

## **INITIAL SLUDGE BATCH 4 TANK 40 DECANT VARIABILITY STUDY WITH FRIT 510**

F.C. Raszewski  
T.B. Edwards  
D.K. Peeler  
D.R. Best  
I.A. Reamer  
R.J. Workman

May 2008

Process Science and Engineering Section  
Savannah River National Laboratory  
Aiken, SC 29808

---

Prepared for the U.S. Department of Energy Under  
Contract Number DEAC09-96SR18500



**DISCLAIMER**

This report was prepared by Washington Savannah River Company (WSRC) for the United States Department of Energy under Contract No. DE-AC09-96SR18500 and is an account of work performed under that contract. Neither the United States Department of Energy, nor WSRC, nor any of their employees makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness, of any information, apparatus, or product or process disclosed herein or represents that its use will not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trademark, name, manufacturer or otherwise does not necessarily constitute or imply endorsement, recommendation, or favoring of same by WSRC or by the United States Government or any agency thereof. The views and opinions of the authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

**Printed in the United States of America**

**Prepared For  
U.S. Department of Energy**

The Savannah River National Laboratory is operated for the U.S. Department of Energy by Washington Savannah River Company.

**Keywords:** *SB4, Frit 510,  
decant, variability, durability*

**Retention:** *permanent*

## **INITIAL SLUDGE BATCH 4 TANK 40 DECANT VARIABILITY STUDY WITH FRIT 510**

F.C. Raszewski  
T.B. Edwards  
D.K. Peeler  
D.R. Best  
I.A. Reamer  
R.J. Workman

May 2008

Process Science and Engineering Section  
Savannah River National Laboratory  
Aiken, SC 29808

---

Prepared for the U.S. Department of Energy Under  
Contract Number DEAC09-96SR18500



## REVIEWS AND APPROVALS

### AUTHORS:

---

F.C. Raszewski, Process Science and Engineering Section                      Date

---

T.B. Edwards, Statistical Consulting Section                      Date

---

D.K. Peeler, Process Science and Engineering Section                      Date

---

D.R. Best, Process Science and Engineering Section                      Date

---

I.A. Reamer, Process Science and Engineering Section                      Date

---

R.J. Workman, Process Science and Engineering Section                      Date

### TECHNICAL REVIEWER:

---

K.M. Fox, Process Science and Engineering Section                      Date

### APPROVERS:

---

J.C. Griffin, Manager, E&CPT Research Programs                      Date

---

C.C. Herman, Manager, Process Engineering Technology Group                      Date

---

J.E. Occhipinti, Manager, Process Cognizant Engineering  
Waste Solidification Engineering                      Date

## EXECUTIVE SUMMARY

Sludge Batch 4 (SB4) is currently being processed in the Defense Waste Processing Facility (DWPF) using Frit 510. The slurry pumps in Tank 40 are experiencing in-leakage of bearing water, which is causing the sludge slurry feed in Tank 40 to become dilute at a rapid rate. Currently, the DWPF is removing this dilution water by performing caustic boiling during the Sludge Receipt and Adjustment Tank (SRAT) cycle. In order to alleviate prolonged SRAT cycle times that may eventually impact canister production rates, decant scenarios of 100, 150, and 200 kilogallons of supernate were proposed for Tank 40 during the DWPF March outage. Based on the results of the preliminary assessment issued by the Savannah River National Laboratory (SRNL), the Liquid Waste Organization (LWO) issued a Technical Task Request (TTR) for SRNL to (i) perform a more detailed evaluation using updated SB4 compositional information and (ii) assess the viability of Frit 510 and determine any potential impacts on the SB4 system. As defined in the TTR, LWO requested that SRNL validate the sludge-only SB4 flowsheet and the coupled operations flowsheet using the 100K gallon decant volume as well as the addition of 3 wt% sodium on a calcined oxide basis.

Approximately 12 historical glasses were identified during a search of the ComPro™ database that are located within at least one of the five glass regions defined by the proposed SB4 flowsheet options. While these glasses meet the requirements of a variability study there was some concern that the compositional coverage did not adequately bound all cases. Therefore, SRNL recommended that a supplemental experimental variability study be performed to support the various SB4 flowsheet options that may be implemented for future SB4 operations in DWPF. Eighteen glasses were selected based on nominal sludge projections representing the current as well as the proposed flowsheets over a WL interval of interest to DWPF (32–42%). The intent of the experimental portion of the variability study is to demonstrate that the glasses of the Frit 510-modified SB4 compositional region (Cases #1–5) are both acceptable relative to the Environmental Assessment (EA) reference glass and predictable by the current DWPF process control models for durability.

Frit 510 is a viable option for the processing of SB4 after a Tank 40 decant and the addition of products from the Actinide Removal Process (ARP). The addition of ARP did not have any negative impacts on the acceptability and predictability of the variability study glasses. The results of the variability study indicate that all of the study glasses (both quenched and centerline canister cooled (ccc)) have normalized releases for boron that are well below the reference EA glass (16.695 g/L). The durabilities of all of the study glasses are predictable using the current Product Composition Control System (PCCS) durability models with the exception of SB4VAR24ccc (Case #2 at 41%). PCCS is not applicable to non-homogeneous glasses (i.e. glasses containing crystals such as acmite and nepheline), thus SB4VAR24ccc should not be predictable as it contains nepheline.

The presence of nepheline has been confirmed in both SB4VAR13ccc and SB4VAR24ccc by X-ray diffraction (XRD). These two glasses are the first results which indicate that the current nepheline discriminator value of 0.62 is not conservative. The nepheline discriminator was implemented into PCCS for SB4 based on the fact that all of the historical glasses evaluated with nepheline values of 0.62 or greater did not contain nepheline via XRD analysis. Although these two glasses do cause some concern over the use of the 0.62 nepheline value for future DWPF glass systems, the impact to the current SB4 system is of little concern. More specifically, the formation of nepheline was observed in glasses targeting 41 or 42% WL. Current processing of the Frit 510–SB4 system in DWPF has nominally targeted 34% WL. For the SB4 variability study glasses targeting these lower WLs, nepheline formation was not observed and the minimal difference in PCT response between quenched and ccc versions supported its absence.

