

# Scaling Opportunities for Bulk Accumulation and Inversion MOSFETs for Gigascale Integration

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# Scaling Opportunities for Bulk Accumulation and Inversion MOSFETs for Gigascale Integration

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*To my parents*

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## SUMMARY

The objective of this research is to comprehensively compare bulk accumulation and inversion MOSFETs, and find application areas where each is superior. Short channel effect (SCE) models for accumulation and inversion MOSFETs are derived that accurately predict threshold voltage, subthreshold swing, and subthreshold current. A source/drain junction depth dependent characteristic length is derived that can be used to rapidly assess the impact of junction depth scaling on minimum channel length. A fast circuit simulation methodology is developed that uses physically based I-V models to simulate inversion and accumulation MOSFET inverter chains, and is found to be accurate over a wide range of supply voltages. The simulation methodology can be used for rapid technology optimization, and performance prediction. Design guidelines are proposed for accumulation MOSFET design; the guidelines result in a low process sensitivity, low SCE, and a subthreshold current less than the allowable limit. The relative performance advantage of accumulation/inversion MOSFETs is gate-technology dependent. In critical comparisons, on-current is evaluated by means of a full band Monte Carlo device simulation. Gate-leakage, and band-to-band tunneling leakage at the drain-substrate region are included in the performance analysis. For mid-bandgap metal gate, accumulation MOSFETs perform better than inversion MOSFETs for hi-performance (HiP) and low-operating power (LOP) applications. For tunable metal gate technology, inversion MOSFETs always perform better than accumulation MOSFETs. For dual poly technology, accumulation MOSFETs perform better than inversion MOSFETs for low standby power (LSTP) applications. A comprehensive scaling analysis has been performed on accumulation and inversion MOSFETs using both SCE models and 2-D simulations. Results show that accumulation MOSFETs can scale better than inversion MOSFETs for mid-bandgap metal gate HiP, and LOP applications; and poly gate LSTP applications.

# CHAPTER I

## INTRODUCTION

### 1.1 *Introduction*

Device miniaturization reduces the physical dimensions of devices, thereby increasing the density of devices on a die. Miniaturization not only results in increased functionality on a chip but also improved performance. The International Technology Roadmap for Semiconductors (ITRS) [1] predicts feature sizes as small as 13nm by 2016. ITRS groups application areas into low standby power (LSTP), low operating power (LOP) and high-performance (HiP). The on-current ( $I_{ON}$ ) and off-current ( $I_{OFF}$ ) requirements of these application areas are shown in Table 1. Device scaling results in a number of effects, some classical and others quantum mechanical. Proper modeling of these effects is quintessential in achieving optimal performance for future technology.

Important classical effects arising from device scaling include threshold voltage rolloff, drain induced barrier lowering (DIBL), and subthreshold swing ( $S$ ) rollop. These effects considerably degrade device performance and limit device scaling. Quantum mechanical (QM) effects arising as a result of scaling include quantization of electron energy in the channel; and tunneling leakage at the gate-channel, gate-overlap, and drain-substrate regions. These effects tend to degrade the device performance. Non-local carrier transport becomes important in short channel length MOSFETs, resulting in performance improvement by means of velocity overshoot [2].

**Table 1:** ITRS application areas and their  $I_{ON}$ , and  $I_{OFF}$  requirements.

<i>application</i>	$I_{ON}$ ( $\mu A/\mu m$ )	$I_{OFF}$ ( $nA/\mu m$ )
Low standby power (LSTP)	400	0.001
Low operating power (LOP)	600	0.3-0.7
High-performance (HiP)	900	300-1000

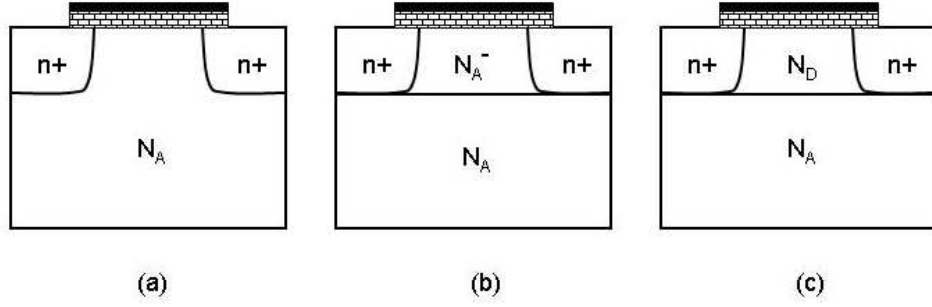


The goal of the proposed research is to comprehensively compare bulk accumulation and inversion devices in order to assess their scalability for gigascale integration. Both physical models and numerical simulations are used to compare the devices. Physically based device models allow physical insight into device scaling phenomena, rapid optimization, and circuit simulation. Numerical device simulations allow inclusion of non-uniform doping, QM effects, and non-local carrier transport.

## 1.2 *Background*

Bulk MOSFETs can be divided into two broad categories: accumulation type, where the current flow arises from majority carriers, and inversion type, where the current flow arises from minority carriers. The various bulk MOSFET structures are shown in Fig. 1. Based on the vertical doping profile, inversion FETs can be further classified into uniformly doped surface channel inversion (UD-SCI) FETs, and retrograde doped surface channel inversion (RD-SCI) FETs. The RD-SCI FET is also known as low impurity channel transistor (LICT) [3], atomic layer doped (ALD) transistor [4], super steep retrograde (SSR) doped FET [5], or epi-MOSFET [6]. The main difference between UD-SCI and RD-SCI FETs is the existence of a lightly doped layer in the RD-SCI device.

The accumulation FET can be further classified into surface channel accumulation (SCA) FET, and buried channel accumulation (BCA) FET. The main difference between BCA and SCA devices is the location where the channel first opens. BCA FET conduction starts in a neutral buried channel, and with increasing applied gate bias, subsequently extends to an accumulated surface layer. On the other hand, SCA FET conduction is limited to a surface accumulation layer. BCA devices normally have highly doped/deep implant layers that prevent the extension of the bulk depletion region all the way to the surface; SCA devices are characterized by lightly doped/shallow implant layers that allow the extension of the bulk depletion region all the way and beyond the Si/SiO<sub>2</sub> interface. As a result, the BCA device can be designed to achieve a low threshold voltage ( $V_T$ ), while the SCA device's lower  $V_T$  boundary is the flat-band voltage ( $V_{FB}$ ). The channel (or tub) and well (or substrate) doping types of various FET types are shown in Table 2.



**Figure 1:** Vertical profile of bulk MOS devices. (a) Uniformly-Doped Surface Channel Inversion (UD-SCI). (b) Retrograde-Doped Surface Channel Inversion (RD-SCI). (c) Buried Channel Accumulation (BCA), Surface Channel Accumulation (SCA), and Fermi-Threshold FET (FF).

**Table 2:** Channel and well doping for different n-FET types.

<i>device</i>	<i>channel/tub-doping</i>	<i>substrate/well doping</i>
UD-SCI	p-type ( $N_A$ )	p-type ( $N_A$ )
RD-SCI	p-type ( $N_A^-$ )	p-type ( $N_A$ )
BCA/SCA	n-type ( $N_D$ )	p-type ( $N_A$ )

The SCI device is the conventional MOSFET [7] commonly used since the inception of MOS technology. BCA/SCA FETs too date back to the beginning of MOS technology [8],[9]. BCA/SCA FETs on insulating substrates [9] were introduced at about the same time as SCI silicon on insulator (SOI) FETs. In single-poly CMOS technology, the n-channel device is generally an SCI device, while the p-channel device is BCA/SCA type. To avoid buried channel operation and the resultant SCE increase [10], dual poly technology was introduced to make both n-MOS and p-MOS devices to be SCI type. But p+ poly gates (used for SCI p-MOSFETs) have problems of Boron penetration [11]; and dual poly technology results in increased process complexity, and reduced circuit density compared to single-poly technology. So accumulation FETs are still used in poly gate CMOS technology [12]-[16]. Accumulation FETs are also used in mid-bandgap metal gate CMOS [17], where the same metal gate is used for both n-MOS and p-MOS FETs.

The lightly doped layer in the RD-SCI FET introduces extra degrees of freedom in device optimization. For a given threshold voltage ( $V_T$ ), the RD-SCI FET is believed to exhibit

lower short channel effects (SCE) compared to the UD-SCI FET [18]. The RD-SCI FET is also believed to result in better current drive capability as a result of low channel doping [19]. However, other studies show that the RD-SCI FET has only a marginal advantage over the UD-SCI FET in terms of drive current [20].

Many modifications have been proposed to the original SCI MOSFET structure in order to overcome SCE. Reducing the source/drain (S/D) junction depth [21] is an important way of minimizing charge sharing and thus SCE. However, ultra-shallow source/drain junctions result in increased source/drain resistance ( $r_{sd}$ ) [22] and thus degrade  $I_{ON}$ . In order to achieve both ultra-shallow junctions and low  $r_{sd}$ , the grooved-gate MOSFET [23], electrically induced source/drain extension MOSFET [24],[25], and raised source/drain MOSFET [22], [26] have been introduced. In order to reduce the source resistance ( $R_s$ , which has a greater impact on  $I_{ON}$  than the drain resistance,  $R_d$  [27]), asymmetric source/drain structures have been introduced [28]. Another method of reducing SCE in structures with deep S/D junctions is to use dielectric pockets [29]. SiGe was used in the S/D regions to fabricate sub-100nm SCI p-MOSFETs with ultra-shallow S/D extensions and good  $I_{ON}$  [30]. All the modifications mentioned above can be easily applied to accumulation FETs. S/D engineering is not considered in this work since it has a similar impact on both accumulation and inversion FETs.

Another way of controlling SCE in inversion FETs is to introduce halos [31], [32] below the S/D region. Halos are high-concentration implants that reduce charge sharing resulting from S/D regions. In an accumulation FET too, halos reduce SCE [33]. Because of the complexity of analytically modeling non-uniform channel doping in the lateral direction, halo-doped MOSFETs are analyzed using 2D numerical simulations in this work. Asymmetric halos have been proposed to take advantage of velocity overshoot [28] in scaled MOSFETs and to improve analog performance [34].

Another way of to improve MOSFET performance is to operate it at a low temperature. The important effects of reducing the operating temperature are a reduction in  $S$  and an increase in channel mobility ( $\mu$ ). There is also an increase in saturation velocity ( $v_{sat}$ ) and more velocity overshoot. The net result of this is an increase in  $I_{ON}$  and a reduction in

$I_{OFF}$  [35].

### 1.3 Motivation

There are reportedly many advantages of accumulation FETs. The low vertical field in the channel region of the accumulation device when operating in buried channel mode results in increased mobility with respect to its SCI counterparts [36]. In addition, the low implant doping concentration in the SCA device will also result in high mobility. The Fermi FET, a device that attempts to take advantage of both these characteristics, has been proposed in [37] and analyzed through simulations in [38]. In this device, the substrate depletion region extends exactly to the surface resulting in minimal vertical electric field in the channel. Its threshold voltage is determined only by the flat band voltage ( $V_{FB}$ ) and the built-in potential of the substrate-channel p-n junction ( $\phi_{bi}$ ) [37]. Thus,  $V_T$  is independent of oxide thickness. The Fermi FET can be identified as the boundary between the BCA and SCA device. It was also determined in [37]-[39] that this device yields the minimum long-channel subthreshold swing possible in bulk devices. Hence, in the search for the optimal bulk device for deep-submicron operation, the Fermi FET will be carefully considered. However, alternate gate materials [40] will be needed to obtain low  $V_T$  SCA/FF devices as a result of the flat-band limitation.

The accumulation FET has been reported to have a higher breakdown voltage [36] and reduced hot-carrier generation [41] compared to SCI FETs. The SCI FET has a higher  $1/f$  noise because of interface states, whereas the BCA FET conducts partially or completely in the bulk and thus has a lower  $1/f$  noise [42].

Since the channel region is doped the same type as the source/drain (S/D) region, the lateral electric field at the source/drain junction is smaller in accumulation FETs compared to inversion FETs [43]. This might lead to accumulation FETs being able to scale to lower channel lengths compared to inversion FETs. Due to a lower vertical field, QM  $V_T$  shift can be expected to be lower in accumulation FETs. Also, because of a lower source/drain-substrate area, accumulation FETs are expected to have a lower junction capacitance when compared to a similar inversion FET structure. The RD-SCI FET has a low dopant induced

$V_T$  fluctuation because of its near-intrinsic channel [44]. Since the SCA FET too has a low channel doping, it is expected to show a similar dopant-induced  $V_T$  fluctuation behavior.

Only a few publications have made clear the distinction between BCA and SCA threshold voltage design [39],[45]-[47]. Although the SCA FET has a lower  $S$  and lower SCE compared to the BCA FET, few publications emphasize operation of the accumulation FET as an SCA FET [38]-[39],[47]. In addition, existing guidelines for design of accumulation FETs to operate as SCA devices are based on 1-D theory [38]-[39],[47]. and do not hold good for short channel devices. New design guidelines based on 2-D theory are needed for designing accumulation FETs so that they operate as SCA devices.

Previous comparisons between accumulation and inversion FETs have yielded conflicting results and have many shortcomings, primarily because of the limited design space considered [10]-[11],[38], [48] -[52]. In addition, many comparisons are for longer channel lengths and thicker oxides [10],[38],[49], where quantum mechanical effects and non-local carrier transport are not significant. In present day devices, both these effects are extremely important, and a re-evaluation of the comparison is needed in such scaled devices. In [11], accumulation FETs with ultra-shallow channel implants are found to be superior to inversion FETs. In [38], SCA FETs are found to be superior to SCI FETs. In [50] and [51], the comparisons are limited to that between metal-gate accumulation and poly-gate inversion FETs, and both find the poly-gate inversion FET to be superior to the accumulation FET. In [10], only hi-performance poly-gate accumulation and inversion FETs are compared, and inversion FETs are found to be scalable to lower supply voltages than accumulation FETs. In [52], a single tub-depth ( $y_i$ ) and substrate doping ( $N_A$ ) value are considered in evaluating the accumulation FET, and the accumulation FET is found to be less scalable than the inversion FET. This work attempts to compare accumulation and inversion MOSFETs for a variety of applications, gate materials and power supply voltages.

## **1.4 Organization**

The rest of the dissertation is organized as follows. In Chapter II, a threshold voltage ( $V_T$ ) rolloff model is proposed that works for both deep junction and shallow junction devices. A

source/drain junction depth dependent characteristic length is proposed that can be used to rapidly assess the impact of junction depth scaling on  $V_T$  rolloff. Then, long channel threshold voltage of accumulation FETs is derived. In Chapter III, subthreshold swing of accumulation and inversion MOSFETs is derived by using the volume inversion principle. Using the Swanson-Meindl methodology, a subthreshold current model for accumulation MOSFETs is developed.

In Chapter IV, a circuit simulation methodology is proposed that is applicable to all FET types, uses physically based I-V models, and is applicable over a wide range of supply voltages. The simulation method can be used for rapid optimization, and predictive circuit modeling.

In Chapter V, design guidelines based on 2-D models are presented on how to design an accumulation FET so that it has a low subthreshold swing and SCE. Surface channel accumulation operation is stressed not only to avoid the high SCE resulting from buried channel operation, but also high process sensitivity and high dopant fluctuation effect.

In Chapter VI, metal gate accumulation and inversion FETs are evaluated. It is found that in long channel regime, the Fermi-FET has the minimum subthreshold swing. In the short channel regime, accumulation FETs have higher SCE than inversion FETs if the gate work-function is tunable.

In Chapter VII, poly gate accumulation and inversion FETs are compared. It is found that accumulation FETs achieve a high  $V_T$  with a low channel doping; this results in a better channel mobility compared to inversion MOSFETs. Accumulation MOSFETs are also found to have a better subthreshold swing, a lower gate-channel tunneling current, and a lower band-to-band tunneling current at the drain-substrate junction.

In Chapter VIII, Monte Carlo simulations are used to accurately evaluate the performance advantage of mid-bandgap metal gate accumulation MOSFETs. Accumulation MOSFETs are found to perform better than inversion MOSFETs for LOP and HiP applications. In Chapter IX, scaling limits for accumulation and inversion MOSFETs are evaluated. Both 2-D simulations and SCE models are used to derive the minimum channel length. Chapter X presents conclusions and recommendations for future work.

## CHAPTER II

### THRESHOLD VOLTAGE MODELING

#### ***2.1 Threshold Voltage Rolloff of Uniformly Doped SCI MOS-FETs***

##### **2.1.1 Introduction**

MOSFET scaling is progressing into the nanometer range. ITRS 2002 [1] projects a channel length of 18 nm for the year 2010. The junction depth for this technology is projected to be 15 nm. Historically, devices have been of a deep junction type, where  $d < y_j$ , with  $d$  being the minimum channel depletion depth and  $y_j$  being the source/drain junction depth. But scaling theory [21] clearly shows that using deep junctions results in increased SCE. So ultra-shallow junction technology is being pursued as one of the key methods of controlling SCE in extremely scaled MOSFETs. In ultra shallow junction MOSFETs, the minimum channel depletion depth is comparable to or greater than the junction depth. Most MOSFET threshold voltage ( $V_T$ ) models proposed to date only hold good for deep junction devices and do not model the impact of junction depth on SCE [53]-[58]. Charge sharing models were used to obtain the  $V_T$  rolloff in [53], and such models become less accurate at short channel lengths. Ratnakumar and Meindl [54] reduced the 2-D Poisson equation to an equivalent Laplace equation and solved it as a series solution. Liu [55] solved the quasi-2-D Poisson equation to obtain the channel potential. Suzuki [56] used a method similar to that in [57] and introduced a channel depletion depth parameter to model the effective depletion depth. Pang [58] used the quasi-2-D Poisson equation to model pocket MOSFETs. A few  $V_T$  rolloff models proposed to date include junction depth dependency but are not accurate for intermediate and shallow junction devices [47],[59]-[60]. Pimbley [59] used the variational approach to find  $V_T$  rolloff. Nguyen [60] considered cylindrical junctions and the equations are too complex to provide clear physical insight. Austin [47] used an approach similar to that in [54].

Existing circuit simulators mostly use BSIM4 models [61] to model bulk MOSFETs; the BSIM4 models use Liu's [55]  $V_T$  rolloff model which holds good only for deep junction devices. The lack of a physically based, junction depth dependent,  $V_T$  rolloff model in BSIM4 would necessitate more fitting parameters and more parameter binning for future technology. This in turn would increase the time required to extract device parameters and impede scalability.

A compact  $V_T$  model is proposed that holds good for both shallow and deep junction MOSFETs. The model provides a junction depth dependent scale length that can be used to rapidly assess the impact of source/drain scaling on minimum channel length ( $L_{min}$ ). The model is physically based and is extremely useful for device optimization, technology prediction, and circuit simulation.

First, the solution methodology is introduced along with the boundary conditions used. The proposed model and some previously published models are then compared with 2-D numerical simulations. Finally, a junction depth dependent scale length is proposed, and  $L_{min}$  extracted from this scale length is compared with ITRS 2002 projections.

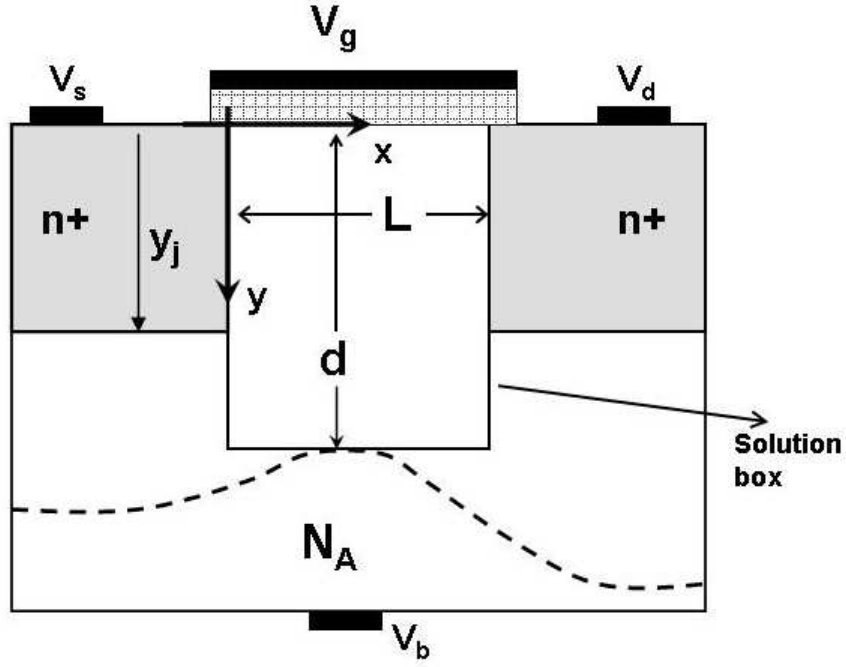
### 2.1.2 Model

Evanescent mode analysis is used to solve the 2-D Poisson equation. The device analyzed in this section has a uniform doping ( $N_A$ ) in the channel and substrate. The analysis will be extended to devices with non-uniform doping in the depth direction, like retrograde doped MOSFETs and buried channel MOSFETs, in the next few sections. In the subthreshold regime, the potential distribution in the rectangular solution box (Fig. 2) is given by the 2-D Poisson equation:

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = \frac{qN_A}{\epsilon_s} \quad (1)$$

The above equation is solved by the method of superposition [54] by assuming  $\psi(x, y) = U(y) + \phi(x, y)$ , where  $U(y)$  is the solution to the 1-D Poisson equation and  $\phi(x, y)$  is the solution to the 2-D Laplace equation.  $\phi(x, y)$  can be thought of as the source/drain effect on the overall potential. The boundary conditions for  $\psi(x, y)$ ,  $U(y)$ , and  $\phi(x, y)$  are shown in Tables 3 and 4.  $U(y)$  is solved by double integration.  $\phi(x, y)$  is solved by separation of





**Figure 2:** Device structure and solution box.

variables:

$$\phi(x, y) = \left( C' \exp(\lambda(x - L)) + D' \exp(-\lambda x) \right) (A \sin(\lambda y) + B \cos(\lambda y)) \quad (2)$$

The eigenvalue  $\lambda$  can be obtained from the top and bottom boundary conditions. The top boundary condition gives,

$$\frac{A}{B} = \frac{C_{ox}}{\lambda \epsilon_s} \quad (3)$$

From Table 4, it can be seen that there are two bottom boundary conditions for  $\phi(x, y)$ .

$$\frac{\partial \phi(x, d)}{\partial y} = 0 \quad (4)$$

$$\phi(x, d) = 0 \quad (5)$$

Only one of (4) or (5) is needed for evaluating  $\lambda$ . Ratnakumar [54], Pimbley [59] and Liu [55] assume the bottom boundary condition to be (4), whereas Frank [62] uses (5). This work clarifies which of the two boundary conditions needs to be used to accurately model  $V_T$  rolloff. The corresponding characteristic length equations obtained from the two bottom boundary conditions are

$$\frac{\partial \phi(x, d)}{\partial y} = 0 \Rightarrow \tan(\lambda' d) = \frac{C_{ox}}{\lambda' \epsilon_s} \quad (6)$$

**Table 3:** Boundary conditions for  $\psi(x, y)$ ; the depletion depth at the source/drain is denoted by  $d_s/d_d$ , and the built-in potential between the source/drain and substrate is denoted by  $\psi_{bi}$ .

Left	$0 \leq y \leq y_j$ $d_s \geq y \geq y_j$	$\psi_{bi} - V_{BS}$ $\psi_{bi} - V_{BS} + \frac{1}{2} \frac{q}{\epsilon_{si}} N_A (y - y_j)^2$ $-(y - y_j) \sqrt{\frac{2qN_A(\psi_{bi} - V_{BS})}{\epsilon_s}}$
Right	$0 \leq y \leq y_j$ $d_d \geq y \geq y_j$	$\psi_{bi} - V_{BS} + V_{DS}$ $\psi_{bi} - V_{BS} + V_{DS} + \frac{1}{2} \frac{q}{\epsilon_{si}} N_A (y - y_j)^2$ $-(y - y_j) \sqrt{\frac{2qN_A(\psi_{bi} - V_{BS})}{\epsilon_s}}$
Top	$0 \leq x \leq L$	$\frac{\partial \psi(x, 0)}{\partial y}$ $= \frac{C_{ox}}{\epsilon_s} (V_G - V_{FB} - V_{BS} - \psi(x, 0))$
Bottom	$0 \leq x \leq L$	$\psi(x, d) = 0$ $\frac{\partial \psi(x, d)}{\partial y} = 0$

**Table 4:** Boundary conditions for  $U(y)$  and  $\phi(x, y)$ .

		$U(y)$	$\phi(x, y)$
Left	$0 \leq y \leq y_j$ $d_s \geq y \geq y_j$	- -	$\phi_{bi} - V_{BS}$ $\psi_{bi} - V_{BS} + \frac{1}{2} \frac{q}{\epsilon_{si}} N_A (y - y_j)^2$ $-(y - y_j) \sqrt{\frac{2qN_A(\psi_{bi} - V_{BS})}{\epsilon_s}}$
Right	$0 \leq y \leq y_j$ $d_d \geq y \geq y_j$	- -	$\psi_{bi} - V_{BS} + V_{DS}$ $\psi_{bi} - V_{BS} + V_{DS} + \frac{1}{2} \frac{q}{\epsilon_{si}} N_A (y - y_j)^2$ $-(y - y_j) \sqrt{\frac{2qN_A(\psi_{bi} - V_{BS})}{\epsilon_s}}$
Top	$0 \leq x \leq L$	$\frac{\partial U(0)}{\partial y}$ $= \frac{C_{ox}}{\epsilon_s} (V_{GS} - V_{FB} - V_{BS} - U(0))$	$\frac{\partial \phi(x, 0)}{\partial y}$ $= \frac{C_{ox}}{\epsilon_s}$
Bottom	$0 \leq x \leq L$	$U(d) = 0$ $\frac{\partial U(d)}{\partial y} = 0$	$\phi(x, d) = 0$ $\frac{\partial \phi(x, d)}{\partial y} = 0$

$$\phi(x, d) = 0 \Rightarrow \tan(\lambda'' d) = \frac{-\lambda'' \epsilon_s}{C_{ox}} \quad (7)$$

Thus,  $\phi(x, y)$  can be written as

$$\phi(x, y) = \sum_{n=1}^{\infty} (C_n \exp(\lambda_n(x - L)) + D_n \exp(-\lambda_n x)) \left( \sin(\lambda_n y) + \frac{\lambda_n \epsilon_s}{C_{ox}} \cos(\lambda_n y) \right) \quad (8)$$

$\lambda$  in (8) can be either  $\lambda'$  or  $\lambda''$ .  $C_n$  and  $D_n$  are evaluated from the left and right boundary conditions. To enable an analytical solution for  $V_T$  rolloff,  $\phi(x, y)$  is approximated by a single term solution. This approximation works very well since the terms involving higher order  $\lambda$ 's decay rapidly<sup>1</sup>.  $V_T$  rolloff is determined as follows: short channel  $V_T$  is determined from the condition  $V_T = V_G|_{\psi_{min}=2\phi_F}$ , where  $\psi_{min}$  is the minimum potential, and  $\phi_F = \frac{kT}{q} \ln\left(\frac{N_A}{n_i}\right)$  is the bulk Fermi level. The short channel  $V_T$  is subtracted from the long channel  $V_T$  ( $V_{T_{long}} = V_G|_{U(0)=2\phi_F}$ ) to yield the threshold voltage shift,  $\Delta V_T$ .

Assuming  $\lambda_1 L \gg 1$  and  $x_m = L/2$  ( $x_m$  is the x-coordinate of the location of the minimum potential) enables a compact  $V_T$  rolloff expression that can provide physical insights.

$$\Delta V_{T_{approx}} = \frac{[\chi_1(\psi_{bi}, y_j) + \chi_1(\psi_{bi} + V_{DS}, y_j)] \exp(-\lambda_1 L/2)}{\kappa_1 - 2 \exp(-\lambda_1 L/2)} \quad (9)$$

The various terms in the above equation are as shown in Table 5. The assumption,  $x_m = L/2$ , does not work well when DIBL is high. When  $V_{DS}$  is greater than a few tenths of a volt, the exact expression for  $\Delta V_T$  (shown in Table 5) would have to be used. The approximate expression for  $\Delta V_T$ , (9), is similar to that in [47]. However, the  $\chi_1$  term is different because of the different boundary condition used in this work.

### 2.1.3 Results and Discussion

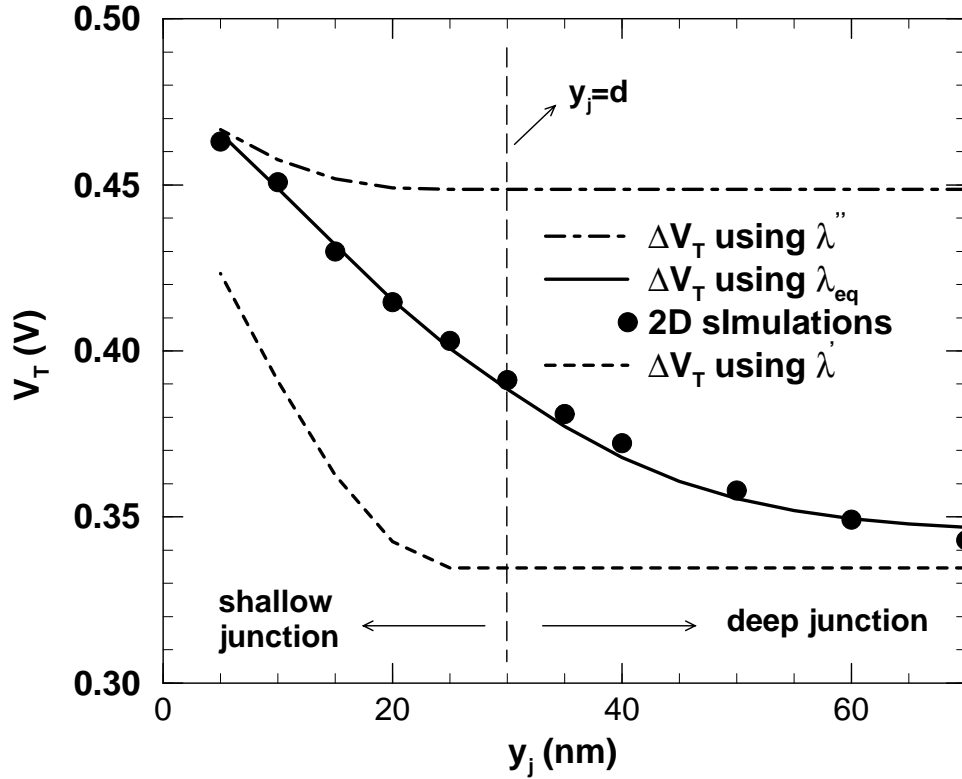
Fig. 3 shows the rolloff model using either  $\lambda'$  or  $\lambda''$ , along with 2-D numerical simulations [63], on a  $V_T$  vs. junction depth plane. It can be seen that for the deep junction case ( $d \ll y_j$ ), the  $\Delta V_T$  model using  $\lambda'$  works better than that using  $\lambda''$ ; for ultra shallow junctions ( $d \gg y_j$ ), the reverse is true. For cases where  $d \approx y_j$ , neither the  $V_T$  rolloff model using  $\lambda'$  nor that using  $\lambda''$  gives a good match with simulations.

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<sup>1</sup>A multiple term solution would have to be considered if SCE is very high. Such a scenario occurs usually when  $\Delta V_T > 200mV$ , at which point the device has too high a SCE and ceases to be of interest to the device engineer.

**Table 5:** Expression for  $\Delta V_T$ .

All cases	$\Delta V_{T_{exact}} = 2\Gamma \cdot \Delta V_{T_{approx}} \left\{ 1 + \sqrt{1 - \frac{\chi_1(\psi_{bi}, y_j) \chi_1(\psi_{bi} + V_{DS}, y_j)}{[\chi_1(\psi_{bi}, y_j) + \chi_1(\psi_{bi} + V_{DS}, y_j)] \Gamma \cdot \Delta V_T}} \right\}$ $\chi(V, y_j) = A_1(V) + B_1(V, y_j)$ $A_1(V) = V + V_{FB} - V_{T_{long}} - \frac{qN_A}{\epsilon_s \lambda_1^2}$ $\Gamma = \frac{\exp(-\lambda_1 L/2)}{\kappa_1 + 2\exp(-\lambda_1 L/2)}$ $\kappa_1 = \frac{1}{2} \left[ 1 + \frac{C_{ox} d}{\epsilon_s} \left( 1 + \left( \frac{\lambda_1 \epsilon_s}{C_{ox}} \right)^2 \right) \right]$ $d = \sqrt{\frac{2\epsilon_s}{qN_A} 2\phi_F} \quad \phi_F = \frac{kT}{q} \ln \left( \frac{N_A}{n_i} \right)$ $V_{T_{long}} = V_{FB} + 2\phi_F + \frac{\sqrt{2q\epsilon_s N_A \cdot 2\phi_F}}{C_{ox}}$
$d \leq y_j$ deep junction	$B_1(V, y_j) = \left[ V - V_{BS} + \frac{qN_A}{\epsilon_s \lambda_1^2} \right] \left[ \frac{\epsilon_s \lambda_1}{C_{ox}} \sin(\lambda_1 d) - \cos(\lambda_1 d) \right]$
$d > y_j$ shallow junction	$B_1(V, y_j) = \frac{qN_A}{\epsilon_s} \left( -\frac{1}{\lambda_1^2} \right) \left[ \cos(\lambda_1 y_j) - \frac{\epsilon_s}{C_{ox}} \sin(\lambda_1 y_j) \right]$ $+ \left[ \frac{qN_A (d_{s/d}(V) - y_j)}{\epsilon_s \lambda_1} \right] \left[ \sin(\lambda_1 y_j) + \frac{\epsilon_s \lambda_1}{C_{ox}} \cos(\lambda_1 y_j) \right]$ $+ \left[ \frac{qN_A (d_{s/d}(V) - d)^2}{2\epsilon_s} \right] \left[ \cos(\lambda_1 d) - \frac{\epsilon_s \lambda_1}{C_{ox}} \sin(\lambda_1 d) \right]$ $- \left[ \frac{qN_A (d - d_{s/d}(V))}{\epsilon_s \lambda_1} \right] \left[ \frac{\epsilon_s \lambda_1}{C_{ox}} \cos(\lambda_1 d) + \sin(\lambda_1 d) \right]$ $d_{s/d}(V) = y_j + \sqrt{\frac{2\epsilon_s}{qN_A} (V - V_{BS})}$

**Figure 3:** Threshold voltage versus junction depth.  $L = 65 \text{ nm}$ ,  $N_A = 2 \times 10^{18} \text{ cm}^{-3}$ ,  $t_{ox} = 1.5 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ . The long channel depletion depth for this device is 30 nm.

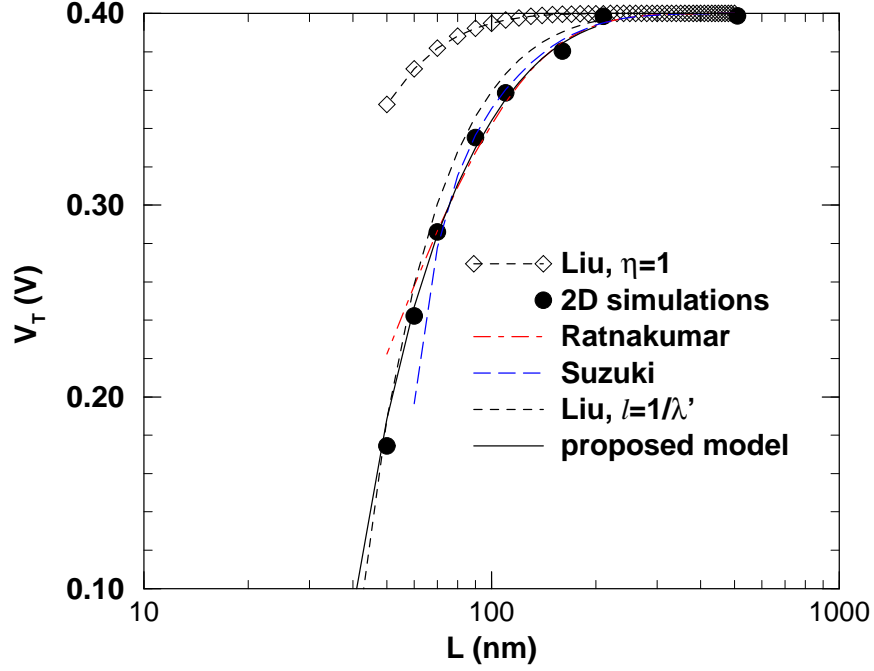
The physical explanation for such a behavior is as follows. For the deep junction case, assuming (5) as the bottom boundary would mean that the source/drain potential is forced to go to zero at  $y = d$ . In reality, the source (drain) potential is fixed at  $y = d$ , and is equal to  $\psi_{bi}$  ( $\psi_{bi} + V_{DS}$ ); here,  $\psi_{bi}$  is the built-in potential between the source/drain and substrate. Assuming (5) as the bottom boundary would underestimate the effect of source/drain on channel potential and thus would underestimate  $V_T$  rolloff. Near the source/drain, at  $y = d$ , the field in the  $y$ -direction is zero. Assuming (4) as the bottom boundary causes the source/drain potential to be fixed to  $\psi_{bi}/(\psi_{bi} + V_{DS})$  at  $y = d$ , and thus is a better boundary condition to apply. For the shallow junction case, assuming (5) as the bottom boundary is more accurate since the source/drain potential would have almost decayed to zero at  $y = d$ . If (4) is assumed as the bottom boundary, the source/drain potential would be fixed to  $\psi_{bi}/(\psi_{bi} + V_{DS})$  at  $y = d$ , and this would cause an overestimation of  $V_T$  rolloff.

