(t)$  of each case in Fig. 4, defined as  $(\int_0^t y^2(s) ds / \int_0^t u_d^2(s) ds)^{\frac{1}{2}}$  under the initial condition  $\phi(\theta)$ , which is larger than  $\gamma$  around  $t = 0$  s.



## 5 Conclusion

The ES and  $H_\infty$  control problem of SSSs with delay and impulse has been investigated in this paper. After introducing the definitions of the maximum, minimum DT, we have applied the relation between the number of switchings and the maximum, minimum DT to prove the ES of SSSs consisting of subsystems that are all Hurwitz stable. For those SSSs comprised of subsystems that are not all Hurwitz stable, a realizable switching law has been employed to study their ES. And then the normal  $L_2$  norm constraint has been derived. The label “weighted” has been removed properly in this paper. Finally, these results have been applied to  $H_\infty$  control and illustrated by a numerical example. In the future, we will first study the ES of nonlinear switching control systems without impulse or with impulse, then investigate the stability of SSSs with switching signals driven by stochastic processes.

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### Availability of data and materials

The data and material used to support the findings of this study are included within the article.

### Competing interests

The authors declare that they have no competing interests.

### Authors' contributions

All authors drafted the manuscript, and they read and approved the submitted version.

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