## TABLE OF CONTENTS

LIST OF TABLES .....	vii
LIST OF FIGURES.....	viii
LIST OF ABBREVIATIONS .....	ix
1.0 Introduction .....	1
2.0 Objective .....	2
3.0 Experimental Procedure .....	2
3.1 Target Glass Compositions .....	2
3.2 Glass Fabrication .....	2
3.3 Property Measurements .....	2
3.3.1 Compositional Analysis .....	2
3.3.2 PCT .....	3
3.3.3 XRD .....	3
4.0 Results and Discussion.....	5
4.1 Statistical Review of Chemical Composition Measurements .....	5
4.1.1 Measurements in Analytical Sequence .....	5
4.1.2 Batch 1 and Uranium Standard Results.....	5
4.1.3 Composition Measurements by Glass Identifier .....	6
4.1.4 Measured versus Targeted Compositions .....	7
4.1.5 MAR Assessment of the SB4/Decant Variability Study (VS) Glasses.....	7
4.2 Crystallization.....	11
4.2.1 Visual Observations .....	11
4.2.2 XRD .....	11
4.3 Statistical Review of PCT Results .....	14
4.3.1 Measurements in Analytical Sequence .....	14
4.3.2 Results for the Samples of the Multi–Element Solution Standard.....	15
4.3.3 Measurements by Glass Identifier.....	15
4.3.4 Normalized PCT Results.....	15
4.3.5 Acceptability of the SB4 VS Glasses .....	20
4.3.6 Predicted versus Measured PCTs .....	22
4.4 A Review of the Nepheline Assessments for DWPF’s SB4 Process Batches .....	23
5.0 Conclusions .....	26
6.0 References .....	27

## LIST OF TABLES

Table 1. Target Compositions of the SB4 Tank 40 Decant Variability Study Glasses .....	4
Table 2. Results of MAR Assessment of SB4 VS Glasses for Measured, Bias-Corrected, and Targeted Compositional Views.....	9
Table 3. Visual Observations of the CCC Glasses .....	12
Table 4. Results from Samples of the Multi-Element Solution Standard.....	15
Table 5. Normalized PCTs by Glass ID/Compositional View .....	17
Table 6. Nepheline Discriminator Values Recorded by DWPF during the Processing of SB4 .....	23
Table 7. Target Compositions of the SB4PS Glasses.....	25
Table 8. Measured Compositions of the SB4PS Glasses .....	25
Table 9. Normalized* PCT Responses of the Frit 510 – SB4 Supplemental Glasses (quenched and ccc).....	26

## LIST OF FIGURES

Figure 1. XRD pattern of the ccc version of the SB4VAR11 glass (Case #1 at 34% WL).....	13
Figure 2. XRD pattern of the ccc version of the SB4VAR13 glass (Case #1 at 42% WL).....	13
Figure 3. XRD pattern of the ccc version of the SB4VAR24 glass (Case #2 at 41% WL).....	14
Figure 4. Effect of heat treatment on log NL[B (g/L)] for Case #1.....	21
Figure 5. Log NL[B (g/L) versus B Del Gp model with a 95% confidence interval for individual PCTs.....	23

## LIST OF ABBREVIATIONS

AD	Analytical Development
ANOVA	Analysis of Variance
ARM	Approved Reference Material
ARP	Actinide Removal Process
B Del Gp	$\Delta G_p$ value for boron
bc	Bias-Corrected
ccc	Centerline Canister Cooling
CPC	Chemical Processing Cell
DWPF	Defense Waste Processing Facility
EA	Environmental Assessment
ICP-AES	Inductively Coupled Plasma-Atomic Emission Spectroscopy
ID	Identification
LM	Lithium Metaborate
LWO	Liquid Waste Organization
MAR	Measure Acceptability Region
NL[B]	Normalized Boron Release
NL[Li]	Normalized Lithium Release
NL[Na]	Normalized Sodium Release
NL[Si]	Normalized Silicon Release
PCCS	Product Composition Control System
PCT	Product Consistency Test
PF	Sodium Peroxide Fusion
ppm	Parts per million
PSAL	Process Science Analytical Laboratory
SB4	Sludge Batch 4
SME	Slurry Mix Evaporator
SRAT	Sludge Receipt and Adjustment Tank
SRNL	Savannah River National Laboratory
T <sub>L</sub> Pred	Liquidus Temperature Prediction
TTR	Technical Task Request
U <sub>std</sub>	Uranium Standard
Visc Pred	Viscosity Prediction
VS	Variability Study
WL	Waste Loading
XRD	X-ray Diffraction

## 1.0 Introduction

Sludge Batch 4 (SB4) is currently being processed in the Defense Waste Processing Facility (DWPF) using Frit 510. The slurry pumps in Tank 40 are experiencing in-leakage of bearing water, which is causing the sludge slurry feed in Tank 40 to become dilute at a rapid rate. Currently, the DWPF is removing this dilution water by performing caustic boiling during the Sludge Receipt and Adjustment Tank (SRAT) cycle. In order to alleviate prolonged SRAT cycle times that may eventually impact canister production rates, decant scenarios of varying amounts of supernate have been proposed for Tank 40. The Savannah River National Laboratory (SRNL) has issued a preliminary assessment evaluating the possible downstream impacts of three (100, 150, and 200 kilogallon) decant scenarios on DWPF glass formulation and the Chemical Processing Cell (CPC).<sup>1</sup> Based on the results of the preliminary assessment issued by the Savannah River National Laboratory (SRNL), the Liquid Waste Organization (LWO) issued a Technical Task Request (TTR) for SRNL to (i) perform a more detailed evaluation using updated SB4 compositional information and (ii) assess the viability of Frit 510 and determine any potential impacts on the SB4 system.<sup>2</sup> As defined in the TTR, LWO requested that SRNL validate the sludge-only SB4 flowsheet and the coupled operations flowsheet using the 100K gallon decant volume as well as the addition of 3 wt% sodium on a calcined oxide basis.