From Fig. 3, it can be seen that when  $d = y_j$ ,  $V_T$  is roughly the average of the values given by  $\lambda'$  and  $\lambda''$ . For intermediate junction cases ( $d \approx y_j$ ), a superposition of  $\lambda'$  and  $\lambda''$  would be needed. A function is proposed that does the necessary superposition:

$$\lambda_{eq} = (\lambda' - \lambda'') \cdot \frac{1}{1 + \exp\left(\frac{d - y_j}{d/2}\right)} + \lambda'' \quad (10)$$

It can be seen that when  $y_j \gg d$ ,  $\lambda_{eq} \approx \lambda'$  and when  $y_j \ll d$ ,  $\lambda_{eq} \approx \lambda''$ . When  $y_j = d$ ,  $\lambda_{eq}$  is the average of  $\lambda'$  and  $\lambda''$ . When  $V_T$  obtained by using  $\lambda_{eq}$  is plotted against  $y_j$ , Fig. 3, it can be seen that the model now agrees well with simulation results over all  $y_j$ . When  $d \gg t_{ox}$ , (10) can be simplified by noting that  $\lambda_n'' \approx (\pi + (n - 1)\pi)/(d + 3t_{ox})$ , and  $\lambda_n' \approx (\pi/2 + (n - 1)\pi)/(d + 3t_{ox})$ . It is to be noted that the proposed  $\Delta V_T$  model only uses the primary eigen value ( $\lambda_{eq1}$ ).

In the proposed model, the minimum channel depletion depth value used is that of a long channel MOSFET. When the source/drain depletion depth is comparable to channel length, the average depletion depth in the channel is considerably greater than the long channel depletion depth. In such a situation, the proposed model will not work well. But in all well-scaled devices, the channel length is considerably greater than the source/drain depletion depth.

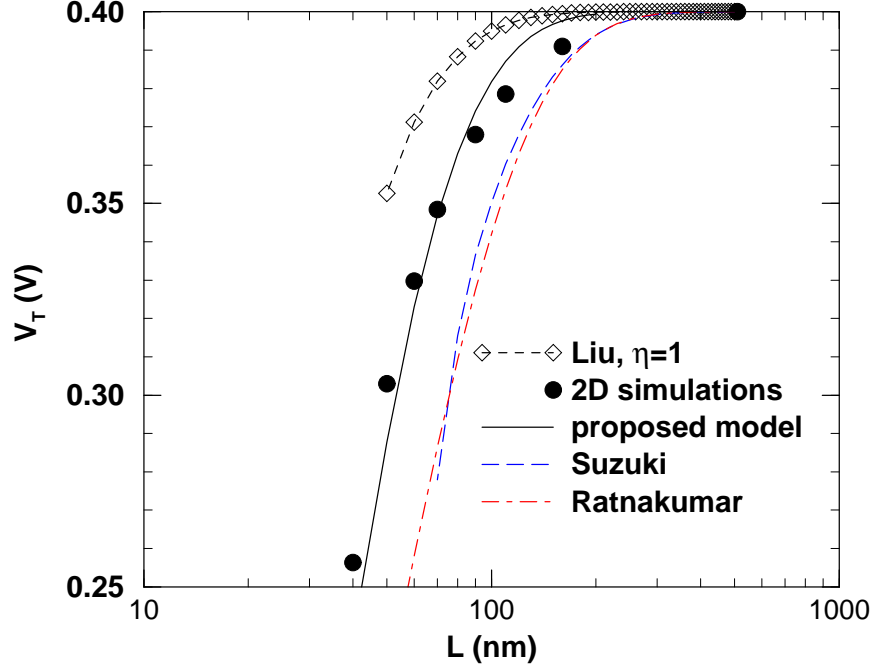


**Figure 4:**  $V_T$  versus  $L$  for a deep junction device;  $y_j = 70 \text{ nm}$ ,  $N_A = 1 \times 10^{18} \text{ cm}^{-3}$ ,  $t_{ox} = 1.5 \text{ nm}$ ,  $V_{DS} = 0.05 \text{ V}$ . The minimum channel depletion depth for this device is 35 nm.

Fig. 4 shows  $V_T$  vs.  $L$  for the deep junction case. For comparison, models of Ratnakumar, Liu and Suzuki are also shown. Ratnakumar's and Suzuki's models agree well with simulation results. Liu's model, with  $\eta = 1$ , severely underestimates rolloff. If  $\lambda'$  is used in Liu's model instead of  $1/l$ , then a good match is seen with the 2-D simulations. Also shown in the figure is the proposed model, which agrees well with simulations.

Fig. 5 shows  $V_T$  vs.  $L$  for the shallow junction case. It can be seen that the proposed model agrees well with simulations. Ratnakumar, Liu and Suzuki assume a deep junction in their models and their models cannot predict the effect of  $y_j$  on  $V_T$ . So a poor match is seen between their models and simulations.

Fig. 6 shows the proposed model versus simulations for various  $y_j$ , in the  $V_T$  vs.  $L$  plane. It can be seen that for all cases, the model agrees well with simulations.  $\lambda_{eq1}$  can be used as a junction depth dependent scale length. Fig. 7 shows the universal  $V_T$  rolloff curve generated by plotting rolloff versus  $L \cdot \lambda_{eq1}$ . The rolloff data is generated for various  $N_A$ ,  $y_j$  and  $L$ . It can be seen that all points lie on a common curve, indicating the fact



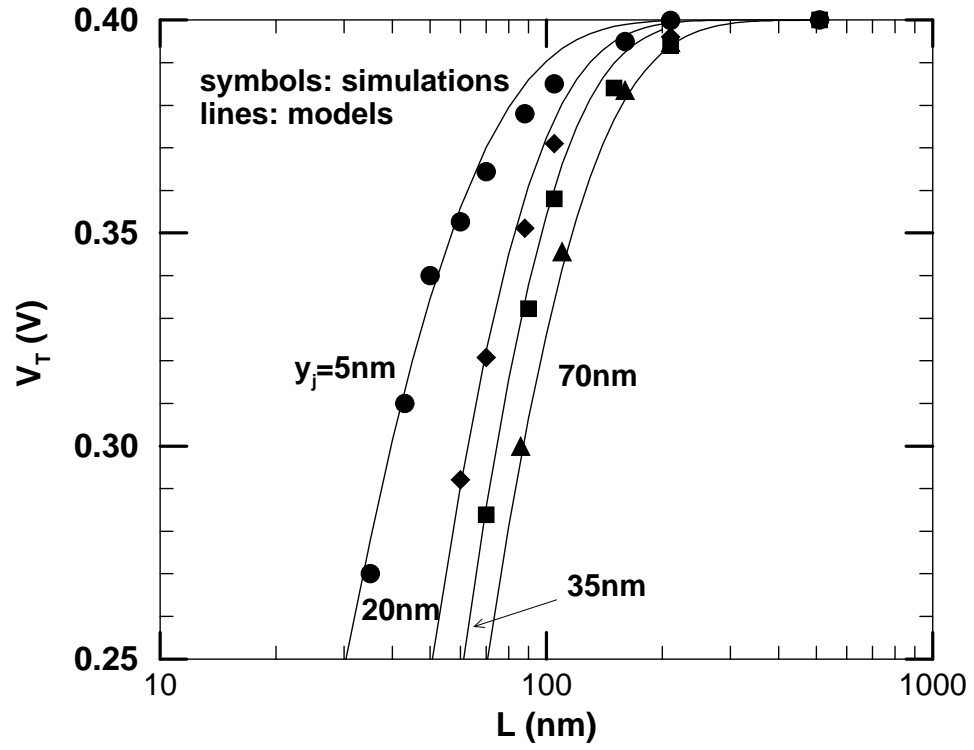
**Figure 5:**  $V_T$  versus  $L$  for a shallow junction device;  $y_j = 20 \text{ nm}$ ,  $N_A = 1 \times 10^{18} \text{ cm}^{-3}$ ,  $t_{ox} = 1.5 \text{ nm}$ ,  $V_{DS} = 0.05 \text{ V}$ . The minimum channel depletion depth for this device is 35 nm.

that  $\lambda_{eq1}$  can be used as a junction depth dependent scale length. This scale length can be used to rapidly analyze the minimum channel length for a given  $t_{ox}$ ,  $y_j$  and  $N_A$ . The relationship between  $L_{min}$  and  $\lambda_{eq1}$  is calibrated using ITRS 2002 parameters for the year 2002. It is found that  $L_{min} = 3.46/\lambda_{eq1}$ . Using this relation,  $L_{min}$  is extracted for various technology generations from 2003-2007 and compared with the ITRS projections, Fig. 8. A close correlation is seen between  $L_{min}$  predictions by the model, and ITRS projections.

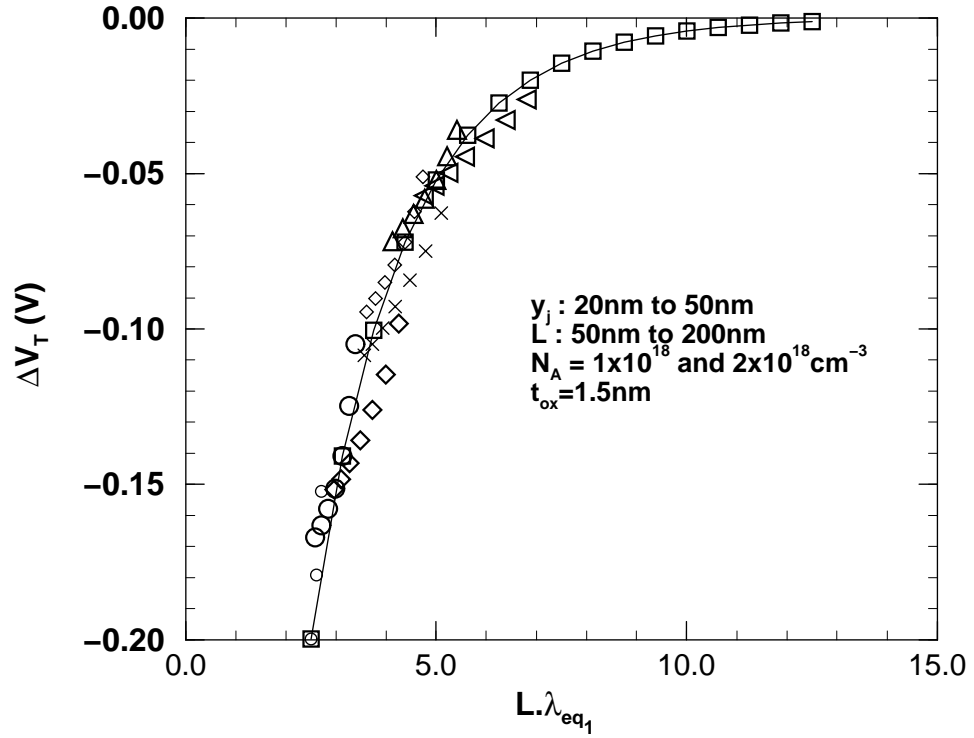
## 2.2 Threshold Voltage Rolloff of Accumulation MOSFETs

### 2.2.1 Introduction

Most previous work on accumulation MOSFET modeling have been limited to 1-D analyses [64]-[65]. A threshold voltage ( $V_T$ ) rolloff model for buried-channel MOSFETs is proposed in [66], but uses fit parameters, and thus cannot be used for predictive modeling; also, charge sharing principle is used to model drain-induced barrier lowering, and the method is not accurate for short channel lengths. Austin [47] proposed a source/drain junction depth dependent  $V_T$  rolloff model for bulk accumulation MOSFETs, but the model is not accurate

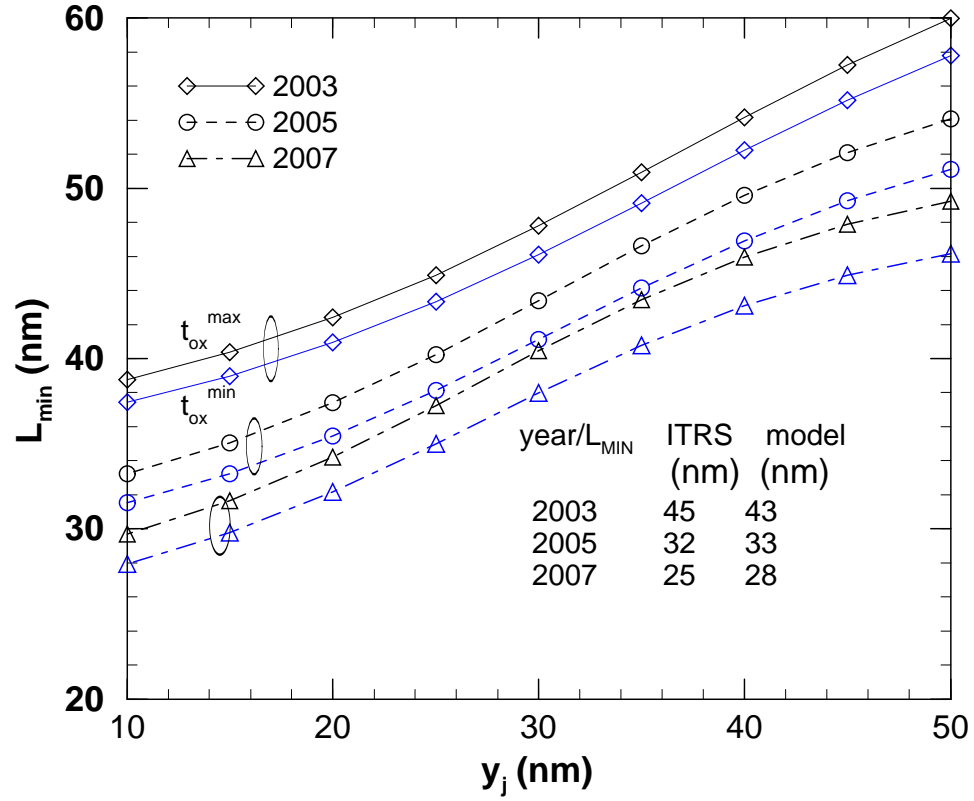


**Figure 6:**  $V_T$  vs.  $L$  for different junction depths;  $N_A = 1 \times 10^{18} \text{ cm}^{-3}$ ,  $t_{ox} = 1.5 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ . The minimum channel depletion depth for this device is 35 nm.



**Figure 7:**  $V_T$  vs.  $L \cdot \lambda_{eq1}$  for various device parameters.





**Figure 8:**  $L_{min}$  projection using  $\lambda_{eq}$ .  $t_{ox}^{min}$  and  $t_{ox}^{max}$  values are taken from ITRS 2002 recommendations for the particular generation.

for intermediate and shallow junction devices. An accurate, source/drain junction depth dependent,  $V_T$  rolloff model for bulk accumulation MOSFETs is proposed, and verified against 2-D simulations.

### 2.2.2 Long Channel Threshold Voltage

The long-channel threshold voltage ( $V_{T_{long}}$ ) of accumulation MOSFETs has been derived previously in various works [47], [64]. But existing  $V_{T_{long}}$  models do not agree well with simulations. Thus, there is a need to look at the derivation of  $V_{T_{long}}$  for accumulation MOSFETs. The device analyzed is shown in Fig. 9. In the subthreshold regime, the 1-D potential in the channel depth direction is given by the 1-D Poisson equation:

$$\begin{aligned}\frac{\partial^2 U}{\partial y^2} &= \frac{qN_D}{\epsilon_s}; & 0 < x < L, \quad 0 < y < y_i \\ &= \frac{qN_A}{\epsilon_s}; & 0 < x < L, \quad y_i < y < d\end{aligned}\tag{11}$$

$L$  is the effective channel length, and  $y_i$  is the tub-depth.  $U(y)$  is solved by double integration:

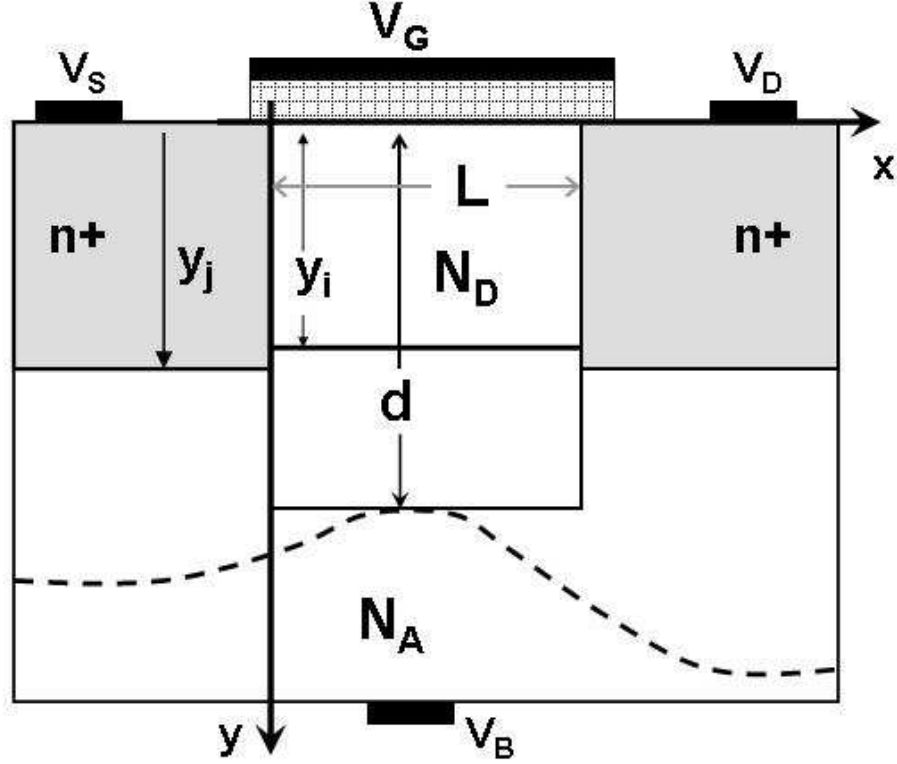
$$\begin{aligned}U(y) &= -\frac{qN_D}{2\epsilon_s}(y - y_i)^2 - \frac{qN_A}{\epsilon_s}(d - y_i)y + \frac{qN_A}{2\epsilon_s}(d^2 - y_i^2) & 0 \leq y \leq y_i \\ &= \frac{qN_A}{2\epsilon_s}(y - d)^2 & y_i \leq y \leq d\end{aligned}\tag{12}$$

The expression for the minimum channel depletion depth ( $d$ ) is shown in Table 6. The long channel threshold voltage ( $V_{T_{long}}$ ) is obtained from  $U(y)$  by finding the gate voltage that gives  $U(y_{ch}) = 2\phi_F$ , where  $\phi_F = \frac{kT}{q} \ln\left(\frac{N_A}{n_i}\right)$  is the bulk Fermi level. For SCA MOSFETs,

$$V_{T_{long}} = V_{FB} + 2\phi_F - \frac{q(N_A + N_D)y_i}{C_{ox}} + \frac{\sqrt{2q\epsilon_s N_A}}{C_{ox}} \left[ 2\phi_F + \frac{qN_A}{2\epsilon_s} \left( 1 + \frac{N_D}{N_A} \right) y_i^2 \right]^{1/2}\tag{13}$$

where  $V_{FB}$  is the flat-band voltage, and  $C_{ox} = \epsilon_{ox}/t_{ox}$  is the oxide capacitance. For BCA MOSFETs,

$$\begin{aligned}V_{T_{long}} &= V_{FB} + \frac{N_D}{N_D + N_A} 2\phi_F + \left( \frac{1}{C_{ox}} \right) \left( \sqrt{\frac{2\epsilon_s N_A N_D}{N_D + N_A}} 2\phi_F - qN_D y_i \right) \\ &\quad + \left( \frac{\epsilon_s}{y_i} \right) \left( \sqrt{\frac{2\epsilon_s N_A N_D}{N_D + N_A}} 2\phi_F - \frac{qN_D y_i}{2} \right)\end{aligned}\tag{14}$$



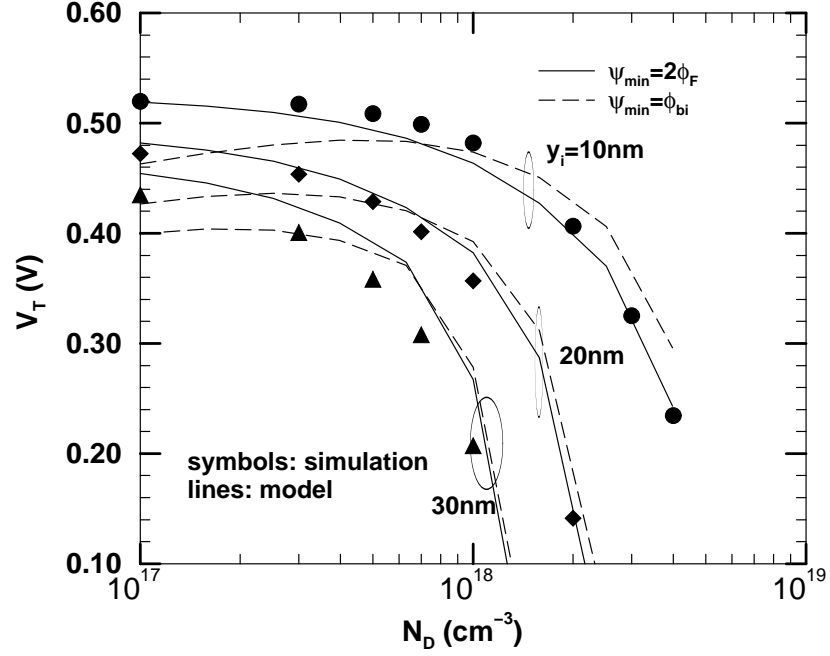
**Figure 9:** Accumulation n-FET structure and terminology.

For the Fermi MOSFET (which is the boundary between the BCA and SCA FET),  $V_{T_{long}}$  is simply given by  $V_{FB} + 2\phi_F$ . For SCA MOSFETs (and inversion MOSFETs), the vertical channel location ( $y_{ch}$ ) is zero. For BCA MOSFETs

$$y_{ch} = \left(1 + \frac{N_A}{N_D}\right) y_i - \frac{N_A}{N_D} d \quad (15)$$

In [47],  $V_{T_{long}}$  is defined to be the gate voltage that gives  $U(y_{ch}) = \phi_{bi}$ ;  $\phi_{bi} = \frac{kT}{q} \ln\left(\frac{N_A N_D}{n_i^2}\right)$  is the built-in potential between the tub and the substrate. This definition results in a non-monotonic dependency of  $V_{T_{long}}$  on channel doping, Fig. 10. It can be seen that the  $V_{T_{long}}$  model based on the definition in [47] does not agree well with 1-D simulation results. On the other hand, the proposed  $V_{T_{long}}$  definition ( $V_T = V_G|_{U(y_{ch})=2\phi_F}$ ) agrees well with simulation results<sup>2</sup>, Figs. 10 and 11. It can be seen that as  $y_i$  increases, the mismatch between the  $V_{T_{long}}$  model and simulations increases. As  $y_i$  increases, the electrons spread more into the depth direction; an integration of the inversion charge in the depth direction would then

<sup>2</sup>In 2-D simulation results,  $V_T$  is defined as the gate voltage required to give a drain current of  $0.1 \mu A/\mu m \times W/L$ .



**Figure 10:** Verification of long channel threshold voltage model with 1-D simulations;  $N_A = 7 \times 10^{17} \text{ cm}^{-3}$ , and  $t_{ox} = 1.5 \text{ nm}$ .

give an accurate estimate of  $V_{T_{long}}$ . Appendix A shows how to extend the threshold voltage model to devices with deep tub-depths, and high SCE ( $\Delta V_T > 200 \text{ mV}$ ). It will be seen in later sections that for  $y_i > 30 \text{ nm}$ , SCE is very high in accumulation FETs; thus the proposed compact model is sufficient for devices analyzed in this work.

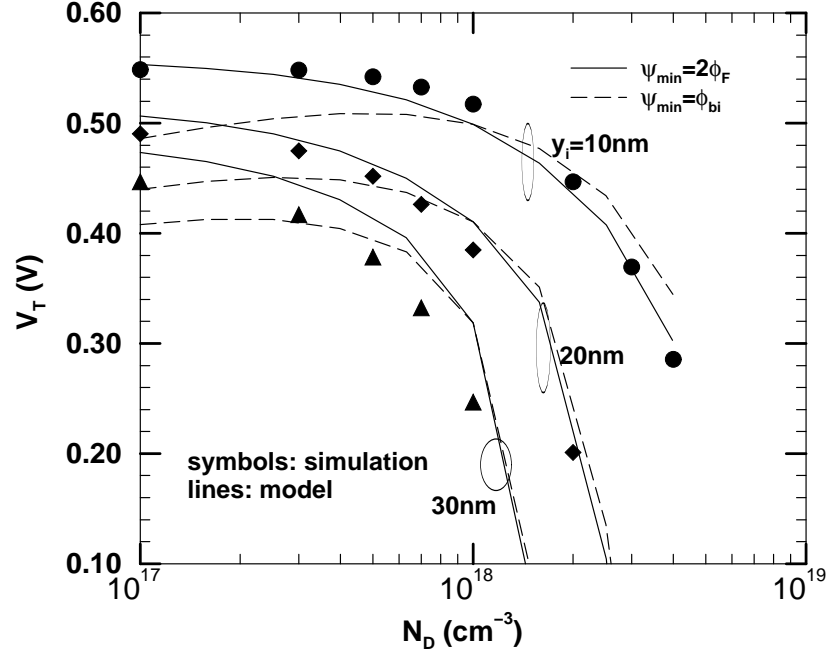
### 2.2.3 Threshold Voltage Rolloff Model

The device analyzed is shown in Fig. 9. In the subthreshold region, the tub ( $N_D$ ) and part of the substrate ( $N_A$ ) are depleted of mobile carriers; the potential distribution in the depleted rectangular region is given by the 2-D Poisson equation:

$$\begin{aligned} \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} &= \frac{qN_D}{\epsilon_s}; & 0 < x < L, \quad 0 < y < y_i \\ &= \frac{qN_A}{\epsilon_s}; & 0 < x < L, \quad y_i < y < d \end{aligned} \quad (16)$$

$L$  is the effective channel length, and  $y_i$  is the tub-depth. (16) is solved by the method of superposition [54]:

$$\psi(x, y) = U(y) + \phi(x, y) \quad (17)$$



**Figure 11:** Verification of long channel threshold voltage model with 1-D simulations;  $N_A = 1 \times 10^{18} \text{ cm}^{-3}$ , and  $t_{ox} = 1.5 \text{ nm}$ .

where  $U(y)$  is the solution to the 1-D Poisson equation and  $\phi(x, y)$  is the solution to the 2-D Laplace equation.  $\phi(x, y)$  can be thought of as the source/drain effect on the overall potential.  $\phi(x, y)$  is solved by the method of separation of variables:

$$\phi(x, y) = \sum_{n=1}^{\infty} (C_n \cdot \exp(\lambda_n(x - L)) + D_n \cdot \exp(-\lambda_n x)) \left( \sin(\lambda_n y) + \frac{\lambda_n \epsilon_s}{C_{ox}} \cos(\lambda_n y) \right) \quad (18)$$

$C_n$  and  $D_n$  are evaluated from the boundary conditions, and are as shown in Table 6. The two possible bottom boundary conditions for  $\psi(x, y)$  result in two different eigenvalues,  $\lambda'$ , and  $\lambda''$ .  $\lambda'$  and  $\lambda''$  are superimposed to obtain  $\lambda$ , Table 6.

From the 2-D potential, an expression for the short-channel threshold voltage shift ( $\Delta V_T$ ) is obtained as follows: the minimum potential point  $(x_m, y_{ch})$  is calculated from  $\frac{\partial \psi(x_m, y_{ch})}{\partial x} = 0$ ; then the gate voltage that gives  $\psi(x_m, y_{ch}) = 2\phi_F$  is the threshold voltage of the device. The difference between this threshold voltage and the long channel threshold voltage ( $V_{T_{long}}$ ) is the short-channel threshold voltage shift ( $\Delta V_T$ ). To enable an analytical solution for  $V_T$  rolloff,  $\phi(x, y)$  is approximated by a single-term solution. This approximation works very well since the terms involving higher order  $\lambda$ 's decay rapidly. The expression for

$\Delta V_T$  is

$$\Delta V_T = 2\Gamma \cdot \Theta \left\{ 1 + \sqrt{1 - \frac{\chi_1(\psi_{bi}, y_j) \chi_1(\psi_{bi} + V_{DS}, y_j)}{[\chi_1(\psi_{bi}, y_j) + \chi_1(\psi_{bi} + V_{DS}, y_j)] \Gamma \cdot \Theta}} \right\} \quad (19)$$

where the various terms are shown in Tables 6 and 7. The tables also show how to extend the threshold voltage rolloff model to uniformly doped (UD) SCI MOSFETs, and retrograde doped (RD) SCI FETs. Fig. 12 compares the proposed threshold voltage rolloff model with 2-D simulations [67]. The model is seen to work well in predicting threshold voltage rolloff of both SCA and BCA MOSFETs.

### ***2.3 Summary***

A compact threshold voltage rolloff model has been proposed that accurately models the effect of junction depth on threshold voltage rolloff. The model is physically based, and is useful for device optimization, technology prediction, and circuit simulation. The model provides a scale length which can be used to rapidly analyze the impact of junction depth scaling on minimum channel length. The model is applicable to both inversion and accumulation MOSFETs, and thus allows easy comparison between the two MOSFET types.

**Table 6:**  $V_T$  rolloff expression for accumulation and inversion FETs.

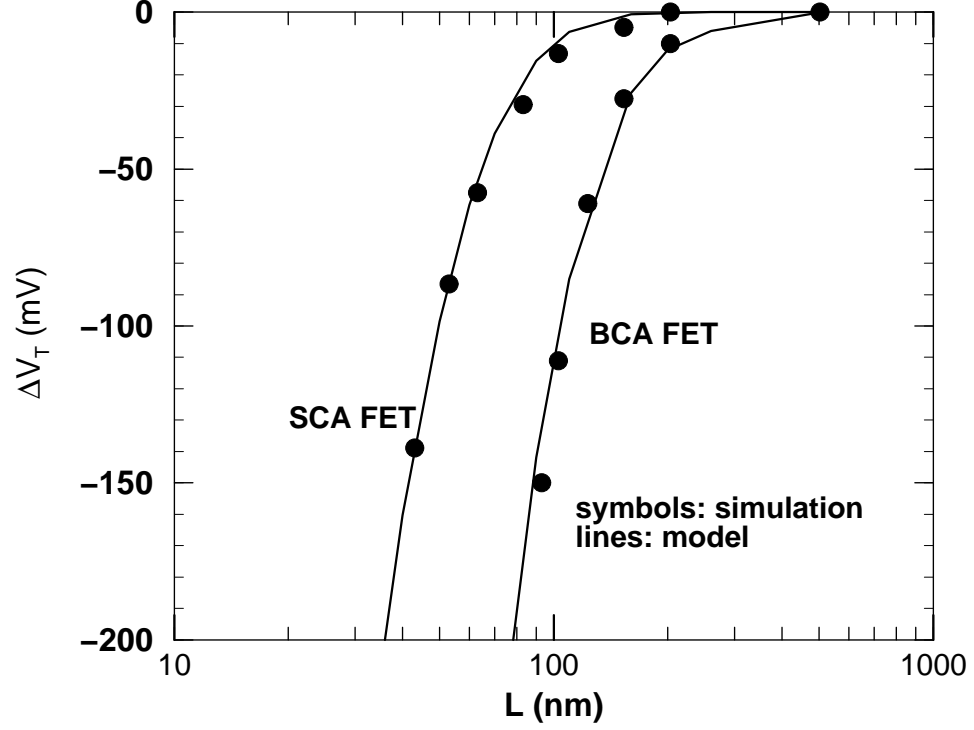
[UD-SCI:  $N_T = -N_A$ ,  $N_W = N_A$ ,  $y_i = 0$ ; RD-SCI:  $N_T = -N_A^-$ ,  $N_W = N_A$ ; SCA/BCA/FF:  $N_T = N_D$ ,  $N_W = N_A$ ]

All Cases:	$D_n = \frac{A_n(\psi_{\text{bis}}) + B_n(\psi_{\text{bis}}, y_j)}{\frac{\epsilon_s \lambda_n}{C_{\text{ox}}} \mathcal{K}_n}$ $C_n = \frac{A_n(\psi_{\text{bid}} + V_{\text{DS}}) + B_n(\psi_{\text{bid}} + V_{\text{DS}}, y_j)}{\frac{\epsilon_s \lambda_n}{C_{\text{ox}}} \mathcal{K}_n}$ $\tan(\lambda' d) = \frac{C_{\text{ox}}}{\lambda' \epsilon_s}; \quad \tan(\lambda'' d) = \frac{-\lambda'' \epsilon_s}{C_{\text{ox}}}$ $\lambda_n = (\lambda'_n - \lambda''_n) \cdot \frac{1}{1 + \exp\left(\frac{d - y_i}{d/2}\right)} + \lambda''_n$ $\Theta = \frac{-[\mathcal{X}_1(\Psi_{\text{bis}}, y_j) + \mathcal{X}_1(\Psi_{\text{bid}} + V_{\text{DS}}, y_j)] \exp(-\frac{\lambda_1 L}{2}) F(y_{\text{ch}})}{\mathcal{K}_1 - 2 \exp(-\frac{\lambda_1 L}{2}) F(y_{\text{ch}})}$ $\Gamma = \frac{\exp(-\lambda_1 L/2) F(y_{\text{ch}})}{\kappa_1 + 2 \exp(-\lambda_1 L/2) F(y_{\text{ch}})}$ $\mathcal{X}_1(V, y_j) = A_1(V)  _{V_{\text{GS}}=V_{\text{T}_{\text{long}}}} + B_1(V, y_j)$ $A_1(V) = V + V_{\text{FB}} - V_{\text{GS}} - \frac{q N_{\text{T}}}{\epsilon_s \lambda_1^2}$ $+ \left[ \frac{q(N_W + N_{\text{T}})}{\epsilon_s \lambda_1^2} \right] \left[ \cos(\lambda_1 y_i) - \frac{\epsilon_s \lambda_1}{C_{\text{ox}}} \sin(\lambda_1 y_i) \right]$ $\Psi_{\text{bis}/D} = \frac{kT}{q} \ln \frac{N_W N_{D_{\text{S/D}}}}{n_i^2}$ $F(y_{\text{ch}}) = \cos(\lambda_1 y_{\text{ch}}) + \frac{C_{\text{ox}}}{\lambda_1 \epsilon_s} \sin(\lambda_1 y_{\text{ch}});$ $\mathcal{K}_1 = \frac{1}{2} \left[ 1 + \frac{C_{\text{ox}} d}{\epsilon_s} \left( 1 + \left( \frac{\lambda_1 \epsilon_s}{C_{\text{ox}}} \right)^2 \right) \right]$ $d = -\frac{\epsilon_s}{C_{\text{ox}}} + \left[ \frac{2\epsilon_s}{q N_W} (V_{\text{G}} - V_{\text{FB}} - V_{\text{B}}) \right. \\ \left. + \left( 1 + \frac{N_{\text{T}}}{N_W} \right) \left( y_i^2 + \frac{2\epsilon_s}{C_{\text{ox}}} y_i \right) + \left( \frac{\epsilon_s}{C_{\text{ox}}} \right)^2 \right]^{1/2}$
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**Table 7:**  $V_T$  roll-off for accumulation and inversion devices.