The following five nominal SB4 sludge compositions were identified to support this study<sup>a,3</sup>:

- Case #1: SB4 Nominal
- Case #2: SB4 after the 100K gallon decant
- Case #3: SB4 after the 100K gallon decant with a 3 wt% Na<sub>2</sub>O addition
- Case #4: SB4 after the 100K gallon decant and with addition of Actinide Removal Process (ARP) J
- Case #5: SB4 after the 100K gallon decant with the addition of 3 wt% Na<sub>2</sub>O and ARP J

These potential SB4 flowsheet modifications (i.e., 100K gallon decant, potential addition of Na<sub>2</sub>O, and/or transitioning to a coupled operations flowsheet) resulted in compositional shifts in the SB4 system as described in WSRC-STI-2008-00017.<sup>3</sup> Nominal sludge compositions (i.e. without any variation in the concentration of individual components) for each case were coupled with the nominal Frit 510 composition over a waste loading (WL) interval of 25–50% in order to define the glass regions of interest. The projected operating windows determined in the assessment suggested that Frit 510 remains a viable option for processing SB4 following the Tank 40 decant based on either a sludge-only or coupled operations flowsheet. In addition, the Na<sub>2</sub>O addition was also determined to be viable if melt rate was reduced due to the decrease in Na<sub>2</sub>O content after the decant. With respect to the SB4 variability study, approximately 12 historical glasses were identified during a search of the ComPro™ database that are located within at least one of the five glass regions defined by the proposed SB4 flowsheet options.<sup>4</sup> While these glasses meet the requirements of a variability study there was some concern that the compositional coverage did not adequately bound all cases. Therefore, SRNL recommended that a supplemental, experimental variability study be performed to support the various SB4 flowsheet options that may be implemented for future SB4 operations in DWPF. Eighteen glasses were selected based on nominal sludge projections representing the current as well as the proposed flowsheets over a WL interval of interest to DWPF (32–42%). The glass selection strategy used to define these glass compositions is described in detail in WSRC-STI-2008-

---

<sup>a</sup> Compositional projections of SB4 with the 100K gallon decant and SB4 with the 100K gallon decant and a 3 wt% Na<sub>2</sub>O addition were provided by LWO, while SRNL subsequently added the ARP/MCU stream to these compositions to assess the scenarios. Compositional information for ARP additions was obtained from X-CLC-S-00113, Rev. 0, Actinide Removal Process Material Balance Calculation with Low Curie Salt Feed, S.G. Subsists, 9/24/2004. Details of these compositions used in this assessment are provided in WSRC-STI-2008-00017.

00017.<sup>3</sup> These eighteen glasses were fabricated and characterized using chemical composition analysis, X-ray Diffraction (XRD) and the Product Consistency Test (PCT).

## 2.0 Objective

The intent of the experimental portion of the variability study is to demonstrate that the glasses of the Frit 510-modified SB4 compositional region (Cases #1–5) are both acceptable relative to the Environmental Assessment (EA) reference glass and predictable by the current process control models for durability.<sup>5–7</sup>

## 3.0 Experimental Procedure

### 3.1 Target Glass Compositions

Target glass compositions of the eighteen SB4 Tank 40 decant variability study glasses are presented in Table 1. The glass identification (ID) represents both the case number (see Section 1.0) and the waste loading. For the glass SB4VAR11, “SB4VAR” refers to the SB4 Variability Study, “1” refers to Case #1 (SB4 Nominal) and “1” refers to the first or lowest WL (34%), whereas SB4VAR54 represents Case #5 (SB4 after the 100K gallon decant with the addition of 3 wt% Na<sub>2</sub>O and ARP J) at the highest WL (41%), and so on.

### 3.2 Glass Fabrication

Each variability study glass was prepared from the proper proportions of reagent-grade metal oxides, carbonates, H<sub>3</sub>BO<sub>3</sub>, and salts in 150 g batches.<sup>8</sup> The raw materials were thoroughly mixed and placed into a 95% platinum / 5% gold, 250 ml crucible. Batched materials were placed into a high-temperature furnace at the target melt temperature of 1150°C.<sup>9</sup> The crucible was removed from the furnace after an isothermal hold at 1150°C for 1 hour. The molten glass was quenched by pouring the liquid onto a clean, stainless steel plate. The glass pour patty was used as a sampling stock for the various property measurements (i.e., chemical composition, durability testing and XRD).

Approximately 25 g of each glass was heat-treated to simulate cooling along the centerline of a DWPF-type canister to gauge the effects of thermal history on the product performance.<sup>7</sup> This cooling schedule is referred to as the centerline canister cooling (ccc) curve.

### 3.3 Property Measurements

#### 3.3.1 Compositional Analysis

To confirm that the as-fabricated glasses met the target compositions, a representative sample from each glass was submitted to the SRNL Process Science Analytical Laboratory (PSAL) for chemical analysis under the auspices of an analytical plan (SRNL-SCS-2008-00003).<sup>10</sup> Two dissolution techniques were utilized by PSAL, sodium peroxide fusion (PF) and lithium-metaborate (LM). Samples prepared by LM were used to measure silver (Ag), aluminum (Al), barium (Ba), calcium (Ca), cadmium (Cd), cerium (Ce), cobalt (Co), chromium (Cr), copper (Cu), iron (Fe), potassium (K), lanthanum (La), magnesium (Mg), manganese (Mn), sodium (Na), niobium (Nb), nickel (Ni), phosphorous (P), lead (Pb), sulfur (S), strontium (Sr), thorium (Th), titanium (Ti), uranium (U), zinc (Zn), and zirconium (Zr) concentrations. Samples prepared by PF were used to measure boron (B), lithium (Li) and silicon (Si) concentrations. Each glass was prepared in duplicate for each cation

dissolution technique (PF and LM). It should be noted that several of the elements in this list (e.g., Ag, Cd, Co, Nb, and Th) are not present in these glasses or are present at very small concentrations. For each study glass, measurements were obtained from samples prepared in duplicate by each of these dissolution methods. All of the prepared samples were analyzed (twice for each element of interest) by Inductively Coupled Plasma–Atomic Emission Spectroscopy (ICP–AES) with the instrumentation being re-calibrated between the duplicate analyses. The analytical plan was developed in such a way as to provide the opportunity to evaluate potential sources of bias and error. Glass standards were also intermittently measured to assess the performance of the ICP–AES instrument over the course of these analyses.

### **3.3.2 PCT**

A 7-day PCT was performed in triplicate on each quenched and ccc glass to assess chemical durability using Method A of the PCT procedure (ASTM C1285-97).<sup>11</sup> Also included in the experimental test matrix was the EA glass, the Approved Reference Material (ARM) glass, and blanks from the sample cleaning batch. Samples were ground, washed, and prepared according to the standard procedure.<sup>11,12</sup> The resulting solutions were sampled (filtered and acidified) and analyzed by PSAL under the auspices of an analytical plan (SRNL-SCS-2008-00050).<sup>13</sup> Samples of a multi-element, standard solution were also included in the analytical plan (as a check on the accuracy of the ICP–AES). Normalized release rates were calculated based on target, measured, and bias–corrected (bc) compositions using the average of the logs of the leachate concentrations.

### **3.3.3 XRD**

Representative samples of quenched and ccc glasses were submitted to SRNL Analytical Development (AD) for XRD analysis. Samples were analyzed under conditions providing a detection limit of approximately 0.5 vol%, i.e. no crystals can be detected if the amount in the sample is less than ~0.5 vol%.

**Table 1. Target Compositions of the SB4 Tank 40 Decant Variability Study Glasses**

Glass ID	Case #1		Case #2				Case #3		Case #4				Case #5					
	SB4VAR11	SB4VAR12	SB4VAR13	SB4VAR21	SB4VAR22	SB4VAR23	SB4VAR24	SB4VAR31	SB4VAR32	SB4VAR33	SB4VAR41	SB4VAR42	SB4VAR43	SB4VAR44	SB4VAR51	SB4VAR52	SB4VAR53	SB4VAR54
Frit	510	510	510	510	510	510	510	510	510	510	510	510	510	510	510	510	510	510
WL	34	38	42	32	35	38	41	32	36	40	32	35	38	41	32	35	38	41
Al <sub>2</sub> O <sub>3</sub>	8.46	9.46	10.46	8.31	9.09	9.86	10.64	8.00	9.01	10.01	8.00	8.75	9.50	10.25	7.71	8.43	9.15	9.88
B <sub>2</sub> O <sub>3</sub>	9.24	8.68	8.12	9.52	9.10	8.68	8.26	9.52	8.96	8.40	9.52	9.10	8.68	8.26	9.52	9.10	8.68	8.26
BaO	0.03	0.03	0.02	0.03	0.03	0.03	0.02	0.03	0.03	0.03	0.02	0.03	0.03	0.02	0.03	0.03	0.03	0.03
CaO	0.93	1.04	1.15	0.91	1.00	1.09	1.17	0.88	0.99	1.10	0.88	0.97	1.05	1.13	0.85	0.93	1.01	1.09
Ce <sub>2</sub> O <sub>3</sub>	0.02	0.02	0.03	0.02	0.02	0.03	0.03	0.02	0.02	0.03	0.02	0.03	0.03	0.03	0.02	0.02	0.03	0.03
Cr <sub>2</sub> O <sub>3</sub>	0.05	0.06	0.07	0.05	0.06	0.06	0.07	0.05	0.06	0.05	0.06	0.06	0.07	0.05	0.05	0.06	0.06	0.06
CuO	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02
Fe <sub>2</sub> O <sub>3</sub>	9.62	10.75	11.88	9.47	10.36	11.25	12.14	9.13	10.27	11.41	9.20	10.06	10.92	11.79	8.87	9.70	10.53	11.37
K <sub>2</sub> O	0.12	0.13	0.15	0.12	0.13	0.14	0.15	0.11	0.13	0.14	0.11	0.12	0.13	0.15	0.11	0.12	0.13	0.14
La <sub>2</sub> O <sub>3</sub>	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02
Li <sub>2</sub> O	5.28	4.96	4.64	5.44	5.20	4.96	4.72	5.44	5.12	4.80	5.44	5.20	4.96	4.72	5.44	5.20	4.96	4.72
MgO	0.91	1.02	1.13	0.90	0.98	1.07	1.15	0.87	0.97	1.08	0.86	0.94	1.02	1.10	0.83	0.90	0.98	1.06
MnO	1.93	2.16	2.39	1.90	2.08	2.26	2.44	1.83	2.06	2.29	1.88	2.06	2.23	2.41	1.82	1.99	2.16	2.33
Na <sub>2</sub> O	12.26	12.76	13.26	10.98	11.26	11.54	11.82	11.93	12.42	12.92	11.34	11.66	11.97	12.28	12.25	12.65	13.04	13.44
NiO	0.54	0.60	0.66	0.53	0.58	0.63	0.68	0.51	0.57	0.63	0.52	0.57	0.62	0.67	0.50	0.55	0.60	0.65
PhO	0.02	0.02	0.03	0.02	0.02	0.03	0.02	0.02	0.03	0.02	0.02	0.03	0.02	0.02	0.02	0.02	0.02	0.03
SO <sub>4</sub>	0.45	0.50	0.55	0.32	0.35	0.38	0.41	0.32	0.36	0.40	0.35	0.38	0.41	0.45	0.35	0.38	0.41	0.45
SiO <sub>2</sub>	47.10	44.41	41.72	48.49	46.47	44.46	42.44	48.46	45.77	43.07	48.46	46.44	44.42	42.40	48.43	46.40	44.38	42.36
TiO <sub>2</sub>	0.01	0.01	0.02	0.01	0.01	0.02	0.02	0.01	0.01	0.02	0.03	0.02	0.03	0.02	0.02	0.03	0.02	0.03
U <sub>3</sub> O <sub>8</sub>	2.94	3.28	3.63	2.89	3.16	3.43	3.70	2.79	3.13	3.48	2.80	3.06	3.32	3.59	2.70	2.95	3.21	3.46
ZnO	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03
ZrO <sub>2</sub>	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.04	0.03	0.03	0.04