$y_j > y_i; \quad d < y_j$	$B_1(V, y_j) = \left[ V - V_{BS} + \frac{qN_W}{\epsilon_s \lambda_1^2} \right] \left[ \frac{\epsilon_s \lambda_1}{C_{ox}} \sin(\lambda_1 d) - \cos(\lambda_1 d) \right]$
$y_j > y_i; \quad d > y_j$	$ \begin{aligned} B_1(V, y_j) = & -\frac{qN_W}{\epsilon_s \lambda_1^2} \left[ \cos(\lambda_1 y_j) - \frac{\epsilon_s \lambda_1}{C_{ox}} \sin(\lambda_1 y_j) \right] \\ & + \left[ \frac{qN_W(d_{s/d}(V) - y_j)}{\epsilon_s \lambda_1} \right] \left[ \sin(\lambda_1 y_j) + \frac{\epsilon_s \lambda_1}{C_{ox}} \cos(\lambda_1 y_j) \right] \\ & - \left( \frac{qN_W(d_s - d)^2}{2\epsilon_s} \right) \left[ \cos(\lambda_1 d) - \frac{\epsilon_s \lambda_1}{C_{ox}} \sin(\lambda_1 d) \right] \\ & + \left[ \frac{qN_W(d - d_{s/d}(V))}{\epsilon_s \lambda_1} \right] \left[ \frac{\epsilon_s \lambda_1}{C_{ox}} \cos(\lambda_1 d) + \sin(\lambda_1 d) \right] \\ \\ & d_{s/d}(V) = y_j + \sqrt{\frac{2\epsilon_s}{qN_W} (V - V_{BS})} \end{aligned} $
$y_j < y_i; \quad d > y_j$	$ \begin{aligned} B_1(V, y_j) = & \frac{qN_T}{\epsilon_s \lambda_1^2} \left[ \cos(\lambda_1 y_j) - \frac{\epsilon_s \lambda_1}{C_{ox}} \sin(\lambda_1 y_j) \right] \\ & + \frac{qN_T}{\epsilon_s \lambda_1} \left[ \frac{N_W(d_s - y_i)}{N_T} + y_j - y_i \right] \\ & \quad \left[ \sin(\lambda_1 y_j) + \frac{\epsilon_s \lambda_1}{C_{ox}} \cos(\lambda_1 y_j) \right] \\ & - \frac{q(N_W + N_T)}{\epsilon_s \lambda_1^2} \left[ \cos(\lambda_1 y_i) - \frac{\epsilon_s \lambda_1}{C_{ox}} \sin(\lambda_1 y_i) \right] \\ & - \left( \frac{qN_W(d_s - d)^2}{2\epsilon_s} \right) \left[ \cos(\lambda_1 d) - \frac{\epsilon_s \lambda_1}{C_{ox}} \sin(\lambda_1 d) \right] \\ & + \left[ \frac{qN_W(d - d_{s/d}(V))}{\epsilon_s \lambda_1} \right] \left[ \frac{\epsilon_s \lambda_1}{C_{ox}} \cos(\lambda_1 d) + \sin(\lambda_1 d) \right] \\ \\ & d_{s/d}(V) = y_j + \sqrt{\left( 1 + \frac{N_T}{N_W} \right) (y_j - y_i)^2 + \frac{2\epsilon_s}{qN_W} (V - V_{BS})} \end{aligned} $





**Figure 12:** Threshold voltage rolloff for SCA and BCA MOSFETs: model vs. 2-D simulations;  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ , and  $V_{DS} = 1.0 \text{ V}$  for both SCA, and BCA MOSFETs. For the SCA FET,  $N_A = 2 \times 10^{18} \text{ cm}^{-3}$ ,  $N_D = 1 \times 10^{17} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ . For the BCA MOSFET,  $N_A = 1 \times 10^{18} \text{ cm}^{-3}$ ,  $N_D = 2 \times 10^{18} \text{ cm}^{-3}$ , and  $y_i = 30 \text{ nm}$ .

## CHAPTER III

### SUBTHRESHOLD CONDUCTION MODELING

#### 3.1 *Introduction*

Static power in gigascale systems is becoming increasingly important, especially in portable systems. Subthreshold swing (S) is an indicator of how well the device can be turned off, and is important in predicting the subthreshold current. Existing models for S in the literature are either semi-empirical [61], [68] or when physical, are applicable only for relatively longer channel lengths [47]. Also, existing S models do not accurately model junction depth effects. An accurate subthreshold swing model is proposed that holds good for both accumulation and inversion MOSFETs. Existing off-current models for accumulation MOSFETs use fit parameters [69]-[70], and thus, are not suitable for predictive modeling. A subthreshold current model for accumulation MOSFETs is proposed based on the Swanson-Meindl approach for inversion MOSFETs.

#### 3.2 *Subthreshold Swing Model*

Subthreshold slope is defined as

$$S^{-1} = \frac{\partial \log(I_D)}{\partial V_g} \quad (20)$$

in the subthreshold region ( $V_G < V_T$ ). The drain current  $I_D$  is dependent on the minimum potential point in the channel (assuming a charge sheet). Thus,  $I_D \propto n$ , where carrier concentration  $n$  is given by  $n = e^{\beta(\psi_{min} - \phi_{Fn})}$ .  $\psi_{min}(y)$  is the minimum potential, and can be extracted from the 2-D potential derived earlier in this work;  $\phi_{Fn}$  is the quasi-Fermi level of electrons (constant in the depth direction). Substituting  $n$  and  $I_D$ , in (20)

$$S^{-1} = \frac{\partial \psi_{min}}{\partial V_G} \quad (21)$$

Comparison of the above model for S with 2-D simulations [63] is shown in Fig. 13, for an RD-SCI device. It can be seen that the point-derivative model fails to capture the steep

subthreshold swing rollup of short channel length MOSFETs.

Fig. 14 plots electron concentration vs. distance from the Si – SiO<sub>2</sub> interface. Defining the inversion layer thickness (ILT) as the depth at which the electron concentration has decayed by two orders of magnitude from its peak value, it can be seen that the 100 nm device has an ILT of 2nm, while the 40 nm device has an ILT of 4nm; the 30 nm device has an ILT of around 7 nm. It can be seen that as the channel length is decreased, even the classical distribution of electrons occupies a reasonable depth below the semiconductor-oxide interface, and the assumption of inversion layer thickness to be zero is invalid. This is the same situation that Chen et al [71] faced in their work on double gate (DG) FET modeling - the DG-FETs have volume inversion and thus the electron concentration has to be integrated over the device depth to calculate S. A similar approach can be adopted for bulk devices.

When the inversion (or accumulation) layer thickness is assumed to be non-zero, the drain current in the subthreshold region is no more dependent on the carrier concentration at a single point; rather, it is now a function of the carrier concentration over the inversion layer thickness. Since the exact inversion layer thickness is not known, it is better to make the drain current a function of carrier concentration over the depletion depth:

$$I_D \propto \int_0^d n \cdot dy \quad (22)$$

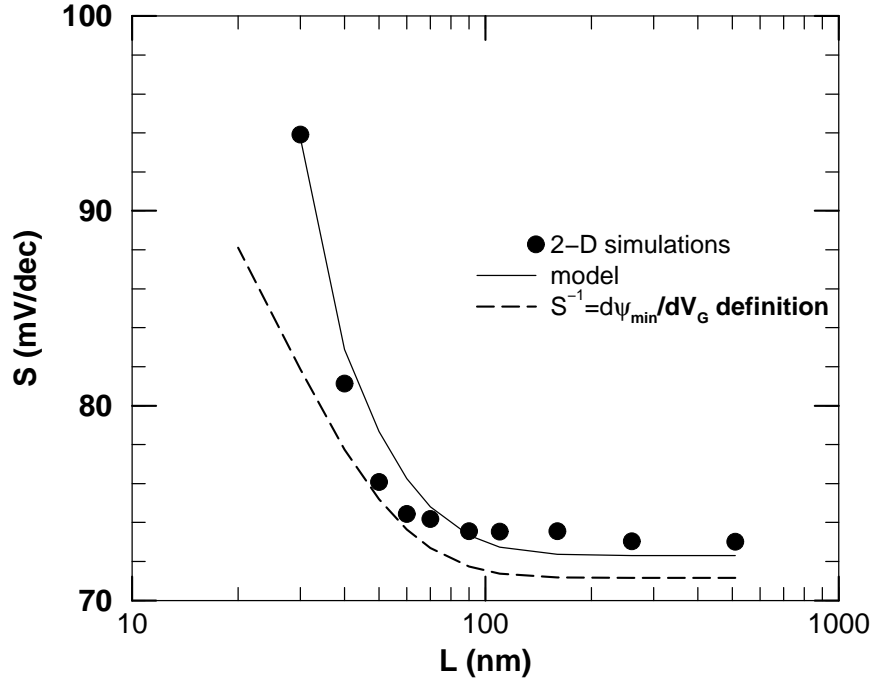
Substituting (22) in (20),

$$S^{-1} = \frac{\int_0^d n \cdot \frac{d\psi_{min}}{dV_g} \cdot dy}{\int_0^d n \cdot dy} \cdot \frac{\beta}{\ln(10)} \quad (23)$$

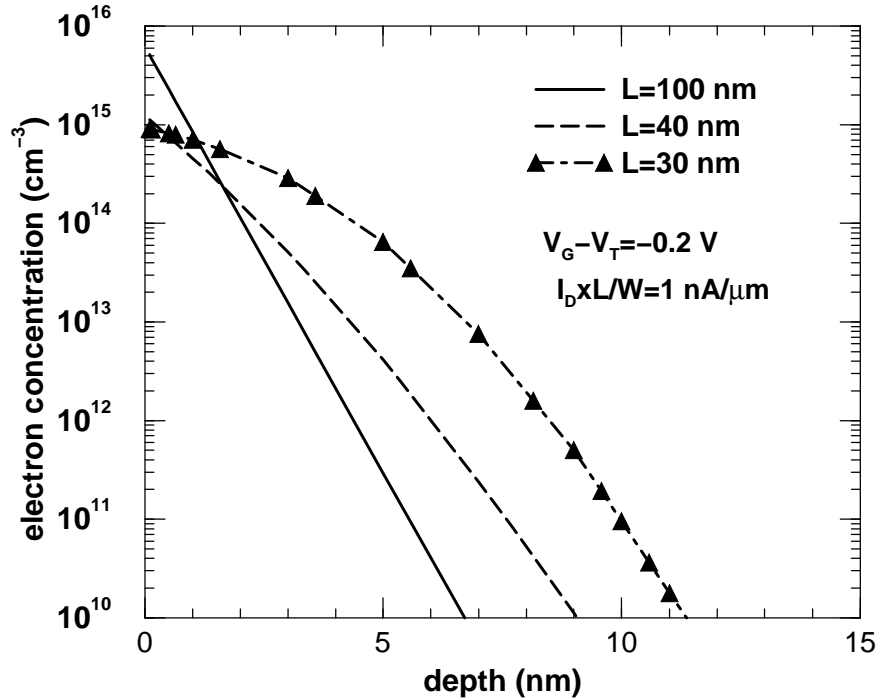
(23) reduces to (21) as  $d \rightarrow 0$ . When this new model is used to calculate S and compared with 2-D simulations, Fig. 13, a good match can be seen between the model and simulations. Fig. 15 compares the subthreshold swing model for BCA/SCA MOSFETs with 2-D simulations; a favorable match is seen between the model and simulations.

### 3.3 Subthreshold Conduction Model

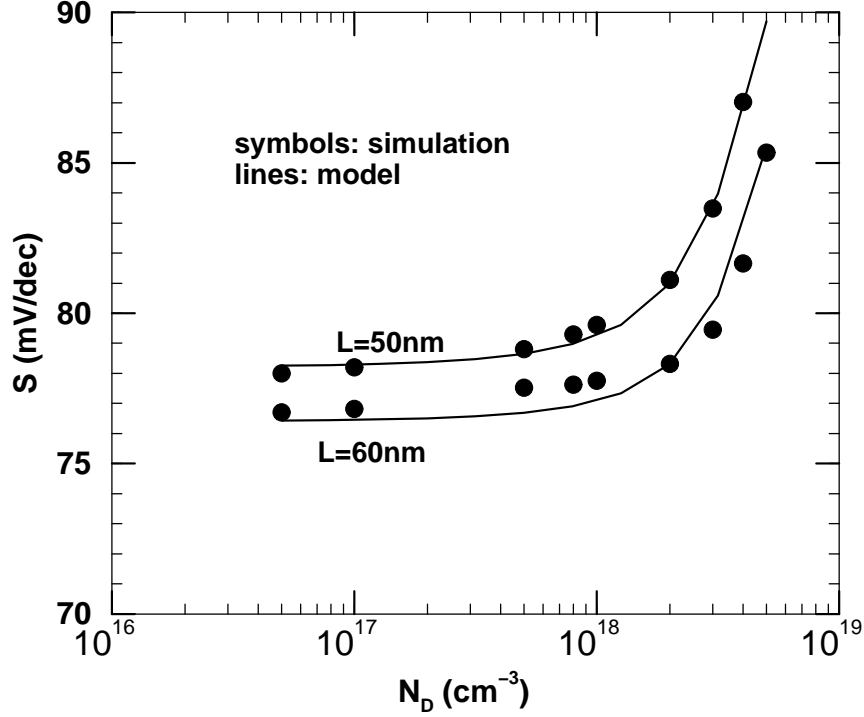
An expression for the subthreshold current of long-channel accumulation FETs is obtained by following the analysis of Swanson and Meindl [72] for bulk inversion MOSFETs. The



**Figure 13:** Comparison of subthreshold swing models with 2-D simulations for an RD-SCI MOSFET;  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 20 \text{ nm}$ ,  $V_{DS} = 0.05 \text{ V}$ ,  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ ,  $N_A^- = 1 \times 10^{17} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ .



**Figure 14:** Electron concentration variation in the depth direction for different channel lengths (from 2-D simulations) for an RD-SCI MOSFET;  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ ,  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ ,  $N_A^- = 1 \times 10^{17} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ .



**Figure 15:** Comparison of subthreshold swing model for accumulation MOSFETs with 2-D simulations;  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ ,  $N_A = 2 \times 10^{18} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ .

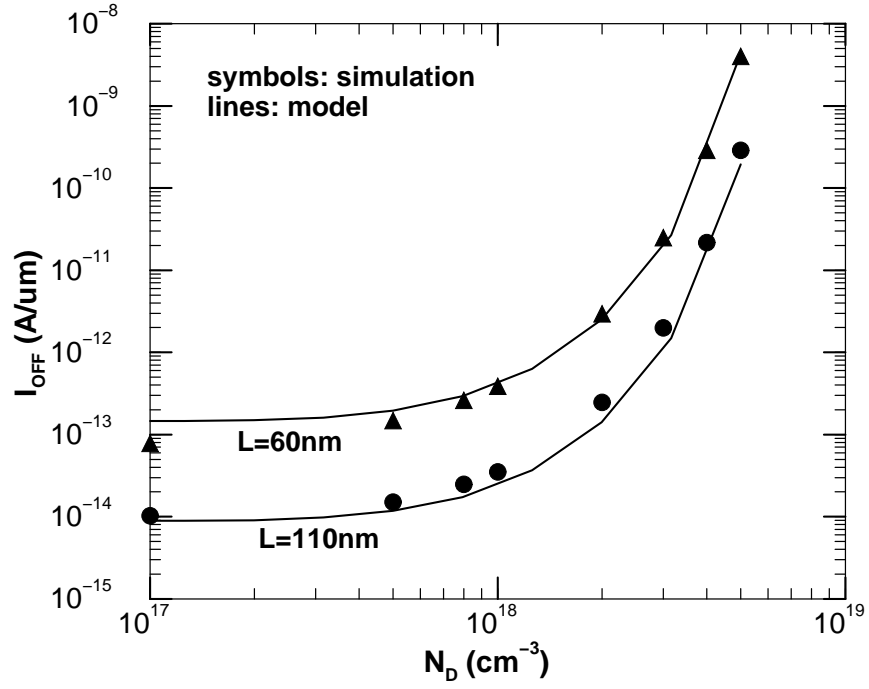
short-channel subthreshold current is obtained by replacing  $S$  and  $V_T$  by their short-channel values:

$$I_{sub} = \frac{W}{L} \mu C_g \frac{\eta}{\beta^2} \exp\left(\frac{V_G - V_T - \frac{n}{\beta}}{\frac{\eta}{\beta}}\right) [1 - \exp(-\beta V_{DS})] \quad (24)$$

Here,  $\eta = \frac{S \cdot \beta}{\ln(10)}$  is the subthreshold swing factor;  $C_g = C_{ox}$  for SCA FETs, and  $C_g = C_{ox} C_{Si} / (C_{ox} + C_{Si})$  for BCA FETs, where  $C_{Si} = \epsilon_s / y_{ch}$ . The subthreshold current model is compared with 2-D simulations for a wide range of channel doping, for both long, and short channel lengths, Fig. 16. A good match is seen between the model and simulations.

### 3.4 Summary

Static power is becoming increasingly important in gigascale systems. Accurate subthreshold swing modeling is critical for subthreshold current prediction, and optimization of  $V_T$  and  $V_{dd}$ . The canonical method of taking a point-derivative to calculate subthreshold swing fails at short channel lengths due to volume inversion. An approach originally formulated for subthreshold swing computation of double gate MOSFETs is applied to accumulation



**Figure 16:** Comparison of off-current model with 2-D simulations for accumulation MOSFETs;  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ ,  $N_A = 2 \times 10^{18} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ .

and inversion MOSFETs. The resulting subthreshold swing model agrees well with 2-D simulations. An expression for subthreshold current of accumulation MOSFETs is formulated based on the Swanson-Meindl approach for inversion MOSFETs.

## CHAPTER IV

### PREDICTIVE CIRCUIT MODELING

#### *4.1 Introduction*

The trend toward device miniaturization makes it necessary to scan a wide range of supply and threshold voltages, and different types of FETs so that optimal performance is obtained. Such a scan is best done by physically based models so that predictive circuit modeling can be done to project, and optimize circuit performance well into the next decade. Circuit simulators like SPICE do not have an easy interface to input user-defined models; circuit simulators also have a higher computation time (compared to analytical techniques) which could result in large computation times for optimization in a multi-dimensional design space. Thus, a computationally efficient methodology that is also easy to implement is needed to use existing FET physical models to predict circuit performance.

The speed and accuracy of  $V_{dd} - V_T$  optimization, and prediction of power-frequency performance depends on both the underlying FET models, and the way these models are used to extract power and timing information. In this work, the MOSFET I-V model proposed by Austin [73] is used. This I-V model is transregional in nature, i.e. all regions of operation are modeled by maintaining continuity across regional boundaries while including lateral and vertical high field effects. The model is entirely physical and avoids any parameter fitting. Therefore, the model is extremely useful for predicting the performance of technology generations over the next decade.

Predictive circuit modeling for near term generations can be done in a way similar to that in [74]. In fact, using physical FET models for threshold voltage and subthreshold swing derived in Chapters II and III, some of the critical BSIM parameters can be calculated physically. The expression for one such parameter - DVT0 ( $V_T$  rolloff coefficient), is

given:

$$DVT0 = \frac{4}{\zeta} \left( 1 - \frac{\gamma \sqrt{2\phi_F} - \frac{qN_A}{\epsilon_{Si}\lambda_1^2}}{\phi_{bi} - 2\phi_F} \right) \quad (25)$$

where,

$$\zeta = \left[ 1 + \frac{C_{ox}d}{\epsilon_{Si}} \left( 1 + \left( \frac{\lambda_1 \epsilon_{Si}}{C_{ox}} \right)^2 \right) \right] (1 + \exp(-\lambda_1 L)) \quad (26)$$

and  $\gamma$  is the body bias factor.

Predictive circuit modeling for long-term future generations cannot be done using the approach proposed in [74], since more than 90% of BSIM parameters are not predicted but kept the same as that for a previous generation. For long-term predictive circuit modeling, a chain of inverters could be considered since worst-case delay of a critical path can be simulated by replacing complex CMOS gates by their worst-case inverters [75]. A number of methods, mostly analytical [73], [76]-[78], have been proposed to model inverter delay. Either most of them are based on the alpha-power law proposed by Sakurai [79], which is unsuitable for predictive modeling since it makes use of fit parameters, or are valid only for a small range of supply voltages [73]. Also, for BCA FETs, which have five regions of operation [80], derivation of an analytical expression for gate delay would be subject to numerous assumptions, which would limit the validity of the delay equation to a small range of supply voltages.

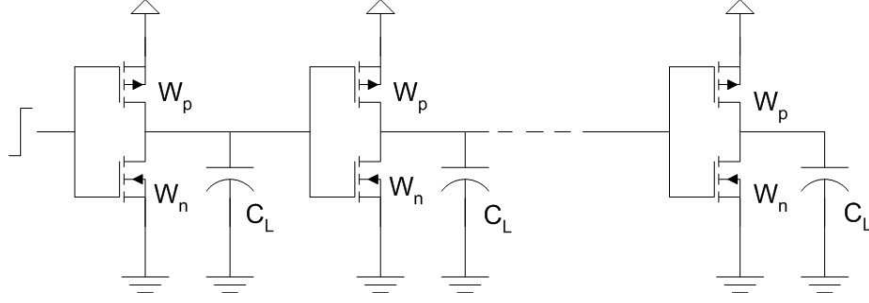
A circuit simulation methodology is proposed that is valid over a wide range of supply voltages, makes use of physical models, and is applicable for a variety of FETs, so that device and technology optimization can be performed by scanning a wide design space. The method is fast as it avoids any numerical integration. The proposed method is called *tick*-based, wherein a “tick” is a point in time. Since BSIM decks are readily available for SCI devices, an SCI FET is considered to validate the tick-based methodology.

## 4.2 Tick Based Method

Consider a critical path modeled by a chain of inverters, Fig. 17. Assuming equal rise and fall times and a step input to the first stage, the delay of the critical path is [81]

$$T_{PD} = \frac{1}{f_{clk}} = \frac{n_{cp} T_{PDn} f_{ineff}}{b} \quad (27)$$





**Figure 17:** An inverter chain used in the tick-based method.

where  $n_{cp}$  is the number of gates in the critical path,  $f_{ineff}$  is the effective fan-in factor,  $b$  is the clock skew factor, and  $T_{PDn}$  is the delay of the second or subsequent stages of the inverter chain. Since short-circuit power is less than 10% of total power in the 50nm generation [81], the short circuit current can be neglected while estimating delay and power to a first order. Thus,  $T_{PDn}$  is just the discharge time through an n-MOSFET. At the output of any stage, it is known that

$$i = -C_L \frac{dV_{out}}{dt} \quad (28)$$

where  $C_L$  is the load capacitance. Integrating both sides,

$$\int_{V_{n-1}}^{V_n} dV_{out} = -\frac{1}{C_L} \int_{t_{n-1}}^{t_n} i \cdot dt \quad (29)$$

The subscript  $n$  represents the current tick, whereas  $n-1$  represents the previous tick. The tick size,  $\Delta t (= t_n - t_{n-1})$ , is made small enough to avoid computational errors. Typically, this value is chosen to be around 1% of the expected delay value. At each tick, circuit parameters ( $V_T$ ,  $V_{in}$ ,  $V_{DSAT}$ ,  $V_{out}$ ) are updated.  $V_{T_n}$  is dependent on  $V_{DS_n}$  (because of DIBL), and thus needs to be updated at each time step.

An SCI device is used to exemplify the application of tick methodology. The SCI device has three regions of operation namely subthreshold, linear/non-saturated and saturated. The I-V equations [47] for the three regions of operation are shown in Table 8.

$V_{GS_n}$  is the input voltage at the present tick. This value is determined based on the input waveform. If the input is a step, then its value is  $V_{dd}$  for  $n \geq 0$ .  $V_{DS}$  is the same as  $V_{out}$ .  $V_T$  is the sum of  $V_{T_{long}}$  (not a function of  $V_{DS}$ ) and  $\Delta V_T$  (which is a function of

**Table 8:** I-V equations for the SCI FET [47].

Subthreshold	$I_d = \frac{W\mu_o C_{ox}}{Lm} \left[ \frac{1}{2\theta} \left( \sqrt{1 + \frac{4\eta\theta}{\beta}} - 1 \right) \right]^2 \left\{ 1 - \exp \left[ -\frac{\beta m}{\eta} V_{DS} \right] \right\} \exp \left\{ \frac{\beta}{\eta} \left[ V_{GS} - V_T - \frac{\eta}{\beta} \right] \right\}$
Linear/ Non-saturated	$I_d = \frac{WC_{ox}\mu_o}{L \left( 1 + \frac{V_d}{LE_c} \right) (1 + \theta(V_{GS} - V_T))} \left\{ (V_{GS} - V_T) V_{DS} - \frac{1}{2} V_{DS}^2 \right\} + \frac{WC_{ox}\mu_o}{L \left( 1 + \frac{V_d}{LE_c} \right) (1 + \theta(V_{GS} - V_T))} \left\{ \frac{4}{3} \phi_F \frac{Q_{BO}}{C_{ox}} \left[ \left( 1 + \frac{V_{DS}}{2 \phi_F } \right)^{3/2} - \left( 1 + \frac{3}{2} \frac{V_{DS}}{2\phi_F} \right) \right] \right\}$
Saturated	$I_d = \frac{WC_{ox}\mu_o}{L(1 + \theta(V_{GS} - V_T))} \left[ \frac{1}{\left( 1 + \frac{V_{DSAT}}{LE_c} \right)} \left\{ (V_{GS} - V_T) V_{DSAT} - \frac{1}{2} V_{DSAT}^2 + \frac{4}{3} \phi_F \frac{Q_{BO}}{C_{ox}} \left[ \left( 1 + \frac{V_{DSAT}}{2 \phi_F } \right)^{3/2} - \left( 1 + \frac{3}{2} \frac{V_{DSAT}}{2\phi_F} \right) \right] \right\} + \frac{1}{m} \left[ \frac{1}{2\theta} \left( \sqrt{1 + \frac{4\eta\theta}{\beta}} - 1 \right) \right]^2 \left\{ 1 - \exp \left[ -\frac{\beta m}{\eta} (V_{DS} - V_{DSAT}) \right] \right\} \right]$

$V_{DS}$ ). The value of  $\Delta V_T$  is found by assuming  $V_{DS} = V_{DS_{n-1}}$ . If a small enough tick size is chosen, then the error resulting from this assumption is extremely small.

First consider the subthreshold region of operation. The term involving  $V_{DS}$  in the drain current equation can be neglected for the most part of the output transition. Denoting the time-independent term in the I-V equation as  $K$ ,

$$I_d = K \cdot \exp \left\{ \frac{\beta}{\eta} \left[ V_{GS_n} - V_{T_n} - \frac{\eta}{\beta} \right] \right\} \quad (30)$$

Using (30) in (28) and integrating,

$$V_{out_n} - V_{out_{n-1}} = -\frac{1}{C_L} K \cdot \exp \left\{ \frac{\beta}{\eta} \left[ V_{GS_n} - V_{T_n} - \frac{\eta}{\beta} \right] \right\} \Delta t \quad (31)$$

$V_{out}|_{n=0} = V_{dd}$  for a falling output. Using this initial condition and the above equation,  $V_{out}$  can be evaluated at each  $n$  until  $V_{out}$  has reached 10% of the maximum value.

If  $V_{dd}$  is so low that the device always operates in the subthreshold region, then the delay can be found using analytical methods. It can be shown that the propagation delay in this case, assuming  $V_{dd} \gg \frac{3kT}{q}$ , is

$$T_{PD} = \frac{C_L V_{DD}}{I_{ON}} \left( 1 - \frac{\eta}{\beta V_{DD}} \right) \quad (32)$$

where  $I_{ON}$  is the on-current.

Next, consider the linear/non-saturated region of operation. In this region, the I-V equation can be rewritten as a sum of three components:  $I_{linear} = I_1 - I_2 + I_3$ , where,

$$\begin{aligned} I_1(V_{DS_n}) &= \kappa (V_{GS_n} - V_{T_n}) V_{DS_n} \\ I_2(V_{DS_n}) &= \kappa \left\{ \frac{1}{2} V_{DS_n}^2 \right\} \\ I_3(V_{DS_n}) &= \kappa \left\{ \frac{4}{3} \phi_F \frac{Q_{BO}}{C_{OX}} \left[ \left( 1 + \frac{V_{DS_n}}{2|\phi_F|} \right)^{3/2} - \left( 1 + \frac{3}{2} \frac{V_{DS_n}}{2\phi_F} \right) \right] \right\} \end{aligned}$$

where,

$$\kappa = \frac{WC_{ox}\mu_o}{L \left( 1 + \frac{V_d}{LE_c} \right) (1 + \theta(V_{GS_n} - V_{T_n}))} \quad (33)$$

Normally,  $I_3$  contributes very little to the overall current. Thus, this part can be evaluated using the  $V_{DS}$  value of the previous tick ( $=V_{DS_{n-1}}$ ). Fig. 18a shows  $V_{out}$  and the various components of  $I_{linear}$  plotted vs. time. To get a better idea of how large  $I_3$  is w.r.t.  $I_{linear}$ , the same curves are plotted as a percentage of the total current. This is shown in Fig. 18b.  $I_3$  is seen to be less than 10% of  $I_{total}$  almost all throughout the decay period. Thus,  $I_3$  can be made time independent. The I-V equation can now be rewritten as

$$I_d = \kappa \left\{ (V_{GS_n} - V_{T_n}) V_{out} - \frac{1}{2} V_{out}^2 \right\} + I_3(V_{out_{n-1}}) \quad (34)$$

Using (34) in (28) and integrating,

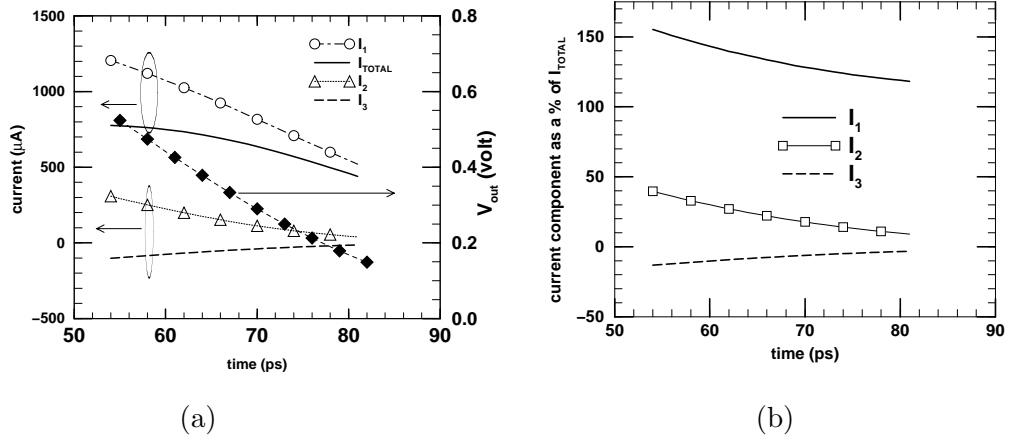
$$\int_{V_{out_{n-1}}}^{V_{out_n}} \frac{dV_{out}}{\left\{ (V_G - V_T) V_{out} - \frac{1}{2} V_{out}^2 + \frac{I_3(V_{out_{n-1}})}{\kappa} \right\}} = \frac{-\kappa}{C_L} \Delta t \quad (35)$$

$$\left[ -2 \frac{\tan^{-1} \left\{ \frac{-V_{out} + b}{\sqrt{2a + b^2}} \right\}}{\sqrt{2a + b^2}} \right]_{V_{out_{n-1}}}^{V_{out_n}} = \frac{-\kappa}{C_L} \Delta t \quad (36)$$

where  $a = I_3(V_{out_{n-1}})/\kappa$ , and  $b = V_{GS_n} - V_{T_n}$ . The above expression gives an analytical equation for  $V_{out_n}$ .

Next, consider the saturated region of operation.  $V_{DSAT_n}$  is a function of  $V_{GS_n}$ , and is a known quantity. Denoting the time independent parts in the I-V equation as  $K'$ , and  $K''$ ,

$$I_D = K' - K'' \cdot \exp \left[ -\frac{\beta m}{\eta} (V_{out} - V_{DSAT_n}) \right] \quad (37)$$



**Figure 18:** (a) Various components of  $I_{linear}$ , and (b) components of  $I_{linear}$  shown as a percentage of the total current;  $\left(\frac{W_p}{L}\right) = 2 \left(\frac{W_n}{L}\right) = 40$ ,  $FO = 1$ , and  $V_{dd} = 1.5$  V.

Using (37) in (28) and integrating,

$$\left[ \frac{\ln \left( K' - K'' \cdot \exp \left\{ -\frac{\beta m}{\eta} (V_{out} - V_{DSAT_n}) \right\} \right)}{\frac{\beta m}{\eta} K'} + \frac{(V_{out} - V_{DSAT_n})}{\frac{\beta m}{\eta} K'} \right]_{V_{out_{n-1}}}^{V_{out_n}} = -\frac{\Delta t}{C_L} \quad (38)$$

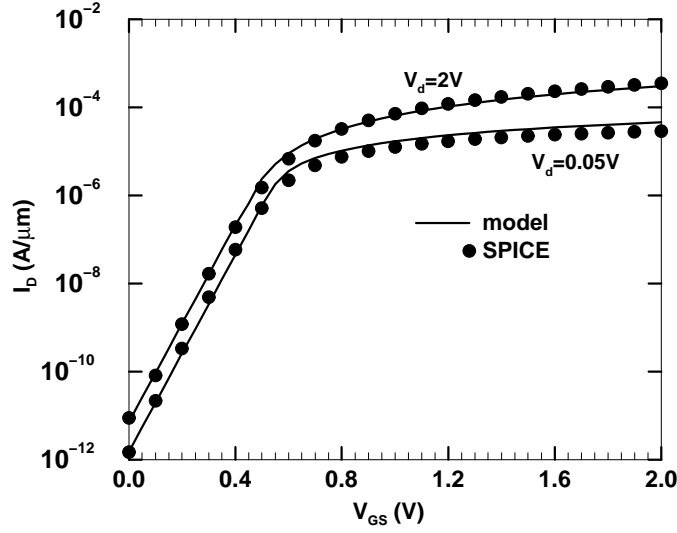
(38) gives an analytical expression for  $V_{out_n}$ .

### 4.3 Tick Method Verification

TSMC 0.25  $\mu m$  process was selected and BISM parameters were obtained from MOSIS [82]. The technology parameters for the TSMC process are shown in Table 9. To account for non-uniform substrate doping, one parameter in the transregional model was adjusted by around 10%; the match between the transregional I-V model and SPICE is shown in Fig. 19.

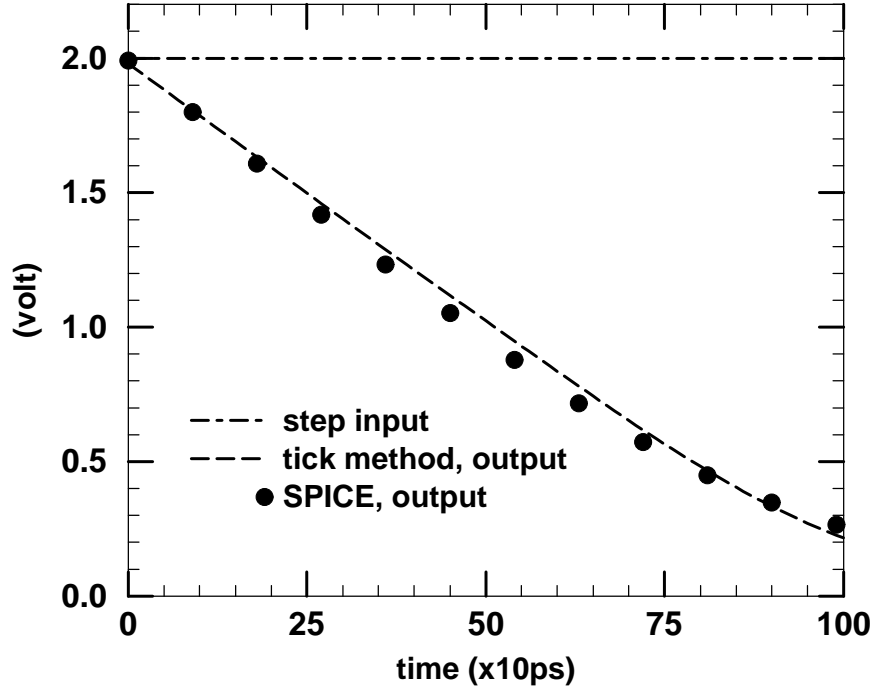
**Table 9:** Technology parameters for TSMC 0.25  $\mu m$  process.

	N-channel	P-channel	units
$V_T$	0.54	-0.50	volt
$t_{ox}$	57	57	Å
$y_j$	100	100	nm
channel doping	$2.35 \times 10^{17}$	$4.16 \times 10^{17}$	$cm^{-3}$



**Figure 19:** I-V curve comparison of transregional MOSFET model and HSPICE for TSMC 0.25  $\mu\text{m}$  n-FETs.

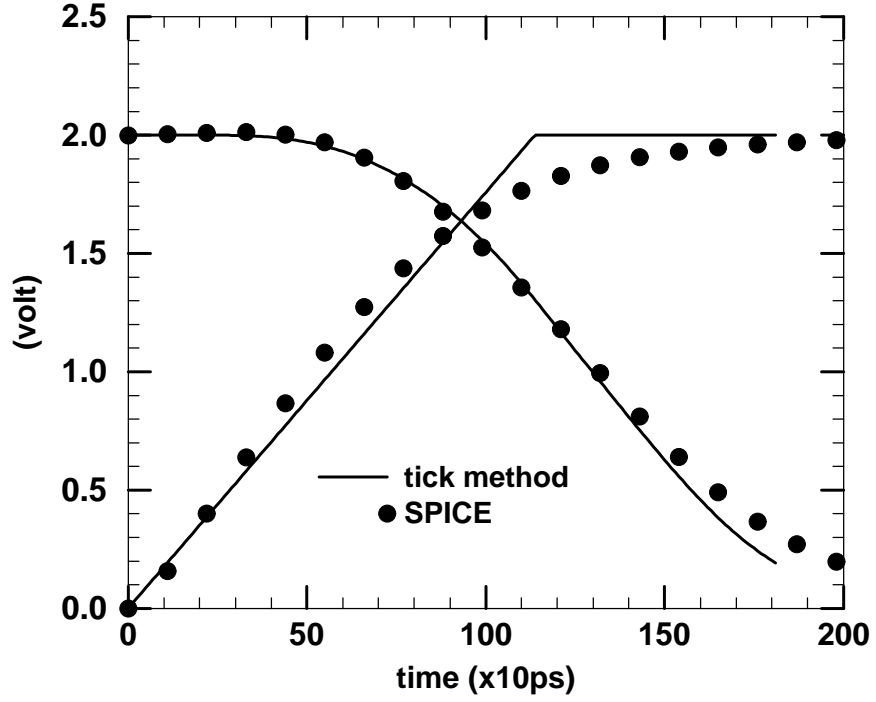
Using the tick method, a chain of inverters is simulated. The input to the first stage is a step waveform. Waveforms at the first stage of the inverter chain are plotted in Fig. 20. A good match is seen between the tick method and HSPICE. From the simulation of the first stage of the inverter chain, delay information is extracted. The input to the second stage of the inverter chain is modeled as a ramp using the delay information from the first stage. Fig. 21 shows waveforms at the input and output of the second stage. Again, a good match is seen between the tick method and SPICE. Next, delay of the second stage of the inverter chain is plotted, for varying  $V_{dd}$ , Fig. 22. This is to confirm that assumptions made in the tick-based method are valid for a wide range of  $V_{dd}$ . A good match is seen between the tick methodology and SPICE, with the maximum error being less than 10% of the actual delay. The tick-based method runs more than 10X faster than a comparable HSPICE simulation. The speed-up is because of the fact that numerical integration is avoided and most calculations are kept analytical.