## 4.0 Results and Discussion

### 4.1 Statistical Review of Chemical Composition Measurements

Table A1 in Appendix A provides the elemental concentration measurements derived from the samples prepared using LM, and Table A3 in Appendix A provides the measurements derived from the samples prepared using PF. Measurements for standards (Batch 1 and a uranium standard, U<sub>std</sub>) that were included in the PSAL analytical plan along with the study glasses are also provided in these two tables.

The elemental concentrations were converted to oxide concentrations by multiplying the values for each element by the gravimetric factor for the corresponding oxide (Table A2 and Table A4). During this process, an elemental concentration that was determined to be below the detection limit of the analytical procedures used by the PSAL was reduced to half of that detection limit as the oxide concentration was determined.

In the following sections, the analytical sequences of the measurements are explored, the measurements of the standards are investigated and used for bias correction, the measurements for each glass are reviewed, the average chemical compositions (measured and bias-corrected) for each glass are determined, and comparisons are made between the measurements and the targeted compositions for the glasses.

#### 4.1.1 Measurements in Analytical Sequence

Exhibit A1 in Appendix A provides plots of the measurements generated by the PSAL for samples prepared using the LM method. The plots are in analytical sequence with different symbols and colors being used to represent each of the study and standard glasses. Similar plots are provided in Exhibit A2 in Appendix A for the samples prepared using the PF method. These plots include all of the measurement data from Tables A1 and A3. While looking for obvious patterns in these plots is difficult, a relatively small value for NiO (0.078 wt%) for one of the uranium standard glasses (U<sub>std</sub>LM2-122) does stand out. Otherwise, a review of these plots indicates no significant patterns or trends in the analytical process over the course of these measurements. Better opportunities for such reviews are provided in the discussions that follow.

#### 4.1.2 Batch 1 and Uranium Standard Results

In this section, the PSAL measurements of the chemical compositions of the Batch 1 and uranium standard (U<sub>std</sub>) glasses are reviewed. These measurements are investigated across the ICP analytical blocks, and the results are used to bias correct the measurements for the study glasses.

Exhibit A3 in Appendix A provides statistical analyses of the Batch 1 and U<sub>std</sub> results generated by the LM prep method by analytical set and calibration block/sub-block for each oxide of interest. The results include analysis of variance (ANOVA) investigations looking for statistically significant differences between the means of these groups for each of the oxides for each of the standards. The results from the statistical tests for the Batch 1 standard may be summarized as follows: the Al<sub>2</sub>O<sub>3</sub>, CaO, Ce<sub>2</sub>O<sub>3</sub> (a detection limit effect), Cr<sub>2</sub>O<sub>3</sub>, CuO, Fe<sub>2</sub>O<sub>3</sub>, K<sub>2</sub>O, MgO, Na<sub>2</sub>O, NiO, TiO<sub>2</sub>, and ZrO<sub>2</sub> measurements indicate a significant ICP calibration effect on the block averages at the 5% significance level. For the U<sub>std</sub>, the Al<sub>2</sub>O<sub>3</sub>, CaO, Ce<sub>2</sub>O<sub>3</sub> (a detection limit effect), Cr<sub>2</sub>O<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub>, K<sub>2</sub>O, MgO, Na<sub>2</sub>O, SiO<sub>2</sub>, TiO<sub>2</sub>, and U<sub>3</sub>O<sub>8</sub> measurements indicate a significant ICP calibration effect on the

block averages at the 5% significance level. The reference values for the oxide concentrations of the standards are given in the header for each set of measurements in the exhibit.

Exhibit A4 in Appendix A provides a similar set of analyses for the measurements derived from samples prepared via the PF method. The results from the statistical tests for the Batch 1 standard may be summarized as follows: the Li<sub>2</sub>O measurements indicate significant ICP calibration effects on the block averages at the 5% significance level. For the U<sub>std</sub>, the Li<sub>2</sub>O measurements indicate significant ICP calibration effects on the block averages at the 5% significance level. The reference values for the oxide concentrations of the standards are given in the header for each set of measurements in the exhibit.

Some of these results provide incentive for adjusting the measurements by the effects of the ICP calibration. Therefore, the oxide measurements of the study glasses are bias corrected for the effect of the ICP calibration on each of the analytical blocks and sub-blocks. The basis for the bias correction is presented as part of Exhibits A3 and A4 – the average measurement for Batch 1 for each ICP block/sub-block for Al<sub>2</sub>O<sub>3</sub>, B<sub>2</sub>O<sub>3</sub>, BaO, CaO, Cr<sub>2</sub>O<sub>3</sub>, CuO, Fe<sub>2</sub>O<sub>3</sub>, Li<sub>2</sub>O, MgO, MnO, Na<sub>2</sub>O, NiO, SiO<sub>2</sub>, and TiO<sub>2</sub> and the average measurement for U<sub>std</sub> for each ICP set/block for U<sub>3</sub>O<sub>8</sub>. Thus, the Batch 1 results serve as the basis for bias correcting all of the selected oxides except uranium. The U<sub>std</sub> results were used to bias correct for uranium. The Batch 1 results were used to conduct the bias correction as long as the reference value for the oxide concentration in the Batch 1 glass was greater than or equal to 0.1 wt%. Thus, applying this approach and based upon the information in the exhibits, the Batch 1 results were used to bias correct the Al<sub>2</sub>O<sub>3</sub>, B<sub>2</sub>O<sub>3</sub>, BaO, CaO, Cr<sub>2</sub>O<sub>3</sub>, CuO, Fe<sub>2</sub>O<sub>3</sub>, K<sub>2</sub>O, Li<sub>2</sub>O, MgO, MnO, Na<sub>2</sub>O, NiO, SiO<sub>2</sub>, and TiO<sub>2</sub> measurements. No bias correction was conducted for Ce<sub>2</sub>O<sub>3</sub>, La<sub>2</sub>O<sub>3</sub>, PbO, SO<sub>4</sub>, ThO<sub>2</sub>, ZnO, or ZrO<sub>2</sub>.