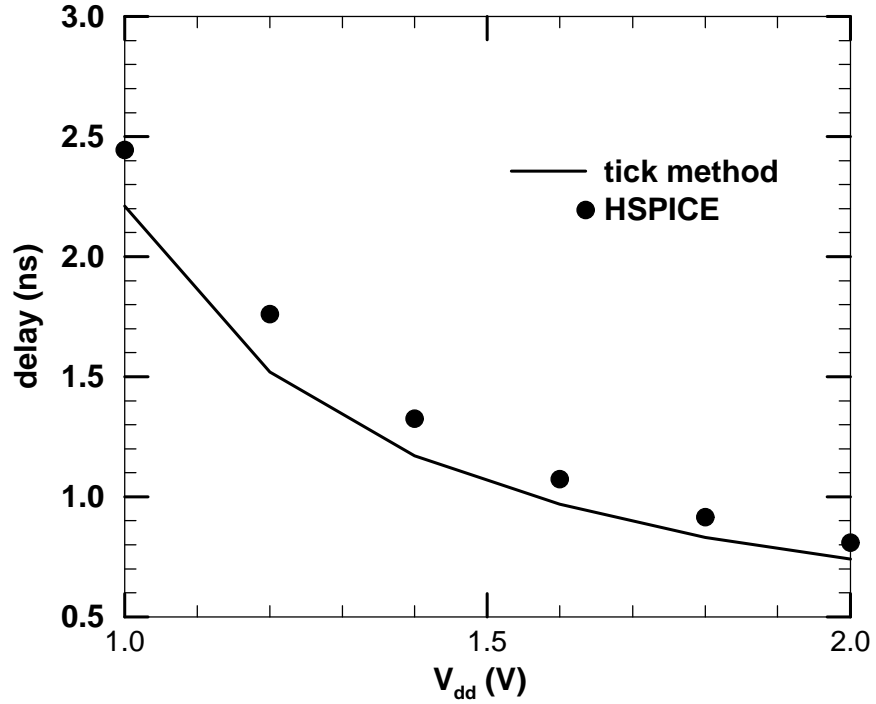
**Figure 20:** Transient waveforms at the first stage of inverter chain;  $\left(\frac{W_p}{L}\right) = 2.5 \left(\frac{W_n}{L}\right) = 50$ ,  $FO = 1$ ,  $C_L = 1 \text{ pF}$ , and  $V_{dd} = 2.0 \text{ V}$ .

#### 4.4 Summary

The tick-based methodology is an extremely useful method to easily use physically based, transregional I-V models to *predict* delay and power-frequency performance of future technology. The method is valid over a wide range of supply voltages, and for a variety of FETs. Numerical integration is avoided, and thus, more than 10X speed improvement over HSPICE is obtained.



**Figure 21:** Input and output waveforms at the second stage of inverter chain;  $\left(\frac{W_p}{L}\right) = 2.5$ ,  $\left(\frac{W_n}{L}\right) = 50$ ,  $FO = 1$ ,  $C_L = 1$  pF, and  $V_{dd} = 2.0$  V.



**Figure 22:** Delay of second stage of inverter chain: comparison between model and HSPICE;  $\left(\frac{W_p}{L}\right) = 2.5$ ,  $\left(\frac{W_n}{L}\right) = 50$ ,  $FO = 1$ , and  $C_L = 1$  pF.

## CHAPTER V

### ACCUMULATION FET DESIGN

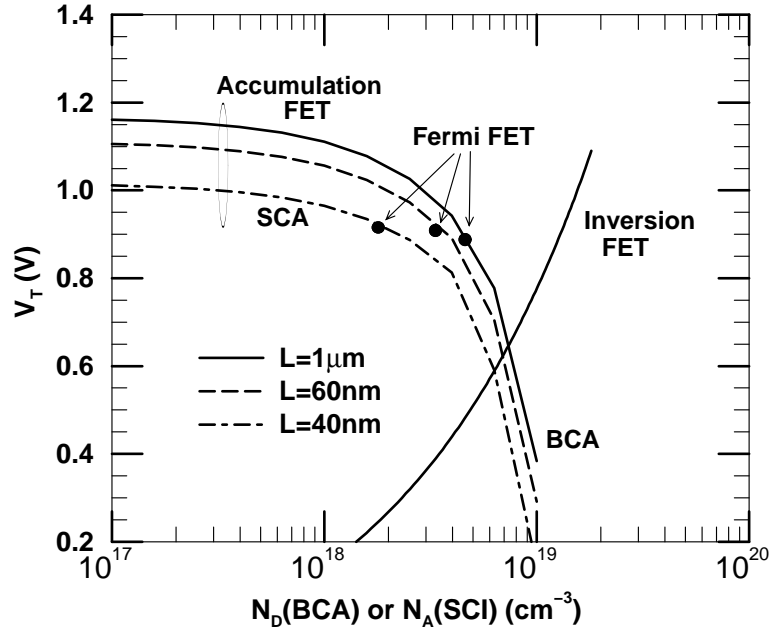
#### **5.1 *Introduction***

The accumulation MOSFET may either operate as an SCA MOSFET or a BCA MOSFET. The main difference between BCA and SCA devices is the location where the channel first opens. BCA MOSFET conduction starts in a neutral buried channel, and with increasing applied gate bias, subsequently extends to an accumulated surface layer [47]. On the other hand, SCA MOSFET conduction is limited to a surface accumulation layer. Because of the steep subthreshold swing rollup and threshold voltage rolloff of BCA MOSFETs, it has been recognized previously that it is better to design accumulation MOSFETs such that they operate as SCA MOSFETs [38],[39]. Guidelines have been provided in [37]-[38], [39], on how to design an accumulation device such that it operates as an SCA MOSFET with minimum long channel subthreshold swing. These guidelines are based on a 1-D solution to the Poisson equation, and do not hold good for short channel devices. New guidelines are given based on a 2-D Poisson equation solution.

#### **5.2 *BCA vs. SCA FETs***

Threshold voltage control of accumulation and inversion MOSFETs is shown in Fig. 23. For low channel doping, the accumulation MOSFET is an SCA MOSFET, whereas for high channel doping, it is a BCA MOSFET. The BCA/SCA MOSFET boundary is the Fermi MOSFET, the device with the minimum long-channel subthreshold slope, and zero oxide field at  $V_G = V_T$  [37]. High channel doping that causes the accumulation MOSFET to be in the BCA regime also results in high process sensitivity ( $dV_T/dy_i$ ), Fig. 24, and high dopant fluctuation effects [44]. Because of high SCE, high process sensitivity, and high dopant fluctuation effects of BCA MOSFETs, it is best to operate the accumulation MOSFET either as an SCA MOSFET or as a BCA MOSFET close to the BCA/SCA MOSFET





**Figure 23:** Threshold voltage (from model) vs. channel doping of poly-gate accumulation and inversion MOSFETs;  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ ,  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ .

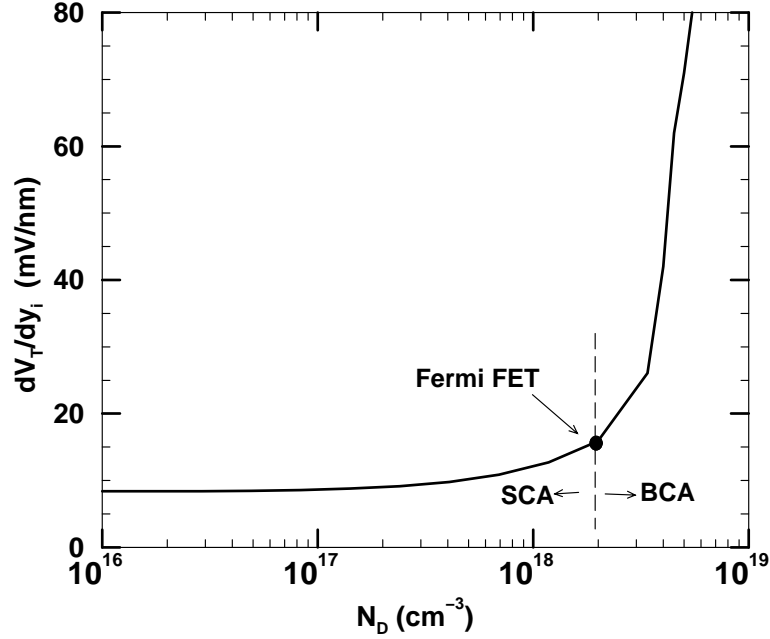
boundary.

### 5.3 Accumulation FET design

Once the 2-D potential in the channel region of the accumulation MOSFET has been solved, the boundary between BCA and SCA MOSFETs can be identified by finding the channel doping that gives a zero vertical field at the Si – SiO<sub>2</sub> interface. Let  $N_{dbound}$  be the channel doping beyond which the SCA MOSFET becomes a BCA MOSFET. The channel doping that gives

$$\left. \frac{\partial \psi}{\partial y}(x_m, 0) \right|_{V_G=V_T} = 0 \quad (39)$$

is  $N_{dbound}$ . For  $N_D > N_{dbound}$ , the location where  $\left. \frac{\partial \psi}{\partial y}(x_m, y) \right|_{V_G=V_T}$  is zero occurs for  $y > 0$ , resulting in buried channel operation. Since the LHS of (39) is a function of  $y_i$ ,  $N_A$ ,  $y_j$ ,  $V_{DS}$ ,  $L$ ,  $t_{ox}$  and  $N_{D_{S/D}}$  (the source/drain doping),  $N_{dbound}$  too is a function of all these parameters. In a manner similar to finding  $N_{dbound}$ , it is possible to find a  $y_{ibound}$  (the boundary channel depth) from (39).  $y_{ibound}$  is a function of  $N_D$ ,  $N_A$ ,  $y_j$ ,  $V_{DS}$ ,  $L$ ,  $t_{ox}$  and  $N_{D_{S/D}}$ . This is as opposed to the long channel boundary depth found in [37]-[38], [39],



**Figure 24:** Effect of a  $1\text{nm}$  tub-depth ( $y_i$ ) variation on threshold voltage for BCA/SCA MOSFETs (from model);  $L = 45\text{ nm}$ ,  $t_{ox} = 15\text{ \AA}$ ,  $y_j = 12\text{ nm}$ ,  $V_{DS} = 1.0\text{ V}$ ,  $N_A = 2.5 \times 10^{18}\text{ cm}^{-3}$ , and  $y_i = 10\text{ nm}$ .

which is only a function of  $N_D$  and  $N_A$ . Table 10 shows  $N_{dbound}$  as a function of channel length, for two different channel depths. The  $N_{dbound}$  derived from long-channel theory (for  $L = 1\text{ }\mu\text{m}$ ) is seen to be different from that derived from 2-D theory. It can be seen from Fig. 23 and Table 10 that an SCA MOSFET at long channel length becomes a BCA MOSFET at shorter channel lengths. Thus, an accumulation MOSFET would have to be designed such that the minimum channel length device (say,  $3\sigma$  less than the nominal channel length) operates as an SCA FET.

Fig. 25 shows the design space for accumulation MOSFETs with a channel length of  $30\text{ nm}$ , generated from 2-D simulations. Also shown are constant  $V_T$  contours. It can be seen that good SCE control makes necessary extremely shallow channel implants. The minimum channel/tub-depth is taken to be  $5\text{ nm}$  due to process limitations. The  $V_T$ <sup>1</sup> range allowable by the design space is  $0.27 < V_T < 0.40\text{ V}$ . Fig. 26 shows the design space generated by the SCE models derived previously in this work. An additional constraint -

<sup>1</sup>ITRS defines  $V_T$  as the gate voltage that gives a drain current of  $1\text{ }\mu\text{A}/\mu\text{m}$ . For  $S = 100\text{ mV/dec}$ , and a channel length of  $30\text{ nm}$ ,  $V_{T|simulation} - V_{T|ITRS} \approx 50\text{ mV}$ .

**Table 10:**  $N_{dbound}$  for various  $L$ ;  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ , and  $V_{DS} = 1.0 \text{ V}$ .

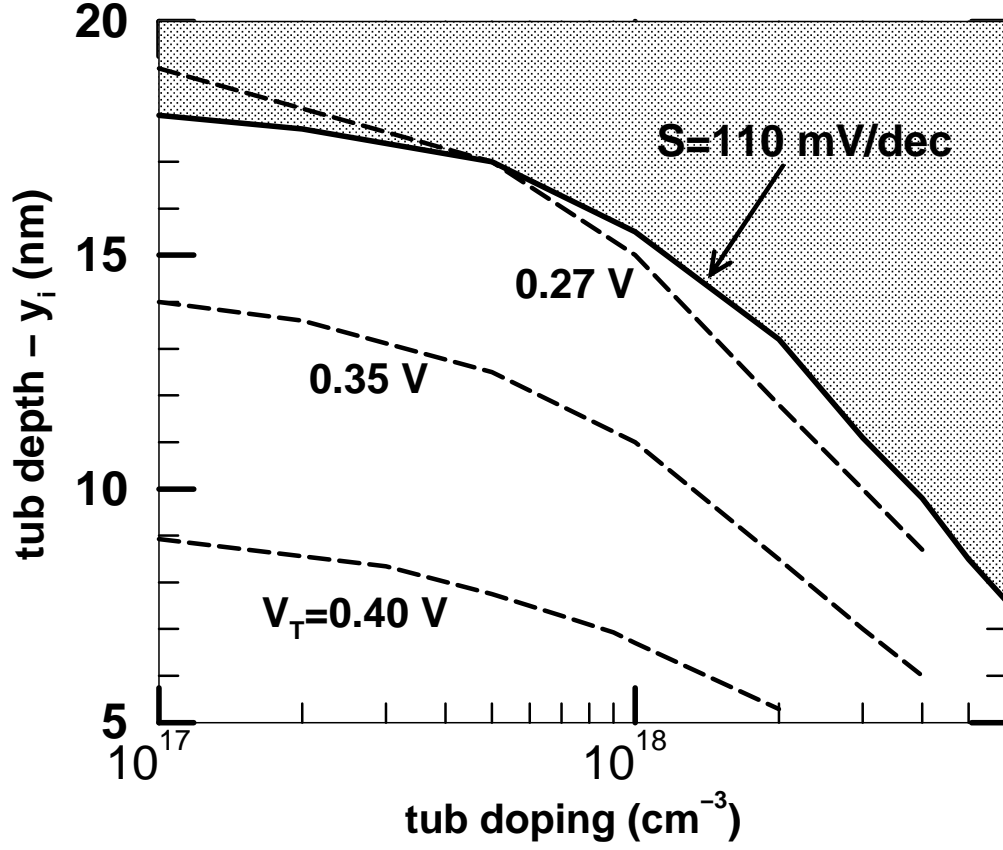
$L$	$y_i = 10 \text{ nm}$	$y_i = 20 \text{ nm}$
$1 \text{ } \mu\text{m}$	$5 \times 10^{18} \text{ cm}^{-3}$	$2 \times 10^{18} \text{ cm}^{-3}$
$60 \text{ nm}$	$3.4 \times 10^{18} \text{ cm}^{-3}$	$1.07 \times 10^{18} \text{ cm}^{-3}$
$40 \text{ nm}$	$1.5 \times 10^{18} \text{ cm}^{-3}$	$6 \times 10^{17} \text{ cm}^{-3}$

that of  $V_T$  sensitivity to tub-depth variation - is included in the design space. It can be seen that at low tub-doping, the design space is bounded by the SCE limit, whereas at high tub-doping, it is bounded by the  $dV_T/dy_i$  limit.

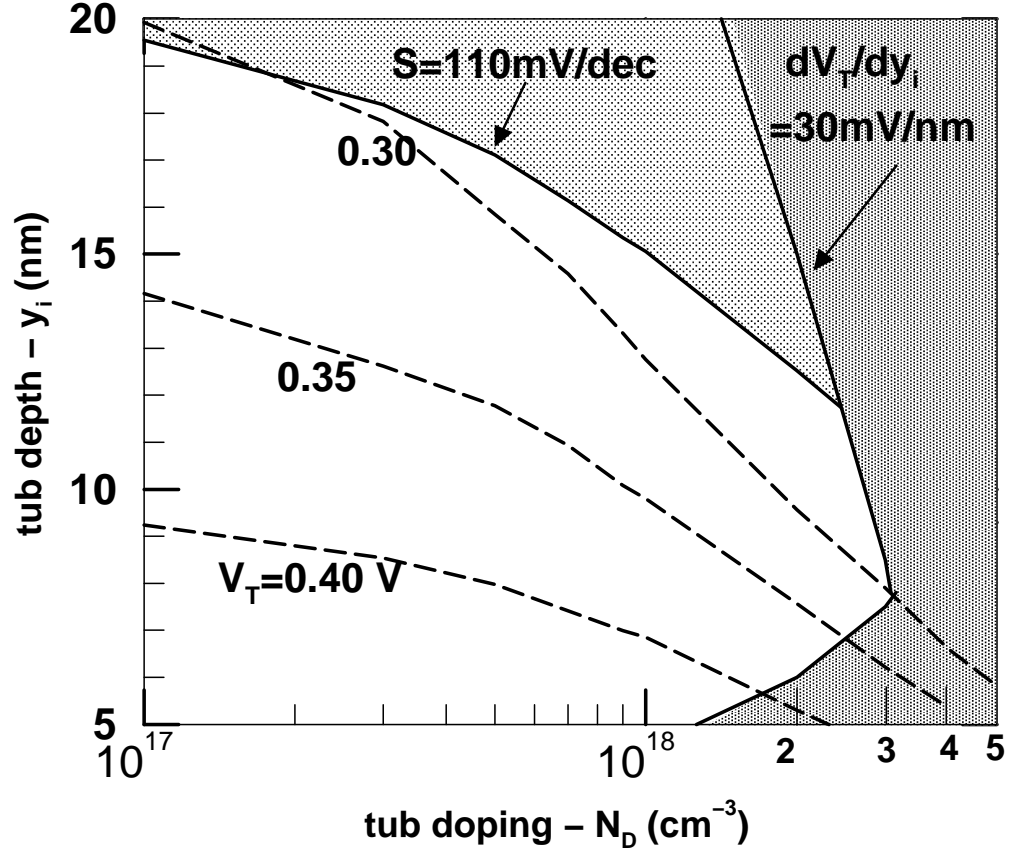
The model-generated design space helps to greatly reduce the multi-dimensional search space for a given application. In the final optimization step, a 2-D simulator can be used to search the reduced design space. As an example, consider the design space shown in Fig. 26. To achieve an  $I_{OFF}$  of  $0.1 \text{ } \mu\text{A}/\mu\text{m}$ , a  $V_T$  of about  $0.36 \text{ V}$  is needed (assuming  $S = 90 \text{ mV/dec}$ ). Reading off the tub-doping and tub-depth values from the  $V_T = 0.35 \text{ V}$  contour in Fig. 26, a 2-D simulator (classical simulations with drift-diffusion transport) is used to scan this set of devices. The optimal device is found to be one with a tub-doping of  $1 \times 10^{18} \text{ cm}^{-3}$  and a tub-depth of  $10 \text{ nm}$ , Fig. 27. Inclusion of velocity-overshoot in the simulations shown in Fig. 27 would shift the optimal device design point since a lower channel doping results in a higher velocity overshoot.

## 5.4 Summary

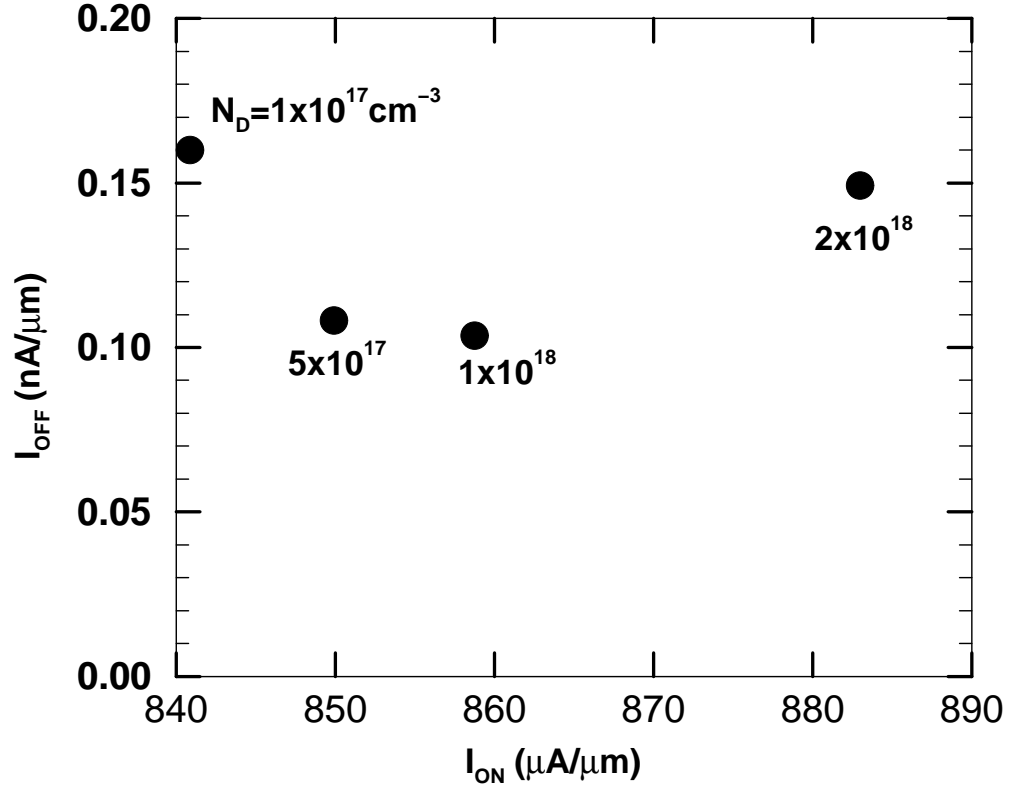
BCA FETs not only have a high subthreshold swing, but also a high process sensitivity, and high dopant fluctuation effects. So, it is best to design an accumulation FET such that it either operates as an SCA FET, or close to the BCA/SCA FET boundary. Based on 2-D theory, the BCA/SCA FET boundary has been derived, and is shown to be different from that derived using 1-D theory. Using the SCE models derived in this work, accumulation FETs can be designed to meet  $V_T$  rolloff, process sensitivity, and off-current requirements. An example design window is shown for  $S < 110 \text{ mV/dec}$ , and  $dV_T/dy_i < 30 \text{ mV/nm}$ .



**Figure 25:** Design space for mid-bandgap metal gate, accumulation n-MOSFETs (from 2-D simulations). Substrate doping,  $N_A = 4 \times 10^{18} \text{ cm}^{-3}$ , and the maximum subthreshold swing is taken to be  $110 \text{ mV/dec}$ . Also shown are constant  $V_T$  contours (dashed lines).  $L = 30 \text{ nm}$ ,  $t_{ox} = 10 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ , and  $V_{dd} = 1.0 \text{ V}$ .



**Figure 26:** Design space for mid-bandgap metal gate, accumulation n-MOSFETs (from models). Substrate doping,  $N_A = 4 \times 10^{18} \text{ cm}^{-3}$ ; the maximum subthreshold swing is taken to be  $110 \text{ mV/dec}$ , and the maximum  $dV_T/dy_i$  is taken to be  $30 \text{ mV/nm}$ . Also shown are constant  $V_T$  contours (dashed lines).  $L = 30 \text{ nm}$ ,  $t_{ox} = 10 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ , and  $V_{dd} = 1.0 \text{ V}$ .



**Figure 27:**  $I_{OFF} - I_{ON}$  from 2-D simulations (drift-diffusion transport);  $N_D$  and  $y_i$  are chosen so as to give a  $V_T$  of 0.35 V.  $L = 30$  nm,  $t_{ox} = 10$  Å,  $y_j = 12$  nm,  $V_{dd} = 1.0$  V,  $N_A = 4 \times 10^{18}$   $cm^{-3}$ , and gate workfunction is 4.63 eV.

## CHAPTER VI

### METAL GATE MOSFETS

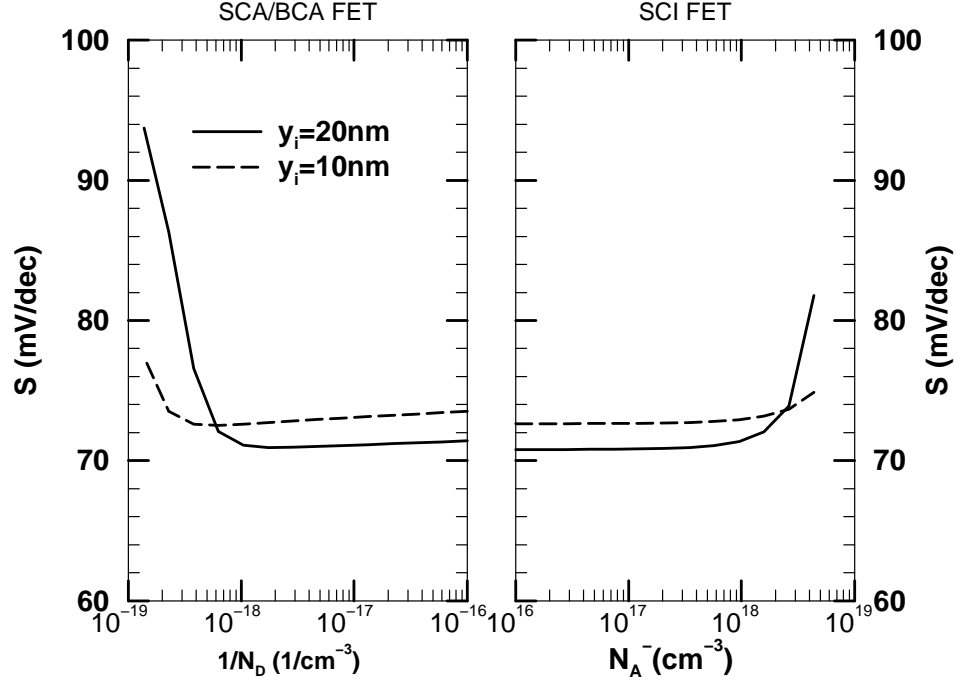
Polysilicon gates have the disadvantage of gate depletion since it increases the effective oxide thickness [83]. Metal gate technology overcomes the gate-depletion problem of poly-gates, and so is being widely pursued as the next promising gate material. With the recent advent of tunable workfunction (WF) metal gates, it has become possible to fabricate metal gates with workfunctions from 4.2 eV to 5.2 eV [40]. CMOS technology can either use a single gate for both n-MOS and p-MOS; or it can use dual metal gate technology. When single metal gate technology is used, the workfunction of the metal is usually at the Si mid-bandgap. When dual metal gate technology is used, the workfunctions of the gates are optimized for the given application [84].

Short channel effect in accumulation MOSFETs is poorly understood in existing literature. Using the physical SCE models derived in previous chapters, accumulation and inversion MOSFET SCE are compared. This is followed by a comparison of accumulation and inversion MOSFETs for tunable metal gate CMOS technology. Then, mid-bandgap metal gate technology is considered.

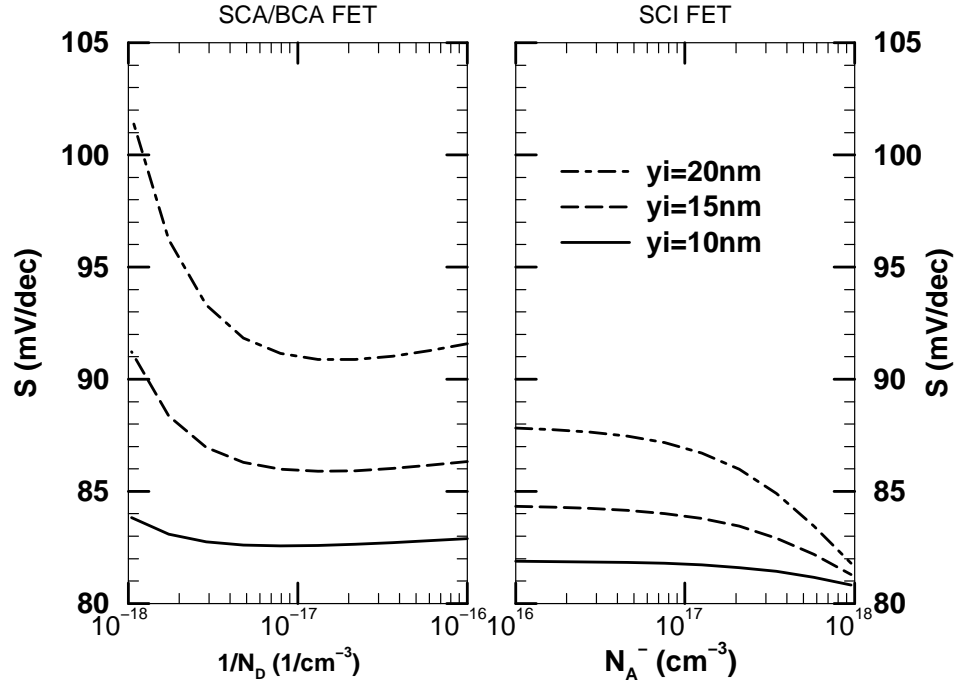
#### ***6.1 SCE comparison of accumulation and inversion MOSFETs***

Long-channel subthreshold swing of accumulation and inversion devices is plotted in Fig. 28. The left hand side of the figure shows accumulation FETs and the right side shows inversion FETs. The x-axis is the tub-doping (inverse of the tub-doping) of the inversion (accumulation) MOSFET. The minimum subthreshold swing occurs for an accumulation FET with a tub-doping around  $1 \times 10^{18} \text{ cm}^{-3}$ , the device being a Fermi FET.

Short channel subthreshold swing is plotted in Fig. 29. For the accumulation FET, S increases rapidly beyond a certain tub-doping (this is the BCA/SCA FET boundary).



**Figure 28:** Long-channel subthreshold swing vs. tub-doping (from models);  $t_{ox} = 15 \text{ \AA}$ , and  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ .



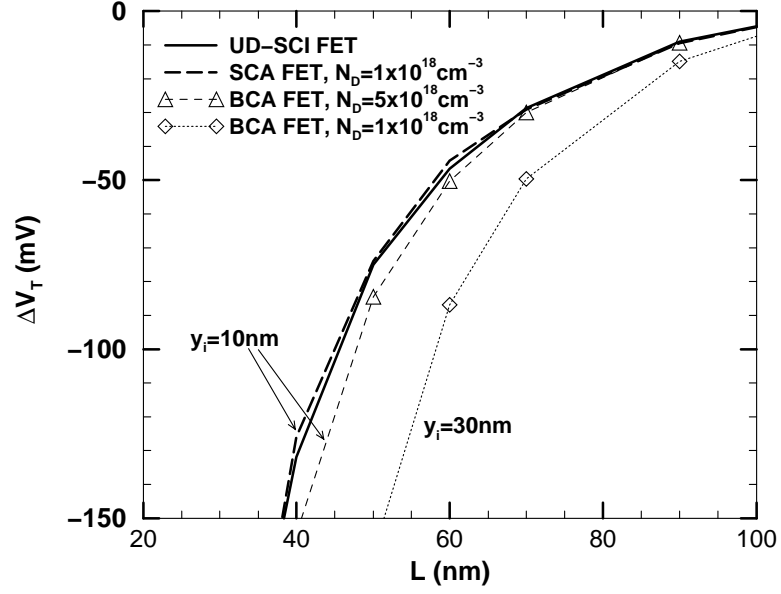
**Figure 29:** Short-channel subthreshold swing vs. tub-doping (from models);  $L = 40 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 20 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ , and  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ .



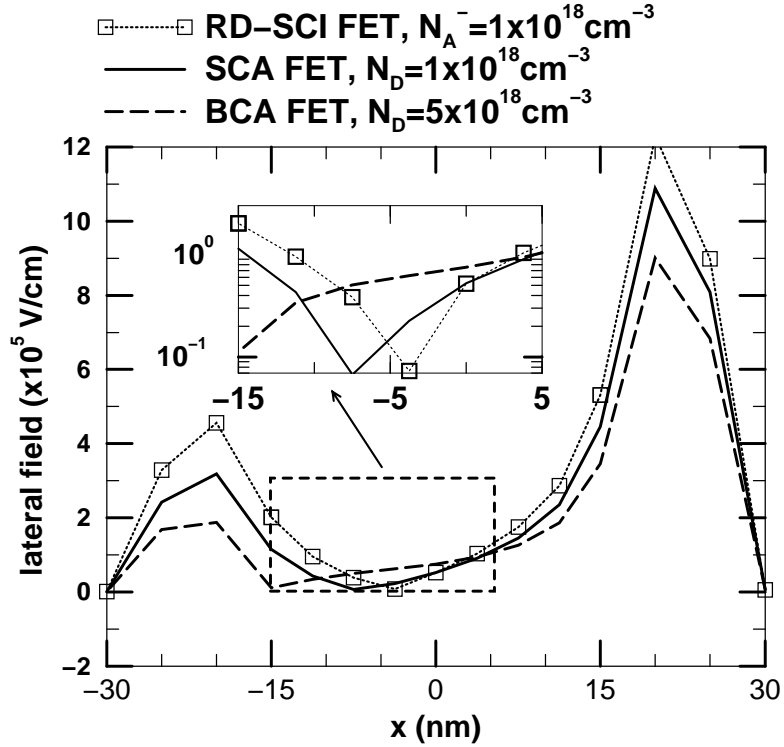
This is because the accumulation FET goes into the buried channel mode of operation when  $N_D > N_{dbound}$ . A different behavior can be seen in the case of inversion FETs - as tub-doping increases,  $S$  decreases; this is because SCE decreases with increasing tub-doping resulting in a decreased  $S$  rollup, and hence an overall decrease in  $S$ . Because of increased SCE, the Fermi-FET is no longer the device with the minimum subthreshold swing in the short-channel regime.

Fig. 30 shows  $V_T$  rolloff for various accumulation and inversion FETs. Because of the counter-doped region in the accumulation FET, the lateral electric field at the source/drain junction is expected to be lower in the accumulation FET than in the inversion FET, resulting in reduced SCE. Fig. 31 plots the lateral field at the surface of three example n-FETs. The RD-SCI device has a peak lateral field at the source that is 60% greater than that of the SCA FET. But accumulation FETs are seen to have a similar or worse  $V_T$  rolloff compared to inversion FETs. Fig. 30 shows that an SCA FET and a UD-SCI FET with the same channel doping are seen to have similar  $V_T$  rolloff curves; an increase in either the tub-doping or tub-depth of the SCA FET results in an increase in  $V_T$  rolloff.

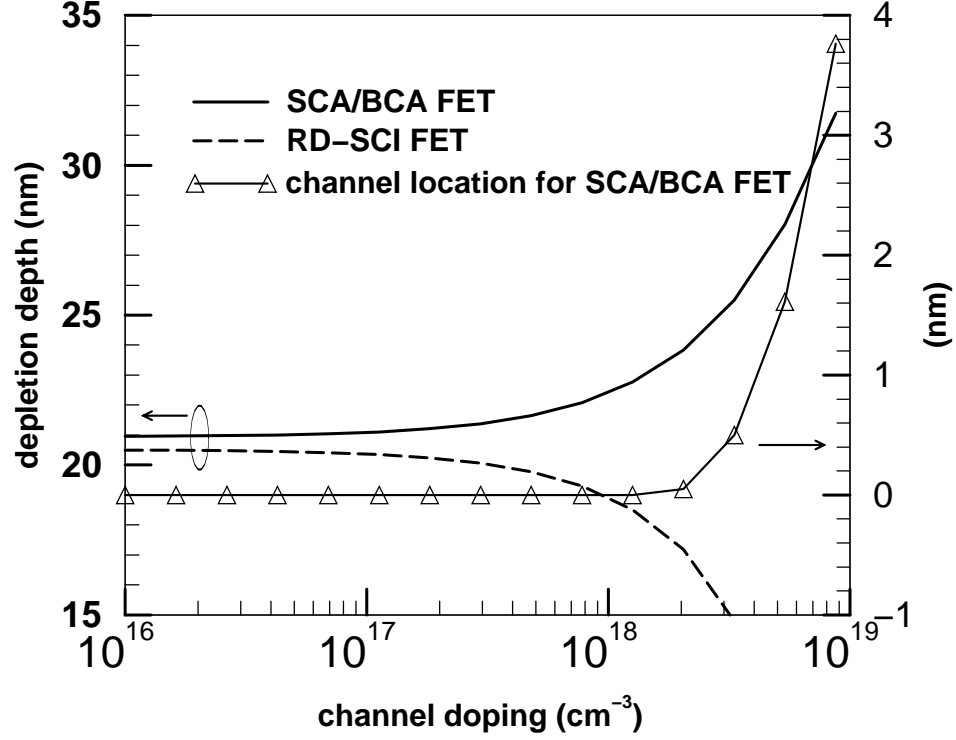
The anomaly of reduced lateral field not leading to reduced SCE can be explained using Fig. 32, where depletion depth and channel location are plotted vs. channel doping. The accumulation FET is seen to have a greater depletion depth compared to the inversion FET. Any reduction in SCE caused by the lowered lateral field in the accumulation FET is offset by this increase in depletion depth. In the long channel regime, the increased depletion depth in the SCA FET compared to the SCI FET results in a reduced subthreshold swing. As the SCA FET channel doping is increased,  $d$  increases, resulting in decreased subthreshold swing. When  $N_D > N_{dbound}$ , the channel location becomes buried (Fig. 32) resulting in a steep subthreshold swing rollup. This is the reason why the device operating at the BCA/SCA FET boundary (i.e. the Fermi FET) has the minimum long-channel subthreshold swing. In the short channel regime, the increased depletion depth in the accumulation FET offsets any reduction in SCE resulting from the reduced lateral field, and results in increased SCE compared to the inversion FET.



**Figure 30:** Threshold voltage rolloff comparison of accumulation and inversion MOSFETs (from 2-D simulations);  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 10 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ , and  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ .



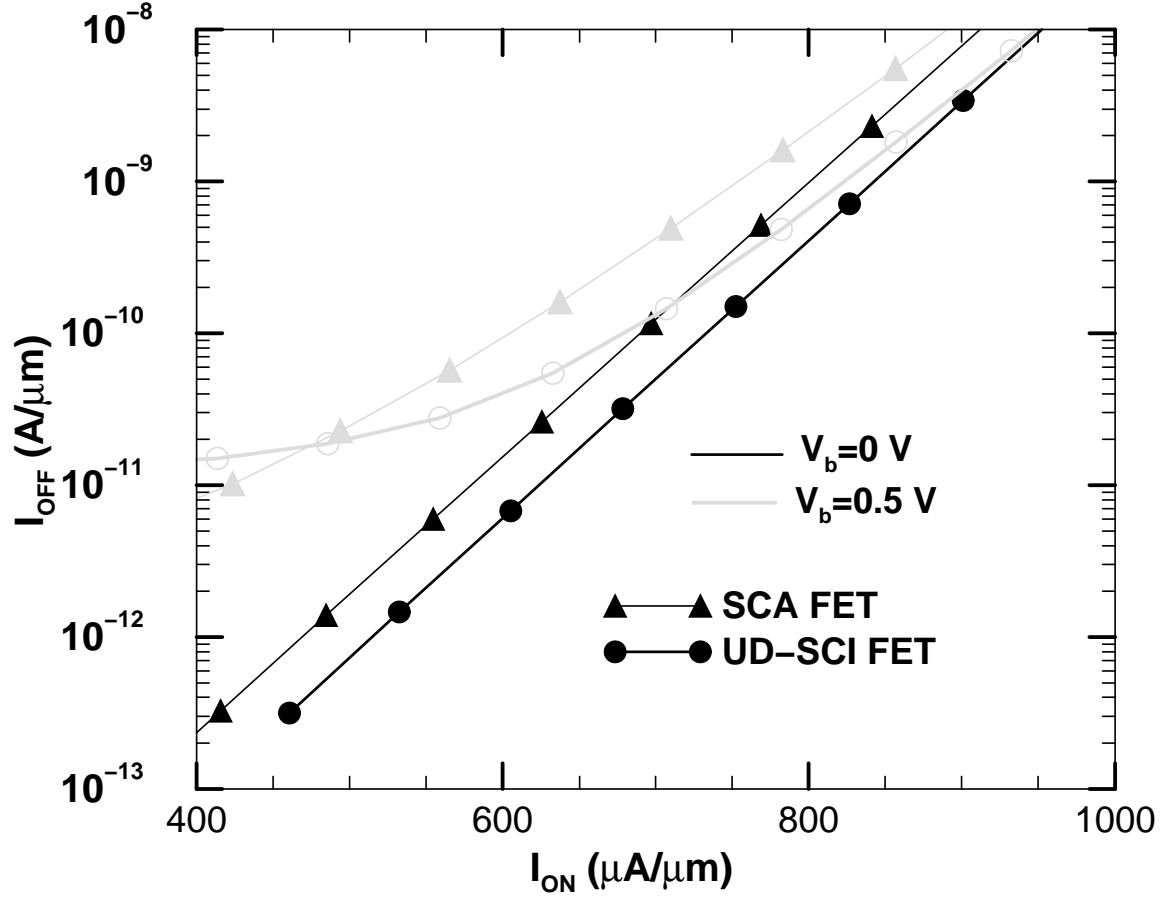
**Figure 31:** Lateral field (from 2-D simulations) at the Si-SiO<sub>2</sub> interface for accumulation and inversion FETs;  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 10 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ ,  $V_{GS} = 0 \text{ V}$ ,  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ .



**Figure 32:** Long-channel depletion depth for accumulation and inversion MOSFETs (from models);  $t_{ox} = 15 \text{ \AA}$ ,  $V_{GS} = 0.2 \text{ V}$ ,  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ .

## 6.2 Tunable Workfunction, Metal Gate CMOS Technology

From the arguments in the previous section, it can be concluded that short-channel accumulation FETs offer no significant performance advantage over inversion FETs either in terms of subthreshold swing, or  $V_T$  rolloff, when the gate WF is tunable. Thus, for good SCE control, it is best to use an inversion device. The optimal inversion and accumulation FET are identified for a given  $I_{ON}$ , and  $I_{OFF}$ - $I_{ON}$  from 2-D simulations using MEDICI [63] are plotted for these optimized structures, Fig. 33. The simulations are classical in nature, with drift-diffusion transport. It can be seen that over a wide range of  $I_{ON}$ , the SCA FET performs worse than the SCI FET. When body-bias is used (e.g. to control die-to-die parameter variations [85]), the situation remains the same. Thus, in the scenario where the gate workfunction is tunable, the inversion MOSFET is better than the accumulation MOSFET.



**Figure 33:**  $I_{OFF}$  -  $I_{ON}$  for tunable WF metal gate CMOS technology (from 2-D simulations);  $L = 55 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 10 \text{ nm}$ , and  $V_{dd} = 1.0 \text{ V}$ . For the SCA FET,  $N_D = 1 \times 10^{18} \text{ cm}^{-3}$ ,  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ . For the UD-SCI FET,  $N_A = 1 \times 10^{18} \text{ cm}^{-3}$ .

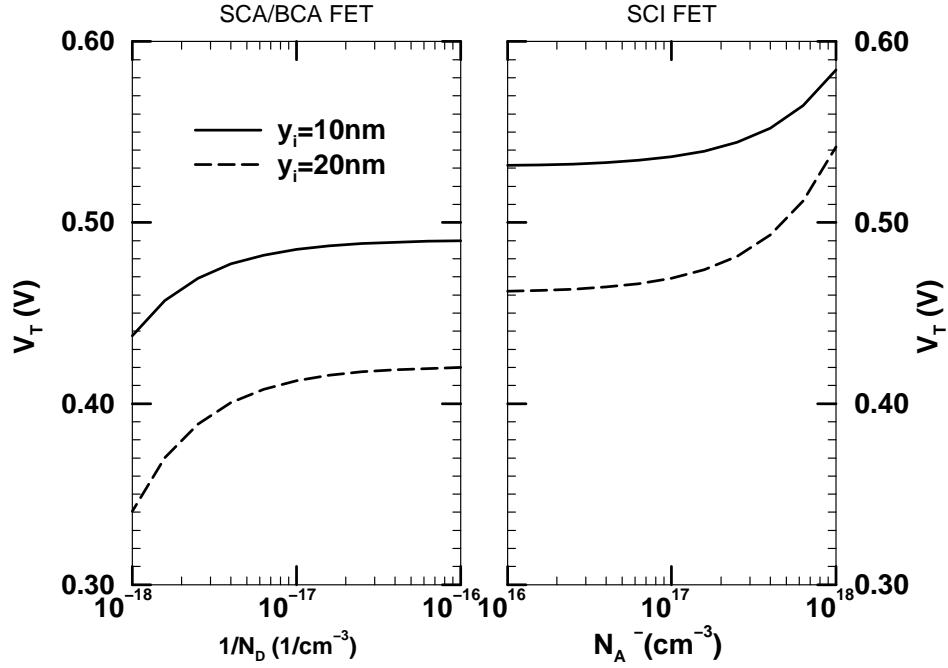
### 6.3 *Single metal gate CMOS*

Many applications limit the gate material to a single metal for both the n-FET and the p-FET. This greatly reduces process complexity and increases circuit density [17]. In single metal gate technology, the gate workfunction will most likely be the Si mid-bandgap value so that equivalent drive currents are obtained from n-MOS and p-MOSFETs [86]. The best metal suitable for such applications is Tungsten (W), which has a workfunction of 4.63 eV. For such applications, the necessary  $V_T$  is obtained by adjusting the channel/substrate doping of the MOSFET.

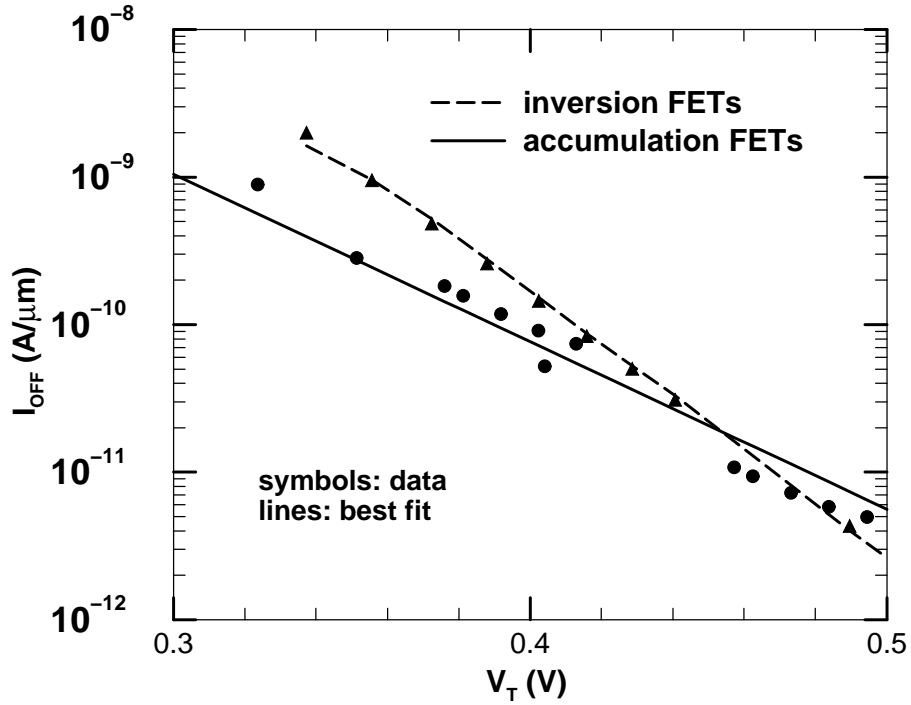
When  $V_T$  of SCA and SCI FETs using a tungsten gate is plotted vs. channel doping, Fig. 34, it can be seen that SCA FETs achieve a  $V_T$  between 0.35 V and 0.5 V, whereas SCI FETs have a  $V_T$  greater than 0.45V. A lower value of  $V_T$  can be obtained with the SCI FET if a higher  $y_i$  and/or lower channel/substrate is used. But, this would result in increased SCE. Fig. 35 shows  $I_{OFF}$  vs.  $V_T$  from 2-D models derived in previous chapters. Accumulation and inversion devices are designed such that the minimum  $I_{OFF}$  is obtained for a given  $V_T$ . A cross-over is seen at  $V_T = 0.46$  V, where the off-current is about  $20$  pA/ $\mu$ m. At low  $V_T$ , the SCI FET has a lower channel/substrate doping compared to the accumulation FET, resulting in higher SCE, and hence a higher  $I_{OFF}$ .

The total channel doping in an accumulation FET is process dependent. If the process is able to achieve super steep Boron doping (for an n-FET), then the total doping in the channel is almost the same as the effective doping ( $N_T = N_D$ ), Fig. 36. On the other hand, if the Boron doping in the n-FET is almost uniform, the total channel doping is the sum of the acceptor and donor impurity concentrations ( $N_T = N_D + N_A$ ). The latter case results in lower channel mobility, and thus lower drive current, compared to the former case. In order to assess processing conditions on device performance, both cases of the accumulation FET will be considered while comparing it to the inversion FET.

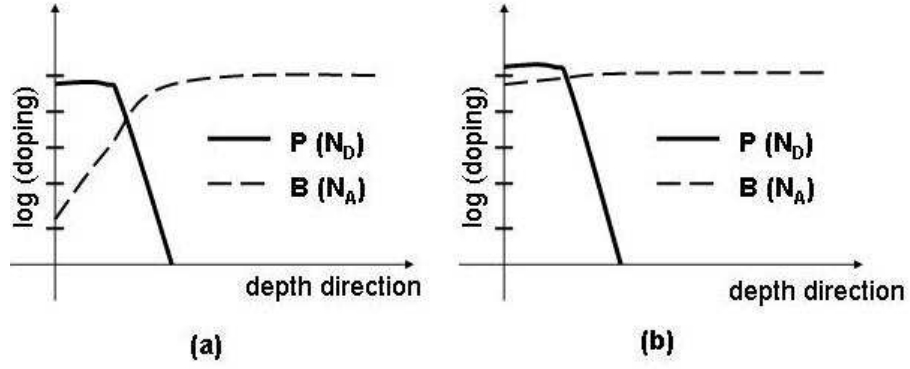
Fig. 37 shows  $I_{OFF}$  vs.  $V_T$  for accumulation and inversion FETs, this time from 2-D simulations. Simulations are done using drift-diffusion transport. The  $I_{OFF}$  vs.  $V_T$  plane has a weak dependence on the mobility models used. Both cases of the accumulation FET ( $N_T = N_D$ , and  $N_T = N_D + N_A$ ) result in the same curve since  $V_T$  is independent of



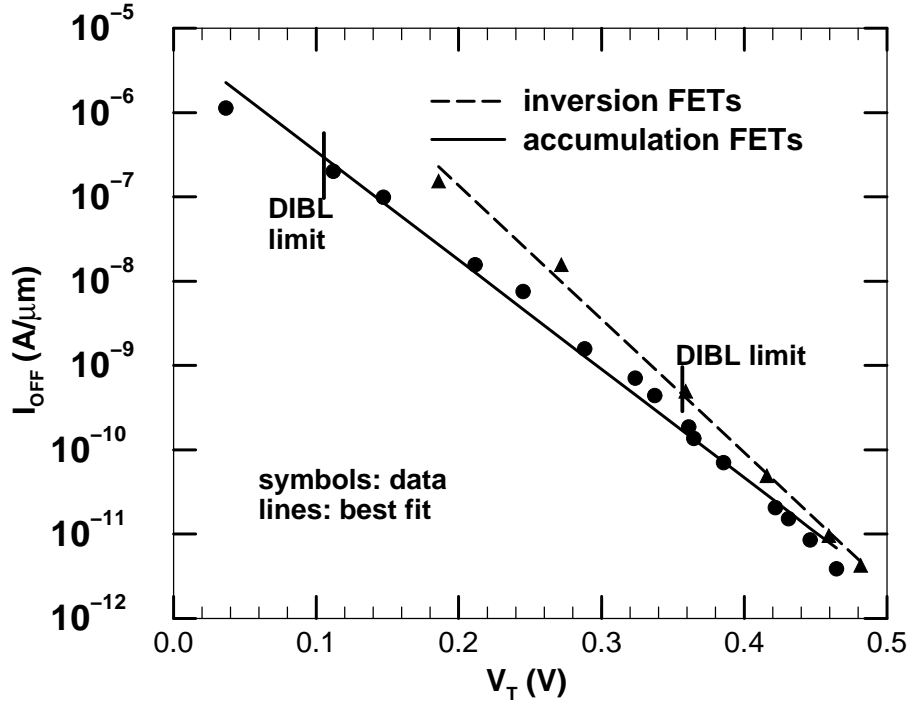
**Figure 34:** Threshold voltage (from models) vs. tub-doping for accumulation and inversion MOSFETs;  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ ,  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ , and gate workfunction is 4.63 eV.



**Figure 35:** Off-current vs. threshold voltage for accumulation and inversion MOSFETs (from models);  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ , and gate workfunction is 4.63 eV.



**Figure 36:** Effect of processing conditions on tub-doping; Phosphorus and Boron profiles are shown for two example n-FETs: (a)  $N_T \approx N_D$ , and (b)  $N_T \approx N_D + N_A$ .



**Figure 37:** Off-current vs. threshold voltage for single metal gate CMOS technology (from 2-D simulations); symbols indicate data points, and lines indicate best fit.  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ , and gate workfunction is  $4.63 \text{ eV}$ . The DIBL limit is taken to be  $100 \text{ mV/V}$ .

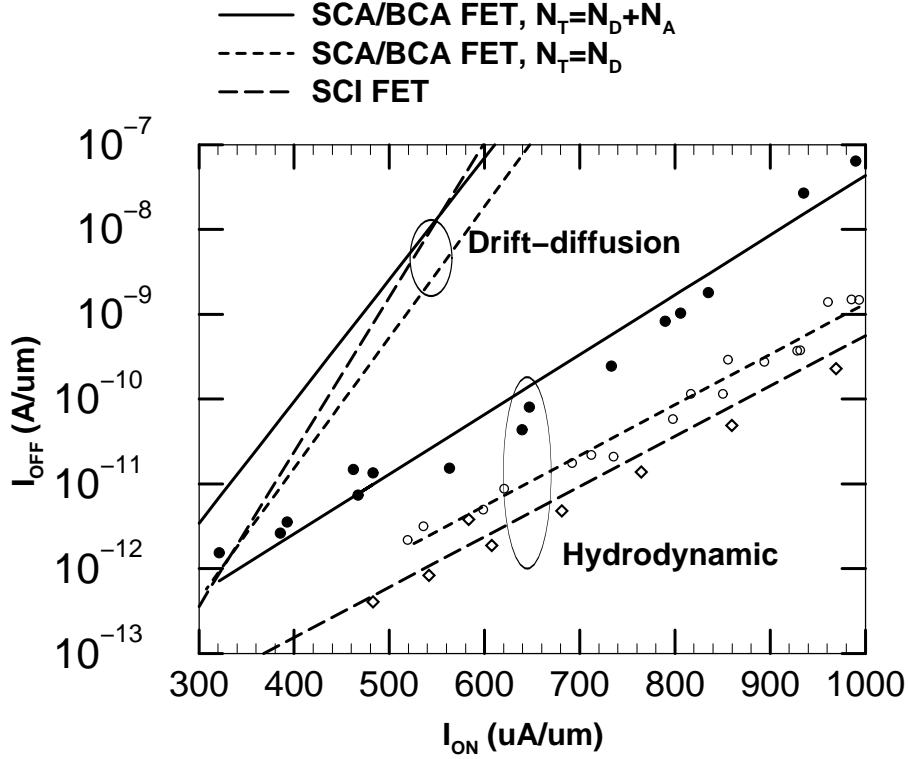
the channel mobility ( $\mu$ ). It can be seen that for  $V_T < 0.4V$ , the accumulation FET has a significantly lower  $I_{OFF}$  than the inversion FET. At lower  $V_T$ , the inversion FET has a significantly higher SCE compared to the accumulation FET. Fig. 37 shows the point where DIBL exceeds 100 mV/V for inversion and accumulation FETs. The inversion FET  $V_T$  is limited to  $V_T > 0.35 V$  because of DIBL. On the other hand, accumulation FETs can achieve a  $V_T$  as low as 0.1 V before reaching the DIBL limit. Additional comparisons between mid-band metal gate accumulation and inversion MOSFETs are given in Appendix B.

Fig. 38 shows  $I_{OFF} - I_{ON}$  curves, from 2-D simulations using both drift-diffusion (DD) and hydro-dynamic (HD) transport. HD simulations include non-local carrier transport, and thus account for velocity overshoot. Both DD and HD simulations include QM  $V_T$  shift by means of the van Dort model [87]; the accuracy of using van Dort QM correction is discussed in Appendix C. In DD simulations, there is a crossover in inversion and accumulation FET curves. The reason for this is the same as that for the  $I_{OFF} - V_T$  crossover. In HD simulations, there is no such crossover, and the inversion FET is always better than the accumulation FET.

The difference between on-current from DD and HD simulations (for a given off-current) is seen to be 100-150%. Non-local carrier transport causes an increase in on-current because of velocity overshoot. Using HD simulations to account for non-local transport has been known to result in spurious velocity overshoot [88]. Reported values of on-current increase due to velocity overshoot are between 10-15% [89]. The spurious velocity overshoot will be studied in detail and alternate simulation methodologies will be looked at to accurately predict the on-current.

To study the effect of velocity overshoot, an accumulation and an inversion device are selected having almost the same off-current (corresponding to  $I_{OFF} \approx 0.5 \text{ nA}/\mu\text{m}$  from Fig. 38). Both have the same  $V_T$ , Table 11. It can be seen that channel doping of the accumulation FET is greater than that of the inversion FET. Hydro-dynamic simulations result in the inclusion of velocity overshoot (compared to drift-diffusion simulations). To understand the dependence of velocity overshoot on channel mobility, analytical expressions





**Figure 38:** Off-current vs. on-current for single metal gate CMOS technology (from 2-D simulations); symbols indicate data points, and lines indicate best fit.  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ , and gate workfunction is  $4.63 \text{ eV}$ .

from [47] are used. In [47], velocity overshoot is included by modifying the effective mobility as

$$\frac{\mu_{\text{eff}}}{1 + \frac{E(x)}{E_c}} \rightarrow \frac{\mu_{\text{eff}}}{1 + \frac{E(x)}{E_c}} + \frac{\lambda_{VO}}{L} \quad (40)$$

where  $\mu_{\text{eff}}$  is the mobility including vertical high field effect,  $E(x)$  is the lateral field,  $E_c$  is the critical field, and  $\lambda_{VO}$  is the velocity overshoot factor.  $\lambda_{VO}$  is given by

$$\lambda_{VO} = 91 \ln [0.16 \mu_{\text{eff}} - 14] \times 10^{-6} \quad (41)$$

From (40), and (41), it can be seen that the velocity overshoot effect increases with channel mobility. Since the inversion FET channel mobility is higher than that of the accumulation FET (Table 11), a higher velocity overshoot occurs in the inversion FET [90]. The amount of this velocity overshoot is overestimated by the un-calibrated HD simulations, resulting in a huge increase in on-current. Thus, using un-calibrated HD simulations, there

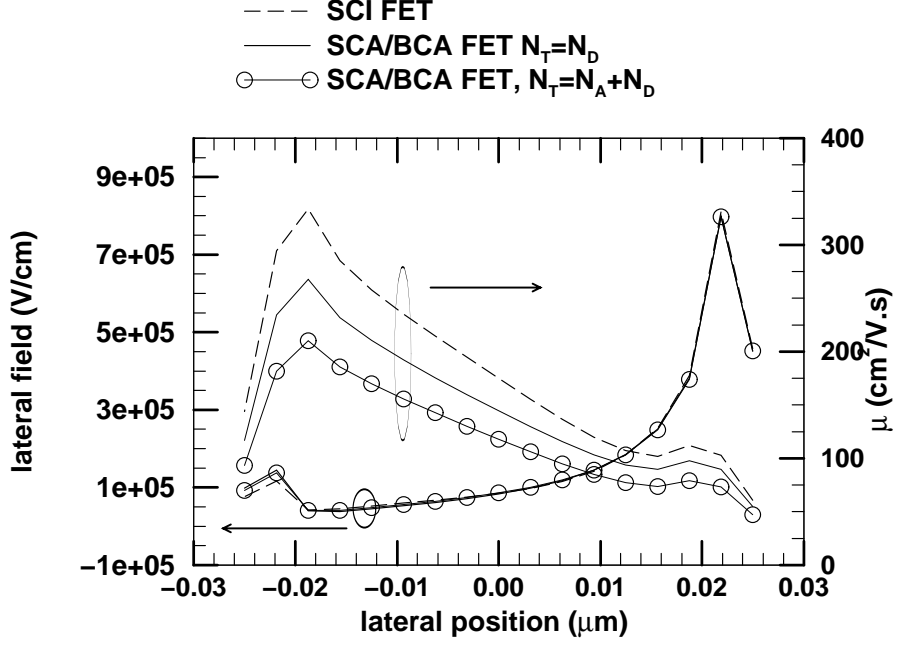
**Table 11:** Velocity Overshoot Effect for non-halo FETs;  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ , and gate workfunction is 4.63 eV.

	SCI FET	BCA/SCA FET $N_T = N_A + N_D$	BCA/SCA FET $N_T = N_D$	units
$N_D/N_A^-$	$4 \times 10^{17}$	$5 \times 10^{17}$	$5 \times 10^{17}$	$\text{cm}^{-3}$
$N_A$	$4 \times 10^{17}$	$8 \times 10^{17}$	$8 \times 10^{17}$	$\text{cm}^{-3}$
$y_i$	-	14	14	nm
$V_T$ - QM, DD	0.55	0.55	0.54	V
$V_T$ - QM, HD	0.51	0.50	0.49	V
$I_{ON}$ - QM, DD	438	437	480	$\mu\text{A}/\mu\text{m}$
$I_{ON}$ - QM, HD	969	733	928	$\mu\text{A}/\mu\text{m}$
$I_{OFF}$ - QM, HD	0.43	0.24	0.37	$\text{nA}/\mu\text{m}$

is no crossover in  $I_{OFF} - I_{ON}$  curves of accumulation and inversion FETs, and inversion FETs perform better than accumulation FETs for a wide range of on-current.

Fig. 39 plots the lateral electric field and channel mobility of the two FET types (corresponding to devices in Table 11). Both accumulation and inversion FETs have almost the same lateral field at the source and in the channel. Channel mobility of the inversion FET is seen to be higher than that of accumulation FETs. Fig. 40 plots velocity in the channel. Velocity in the inversion FET is seen to be higher than that in accumulation FETs, and this is because of the increased channel mobility in the inversion FET. Thus, while drift-diffusion simulations predict better performance with well-processed accumulation MOSFETs, hydro-dynamic simulations predict the opposite. Because of the disparity between drift-diffusion and hydro-dynamic simulation results and because hydro-dynamic simulations predict an unrealistic (100-150%) increase in on-current compared to drift-diffusion simulations, alternative device simulation strategies would have to be used to accurately assess the scaling potential of accumulation and inversion MOSFETs. This will be done in chapter VIII, where Monte Carlo device simulations will be used to predict the drive-current.

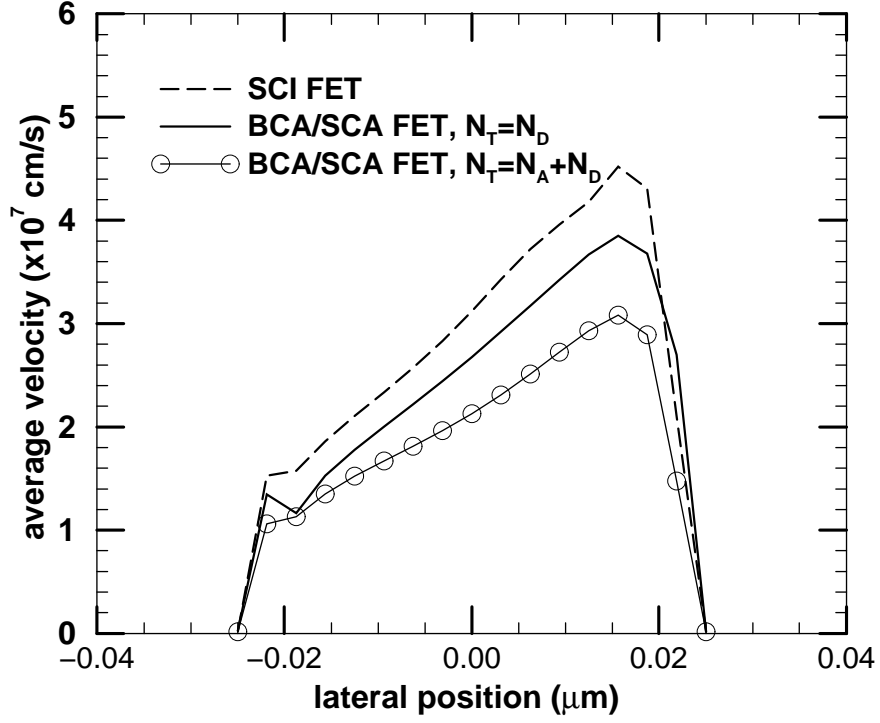
The results presented until now are for MOSFETs without halo doping. The next plot



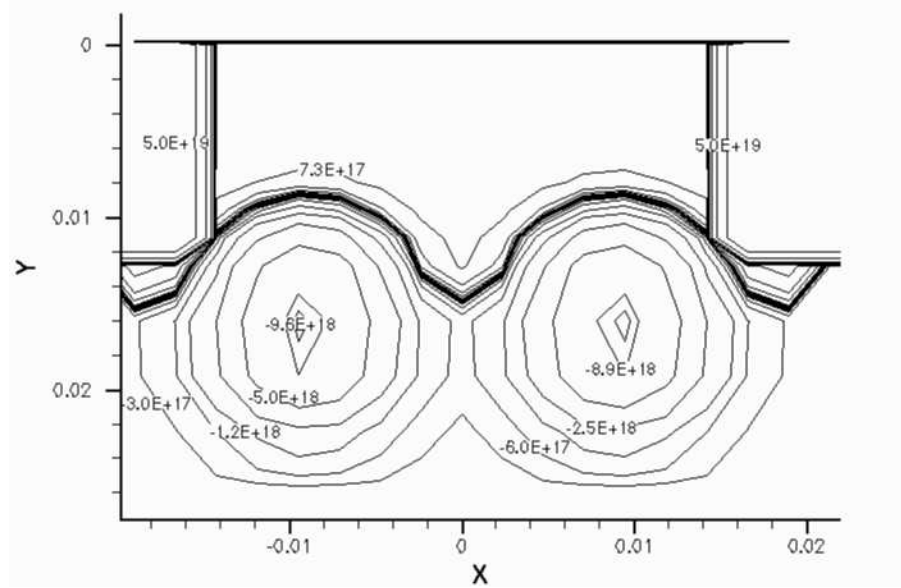
**Figure 39:** Lateral field and mobility vs. lateral position (from 2-D simulations);  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ ,  $V_{GS} - V_T = 0.5 \text{ V}$ , and gate workfunction is 4.63 eV. Device doping is given in Table 11.

will be for halo-doped MOSFETs with a channel length of 30 nm. Fig. 41 shows the halo doping profile. The halo is generated by an analytic function, and is described in Appendix D. The  $I_{OFF} - I_{ON}$  plot for halo devices, Fig. 42, shows that a BCA/SCA n-FET with a steep Boron doping can achieve better performance than the inversion FET for  $I_{ON} > 700 \mu\text{A}/\mu\text{m}$ . The increased velocity overshoot seen in non-halo SCI FETs is not present in the SCI FET with halo doping since halos reduce the effective carrier mobility. Table 12 shows doping, off-current and on-current of halo-doped devices. It can be seen that although channel and substrate doping of the accumulation FET is higher than that of the inversion FET, the on-current of the inversion FET is comparable to that of the accumulation FET. Both accumulation and inversion MOSFETs have  $\Delta V_T(30\% \delta L)$  (i.e. reduction in  $V_T$  for a 30% reduction in channel length) less than 100 mV for the range of  $I_{ON}$  shown.

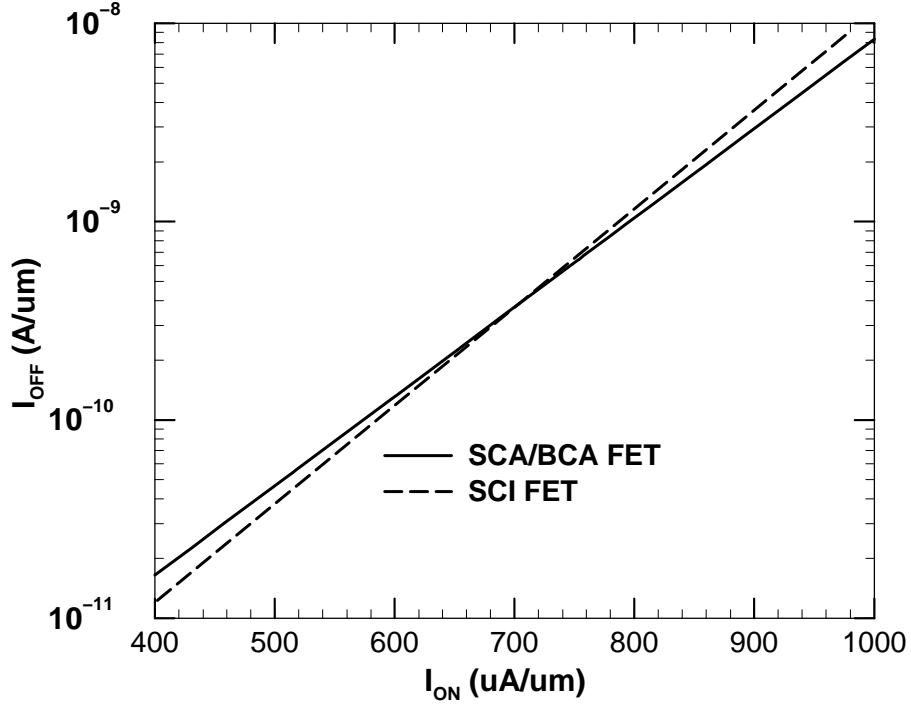
Fig. 43 plots  $I_{OFF} - I_{ON}$  for non-halo FETs, with  $V_{dd} = 0.5 \text{ V}$ . The simulations are classical in nature with drift-diffusion transport since both QM  $V_T$  shift and non-local



**Figure 40:** Average velocity vs. lateral position (from 2-D simulations);  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{DS} = 1.0 \text{ V}$ ,  $V_{GS} - V_T = 0.5 \text{ V}$ , and gate workfunction is  $4.63 \text{ eV}$ . Device doping is given in Table 11.



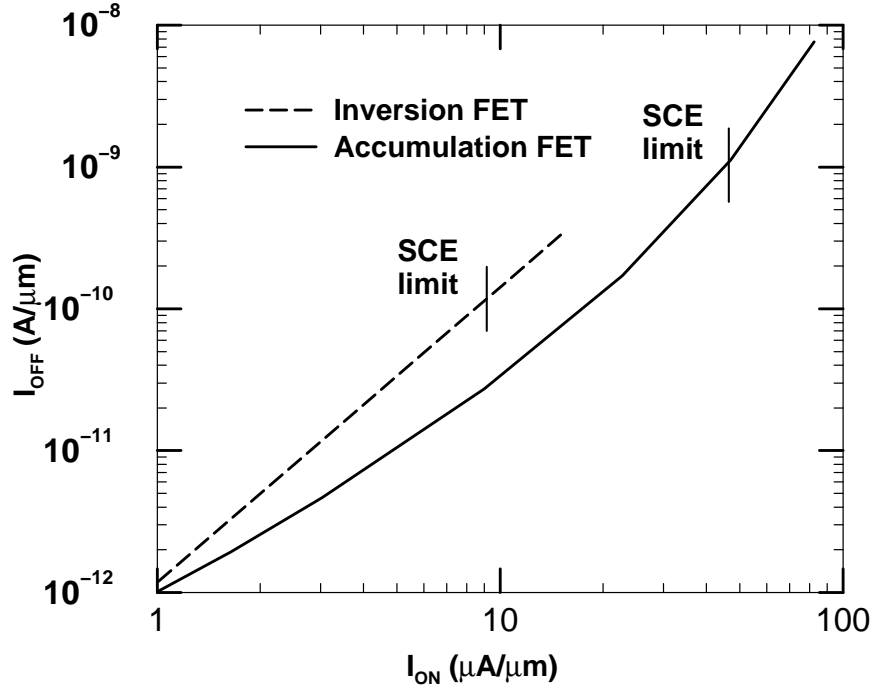
**Figure 41:** Halo doping profile for a  $30 \text{ nm}$  channel length accumulation FET.



**Figure 42:** Off-current vs. on-current for  $L = 30nm$  FETs (from 2-D simulations);  $L = 30 nm$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 nm$ ,  $V_{dd} = 0.9 V$ , and gate workfunction is 4.63 eV. The MOSFETs are halo-doped with a peak halo doping of  $1 \times 10^{19} \text{ cm}^{-3}$ .

**Table 12:** Velocity Overshoot Effect for halo-FETs;  $L = 30nm$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 nm$ ,  $V_{dd} = 0.9 V$ , and gate workfunction is 4.63 eV.