The bias correction was conducted as follows. For each oxide, let  $\bar{a}_{ij}$  be the average measurement for the i<sup>th</sup> oxide at analytical block j for Batch 1 (or U<sub>std</sub> for uranium), and let t<sub>i</sub> be the reference value for the i<sup>th</sup> oxide for Batch 1 (or for U<sub>std</sub> if uranium). (The averages and reference values are provided in Exhibits A3 and A4.) Let  $\bar{c}_{ijk}$  be the average measurement for the i<sup>th</sup> oxide at analytical block j for the k<sup>th</sup> glass. The bias adjustment was conducted as follows

$$\bar{c}_{ijk} \bullet \left( 1 - \frac{\bar{a}_{ij} - t_i}{\bar{a}_{ij}} \right) = \bar{c}_{ijk} \bullet \frac{t_i}{\bar{a}_{ij}}$$

Bias-corrected measurements are indicated by a “bc” suffix, and such adjustments were performed for all of the oxides of this study except for Ce<sub>2</sub>O<sub>3</sub>, La<sub>2</sub>O<sub>3</sub>, PbO, SO<sub>4</sub>, ThO<sub>2</sub>, ZnO, and ZrO<sub>2</sub>. Both measured and measured “bc” values are included in the discussion that follows. Since no bias correction was performed on Ce<sub>2</sub>O<sub>3</sub>, La<sub>2</sub>O<sub>3</sub>, PbO, SO<sub>4</sub>, ThO<sub>2</sub>, ZnO, and ZrO<sub>2</sub>, the original values are included for completeness (e.g., to allow a sum of oxides to be computed for the bias-corrected results).

#### **4.1.3 Composition Measurements by Glass Identifier**

Exhibits A5 and A6 in Appendix A provide plots of the oxide concentration measurements by Glass ID (including Batch 1 and U<sub>std</sub>) by analytical solution ID for the LM and PF preparation methods, respectively, for each set of analyses. Different symbols and colors are used to represent the different glasses. These plots show the individual measurements across the duplicates of each preparation

method and the two ICP calibrations within each analytical set. A review of the plots presented in these exhibits reveals the repeatability of the four individual, oxide values for each glass. The Al<sub>2</sub>O<sub>3</sub> results in set 1 for SB4VAR23 show differences that appear to be due to a dissolution effect for this glass. Although Al<sub>2</sub>O<sub>3</sub> differences are observed, all of the data were used to compute measured and measured bias corrected compositional views. A considerable amount of scatter is observed in the Fe<sub>2</sub>O<sub>3</sub> results for both sets of analyses. These issues will not have any impact on the conclusions of this report.

#### ***4.1.4 Measured versus Targeted Compositions***

The four measurements for each oxide of each glass (over both preparation methods) were averaged to determine a representative chemical composition for each glass. These determinations were conducted both for the measured and for the bias-corrected data. A sum of oxides was also computed for each glass based upon both the measured and bias-corrected values. Exhibit A7 in Appendix A provides plots showing results for each glass for each oxide to help highlight the comparisons among the measured, bias-corrected, and targeted values.

Some observations from the plots of Exhibit A7 are offered: In general, there were some difficulties in reaching the targeted concentrations for Fe<sub>2</sub>O<sub>3</sub> (measured values generally lower than targeted) and SiO<sub>2</sub> (measured values generally higher than targeted). In addition, the SO<sub>4</sub> concentration for SB4VAR21 appears to be low (53% below its targeted value). Table A4 in Appendix A provides a summary of the average compositions as well as the targeted compositions and some associated differences and relative differences. Notice that the targeted sums of oxides for the standard glasses are not 100% due to incomplete coverage of the oxides in the Batch 1 and U<sub>std</sub> glasses. All of the oxide sums (both measured and bias-corrected) for the study glasses fall within the interval of 95 to 105 wt%. Entries in Table A4 show the relative differences between the measured or bias-corrected values and the targeted values. These differences are shaded when they are greater than or equal to 5%. Overall, the comparisons between the measured and targeted compositions suggest only minor difficulties in reaching the targeted compositions for some of the oxides for some of the glasses.

#### ***4.1.5 MAR Assessment of the SB4/Decant Variability Study (VS) Glasses***

Another assessment that can be made for these SB4 VS glasses is how well they satisfy the Measurement Acceptability Region (MAR) criteria of DWPF's Product Composition Control System (PCCS). All of the glasses that were selected for this study satisfied these criteria. That is, the targeted composition for each of these glasses fell within the MAR of PCCS as described in WSRC-STI-2008-00017.<sup>3</sup> In this section, the results of the MAR assessment of the measured and measured bias-corrected compositions for these glasses are presented along with the results for the targeted compositions.