	SCI FET	BCA/SCA FET $N_T = N_A + N_D$	BCA/SCA FET $N_T = N_D$	units
$N_D/N_A^-$	$4 \times 10^{17}$	$5 \times 10^{17}$	$5 \times 10^{17}$	$cm^{-3}$
$N_A$	$4 \times 10^{17}$	$6 \times 10^{17}$	$8 \times 10^{17}$	$cm^{-3}$
$y_i$	-	14	14	nm
$V_T$ - QM, HD	0.58	0.54	0.55	V
$I_{ON}$ - QM, HD	594	621	656	$\mu A/\mu m$
$I_{OFF}$ - QM, HD	0.10	0.40	0.21	$nA/\mu m$
$\Delta V_T(30\% \delta L)$	87	84	82	mV



**Figure 43:** Off-current vs. on-current for low  $V_{dd}$  applications (from 2-D classical DD simulations);  $L = 30 \text{ nm}$ ,  $t_{ox} = 10 \text{ Å}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{dd} = 0.5 \text{ V}$ , and gate workfunction is 4.63 eV. The SCE limit is taken to be  $S < 100 \text{ mV/dec}$ .

transport can be neglected at low drive currents. The SCE limit is taken to be  $S < 100 \text{ mV/dec}$ . Accumulation FETs are seen to have a lower  $I_{OFF}$  and a lower SCE (for a given  $I_{ON}$ ) compared to SCI FETs. Thus, single metal gate accumulation FETs are also useful for ultra-low power applications.

## 6.4 Summary

The accumulation FET has an increased depletion depth compared to the inversion FET. In the long-channel regime, this results in a lower subthreshold swing; in the short-channel regime, this results in worse SCE compared to the inversion FET. So, if the gate WF is tunable, short-channel inversion MOSFETs have better SCE control than accumulation FETs. For mid-band metal gate HiP and LOP applications, there is a disparity between drift-diffusion and hydro-dynamic simulations; Monte Carlo simulations would have to be used to accurately assess the scaling potential of accumulation and inversion MOSFETs for such applications. For HiP applications with single metal gate CMOS, well-designed

halos result in better performance using accumulation FETs than with inversion FETs. For ultra-low power, single metal gate CMOS applications, accumulation FETs perform much better than inversion FETs due to lower SCE.

## CHAPTER VII

### POLY GATE MOSFETS

#### 7.1 *Introduction*

Poly-gate MOSFETs have been the workhorse of CMOS technology. Inversion n-FETs use n+ poly as the gate material to obtain enhancement operation. Accumulation n-FETs need to use p+ poly as the gate material in order to obtain enhancement mode operation. When poly gates are used,  $V_T$  of the transistors will have to be adjusted by changing the channel/substrate doping.

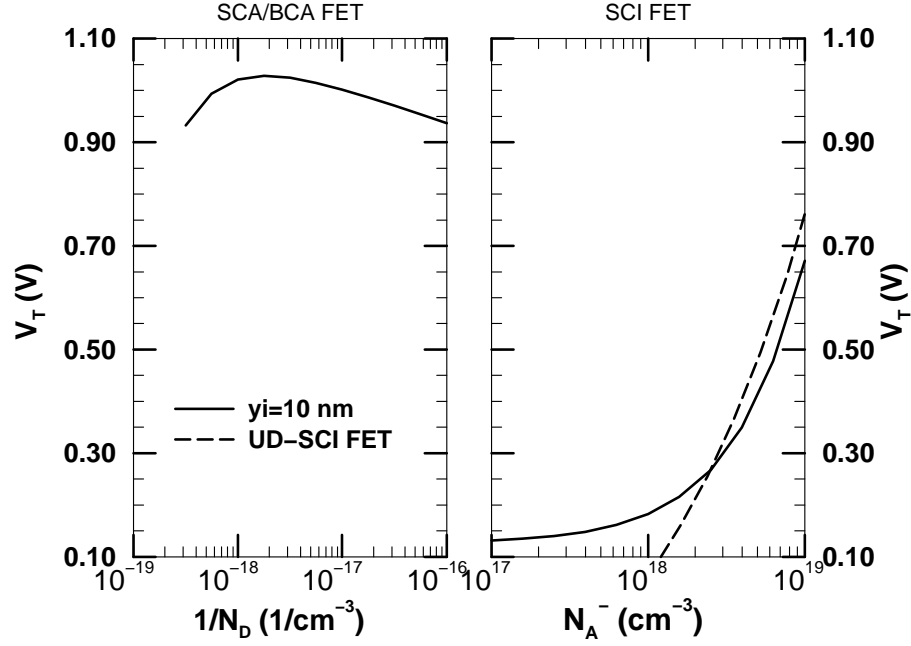
Fig. 44 plots  $V_T$  vs. channel doping, and it can be seen that the SCA FET has a  $V_T$  of around 1 V for a wide range of channel doping, whereas the SCI FET can achieve a high  $V_T$  only with very high channel and substrate doping. At such a high doping, the SCI FET has many shortcomings:

- very low channel mobility
- high band-to-band tunneling (BTBT) leakage at the drain-substrate junction
- high subthreshold slope (since  $d$  decreases as  $N_A$  increases)

In contrast, the SCA FET uses a lightly doped channel and has a low S, thus resulting in good on-current and off-current. Also, BTBT leakage in accumulation FETs can be kept to low levels since a p-n junction is absent in the lateral direction in the channel.

Fig. 44 shows that the UD-SCI FET needs a doping in excess of  $1 \times 10^{19} \text{ cm}^{-3}$  to achieve a  $V_T$  of 0.8V. The curves in Fig. 44 were generated using the Boltzmann distribution, and did not include the effect of QM  $V_T$  shift. Even if the Fermi-Dirac distribution (which would be more accurate at high doping) is used and QM effects are included, a very high doping ( $> 6 \times 10^{18} \text{ cm}^{-3}$ ) would still be needed to achieve a  $V_T$  of 0.8 V. Fig. 45 shows a plot of S vs.  $V_T$  for the inversion and accumulation FETs. Comparing this to Fig. 44, it can be seen that the SCA FET has a better S than the SCI FET for  $V_T > 0.5\text{V}$ . In addition to





**Figure 44:** Threshold voltage vs. tub-doping for poly-gate accumulation and inversion MOSFETs (from models);  $L = 70 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 20 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ ,  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ . The gate workfunction is 5.19 eV for accumulation FETs, and 4.19 eV for inversion FETs.

SCE models, models for BTBT leakage, and gate tunneling are needed to comprehensively compare poly gate accumulation and inversion MOSFETs.

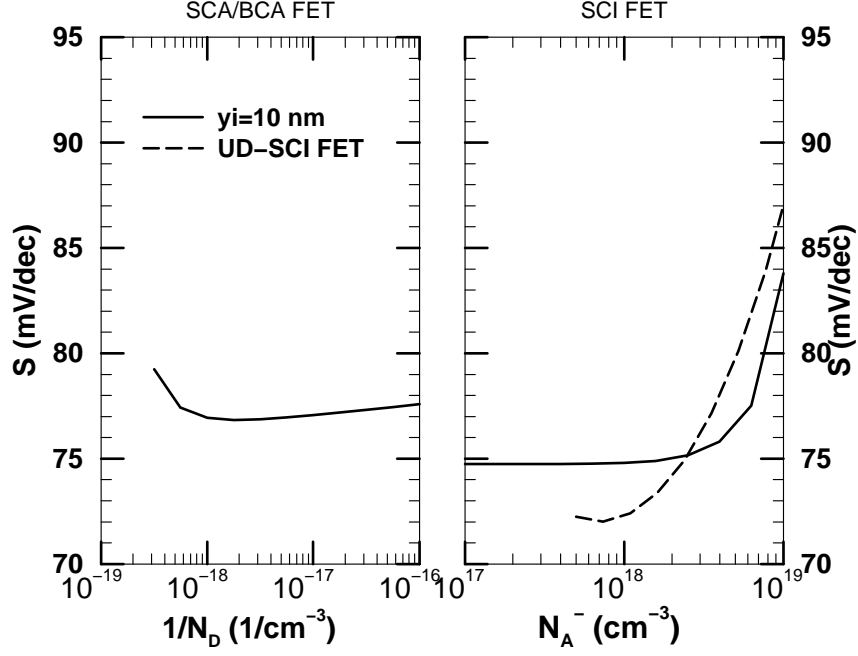
## 7.2 Band to Band Tunneling Leakage

As the channel/substrate doping in a MOSFET increases, BTBT leakage at the drain-substrate and drain-channel region becomes appreciable. The BTBT leakage model is derived by making the triangular barrier approximation for a p-n junction [43]:

$$J_t = \frac{\sqrt{2m^*}q^3EV}{4\pi^2\hbar^2E_g^{1/2}} \exp\left(-\frac{4\sqrt{2m^*}E_g^{1/2}}{3qE\hbar}\right) \quad (42)$$

where  $E$  is the electric field at the junction,  $E_g$  is the bandgap,  $V$  is the applied voltage,  $m^*$  is the effective mass, and  $\hbar = h/(2\pi)$  ( $h$  is Planck's constant). The electric field at the drain-substrate junction can be estimated to a first order by 1-D electrostatics. The electric field expression is obtained from abrupt p-n junction theory:

$$E = A0. \frac{qN'_D x_n}{\epsilon_s} \quad (43)$$



**Figure 45:** Subthreshold swing vs. tub-doping for poly-gate accumulation and inversion MOSFETs (from models);  $L = 70 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 20 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ ,  $N_A = 2.5 \times 10^{18} \text{ cm}^{-3}$ . The gate workfunction is 5.19 eV for accumulation FETs, and 4.19 eV for inversion FETs.

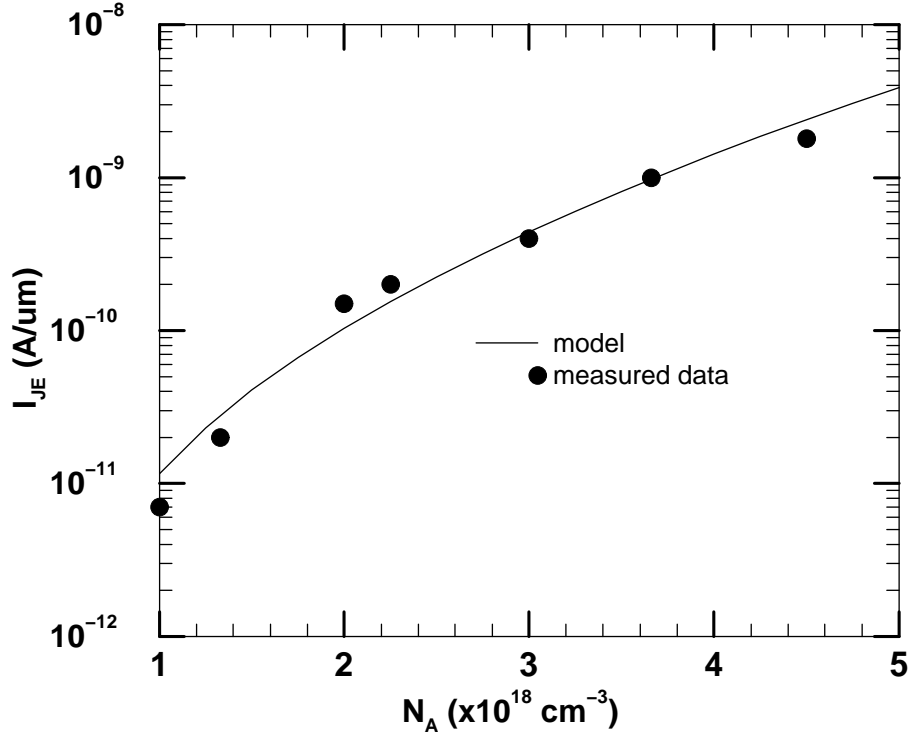
where  $N'_{D_D} = A1.N_{D_D}$  is the modified drain doping, and  $x_n$ , the depletion depth on the drain side is given by

$$x_n = \sqrt{\frac{2\epsilon_s}{q} \left( \frac{N'_A}{(N'_A + N'_{D_D})N'_{D_D}} \right) \psi_{bi}} \quad (44)$$

$N'_A = A2.N_A$  is the modified channel doping.  $A0$ ,  $A1$ , and  $A2$  are model parameters to account for non-uniform doping at the drain-substrate junction. The model is compared to measurements from [91], Fig. 46. A good match is seen between the model and measurements.

### 7.3 Accumulation vs. Inversion FETs

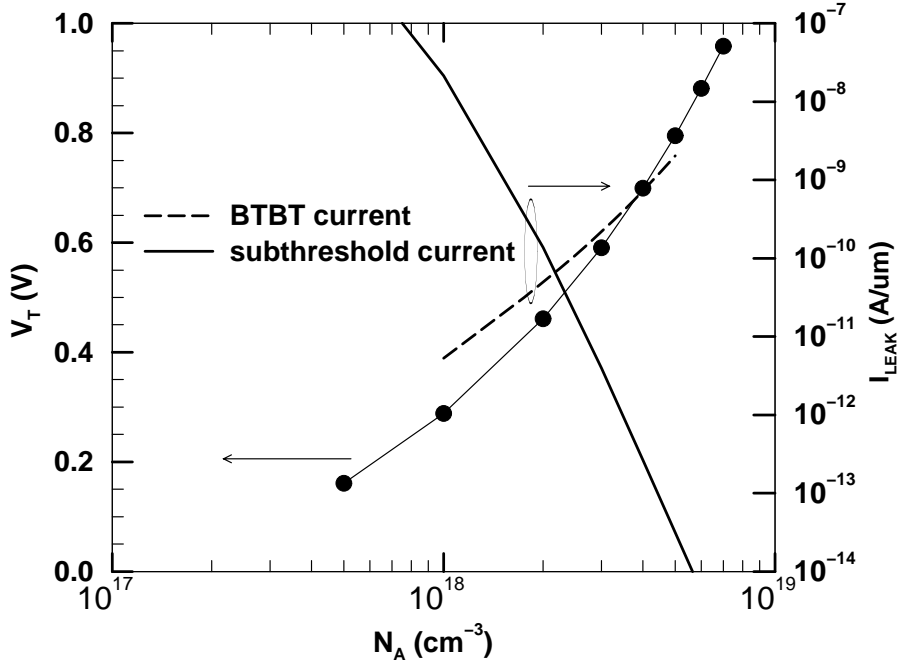
In this chapter, BTBT leakage is assumed to occur only in the drain-channel region, since the drain-substrate region can be tailored to be p-i-n type to avoid BTBT leakage. In an accumulation FET, considerable BTBT leakage occurs only if the substrate doping is high and the tub-depth is much less than the junction depth. For poly-gate applications, the substrate doping of accumulation FETs is kept below  $2.5 \times 10^{18} \text{ cm}^{-3}$ , resulting in negligible



**Figure 46:** BTBT leakage at drain-channel region vs. channel doping: model verification with measured data from [91];  $V_{DS} = 1.3 \text{ V}$ , and  $T = 100 \text{ }^\circ\text{C}$ .

BTBT leakage. In an inversion FET, the channel and substrate doping need to be high to achieve high  $V_T$ . Fig. 47 shows subthreshold and BTBT leakage vs. doping, for inversion MOSFETs. It can be seen that BTBT leakage limits the minimum off-current of inversion MOSFETs to 60 pA/um. The ITRS [1] recommended off-current for low standby power (LSTP) systems is 1 pA/um or less. The SCI FET is unable to achieve  $I_{OFF}$  less than 1 pA/um because of the onset of BTBT leakage.

In an SCI FET, the electric field points into the oxide-semiconductor interface (looking from the top), and hence attracts carriers towards the interface. In a BCA FET, the electric field points out of the Si – SiO<sub>2</sub> interface; thus, in a BCA FET, electrons experience a force that repels them away from the Si – SiO<sub>2</sub> interface and deeper into the tub region. Hence, a BCA n-MOSFET has a higher barrier for electrons tunneling through the oxide, Fig. 48. Thus, the accumulation n-MOSFET can use a thinner oxide than the SCI n-MOSFET, and thereby achieve a better performance. The tunneling model used is similar to that in [92], and is explained in Appendix E.

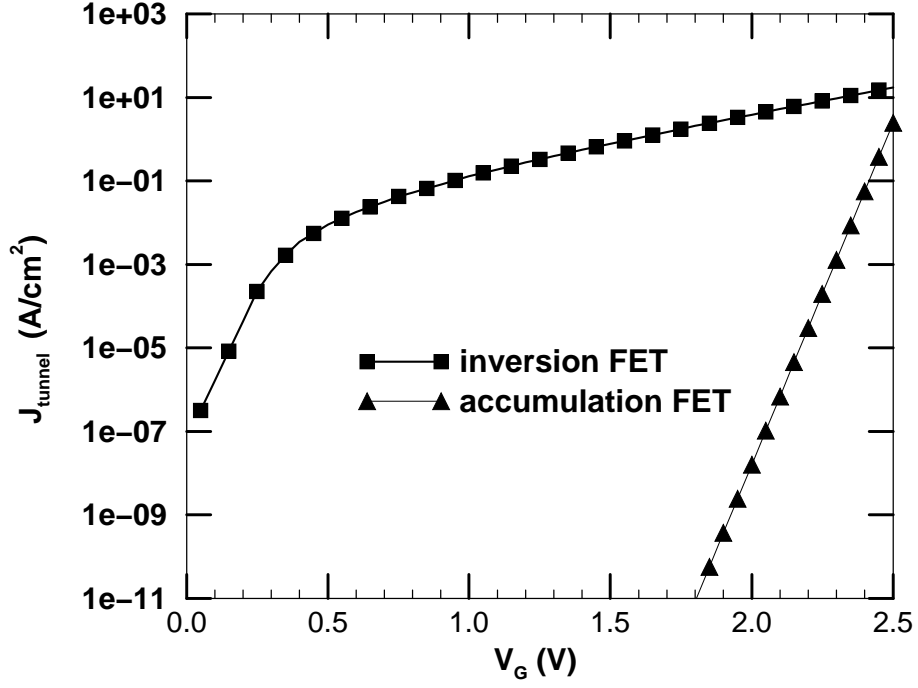


**Figure 47:** BTBT leakage at drain-channel region, and subthreshold leakage (from models) for poly-gate, uniformly-doped, inversion n-MOSFETs;  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $V_{dd} = 1.0 \text{ V}$ , and gate workfunction is  $4.63 \text{ eV}$ .

A chain of inverters is simulated using the tick-based circuit simulation methodology to find the power-frequency ( $P - f_{clk}$ ) performance of circuits using either accumulation or inversion FETs. Fig. 49 shows  $P - f_{clk}$  curves for inverter chains using either accumulation or inversion FETs. The devices use halo doping to obtain reduced SCE. It can be clearly seen that for high performance applications, the SCI FET chain performs better, whereas for LSTP applications, the SCA FET chain performs better. For LSTP applications, the SCA FET has more than an order of magnitude lower standby power than the SCI FET (for the same dynamic power and frequency).

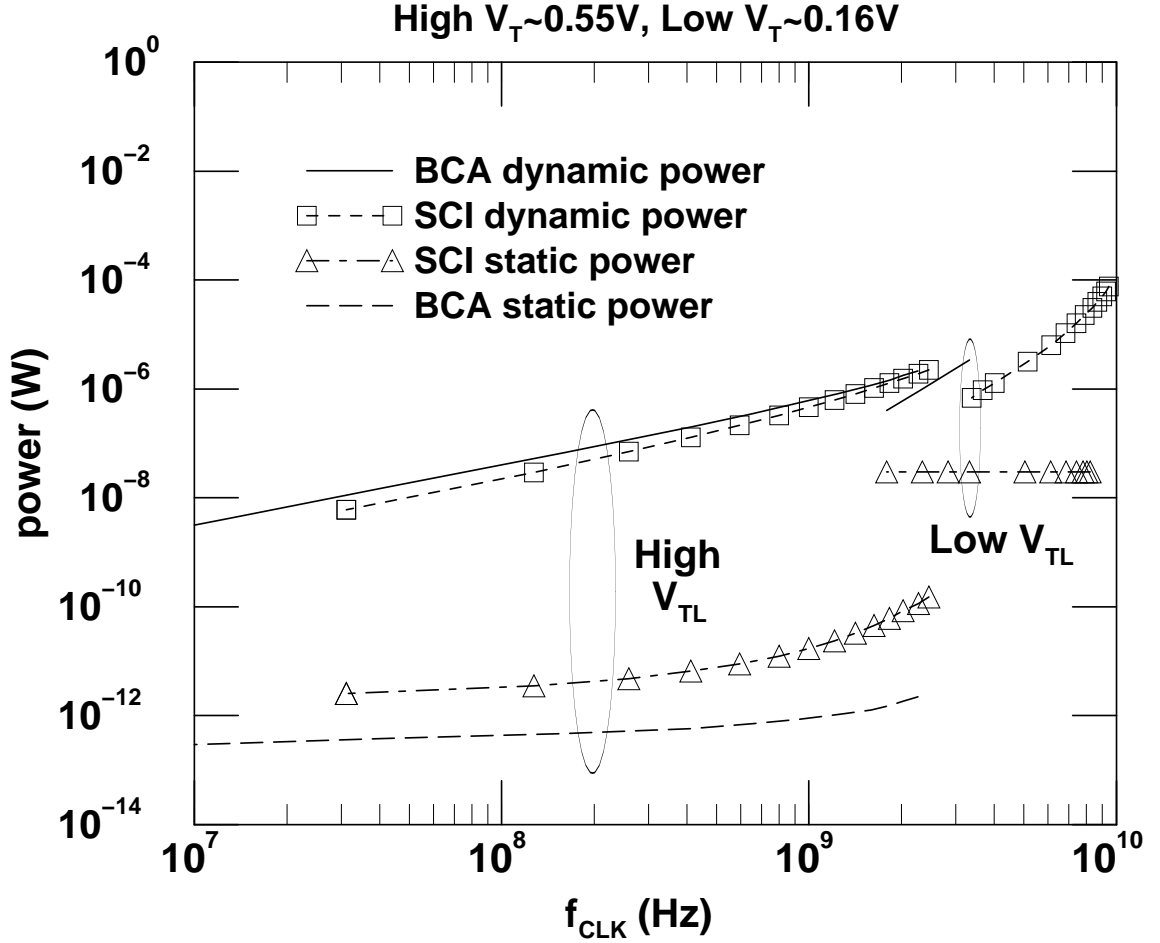
## 7.4 Summary

For dual polysilicon gate CMOS, accumulation FETs have an advantage over inversion FETs for low standby power applications. To achieve a high  $V_T$ , the SCI FET needs a very high channel channel doping. This causes a low channel mobility (and hence a low  $I_{ON}$ ), high BTBT leakage at the drain-channel junction, high  $\sigma V_T$  and a high S. On the other



**Figure 48:** Gate tunneling current density (from models) comparison of poly-gate BCA/SCA and SCI n-FETs for 15 Å gate oxide.

hand, the SCA FET can achieve a high  $V_T$  by using a lightly doped channel and a substrate doping that is low enough to avoid BTBT leakage, but high enough to control SCE. Thus the SCA FET has a high channel mobility, negligible BTBT leakage and a low  $\sigma V_T$ . Also, because of a higher barrier for gate-channel electron tunneling in an accumulation n-FET, it has a much lower gate oxide tunneling than an inversion n-FET. A chain of inverters using either inversion or accumulation FETs are simulated, and it is found that for LSTP applications, an SCA FET inverter chain has a 1-order of magnitude lower static power (for the same dynamic power and frequency) than an SCI FET inverter chain.



**Figure 49:**  $P - f_{clk}$  for poly gate accumulation and inversion FET inverter chains with  $L_{eff}=50nm$ . High  $V_T$  case:  $t_{ox}=15\text{\AA}$  for SCA FET,  $t_{ox}=23\text{\AA}$  for SCI FET,  $y_j=32nm$ ,  $y_{iBCA}=10nm$ ,  $N_{ABCA}=2.4 \times 10^{18} \text{ cm}^{-3}$ ,  $FO=2$ ,  $C_w=0$ ,  $n_{cp}=12$ ; low  $V_T$  case:  $t_{ox}=15\text{\AA}$ ,  $y_j=y_{iBCA}=10nm$ ,  $N_{ABCA}=8 \times 10^{18} \text{ cm}^{-3}$ ,  $FO=2$ ,  $C_w=10fF$ ,  $n_{cp}=7$ .  $V_{dd}$  varies in both high and low  $V_T$  cases.

## CHAPTER VIII

### MONTE CARLO DEVICE SIMULATION

#### *8.1 Introduction*

When simulating semiconductor devices, a variety of transport models can be used: drift-diffusion, hydro-dynamic, solutions of the Boltzmann transport equation (BTE), and quantum transport. The accuracy of a device simulation depends on the transport model used. In the drift diffusion approach, the first two moments of the BTE are used to describe carrier transport (the two resulting equations are the continuity equation, and the current flow equation) [93]. The two equations are coupled to Poisson's equation, and solved self-consistently to find the carrier density and electrostatic potential. The drift-diffusion approach assumes that the current changes slowly on the scale of the momentum relaxation time, and does not treat nonlocal effects like velocity overshoot.

For Si MOSFET channel lengths less than a few hundred nanometres, non-local effects become important. These effects can be captured by the momentum-energy balance equations. In this approach, the energy gradient is included in the current equation, and mobility is a function of carrier energy (rather than the local electric field as in the drift-diffusion approach). In the hydro-dynamic/energy transport approach, the first three moments of the BTE are solved; the extra equation that results is the energy balance equation. There are many forms of the HD model because of different assumptions made in deriving them [94]. HD model parameters are usually extracted from a self-consistent MC simulation or from measurements.

For small devices (for Si MOSFET channel lengths less than a few tens of nanometres), the BTE should be solved. The BTE is a semi-classical approach to describing carrier transport - it describes the evolution of the carrier trajectory by using a combination of classical mechanics, and quantum mechanics (by way of probabilistic scattering rates) [95].

The BTE is given by

$$\frac{\partial f}{\partial t} + \vec{v} \cdot \nabla_r f + \frac{e\vec{E}}{\hbar} \cdot \nabla_p f = \left. \frac{\partial f}{\partial t} \right|_{coll} + s(\vec{r}, \vec{p}, t) \quad (45)$$

where,

$$\nabla_r f = \frac{\partial f_x}{\partial x} \hat{x} + \frac{\partial f_y}{\partial y} \hat{y} + \frac{\partial f_z}{\partial z} \hat{z} \quad (46)$$

$$\nabla_p f = \frac{\partial f_x}{\partial p_x} \hat{x} + \frac{\partial f_y}{\partial p_y} \hat{y} + \frac{\partial f_z}{\partial p_z} \hat{z} \quad (47)$$

$f(\vec{r}, \vec{p}, t)$  is the distribution function that gives the probability of finding carriers at time  $t$ , located at a position  $\vec{r}$  with momentum  $\vec{p}$ , and  $\vec{E}$  is the electric field. The BTE accounts for all possible mechanisms by which  $f$  might change including collisions and external fields. For classical particles,  $\vec{v} = \vec{p}/m^*$ , whereas for electrons in semiconductors,  $\vec{v} = \nabla_p E(\vec{p})$ .  $\left. \frac{\partial f}{\partial t} \right|_{coll}$  describes collisions, whereas  $s(\vec{r}, \vec{p}, t)$  describes carrier generation recombination processes.

Under low fields when the scattering is elastic and isotropic, the relaxation time approximation is widely used - this greatly simplifies the solution of the BTE. But there exist many situations where the collisions are neither elastic nor isotropic - e.g. electrons with a few tens of eV energy, and in these cases numerical techniques are necessary. Proposed numerical approaches to solve the BTE include Monte Carlo, cellular automata, scattering matrix, and spherical harmonic methods. Of these, the Monte Carlo method has achieved the most success because of its ease of programming. For Si MOSFET channel lengths less than a few nanometres, the quantum transport equation would have to be solved to accurately simulate device behavior. Some methods proposed for solving the quantum equation are Wigner transformation [96], and non-equilibrium Green's function method [97].

## 8.2 The Monte Carlo Approach

The motivation behind using MC methods is that it is an elegant way to solve the BTE. The BTE is an integro-differential equation, and very difficult to solve; it is much easier to simulate the trajectories of individual carriers as they move through a device under the influence of electric fields and random scattering forces. If a large number of such paths are simulated, then the average value of the extracted parameters will closely agree with



the exact solution of the BTE. MC method is frequently the standard against which the validity of simpler approaches is gauged.

There are two possible ways to use the Monte Carlo technique to simulate semiconductor devices [93]. In the ensemble Monte Carlo (EMC) approach, an ensemble of particles are followed within the device, in parallel. In the single particle Monte Carlo (SPMC) approach, carriers are followed one at a time - the carrier is injected from a contact and followed until it exits the device through the same or another contact. To simulate each operating point of a MOSFET using the single particle MC simulator SPARTA [98], takes about 12-16 hours. The same takes 24-30 hrs. using the ensemble MC simulator DEGAS [99]. For comparison, drift-diffusion (DD) simulations take less than a minute, and hydro-dynamic (HD) simulations take about 10 minutes. There are two possible ways to keep MC simulations to a minimum.

In the first method, a calibrated drift diffusion method can be used; the saturation velocity ( $v_{sat}$ ) would have to be altered to account for velocity overshoot. The exact value of  $v_{sat}$  necessary in the DD simulation can be calibrated with the help of a MC simulation at high  $V_{DS}$  [100]. The drawback of such an approach is that the value of  $v_{sat}$  would be different for different channel doping (since velocity overshoot is dependent on channel mobility and channel length). Thus,  $v_{sat}$  would have to be individually extracted from MC simulations for different structures, which would not result in any savings in time compared to the MC simulation approach. The second approach is to use a calibrated hydro-dynamic method; surface roughness mobility parameters in the HD simulation are adjusted so that the on-current matches well with MC simulations. The calibration is explained in further detail in Appendix F. The reliability of this method is tested against MC simulation results, Table 13. It can be seen that HD simulations have an error within 6% of MC simulations, which is acceptable given the huge savings in computation time.

Using the single particle Monte Carlo (MC) simulator SPARTA [98], halo-doped accumulation and inversion MOSFETs are simulated. Before comparing the DD simulation output with that of MC simulation for high drain voltages, the DD mobility model parameters should be adjusted so that the output agrees well with MC simulations for low

**Table 13:** On-current comparison from various simulations;  $L = 30 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ ,  $N_A = 1 \times 10^{18} \text{ cm}^{-3}$ ,  $N_D = N_A^- = 1 \times 10^{17} \text{ cm}^{-3}$  and  $y_i = 20 \text{ nm}$ . The devices are halo-doped. The source/drain doping is  $5 \times 10^{19} \text{ cm}^{-3}$ .

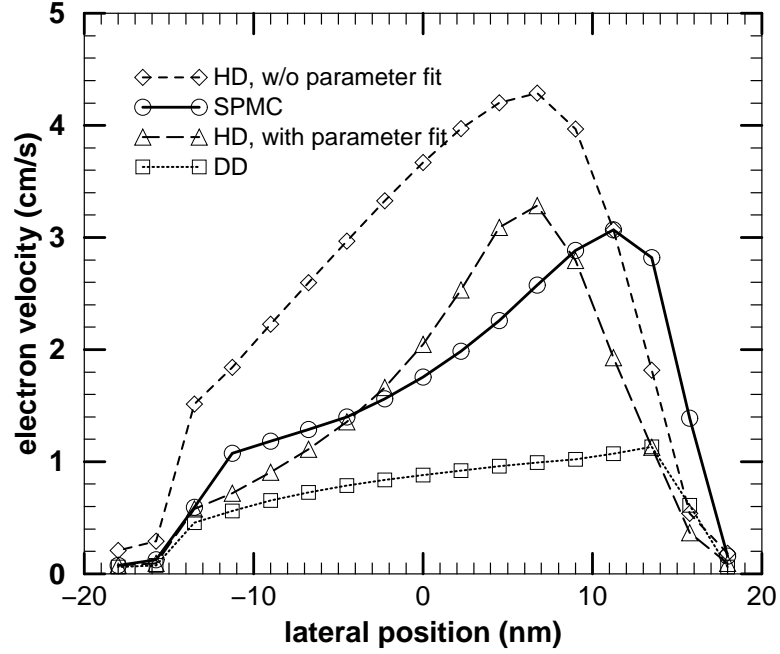
device	$V_{dd}$ (V)	DD $I_{ON}$ ( $\mu\text{A}/\mu\text{m}$ )	HDWOP $I_{ON}$ ( $\mu\text{A}/\mu\text{m}$ )	HDWP $I_{ON}$ ( $\mu\text{A}/\mu\text{m}$ )	MC $I_{ON}$ ( $\mu\text{A}/\mu\text{m}$ )	% error in HDWP w.r.t. MC result
accumulation	0.9	295	647	351	354	0.0
accumulation	1.0	431	-	530	513	3.3
inversion	0.9	269	-	310	328	5.4

drain voltages [89]. In drift-diffusion simulations, the surface roughness mobility parameters need to be adjusted to match MC simulation output, at low drain voltages. The Darwish mobility model [101] is used to model mobility degradation due to surface roughness. The surface scattering ratio,  $s$  (where  $s=1.0$  means that the scattering is purely specular, and  $s=0$  means that the scattering is purely diffuse), is taken to be 0.85 in MC simulations [89].

Fig. 50 compares the channel velocity of four simulations - DD, MC, HD with parameters fit to MC simulation (HDWP) and HD without any parameter fit (HDWOP). It can be seen that HDWOP predicts a huge velocity overshoot in the channel compared to the MC simulation. The source side velocity is what determines the on-current in a MOSFET. Fig. 51 plots velocity (at different distances from the source) vs. on-current. It can be seen that the points lie on a straight line, confirming that source-side velocity (and not peak channel velocity) determines the on-current. From the MC simulations, it is found that for  $L_{eff} = 30 \text{ nm}$  accumulation MOSFETs with halos, on-current increases by about 20% because of velocity overshoot, Table 13. HDWOP simulations predict more than a 100% increase in on-current (compared to DD simulations). The increase is about 21% with HDWP, for inversion MOSFETs.

### 8.3 Mid-bandgap Metal Gate MOSFETs Revisited

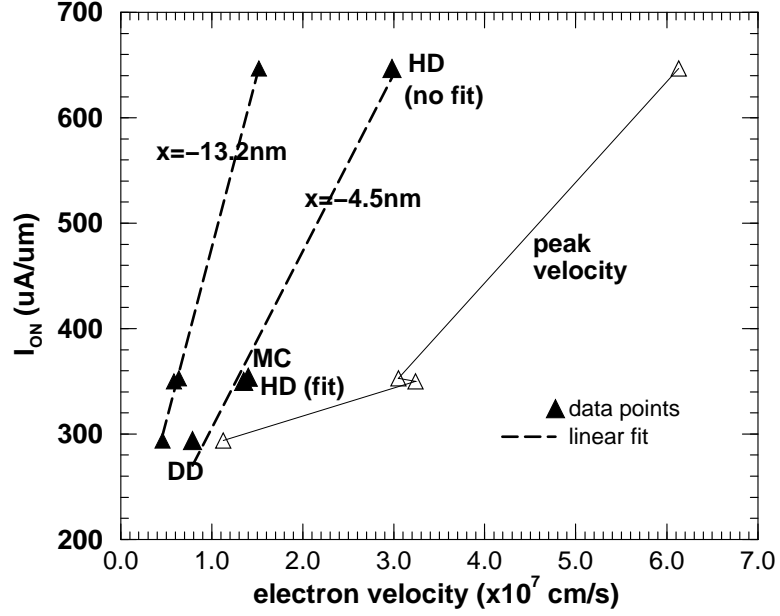
In section 6.3, mid-bandgap metal gate n-MOSFETs were compared. It was found that for halo doped MOSFETs with a channel length of 30 nm, accumulation MOSFETs had a



**Figure 50:** Absolute electron velocity vs. lateral position for a mid-bandgap metal gate accumulation n-MOSFET (from 2-D simulations), 1 nm below the Si – SiO<sub>2</sub> interface;  $L = 30$  nm,  $t_{ox} = 15$  Å,  $y_j = 12$  nm,  $V_{GS} = V_{DS} = 1.0$  V,  $N_A = 1 \times 10^{18}$  cm<sup>-3</sup>,  $N_D = 1 \times 10^{17}$  cm<sup>-3</sup>, and  $y_i = 20$  nm. QM  $V_T$  shift was included by means of a 70 mV shift in the gate workfunction. The accumulation MOSFET is halo-doped with a peak halo doping of  $1 \times 10^{19}$  cm<sup>-3</sup>, and a source/drain doping of  $5 \times 10^{19}$  cm<sup>-3</sup>. The surface-scattering ratio in the Monte Carlo simulations is taken to be 0.85. In the legend, SPMC refers to Single Particle MC simulation.

marginal advantage over inversion MOSFETs for hi-performance applications. The transport model used to arrive at this result was hydro-dynamic, with default mobility model parameters. However, it was seen in the previous section that HDWOP severely overestimates on-current increase due to velocity overshoot. Thus, the comparison would have to be repeated using a calibrated mobility model, using the HD transport model. Alternatively, MC simulations can be used to perform the comparison.

MOSFETs with a channel length of 30 nm, and with halos, are simulated using HDWP, and Monte Carlo simulations, Fig. 52. The simulations assume a gate workfunction of 4.70 eV, including a gate workfunction shift of 70 mV to account for quantum mechanical centroid shift. The maximum allowable subthreshold swing is assumed to be 110 mV/dec. It can be seen that once again HDWP simulations have less than a 5% error compared



**Figure 51:** On-current vs. electron velocity for a mid-bandgap metal gate accumulation n-MOSFET (from 2-D simulations); the source is at  $x = -15 \text{ nm}$ .  $L = 30 \text{ nm}$ ,  $t_{ox} = 15 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ ,  $N_A = 1 \times 10^{18} \text{ cm}^{-3}$ ,  $N_D = 1 \times 10^{17} \text{ cm}^{-3}$ , and  $y_i = 20 \text{ nm}$ . QM  $V_T$  shift was included by means of a 70 mV shift in the gate workfunction. The accumulation MOSFET is halo-doped with a peak halo doping of  $1 \times 10^{19} \text{ cm}^{-3}$ , and a source/drain doping of  $5 \times 10^{19} \text{ cm}^{-3}$ . The surface-scattering ratio ( $s$ ) in the MC simulation is taken to be 0.85.

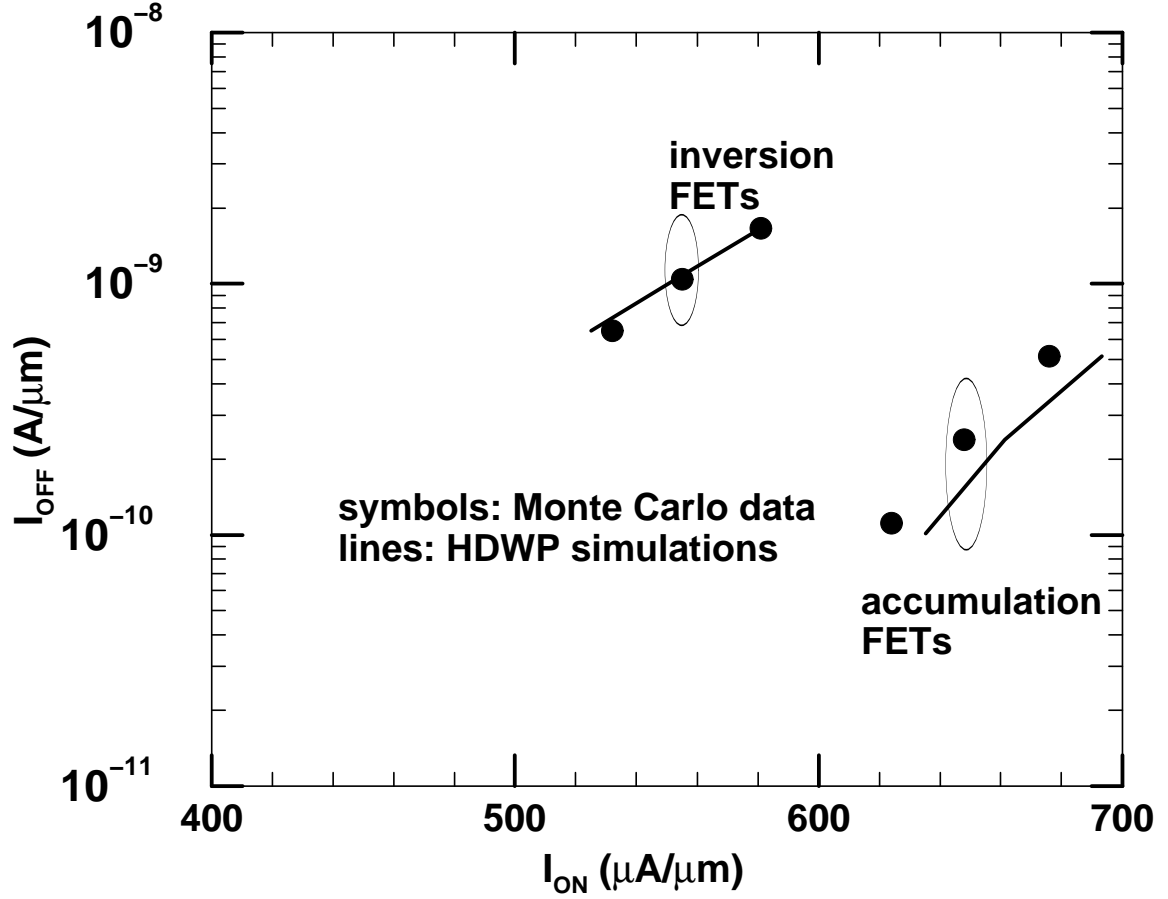
to MC simulations. Accumulation MOSFETs are seen to have a 17% greater maximum on-current compared to inversion MOSFETs. A second set of simulations is done using the HDWP method with the van Dort model [87] to include quantum correction, Fig. 53. It can be seen that the on-current advantage of accumulation MOSFETs increases from 17% to 45% when quantum effects are included by means of the van Dort method. The increase in advantage is because accumulation MOSFETs have a lower vertical field resulting in a lower QM  $V_T$  shift compared to inversion MOSFETs.

## 8.4 Summary

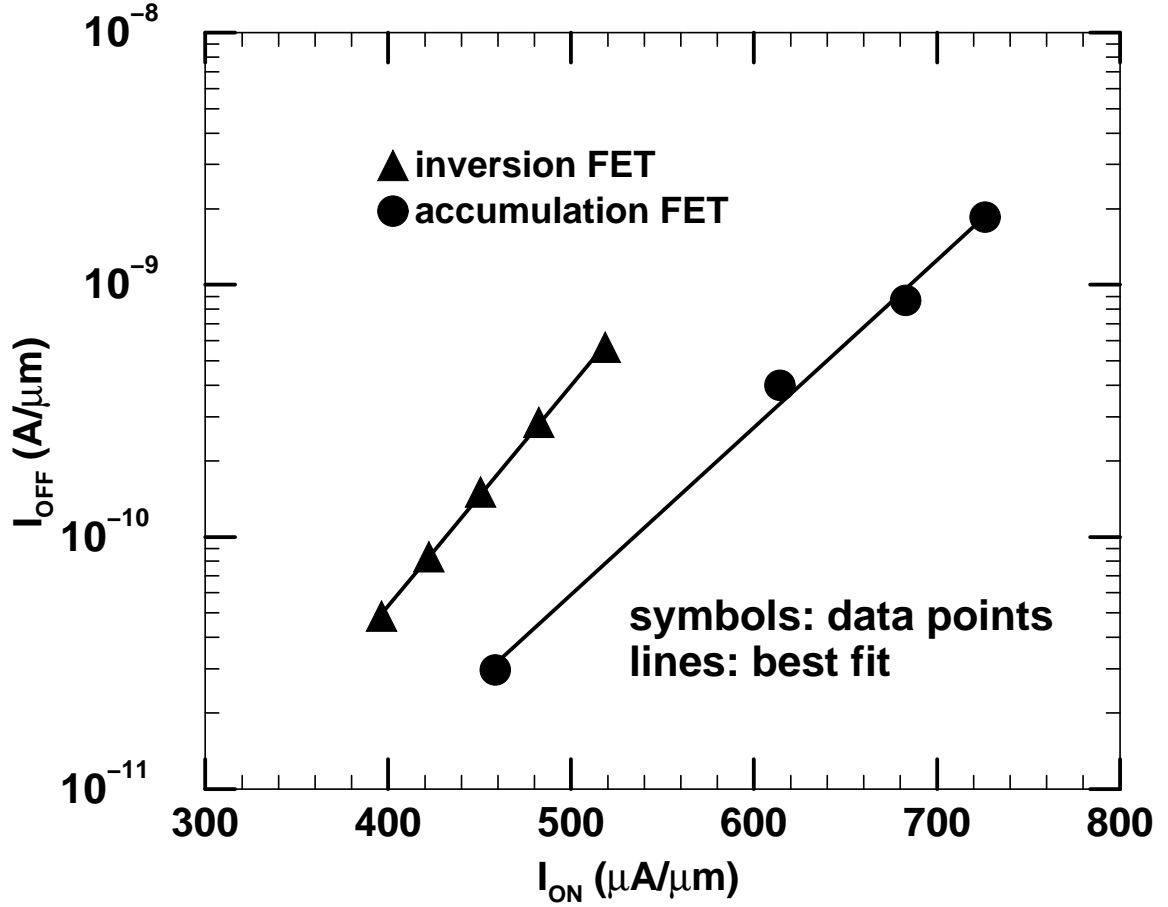
- Drift-diffusion simulations do not include non-local effects, and thus cannot be applied to MOSFETs with channel lengths less than a few hundred nanometres. HD simulations need to be used to include non-local effects. However, there are a number of ways of implementing the HD models. In the literature, there is no clear consensus

as to which HD method is most effective to accurately simulate non-local effects.

- MC simulations give reference data in the absence of experimental data. HD mobility model parameters can be calibrated to give the same output as MC simulations. HD simulations with calibrated mobility model parameters give on-currents within 6% of the MC simulation output, with huge savings in computation time.
- For 30 nm MOSFETs with halos, with  $V_{dd} = 1.0\text{ V}$  and a 1 nm gate oxide thickness, accumulation MOSFETs have a 25% greater on-current compared to inversion MOSFETs (for the same off-current). Also, the maximum achievable on-current is 45% greater with accumulation MOSFETs (for  $S < 110\text{ mV/dec}$ ).



**Figure 52:** Off-current vs. on-current for mid-bandgap metal gate n-MOSFETs;  $L = 30 \text{ nm}$ ,  $t_{\text{ox}} = 10 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ , and  $V_{\text{dd}} = 1.0 \text{ V}$ . The MOSFETs are halo-doped with a peak halo doping of  $1 \times 10^{19} \text{ cm}^{-3}$ , and a source/drain doping of  $5 \times 10^{19} \text{ cm}^{-3}$ . The maximum subthreshold swing is taken to be  $110 \text{ mV/dec}$ . Quantum mechanical  $V_T$  shift is included by means of a  $70 \text{ mV}$  shift in the gate workfunction.



**Figure 53:** Off-current vs. on-current for mid-bandgap metal gate n-MOSFETs (from HDWP simulations);  $L = 30 \text{ nm}$ ,  $t_{ox} = 10 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ , and  $V_{dd} = 1.0 \text{ V}$ . The MOSFETs are halo-doped with a peak halo doping of  $1 \times 10^{19} \text{ cm}^{-3}$ , and a source/drain doping of  $5 \times 10^{19} \text{ cm}^{-3}$ . The maximum subthreshold swing is taken to be  $110 \text{ mV/dec}$ . Quantum mechanical  $V_T$  shift is included by means of van Dort method.

## CHAPTER IX

### SCALING LIMITS

#### 9.1 *Introduction*

MOSFET scaling is one of the main drivers of silicon technology - in addition to gains in increased functionality per unit area, and speed, there is also a reduction in the amount of dynamic power dissipated per cycle per device. But device scaling is limited by SCE and related phenomena, and process limitations. Process variations cause the MOSFET gate length to vary across the die, resulting in a  $3\sigma$  value of about 10-30% of the gate length. This results in MOSFETs with various channel lengths across the wafer, and the MOSFET with the shortest length (say,  $L_G = L_{nom} - 3\sigma$ ) will have the worst off-current. The nominal channel length MOSFET will have to be designed such that the worst case device (i.e.  $L_G = L_{nom} - 3\sigma$ ) has a leakage within one to two orders of magnitude of the nominal device. This translates to a maximum  $V_T$  reduction of 100-200 mV for the worst case device compared to the nominal device ( $I_{OFF} = I_0 10^{-V_T/S}$ ).

Process variations also cause variations in oxide thickness, and dopant fluctuation effect, but these effects have a far lesser impact on device scaling than channel length variation. In case of SOI MOSFETs, variation in silicon film thickness may also limit device scaling [102]. The MOSFET channel length limit depends on the particular application [103] and the gate technology [104]. The different application areas defined by ITRS (Table 1) have different off-current and  $V_T$  requirements. This leads to different limits on the maximum channel doping, and minimum oxide thickness for the various applications, leading to different minimum effective channel lengths ( $L_{min}$ ). Previous efforts on deriving scaling limits have many short comings. Most previous works on determining the device scaling limit do not consider application dependent limits [105], [106]. Frank [103] derived scaling limits for bulk SCI MOSFETs for various applications, but considered tunable workfunction gates only. The minimum channel length in [103] is mainly based on BTBT leakage considerations



at the drain-channel region.

In this chapter, different bulk MOSFETs - accumulation, retrograde doped SCI (RD-SCI), and uniformly doped SCI (UD-SCI) - will be considered while evaluating device scaling limits. Different application areas as well as different gate technologies will be considered. The scaling limits will be derived both from 2-D simulations and SCE models. Such an effort clarifies the advantage of various device types, and gate technologies, for different applications.

## ***9.2 Minimum Channel Length Determination***

Random variations in gate length (and hence effective channel length) is the limiting factor in device scaling. The  $3\sigma$  value of gate length is anywhere from 10-30% of the nominal value. The device with the worst-case on-current is one with a gate length of  $L_{nom} + 3\sigma$ , whereas the device with the worst-case off-current is one with a gate length of  $L_{nom} - 3\sigma$ . Both the reduction in on-current and increase in off-current will have to be considered when evaluating the nominal channel length for a given system. But for determining the minimum channel length, only the increase in off-current needs to be considered; the increased off-current will limit integration (i.e., the maximum number of devices on a die). The decreased on-current among longer-channel devices does not limit integration; it limits the maximum speed at which the system can operate, and this can be taken care of by tweaking  $V_{dd}$ ,  $V_T$ , and width of the devices.

There are a number of ways to determine the minimum channel length. Assuming a maximum of one-order of magnitude off-current increase (when channel length reduces from  $L_{nom}$  to  $L_{nom} - 3\sigma$ ), the maximum  $V_T$  shift is limited to 100 mV. This criterion is the one that is directly related to limits imposed on device design by integration requirements and process limits. Other criteria that can be used to quantify the minimum channel length are maximum allowable DIBL (usually less than 100 mV/V), maximum allowable subthreshold swing (usually less than 120 mV/dec), and maximum allowable  $V_T$  shift from the long-channel value. Note that these criteria are imposed on the nominal channel length device and are an indirect measure of the impact of integration requirements and process

limitations on device design.

Both 2-D simulations (with drift-diffusion transport), and SCE models are used to derive the minimum channel length. RD-SCI and accumulation devices are assumed to have a channel depth of 10 nm. For accumulation FETs, it is seen from Fig. 25 that for  $y_i > 15$  nm, the SCE limit is not satisfied for most channel doping. In case of RD-SCI FETs too, having a channel depth greater than about 15 nm will lead to a higher SCE. The RD-SCI FET is assumed to have a low-doped tub (with a doping of  $1 \times 10^{17} \text{ cm}^{-3}$  or less). From Fig. 24 it can be seen that a high  $N_D$  results in high process sensitivity, and thus  $dV_T/dy_i$  limits the maximum allowable  $N_D$ . Accumulation MOSFETs are assumed to have a maximum allowable channel doping ( $N_D$ ) of  $5 \times 10^{18} \text{ cm}^{-3}$ . All devices are assumed to have a source/drain junction depth of 12 nm with a  $5 \times 10^{20} \text{ cm}^{-3}$  doping. Poly-gate devices are assumed to have a poly-depletion of 0.2 nm [50]. The supply voltage is taken to be 1 V for all applications. All channel length values reported are effective values.

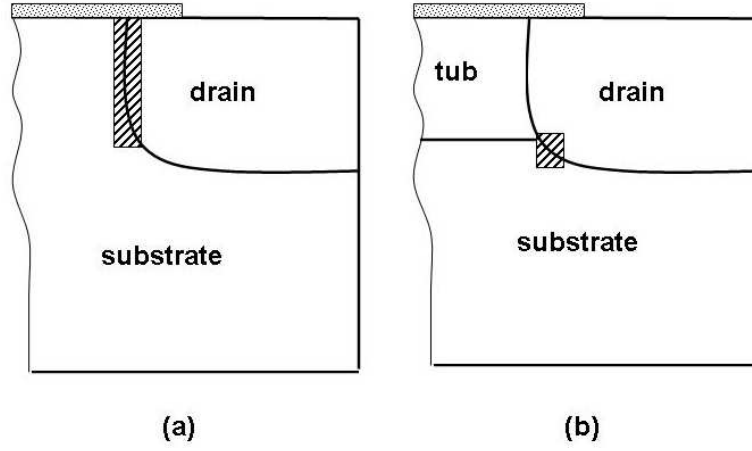
The following procedure is followed to obtain the minimum channel length.

- Based on BTBT leakage requirements at the drain-substrate region, the maximum allowable substrate doping is determined. BTBT leakage current is limited to 50% of the allowable subthreshold leakage current. In UD-SCI devices, BTBT leakage is assumed to occur over a 10 nm length, independent of channel length. In accumulation and RD-SCI devices, BTBT leakage is assumed to occur over a 2 nm length, independent of channel length, Fig. 54.
- The minimum allowable oxide thickness ( $t_{ox}|_{min}$ ) would need to be calculated based on the allowable gate leakage current ( $I_{gate}$ ). Assuming that hi-K dielectrics are possible in the future, the oxide thickness is assumed to be 10 Å for HiP and LOP applications. For LSTP applications using inversion devices, it is assumed to be 23 Å. For LSTP applications using accumulation MOSFETs,  $t_{ox}|_{min}$  is calculated using the gate-channel tunneling current model (Appendix E), by making  $I_{gate} < 0.1 I_{sub}$ .
- The gate workfunction is fixed to 4.63 eV for mid-bandgap metal gate FETs, to

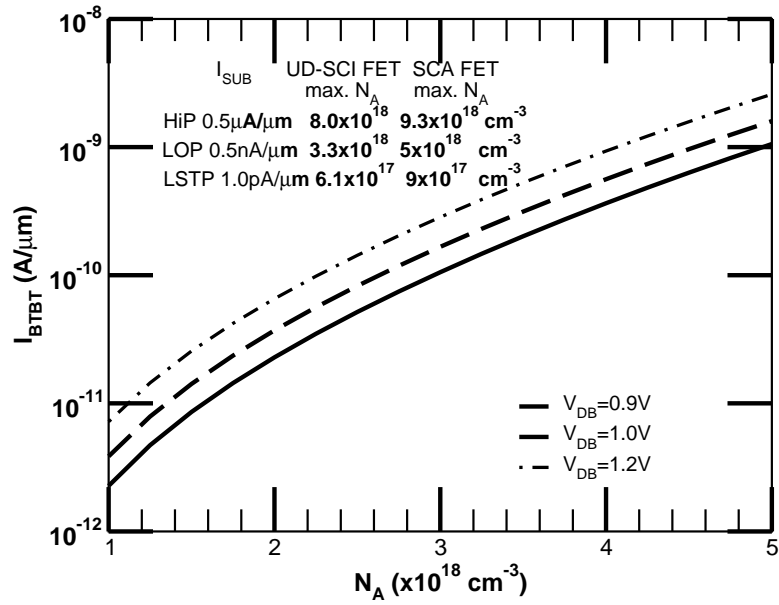
4.19 eV for poly-gate inversion n-FETs, and to 5.19 eV for poly-gate accumulation n-FETs. In case of tunable workfunction metal gates, the gate workfunction is assumed to be able to take on any value between 4 eV to 5.3 eV.

- The device with the highest substrate doping ( $N_A$ ) results in the lowest  $L_{min}$ . So, in case of tunable workfunction gates, all devices are assumed to have the highest allowable  $N_A$ .
- A device with the highest allowable  $N_A$  may not meet the  $V_T$  criterion. In case the  $V_T$  has to be increased, either  $L$  can be increased, or  $t_{ox}$  can be increased. In case  $V_T$  has to be decreased,  $N_A$  can be decreased or if the device is an accumulation FET,  $N_D$  (tub-doping) can be increased.
- Using 2-D numerical simulations, the minimum channel length that meets the SCE requirement ( $S < 110 \text{ mV/dec}$ ) is determined. The search can be done by a binary search.
- Using SCE models, the minimum channel length can be computed much faster than using 2-D simulations. From Fig. 7 it can be seen that  $V_T$  rolloff follows a universal curve. This curve shows that to achieve a  $V_T$  rolloff of less than 120 mV,  $L\lambda_{eq1}$  needs to be less than  $\pi$ . At this point, a 30% reduction in channel length results in about a 100 mV reduction in  $V_T$ . Thus, for  $\Delta V_T < 120 \text{ mV}$ , and  $\Delta V_T(30\%\delta L) < 100\text{mV}$ ,  $L_{min} = \pi/\lambda_{eq1}$ .  $V_T$  for the device with  $L = L_{min}$  is simply  $V_{T_{long}} - 0.12 \text{ V}$ .  $\lambda_{eq1}$  can be determined analytically from (10), and is a function of the minimum channel depletion depth, source/drain junction depth, and oxide thickness.

Using the BTBT leakage model described in section 7.2, the maximum allowable  $N_A$  is determined, Fig. 55. Tables 14-19 show the minimum channel lengths determined from both 2-D numerical simulations, and SCE models, for various gate technologies and applications. Table 20 shows  $L_{min}$  computed from both models and simulations. It can be seen that for tunable workfunction gates, inversion devices are always better than accumulation devices. For mid-bandgap metal gates, accumulation MOSFETs have a lower  $L_{min}$  than



**Figure 54:** BTBT leakage - the hatched area shows the BTBT leakage region: (a) UD-SCI MOSFET showing BTBT leakage over a 10 nm length; (b) accumulation and RD-SCI MOSFETs showing BTBT leakage over a 2 nm length.



**Figure 55:** Maximum allowable substrate doping ( $N_A|_{max}$ ) determined by BTBT leakage;  $N_A|_{max}$  for RD-SCI FETs is the same as that for accumulation FETs.

**Table 14:** Minimum channel length for bulk accumulation MOSFETs for various gate technologies, and applications (from 2-D simulations). The maximum subthreshold swing is limited to 110 mV/dec. The channel depth ( $y_i$ ) is assumed to be 10 nm. “Tun” refers to tunable workfunction metal gate.

application	gate WF (eV)	$I_{OFF}$ (nA/ $\mu m$ )	$V_T$ (V)	$S$ (mV/dec)	$N_A$ ( $cm^{-3}$ )	$N_D$ ( $cm^{-3}$ )	$t_{ox}$ (Å)	$L_{min}$ (nm)
HiP	4.63	300	0.05	110	$2.7 \times 10^{18}$	$5 \times 10^{18}$	10	34
LOP	4.63	2.0	0.30	112	$5 \times 10^{18}$	$1 \times 10^{17}$	10	25
LSTP	4.63	0.002	0.48	84	$9 \times 10^{17}$	$1 \times 10^{17}$	23	62
HiP	Tun	300	0.05	110	$9 \times 10^{18}$	$1 \times 10^{17}$	10	22
LOP	Tun	1.0	0.30	110	$5 \times 10^{18}$	$1 \times 10^{17}$	10	25
LSTP	Tun	0.001	0.50	110	$9 \times 10^{17}$	$1 \times 10^{17}$	23	43
HiP	5.19	600	0.02	110	$1 \times 10^{17}$	$5 \times 10^{18}$	12	80
LOP	5.19	2.0	0.31	110	$7 \times 10^{17}$	$5 \times 10^{18}$	12	53
LSTP	5.19	0.0008	0.71	111	$9 \times 10^{17}$	$1 \times 10^{17}$	12	40

inversion MOSFETs for HiP and LOP applications. For poly-gate applications, accumulation MOSFETs show better performance for LSTP applications. These  $L_{min}$  advantages mirror the findings on accumulation MOSFET performance advantage in chapters VI-VIII.

### 9.3 Summary

The minimum effective channel length,  $L_{min}$ , has been derived for different gate technologies and applications. BTBT leakage at the drain-substrate region limits the maximum allowable  $N_A$ . Gate tunneling leakage limits the minimum allowable oxide thickness. Based on physical models, the maximum allowable  $N_A$ , and the minimum allowable  $t_{ox}$  have been quantified for various applications, and device types. Using SCE models,  $L_{min}$  is found to be  $\pi/\lambda_{eq1}$ .  $L_{min}$  found using the models agrees well with that found using 2-D simulations. Accumulation MOSFETs show a lower  $L_{min}$  than inversion MOSFETs for three applications: mid-bandgap metal gate HiP, mid-bandgap metal gate LOP, and poly-gate LSTP applications.

**Table 15:** Minimum channel length for bulk RD-SCI MOSFETs for various gate technologies, and applications (from 2-D simulations). The maximum subthreshold swing is limited to 110 mV/dec. The channel depth ( $y_i$ ) is assumed to be 10 nm. “Tun” refers to tunable workfunction metal gate.

application	gate WF (eV)	$I_{OFF}$ (nA/ $\mu m$ )	$V_T$ (V)	$S$ (mV/dec)	$N_A$ ( $cm^{-3}$ )	$N_D$ ( $cm^{-3}$ )	$t_{ox}$ (Å)	$L_{min}$ (nm)
HiP	4.63	500	0.05	202	$1 \times 10^{16}$	$1 \times 10^{16}$	10	100
LOP	4.63	2.0	0.30	112	$4.5 \times 10^{18}$	$1 \times 10^{17}$	10	28
LSTP	4.63	0.002	0.51	84	$9 \times 10^{17}$	$1 \times 10^{17}$	23	60
HiP	Tun	300	0.05	110	$9 \times 10^{18}$	$1 \times 10^{17}$	10	21
LOP	Tun	1.0	0.30	110	$5 \times 10^{18}$	$1 \times 10^{17}$	10	24
LSTP	Tun	0.001	0.50	110	$9 \times 10^{17}$	$1 \times 10^{17}$	23	42
HiP	4.19	300	0.04	88	$9 \times 10^{18}$	$1 \times 10^{17}$	14	28
LOP	4.19	2.0	0.21	83	$5 \times 10^{18}$	$1 \times 10^{17}$	18	50
LSTP	4.19	0.001	0.50	110	$9 \times 10^{17}$	$1 \times 10^{17}$	67	82

**Table 16:** Minimum channel length for bulk UD-SCI MOSFETs for various gate technologies, and applications (from 2-D simulations). The maximum subthreshold swing is limited to 110 mV/dec. “Tun” refers to tunable workfunction metal gate.

application	gate WF (eV)	$I_{OFF}$ (nA/ $\mu m$ )	$V_T$ (V)	$S$ (mV/dec)	$N_A$ ( $cm^{-3}$ )	$t_{ox}$ (Å)	$L_{min}$ (nm)
HiP	4.63	500	0.05	202	$1 \times 10^{16}$	10	100
LOP	4.63	2.0	0.32	110	$9 \times 10^{17}$	10	36
LSTP	4.63	0.002	0.48	85	$6 \times 10^{17}$	23	60
HiP	Tun	500	0.05	110	$8 \times 10^{18}$	12	16
LOP	Tun	1.0	0.30	110	$3 \times 10^{18}$	12	23
LSTP	Tun	0.001	0.50	110	$6 \times 10^{17}$	23	42
HiP	4.19	500	0.05	104	$6 \times 10^{18}$	12	20
LOP	4.19	1.0	0.30	110	$3 \times 10^{18}$	25	33
LSTP	4.19	0.001	0.52	108	$6 \times 10^{17}$	70	86

**Table 17:** Minimum channel length for bulk accumulation MOSFETs for various gate technologies, and applications (from SCE models). The maximum  $V_T$  rolloff is limited to 120 mV. “Tun” refers to tunable workfunction metal gate.

application	gate WF (eV)	$V_T$ (V)	$N_A$ ( $cm^{-3}$ )	$N_D$ ( $cm^{-3}$ )	yi (nm)	$t_{ox}$ (Å)	$L_{min}$ (nm)
HiP	4.63	0.05	$2.7 \times 10^{18}$	$5 \times 10^{18}$	10	10	36
LOP	4.63	0.30	$5 \times 10^{18}$	$1 \times 10^{17}$	10	10	26
LSTP	4.63	0.50	$9 \times 10^{17}$	$1 \times 10^{17}$	10	39	74
HiP	Tun	0.05	$9 \times 10^{18}$	$1 \times 10^{17}$	10	10	23
LOP	Tun	0.30	$5 \times 10^{18}$	$1 \times 10^{17}$	10	10	26
LSTP	Tun	0.50	$9 \times 10^{17}$	$1 \times 10^{17}$	10	23	62
HiP	5.19	0.07	$1 \times 10^{17}$	$5 \times 10^{18}$	10	12	130
LOP	5.19	0.31	$4 \times 10^{17}$	$5 \times 10^{18}$	10	12	74
LSTP	5.19	0.73	$9 \times 10^{17}$	$1 \times 10^{17}$	10	12	48

**Table 18:** Minimum channel length for bulk RD-SCI MOSFETs for various gate technologies, and applications (from SCE models). The maximum  $V_T$  rolloff is limited to 120 mV. “Tun” refers to tunable workfunction metal gate.

application	gate WF (eV)	$V_T$ (V)	$N_A$ ( $cm^{-3}$ )	$N_D$ ( $cm^{-3}$ )	yi (nm)	$t_{ox}$ (Å)	$L_{min}$ (nm)
HiP	4.63	0.05	$5 \times 10^{16}$	$5 \times 10^{16}$	10	10	157
LOP	4.63	0.30	$2.5 \times 10^{18}$	$1 \times 10^{17}$	10	10	32
LSTP	4.63	0.50	$9 \times 10^{17}$	$1 \times 10^{17}$	10	33	67
HiP	Tun	0.05	$9 \times 10^{18}$	$1 \times 10^{17}$	10	10	23
LOP	Tun	0.30	$5 \times 10^{18}$	$1 \times 10^{17}$	10	10	26
LSTP	Tun	0.50	$9 \times 10^{17}$	$1 \times 10^{17}$	10	23	62
HiP	4.19	0.05	$9 \times 10^{18}$	$1 \times 10^{17}$	10	14	26
LOP	4.19	0.30	$5 \times 10^{18}$	$1 \times 10^{17}$	10	28	38
LSTP	4.19	0.50	$9 \times 10^{17}$	$1 \times 10^{17}$	10	70	105

**Table 19:** Minimum channel length for bulk UD-SCI MOSFETs for various gate technologies, and applications (from SCE models). The maximum  $V_T$  rolloff is limited to 120 mV. “Tun” refers to tunable workfunction metal gate.

application	gate WF (eV)	$V_T$ (V)	$N_A$ ( $cm^{-3}$ )	$t_{ox}$ (Å)	$L_{min}$ (nm)
HiP	4.63	0.05	$5 \times 10^{16}$	10	157
LOP	4.63	0.30	$1.5 \times 10^{18}$	10	36
LSTP	4.63	0.50	$6 \times 10^{17}$	33	76
HiP	Tun	0.05	$8 \times 10^{18}$	10	20
LOP	Tun	0.30	$3 \times 10^{18}$	10	27
LSTP	Tun	0.50	$6 \times 10^{17}$	23	70
HiP	4.19	0.05	$3.5 \times 10^{18}$	12	28
LOP	4.19	0.30	$3 \times 10^{18}$	21	38
LSTP	4.19	0.50	$6 \times 10^{17}$	70	119

**Table 20:** Minimum channel length for various FET types, gate technologies, and applications - comparison between 2-D simulations and models. In the 2-D simulations, the maximum subthreshold swing is limited to 110 mV/dec. In the models, the maximum  $V_T$  rolloff is limited to 120 mV. The channel depth ( $y_i$ ) is assumed to be 10 nm for accumulation and RD-SCI MOSFETs. All channel length values are in nanometres.

Gate type		Ioff (nA/um)	Vt (V)	Accum. FET Sim. Models	RD-SCI FET Sim. Models	UD-SCI FET Sim. Models
mid band gap	HiP	500	0.05	34 36	>100 157	>100 157
	LOP	1	0.3	25 26	28 32	36 36
	LSTP	0.001	0.5	62 74	60 67	60 76
tunable metal gate	HiP	500	0.05	22 23	21 23	16 20
	LOP	1	0.3	25 26	24 26	23 27
	LSTP	0.001	0.5	43 62	42 62	42 70
poly gate	HiP	500	0.05	80 130	28 26	20 28
	LOP	1	0.3	53 74	50 38	33 38
	LSTP	0.001	0.5	40 48	82 105	86 119



## CHAPTER X

### CONCLUSIONS

The primary objective of the current research has been to comprehensively compare accumulation and inversion bulk FETs, and find application areas where each is superior. To provide clear physical insight, physically based models for short channel effect (SCE) and related phenomena were derived. Both SCE models and 2-D numerical simulations are used to perform the comparison, and to project the minimum channel length ( $L_{min}$ ).

- Threshold voltage models were derived that can accurately predict the impact of source/drain junction depth. A junction depth dependent characteristic length was derived that can be used to rapidly assess the impact of junction depth scaling on  $V_T$ .
- It was shown that existing theory does not correctly model long-channel  $V_T$  of accumulation MOSFETs. A simple modification was proposed that is accurate over a wide range of channel depths and doping.
- Subthreshold swing (S) rollup is modeled using the volume inversion approach. Using the models for  $V_T$  and S, a subthreshold conduction model is derived based on the Swanson-Meindl approach.
- A circuit simulation methodology is developed that can simulate both inversion and accumulation FET inverter chains, and is found to be accurate over a wide range of supply voltages. The simulation methodology can be used for rapid technology optimization, and performance prediction.
- Design guidelines for accumulation MOSFET design are proposed. Surface channel operation is stressed; buried channel operation not only results in increased SCE, but also high dopant fluctuation effects, and process sensitivity. Based on 2-D theory, the SCA/BCA boundary is derived. It is shown that an SCA FET at long channel lengths

can operate as a BCA FET at shorter channel lengths.

- A  $y_i$  (tub-depth) vs.  $N_D$  (tub-doping) design plane for accumulation MOSFETs is introduced. At lower  $N_D$ , the allowable design space is limited by  $V_T$  rolloff requirements, whereas at higher  $N_D$ , it is limited by process sensitivity requirements.
- The relative advantages of accumulation MOSFETs over inversion MOSFETs is found to be gate-technology dependent, and also application dependent. Three different gate technologies are considered while comparing accumulation and inversion MOSFETs: tunable metal gate, mid-bandgap metal gate, and dual poly gate. Three different application areas (as recommended by ITRS) are considered: hi performance (HiP), low operating power (LOP), and low standby power (LSTP). The off-current and  $V_T$  requirements for the various applications are shown in Table 1.
- The accumulation FET has an increased depletion depth compared to a similarly doped inversion FET. For long channel operation, this results in the Fermi-FET being the device with the minimum subthreshold swing. For short channel operation, this results in increased SCE in accumulation FETs. Thus, for tunable workfunction gates, inversion FETs have better SCE control than accumulation FETs.
- In case of mid-bandgap metal gate, accumulation FETs perform better than inversion devices for HiP and LOP applications. Accumulation devices have a lower SCE, and lower QM  $V_T$  shift compared to inversion devices. Full-band Monte Carlo simulations show that at  $L_{eff} = 30 \text{ nm}$ , the accumulation MOSFET can achieve a 30-40% better on-current than an inversion MOSFET with a comparable SCE.
- In case of dual poly applications, accumulation MOSFETs perform better than inversion MOSFETs for LSTP applications; because of a higher tunneling barrier, accumulation n-MOSFETs have orders of magnitude lower gate tunneling current compared to inversion n-MOSFETs. Thus, accumulation n-FETs can use a thinner oxide, and thereby achieve better performance than inversion n-MOSFETs. Also, BTBT leakage at the drain-substrate junction is much lower in case of accumulation MOSFETs.

This results in a higher allowable substrate doping, and thus better SCE control.

- $L_{min}$  for accumulation and inversion MOSFETs was projected using both SCE models and 2-D simulations. For HiP applications with mid-bandgap metal gate, accumulation FETs provide more than four generations of further scaling compared to inversion FETs. The corresponding numbers for LOP with mid-bandgap gate, and LSTP with poly gate are one-half generation, and two generations respectively.

### ***10.1 Future Work Recommendations***

- This work did not include compact modeling of SCE in halo-doped MOSFETs. Halo-doped MOSFETs are widely used for better control of SCE, and thus need to be modeled accurately. Existing  $V_T$  models for halo-FETs are either parameter fit [61], or quasi-physical [58]; none of the existing models can predict the impact of source/drain junction depth on  $V_T$ .
- SOI structures were not considered in this work. The results presented in this work are equally applicable to partially depleted (PD) SOI structures. Fully depleted (FD) SOI accumulation FETs need to be compared with FD-SOI inversion MOSFETs for possible advantages.
- Accumulation MOSFETs have a higher  $g_m$  (transconductance), and thus perform better than inversion MOSFETs for many analog applications. This needs to be more thoroughly explored by actual circuit simulations.
- Accumulation MOSFETs have a lower  $1/f$  noise compared to inversion MOSFETs. This aspect was not considered in this work since the emphasis was mostly on digital applications.

## APPENDIX A

### THRESHOLD VOLTAGE MODEL FOR DEVICES WITH A DEEP TUB OR HIGH SCE

In Chapter 2,  $V_T$  rolloff is derived by assuming a single term solution for  $\phi(x, y)$ . The single term solution approximation for deriving a compact model for  $V_T$  rolloff works well only when  $\Delta V_T < 200 \text{ mV}$ . To accurately model high SCE devices, two additional factors need to be considered: a multiple term solution would have to be used for evaluating the 2-D potential (since the higher order terms become comparable to the first term in the expansion for  $\phi(x, y)$ ), and subthreshold current is no more determined by just the carrier concentration at the minimum potential point.