Table 2 provides the percent waste loading (%WL), the frit, the glass identifier with compositional view, the B Del Gp Value ( $\Delta G_p$  value for boron), the normalized leachate for boron in grams/Liter (NL[B (g/L)]), the liquidus temperature prediction in degrees Celsius (T<sub>L</sub> Pred (°C)), the viscosity prediction in Poise (Visc Pred (P)), the sum of oxides (in wt%), the Al<sub>2</sub>O<sub>3</sub> concentration (in wt%), the Na<sub>2</sub>SO<sub>4</sub> concentration (in wt%), and the total alkali concentration (R<sub>2</sub>O) as a wt%, the nepheline value, and the overall MAR assessment.<sup>b</sup> With the exception of SB4VAR54 (target and measured bc), all of the MAR results for these glass compositional views indicate that they would pass the PCCS

<sup>b</sup> Although the PCCS limit of 0.88 wt% Na<sub>2</sub>SO<sub>4</sub> was not used during the MAR assessment, both the projected and measured Na<sub>2</sub>SO<sub>4</sub> concentrations for all SB4 cases meet this criterion.

MAR and be both processable and acceptable by the DWPF. As for the SB4VAR54 glass, it was noted during the glass selection process that the targeted composition failed the low viscosity criterion.<sup>3</sup> The measured composition has a slightly higher predicted viscosity (27.2 Poise) as compared to both the target and measured bias corrected compositional views of 24.4 and 24.6 Poise respectively, which both fail the low viscosity constraint.

**Table 2. Results of MAR Assessment of SB4 VS Glasses for Measured, Bias-Corrected, and Targeted Compositional Views**

Glass ID	%WL	Compositional View	B Del Gp	NL[B (g/L)]	T <sub>L</sub> Pred (°C)	Visc Pred (P)	Sum of Oxides wt%	Al <sub>2</sub> O <sub>3</sub> wt%	Na <sub>2</sub> SO <sub>4</sub> wt%	R <sub>2</sub> O wt%	Nepheline Value	MAR Status
SB4VAR11	34	measured	-9.991	0.81	885.6	39.7	98.5	8.54	0.61	17.48	0.69	All Constraints Met
SB4VAR11	34	measured bc	-10.107	0.85	896.6	37.4	100.4	8.69	0.61	17.71	0.70	All Constraints Met
SB4VAR11	34	targeted	-10.169	0.87	897.6	35.1	99.6	8.46	0.66	17.66	0.69	All Constraints Met
SB4VAR12	38	measured	-9.743	0.73	944.8	35.2	100.0	9.49	0.66	17.52	0.67	All Constraints Met
SB4VAR12	38	measured bc	-9.935	0.79	940.3	34.3	101.2	9.70	0.66	17.83	0.67	All Constraints Met
SB4VAR12	38	targeted	-10.110	0.85	941.9	30.0	99.5	9.46	0.74	17.85	0.67	All Constraints Met
SB4VAR13	42	measured	-9.854	0.77	960.6	33.3	100.6	10.39	0.75	17.87	0.65	All Constraints Met
SB4VAR13	42	measured bc	-9.867	0.77	977.8	29.2	100.4	10.57	0.75	17.94	0.64	All Constraints Met
SB4VAR13	42	targeted	-10.052	0.83	981.9	25.2	99.4	10.46	0.82	18.05	0.64	All Constraints Met
SB4VAR21	32	measured	-8.994	0.53	893.3	53.5	100.5	8.37	0.22	16.37	0.72	All Constraints Met
SB4VAR21	32	measured bc	-9.041	0.55	909.3	47.6	99.9	8.51	0.22	16.46	0.72	All Constraints Met
SB4VAR21	32	targeted	-9.206	0.58	909.9	44.6	99.7	8.31	0.47	16.54	0.72	All Constraints Met
SB4VAR22	35	measured	-8.831	0.50	944.3	49.1	101.3	9.05	0.51	16.38	0.71	All Constraints Met
SB4VAR22	35	measured bc	-8.953	0.53	945.1	45.0	100.2	9.26	0.51	16.55	0.70	All Constraints Met
SB4VAR22	35	targeted	-9.070	0.55	947.6	41.0	99.7	9.09	0.51	16.59	0.70	All Constraints Met
SB4VAR23	38	measured	-8.495	0.43	966.7	47.6	99.3	10.29	0.52	16.32	0.68	All Constraints Met
SB4VAR23	38	measured bc	-8.511	0.44	983.6	42.1	99.1	10.47	0.52	16.39	0.67	All Constraints Met
SB4VAR23	38	targeted	-8.933	0.52	982.4	37.4	99.6	9.86	0.56	16.64	0.68	All Constraints Met
SB4VAR24	41	measured	-8.602	0.45	988.2	41.6	98.5	10.63	0.56	16.46	0.66	All Constraints Met
SB4VAR24	41	measured bc	-8.680	0.47	999.9	39.1	100.5	10.82	0.56	16.66	0.66	All Constraints Met
SB4VAR24	41	targeted	-8.796	0.49	1014.7	33.8	99.6	10.64	0.60	16.69	0.65	All Constraints Met
SB4VAR31	32	measured	-10.068	0.84	872.7	39.6	99.4	8.09	0.46	17.40	0.71	All Constraints Met
SB4VAR31	32	measured bc	-10.095	0.85	875.3	35.8	98.3	8.11	0.46	17.39	0.71	All Constraints Met
SB4VAR31	32	targeted	-10.123	0.86	877.6	38.1	99.7	8.01	0.47	17.49	0.71	All Constraints Met
SB4VAR32	36	measured	-9.924	0.79	922.3	35.9	99.7	9.09	0.52	17.54	0.68	All Constraints Met
SB4VAR32	36	measured bc	-10.024	0.82	923.9	31.3	98.9	9.11	0.52	17.59	0.68	All Constraints Met
SB4VAR32	36	targeted	-10.054	0.83	924.5	33.0	99.6	9.01	0.53	17.67	0.68	All Constraints Met
SB4VAR33	40	measured	-9.801	0.75	952.6	28.3	97.2	9.78	0.55	17.42	0.65	All Constraints Met
SB4VAR33	40	measured bc	-10.057	0.83	949.9	25.7	97.4	10.15	0.55	17.86	0.65	All Constraints Met