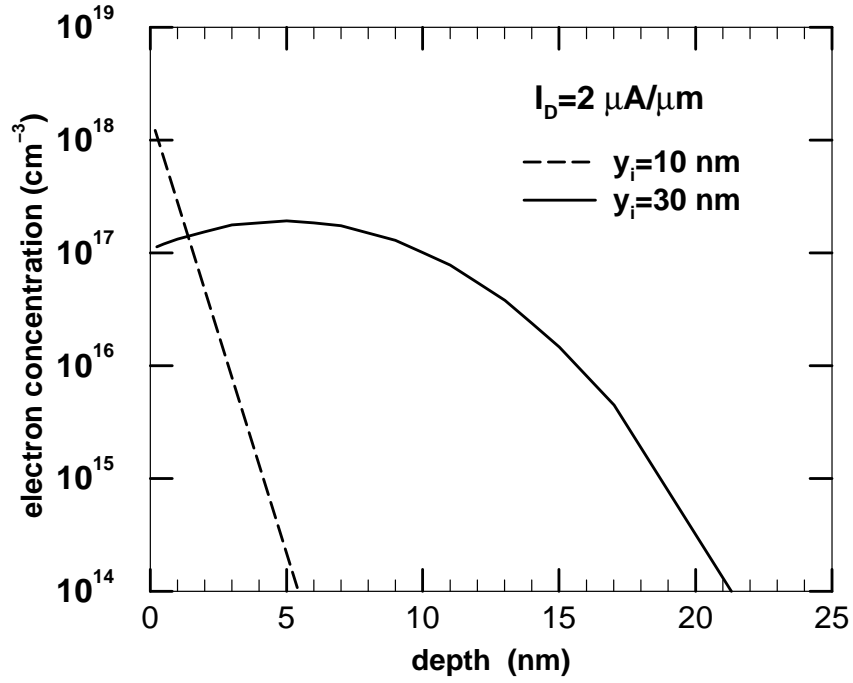
While deriving the long channel  $V_T$  of accumulation MOSFETs in section 2.2.2, it was assumed that  $V_T$  is determined by the minimum potential point. In reality, as the tub-depth increases in an accumulation MOSFET, the device tends to become buried channel type, and the electrons spread somewhat uniformly in a 5-10 nm range around the minimum potential point, Fig. 56. Thus, an integration of electron concentration in the depth direction would be needed to accurately determine  $V_T$  of accumulation devices with a deep tub. It can be seen from Fig. 14 that as channel length is reduced with all other parameters remaining constant, the inversion layer thickness increases even with the classical distribution (i.e. without including the quantum centroid shift). Thus, for devices with very high SCE,  $V_T$  would have to be determined by integrating the electron concentration in the depth direction. The drain current using the integration approach is

$$I \propto \int_0^d n_i \cdot e^{(\psi(x_m, y) - \phi_{Fn})/kT} dy \quad (48)$$

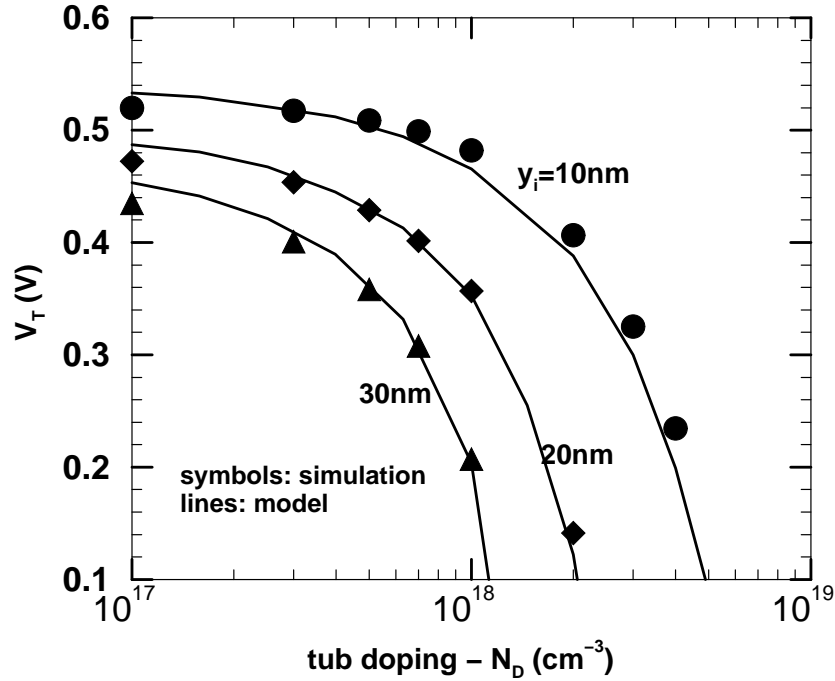
$x_m$  is the x-coordinate of the minimum potential point, and  $\phi_{Fn}$  is the electron quasi-Fermi level. It has been established from 2-D MEDICI simulations that the difference between the electron quasi-Fermi level and the bulk Fermi level is about 15 mV for a moderately doped

substrate ( $N_A > 1 \times 10^{17} \text{ cm}^{-3}$ ), for both high and low drain voltages. So  $\phi_{Fn}$  in (48) is taken to be  $\phi_F$ , the bulk Fermi level; as will be seen later, this approximation introduces little error in the calculation of  $V_T$  rolloff and DIBL. Let the right hand side of (48) be denoted by  $Q_i$ , the inversion areal charge density (IACD). The threshold voltage is determined as the gate voltage at which  $Q_i$  reaches a certain density, and thus the model is labeled constant inversion areal charge density (CIACD) model. Let  $Q_{T_i}$  be the threshold IACD. From studying a handful of long-channel devices,  $Q_{T_i}$  is determined to be  $1.8 \times 10^{11} \text{ cm}^{-2}$ .

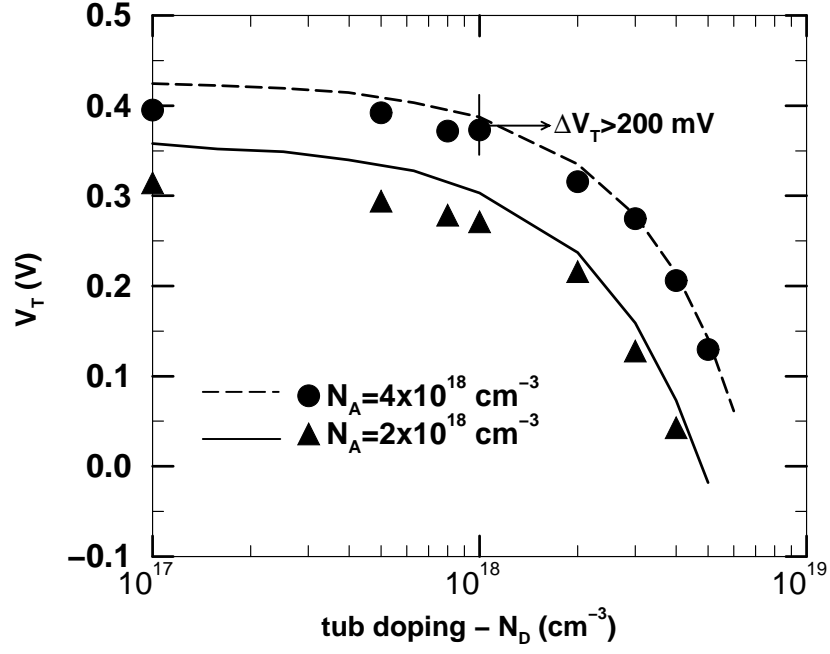
Fig. 57 shows threshold voltage vs. tub-doping for long channel MOSFETs. Only a single term solution is used to calculate  $\psi(x_m, y)$  in all the graphs shown in this appendix. The CIACD model is seen to give a good match with 2-D simulations for a wide range of tub-depth and tub-doping. From Fig. 11 it can be seen that the compact model starts diverging from simulations for high  $y_i$ , whereas the CIACD model is accurate even for high  $y_i$ . Fig. 58 shows the CIACD model vs. 2-D simulations for a short channel device. Also shown is the point where  $\Delta V_T$  becomes greater than 200 mV, for  $N_A = 4 \times 10^{18} \text{ cm}^{-3}$ . The CIACD model is able to predict  $V_T$  rolloff accurately for devices with  $\Delta V_T$  as high as 400 mV. Fig. 59 shows threshold voltage vs. tub-depth for a short channel device, this time on a  $V_T - y_i$  plane. Once again, the CIACD model works well for high SCE devices. The compact model is clearly limited to devices with  $\Delta V_T < 200 \text{ mV}$ . The disadvantage of using the CIACD model is that it takes more time (5X-10X) than the compact model to evaluate  $\Delta V_T$ . But the time taken by the CIACD model is still far less than the time taken by a 2-D simulator to evaluate  $\Delta V_T$ .



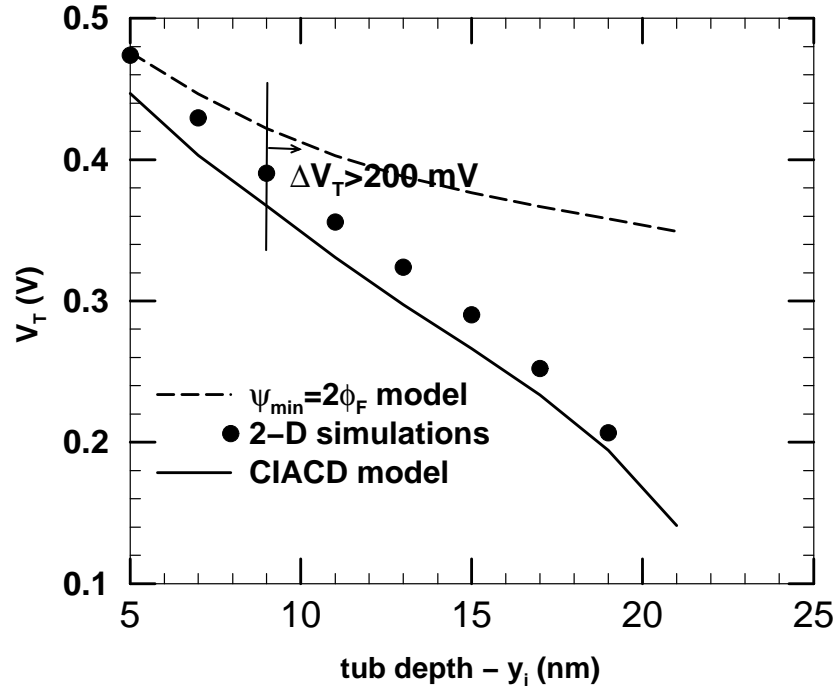
**Figure 56:** Carrier concentration in the middle of the channel in long channel accumulation MOSFETs (from 2-D drift-diffusion simulations);  $L = 200 \text{ nm}$ ,  $V_{DS} = 0.05 \text{ V}$ ,  $N_A = 1 \times 10^{18} \text{ cm}^{-3}$ ,  $N_D = 1 \times 10^{18} \text{ cm}^{-3}$ , and  $t_{ox} = 1 \text{ nm}$ . The gate workfunction of the devices are adjusted so that both devices have the same drain current of  $2 \text{ } \mu\text{A}/\mu\text{m}$  for  $V_{GS} = 0.5 \text{ V}$ .



**Figure 57:** Long channel  $V_T$  of accumulation MOSFETs: CIACD model vs. simulations;  $N_A = 1 \times 10^{18} \text{ cm}^{-3}$ , and  $t_{ox} = 1.5 \text{ nm}$ .



**Figure 58:** Short channel  $V_T$  of accumulation MOSFETs: CIACD model vs. simulations;  $L = 30 \text{ nm}$ ,  $t_{ox} = 10 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ ,  $y_i = 10 \text{ nm}$ , and gate workfunction is 4.63 eV.



**Figure 59:** Short channel  $V_T$  of accumulation MOSFETs: CIACD model vs. simulations;  $L = 30 \text{ nm}$ ,  $t_{ox} = 10 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ ,  $N_A = 4 \times 10^{18} \text{ cm}^{-3}$ ,  $N_D = 1 \times 10^{18} \text{ cm}^{-3}$ , and gate workfunction is 4.63 eV.

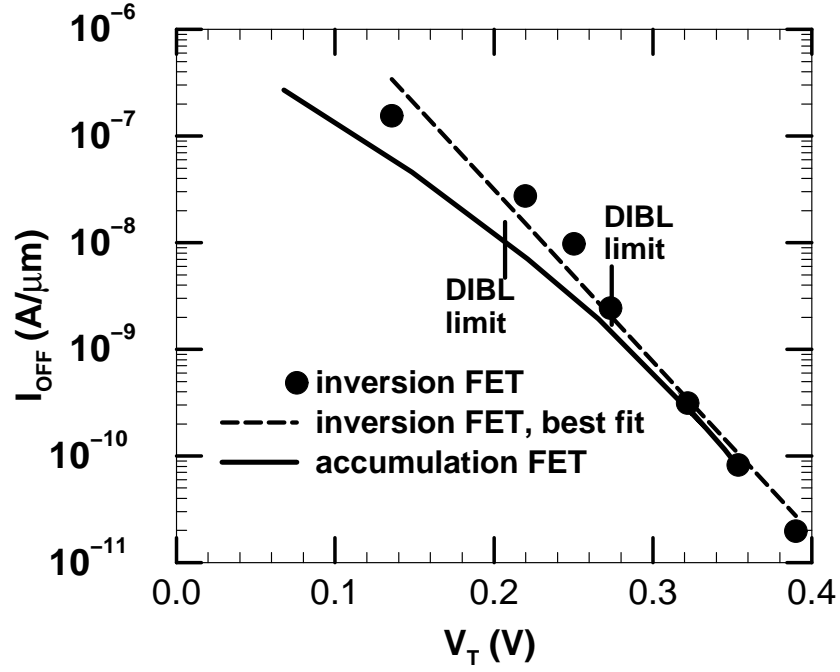
## APPENDIX B

### MID-BAND METAL GATE MOSFETS

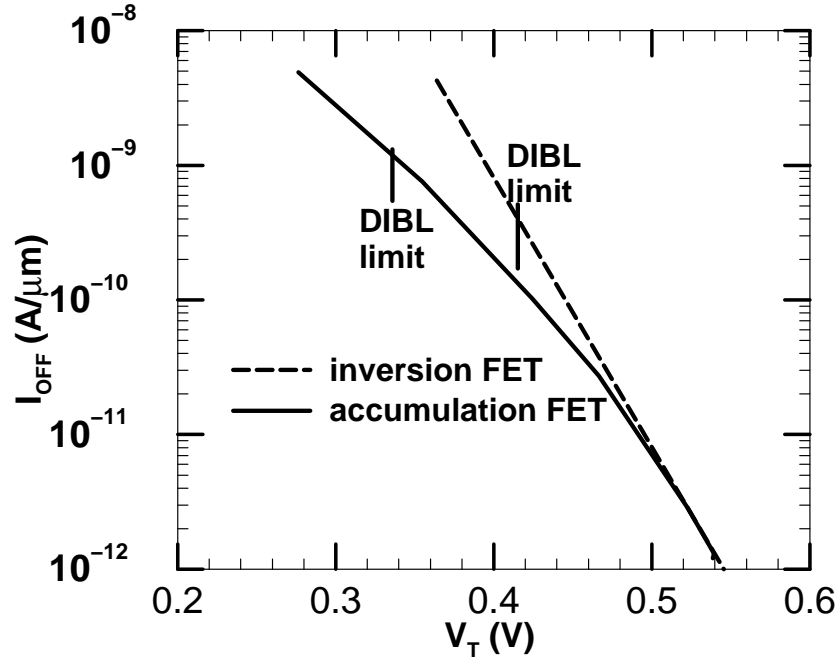
Additional comparisons between mid-band metal gate accumulation and inversion MOSFETs are provided in this appendix. Fig. 60 shows off-current vs. threshold voltage for  $L = 30 \text{ nm}$  n-MOSFETs. Both RD-SCI and UD-SCI MOSFETs are considered while evaluating inversion FETs. For  $V_T < 0.3 \text{ V}$ , accumulation MOSFETs show a better performance than inversion MOSFETs in terms of a better off-current for a given threshold voltage. DIBL limits the minimum achievable  $V_T$  of inversion n-MOSFETs to 0.3 V and that of accumulation n-MOSFETs to 0.2 V. Fig. 61 shows off-current vs. threshold voltage for  $L = 30 \text{ nm}$  p-MOSFETs. Accumulation MOSFETs are seen to perform better than inversion MOSFETs for  $V_T < 0.45 \text{ V}$ . DIBL limits the minimum achievable  $V_T$  of inversion p-MOSFETs to 0.4 V, and that of accumulation p-MOSFETs to 0.3 V.

Fig. 62 shows off-current vs. on-current for accumulation and inversion n-MOSFETs. Poly-gate inversion MOSFETs are assumed to have a poly-doping of  $5 \times 10^{19} \text{ cm}^{-3}$ . Mid-band metal gate accumulation MOSFETs are seen to have a better on-current (for a given off-current) than either mid-band metal-gate or poly-gate inversion MOSFETs.

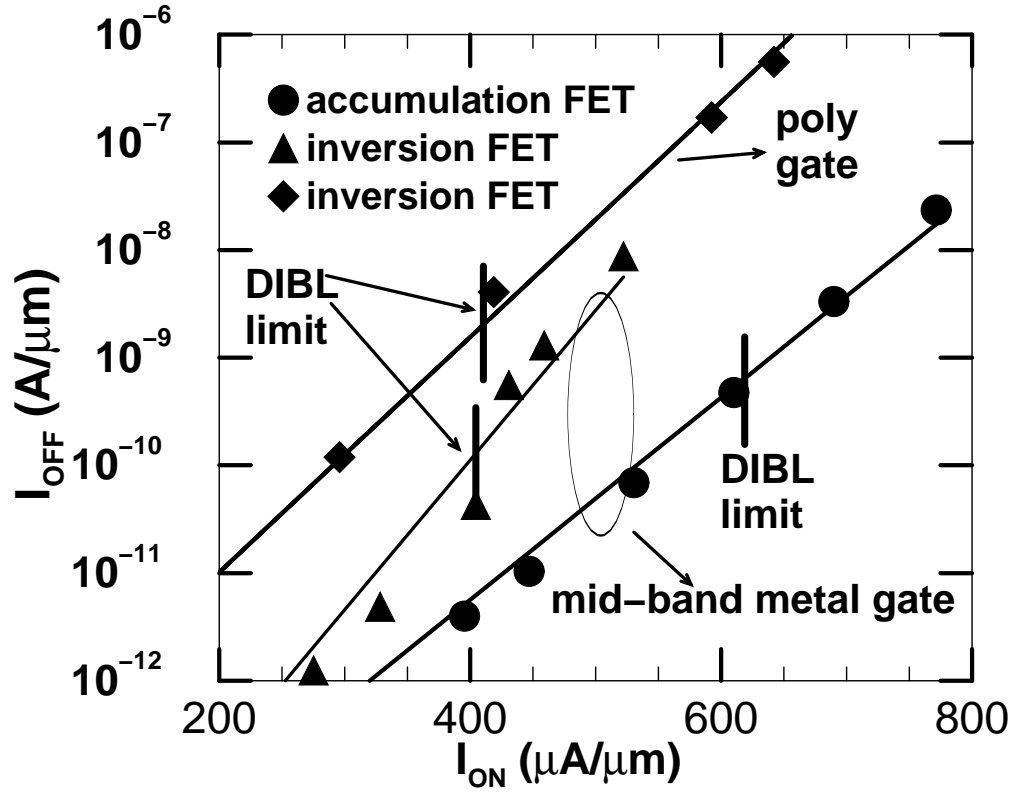




**Figure 60:** Off-current vs. threshold voltage for n-MOSFETs (from 2-D classical DD simulations).  $L = 30 \text{ nm}$ ,  $t_{ox} = 10 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ , and gate workfunction is 4.63 eV. For accumulation MOSFETs,  $N_A = 4 \times 10^{18} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ . The DIBL limit is taken to be 100 mV/V.



**Figure 61:** Off-current vs. threshold voltage for p-MOSFETs (from 2-D classical DD simulations).  $L = 30 \text{ nm}$ ,  $t_{ox} = 10 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ ,  $V_{dd} = 1.0 \text{ V}$ , and gate workfunction is 4.63 eV. For accumulation MOSFETs,  $N_A = 4 \times 10^{18} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ . The DIBL limit is taken to be 150 mV/V.



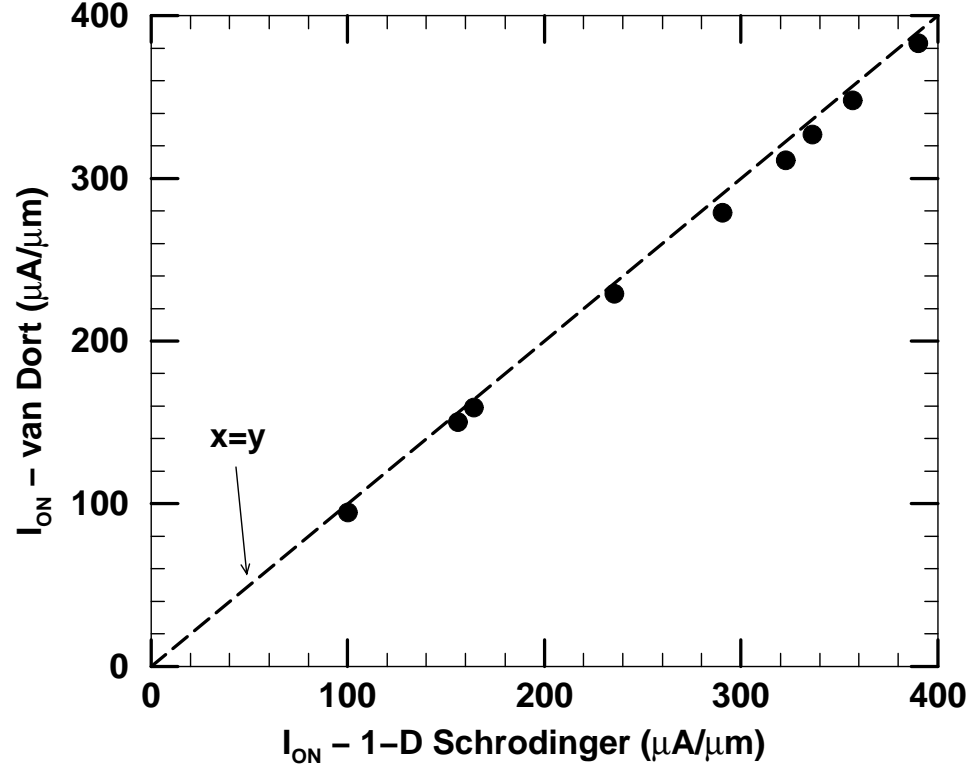
**Figure 62:** Off-current vs. on-current for n-MOSFETs (from 2-D DD simulations including QM  $V_T$  shift);  $L = 30 \text{ nm}$ ,  $t_{ox} = 10 \text{ \AA}$ ,  $y_j = 12 \text{ nm}$ , and  $V_{dd} = 1.0 \text{ V}$ ; the gate workfunction is 4.63 eV for mid-band metal gate MOSFETs, and 4.19 eV for poly gate inversion MOSFETs. For accumulation MOSFETs,  $N_A = 4 \times 10^{18} \text{ cm}^{-3}$ , and  $y_i = 10 \text{ nm}$ . Symbols indicate data points and lines indicate best fit. The DIBL limit is taken to be 100 mV/V.

## APPENDIX C

### QUANTUM CORRECTION FOR $V_T$ IN SIMULATIONS

Device simulators provide the user with a variety of options to include quantum mechanical (QM)  $V_T$  shift in simulations. These include 1-D Schrödinger-Poisson solution coupled to 2-D Poisson solution, the density gradient method, and the van Dort method [87]. The 1-D Schrödinger solution is the most accurate among the three. But simulations using it tend to be slow, and often lead to convergence problems. The van Dort method is less physical, but leads to fast convergence. The density gradient method is numerically robust but needs a lot of calibration effort for the mobility and recombination-generation models.

In this work, van Dort correction is used to include QM effects. Fig. 63 shows a comparison of on-current output from van-Dort and 1-D Schrödinger solutions. It can be seen that the two agree over a wide range of on-current. This confirms that van Dort method is an accurate way of including quantum mechanical  $V_T$  shift in 2-D device simulations.



**Figure 63:** Comparison of on-current from 1-D Schrödinger and van Dort methods. The devices are inversion type, and have various channel and substrate doping. Symbols indicate data points, and the dashed line is the “ $x = y$ ” line.  $L = 45 \text{ nm}$ ,  $t_{ox} = 15 \text{ Å}$ ,  $y_j = 12 \text{ nm}$ , and  $V_{dd} = 1.0 \text{ V}$ .

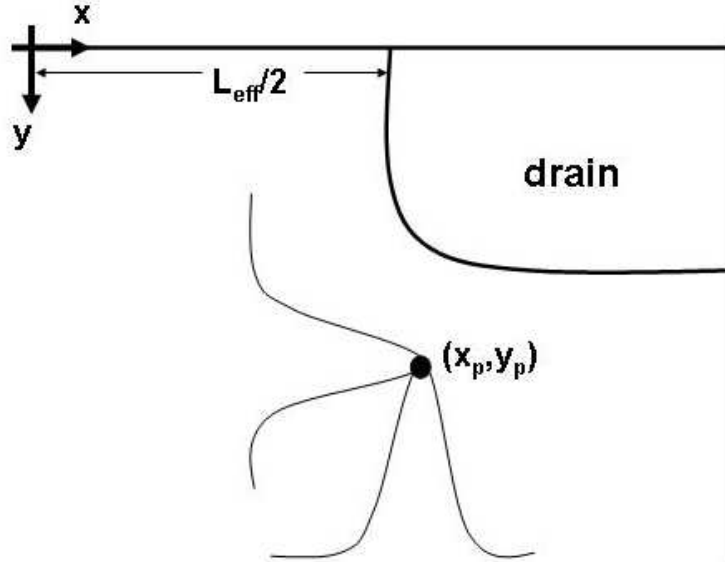
## APPENDIX D

### HALO PROFILE DESCRIPTION

Halo-doped devices used in this work use analytical formulae to generate the halo profiles. Source and drain halos are symmetrical, and are generated by a product of two Gaussian functions [107]. Suppose  $(x_p, y_p)$  is the co-ordinate of the peak halo doping, Fig. 64. Let  $N_p$  be the peak halo doping. Then the drain-halo is generated by

$$f(x, y) = N_p \cdot \exp\left(\frac{x - x_p}{\sigma_x}\right) \cdot \exp\left(\frac{y - y_p}{\sigma_y}\right) \quad (49)$$

The origin of the co-ordinate system is assumed to be in the middle of the channel, at the Si – SiO<sub>2</sub> interface. For the 30 nm channel length MOSFETs considered in chapter VIII, the halo parameters are as follows:  $x_p = L_{eff}/2 + 5$ ,  $y_p = 22$ ,  $N_p = 1 \times 10^{19} \text{ cm}^{-3}$ ,  $\sigma_x = 4$ , and  $\sigma_y = 3.4$ .  $x$ ,  $y$ , and  $\sigma$  values are in nanometres.



**Figure 64:** Halo-doping at the drain-end of a MOSFET. Two 1-D Gaussian functions are superposed to obtain the halo doping, with the peak doping being  $N_p$ , at  $(x_p, y_p)$ .

## APPENDIX E

### GATE TUNNELING MODEL

The gate tunneling model from [92] is used in this work. The model is physically based and uses no fitting parameters. The model can be easily modified to include accumulation devices. The gate tunneling current density is calculated by multiplying the electron density and the tunneling probability at the Si – SiO<sub>2</sub> interface [92]. Since the potential profiles of accumulation and inversion devices are different, the tunneling probabilities too are different. The tunneling probability is given as

$$D(E_x) = \exp\left(-\gamma\sqrt{E_B - E_x}\right) \quad (50)$$

where  $\gamma$  is  $4\pi t_{ox}\sqrt{2m_{ox}}/h$ .  $E_B$  is the barrier height, and  $E_x$  is the electron energy.  $t_{ox}$  is the physical oxide thickness, and  $m_{ox} = 0.32m_0$  is the effective electron mass in the oxide. The barrier height is approximated by a rectangular barrier.

$$E_B = q\left(3.1 - \frac{V_{ox}}{2}\right) \quad (51)$$

$V_{ox}$  is the voltage drop across the oxide layer, and it is positive when the field points into the oxide (looking from the top of the Si – SiO<sub>2</sub> interface). When the field points out of the oxide, electrons no longer experience an attractive force towards the Si – SiO<sub>2</sub> interface, and  $V_{ox}$  is then negative.

The gate tunneling density is given as

$$J_{tunnel} = \frac{4\pi m^* q}{h^3} (kT)^2 \left(1 + \frac{\gamma kT}{q\sqrt{E_B}}\right) \exp\left(\frac{q\phi_S - q\phi_F - E_G/2}{kT}\right) \exp\left(-\gamma\sqrt{E_B}\right) \quad (52)$$

where,

$m^* = 0.19m_0$  is the electron transverse mass

$\phi_S$  is the surface potential

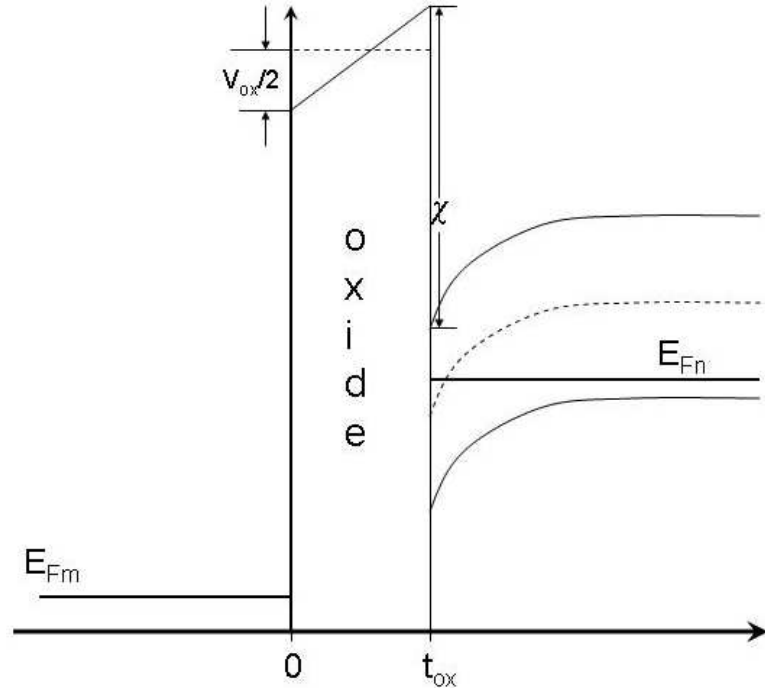
$\phi_F$  is the Fermi level in the bulk

$E_G$  is the Si bandgap energy

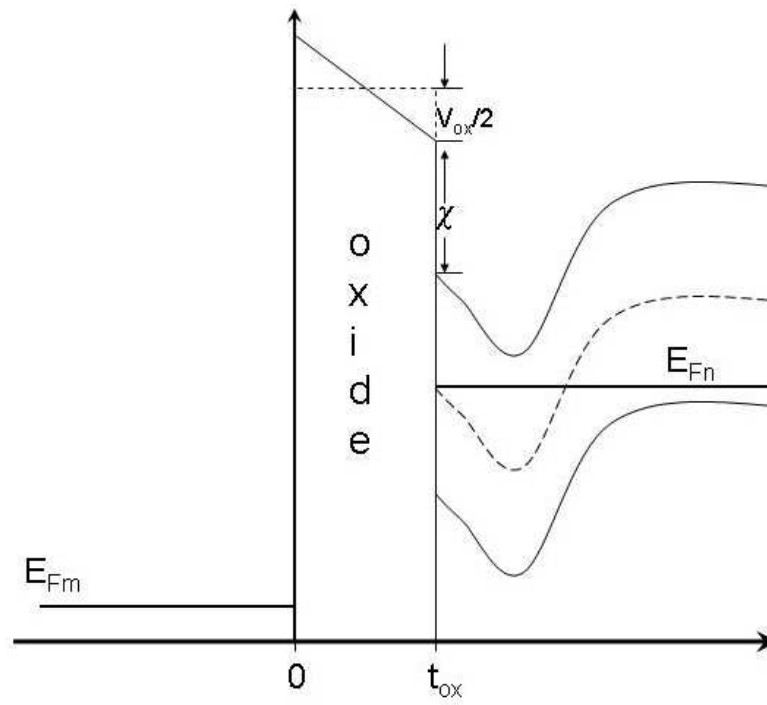
$k$  is Boltzmann's constant

$T$  is the temperature in °K

In case of buried channel MOSFETs, the barrier for gate-channel electron tunneling is higher compared to inversion devices, Figs. 65 and 66; this results in orders or magnitude lower gate tunneling current in BCA FETs.



**Figure 65:** Band-diagram for an inversion device in moderate-inversion regime.



**Figure 66:** Band-diagram for an accumulation device in moderate-conduction regime.



## APPENDIX F

### HYDRO-DYNAMIC MODELS

The simulator DESSIS is used for all hydro-dynamic simulations reported in this work. In DESSIS [67], the set of equations solved for electrons in the hydro-dynamic approach is

$$\vec{J}_n = \mu_n \left( n \nabla E_C + k_B T_n \nabla n + f_n^{td} k_B n \nabla T_n - 1.5 n k_B T_n \nabla \ln m_E \right) \quad (53)$$

$$\frac{\partial W_n}{\partial t} + \nabla \cdot \vec{S}_n = \vec{J}_n \cdot \nabla E_C + \left. \frac{dW_n}{dt} \right|_{coll} \quad (54)$$

$$\vec{S}_n = -\frac{5r_n}{2} \left( \frac{k_B T_n}{q} \vec{J}_n + f_n^{hf} \hat{\kappa}_n \nabla T_n \right) \quad (55)$$

$$S_L = -\kappa_L \nabla T_L \quad (56)$$

where  $\hat{\kappa}_n = \frac{k_B^2}{q} n \mu_n T_n$ .  $T_n$  is the electron temperature,  $E_C$  is the conduction band energy,  $n$  is the electron concentration, and  $m_E$  is the effective electron mass.  $r_n$ ,  $f_n^{td}$ , and  $f_n^{hf}$  are the energy flux, thermal diffusion, and heat flux parameters respectively. They are fixed at the default values of 0.6, 0 and 1 respectively, which correspond to Stratton's [108] energy balance formulation. A similar set of equations can be formulated for holes.

To fit HD simulation output to Monte Carlo (MC) data, the parameters mentioned above can be varied; or the electron (or hole) relaxation time can be varied; or the mobility model parameters related to surface roughness mobility can be varied. Varying the HD model parameters does not give a satisfactory match with MC data. Varying the electron relaxation time is not physical [94]. So, the best option is to vary surface roughness mobility parameters to achieve a fit with MC data.

Surface roughness mobility is modeled by using the Darwish mobility model [101]. The surface mobility contribution due to acoustic phonon scattering has the form [67]

$$\mu_{ac} = \frac{B}{F_{\perp}} + \frac{C (N_i/N_O)^{\lambda}}{F_{\perp}^{1/3} (T/T_0)^k} \quad (57)$$

The contribution due to surface roughness scattering is given by

$$\mu_{sr} = \left( \frac{(F_{\perp}/F_{ref})^{A^*}}{\delta} + \frac{F_{\perp}^3}{\eta} \right)^{-1} \quad (58)$$

The contributions from  $\mu_{ac}$  and  $\mu_{sr}$  are combined with the contribution from bulk mobility ( $\mu_b$ ) according to Mathiessen's rule:

$$\frac{1}{\mu} = \frac{1}{\mu_b} + \frac{1}{\mu_{ac}} + \frac{1}{\mu_{sr}} \quad (59)$$

The exponent  $A^*$  is given by

$$A^* = A + \frac{\alpha_{\perp}(n+p)}{((N_i + N_1)/N_{ref})^{\nu}} \quad (60)$$

In the above equations,  $F_{\perp}$  is the vertical field. The normal electric field can be damped by adjusting the the exponential decay factor:

$$F_{\perp} \rightarrow F_{\perp} \exp\left(-\frac{l}{l_{crit}}\right) \quad (61)$$

The various parameters are calibrated and their values are shown in Table 21 for a 1 nm gate oxide thickness.

**Table 21:** Darwish model parameters for electrons in Silicon.

parameter	accumulation FET	inversion FET	units
B	1.97x10 <sup>7</sup>	(2 + (N <sub>A</sub> /10 <sup>17</sup> - 4)x0.1)x10 <sup>7</sup>	cm/s
C	3.01x10 <sup>6</sup>	2.41x10 <sup>6</sup>	cm <sup>5/3</sup> /(V <sup>2/3</sup> s)
N <sub>0</sub>	1	1	cm <sup>-3</sup>
$\lambda$	-0.168	-0.168	-
$k$	1	1	-
$\delta$	3.5x10 <sup>18</sup>	3.510 <sup>18</sup>	cm <sup>2</sup> /(Vs)
A	2.58	2.58	-
$\alpha_{\perp}$	0	0	cm <sup>-3</sup>
N <sub>1</sub>	1	1	cm <sup>-3</sup>
$\nu$	0.0767	0.0767	-
$\eta$	5.82x10 <sup>30</sup>	5.82x10 <sup>30</sup>	V <sup>2</sup> /(cm.s)
$l_{crit}$	10	10	nm

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