**Table 2 cont. Results of MAR Assessment of SB4 VS Glasses for Measured, Bias-Corrected, and Targeted Compositional Views**

Glass ID	%WL	Compositional View	B Del Gp Value	NL[B (g/L)]	T <sub>r</sub> Pred (°C)	Visc Pred (P)	Sum of Oxides	Al <sub>2</sub> O <sub>3</sub> wt%	Na <sub>2</sub> SO <sub>4</sub> wt%	R <sub>2</sub> O wt%	Nepheline Value	MAR Status w/o Na <sub>2</sub> SO <sub>4</sub>
SB4VAR33	40	targeted	-9.986	0.81	967.1	28.0	99.6	10.01	0.59	17.86	0.65	All Constraints Met
SB4VAR41	32	measured	-9.468	0.65	889.0	48.2	102.1	8.14	0.49	16.96	0.72	All Constraints Met
SB4VAR41	32	measured bc	-9.598	0.69	889.9	44.0	101.0	8.32	0.49	17.14	0.71	All Constraints Met
SB4VAR41	32	targeted	-9.546	0.67	884.8	41.6	99.7	8.00	0.51	16.90	0.71	All Constraints Met
SB4VAR42	35	measured	-9.094	0.56	932.5	43.9	100.0	8.68	0.52	16.59	0.70	All Constraints Met
SB4VAR42	35	measured bc	-9.217	0.59	933.0	40.1	99.0	8.88	0.52	16.76	0.69	All Constraints Met
SB4VAR42	35	targeted	-9.441	0.64	931.3	37.8	99.6	8.75	0.56	16.98	0.69	All Constraints Met
SB4VAR43	38	measured	-8.936	0.52	969.1	40.3	100.4	9.41	0.59	16.65	0.68	All Constraints Met
SB4VAR43	38	measured bc	-9.119	0.56	964.3	39.3	101.6	9.63	0.59	16.95	0.68	All Constraints Met
SB4VAR43	38	targeted	-9.336	0.62	965.1	34.1	99.6	9.50	0.61	17.07	0.67	All Constraints Met
SB4VAR44	41	measured	-9.033	0.54	970.0	38.6	98.5	10.26	0.61	16.90	0.66	All Constraints Met
SB4VAR44	41	measured bc	-9.110	0.56	981.9	36.4	100.5	10.44	0.61	17.11	0.66	All Constraints Met
SB4VAR44	41	targeted	-9.231	0.59	996.1	30.4	99.6	10.25	0.66	17.15	0.65	All Constraints Met
SB4VAR51	32	measured	-10.210	0.89	861.1	38.6	98.9	7.79	0.49	17.57	0.71	All Constraints Met
SB4VAR51	32	measured bc	-10.432	0.97	856.6	37.2	100.2	7.96	0.49	17.91	0.71	All Constraints Met
SB4VAR51	32	targeted	-10.417	0.97	864.4	35.8	99.7	7.71	0.51	17.80	0.71	All Constraints Met
SB4VAR52	35	measured	-10.152	0.87	893.1	36.7	99.2	8.58	0.53	17.74	0.69	All Constraints Met
SB4VAR52	35	measured bc	-10.261	0.91	904.3	34.6	101.1	8.73	0.53	17.97	0.69	All Constraints Met
SB4VAR52	35	targeted	-10.393	0.96	899.2	31.8	99.6	8.43	0.56	17.96	0.69	All Constraints Met
SB4VAR53	38	measured	-10.392	0.96	907.9	33.4	100.4	9.17	0.57	18.18	0.67	All Constraints Met
SB4VAR53	38	measured bc	-10.414	0.97	924.3	29.4	100.1	9.33	0.57	18.25	0.67	All Constraints Met
SB4VAR53	38	targeted	-10.371	0.95	931.3	28.0	99.6	9.16	0.61	18.13	0.67	All Constraints Met
SB4VAR54	41	measured	-10.124	0.86	956.7	27.2	99.4	9.86	0.64	18.05	0.65	All Constraints Met
SB4VAR54	41	measured bc	-10.238	0.90	957.3	24.6	98.5	10.09	0.64	18.23	0.64	Ivisc
SB4VAR54	41	targeted	-10.347	0.94	960.8	24.4	99.6	9.88	0.66	18.30	0.64	Ivisc

## 4.2 Crystallization

### 4.2.1 Visual Observations

Prior to discussing the visual observations, a brief explanation of the terms used to describe the as-fabricated (quenched) and ccc glasses is necessary. “Surface” refers to the top of the sample that has not touched the steel plate during quenching or the walls of the crucible during the ccc treatment. The term “bulk” refers to the cross-section of the glass sample. “Homogeneous” indicates that there is no crystallization evident on the surface or in the bulk of the glass. Other terms such as “haze”, “clusters”, and/or “silver/metallic patches” imply that the surface or bulk of the glass contains crystals or some other characteristic feature. “Black and shiny” implies that crystallization is not apparent to the un-aided eye.

The surface and bulk of each as-fabricated (quenched) glass were “black and shiny,” which indicates that the glasses are free of crystallization and homogeneous.

Crystallization is much more prevalent in the ccc glasses given that the kinetics for crystallization are more favorable during the slow cooling of the ccc treatment. Only three of the ccc glasses were determined to be homogeneous based on visual observations as shown in Table 3, which is not surprising as these glasses had a target WL of only 32%. The remainder of the ccc glasses did contain some degree of crystallization on the surface, characterized by “haze” and “silver/metallic patches.” Historically, metallic-like features on the surface of DWPF glasses are due to the precipitation of spinels during the slower cooling process. Crystallization was not present in the bulk of any glasses, except SB4VAR24 (Case #2 at 41% WL), which contained patches of silver/metallic crystals on the surface that extended 3 mm into the bulk.

### 4.2.2 XRD

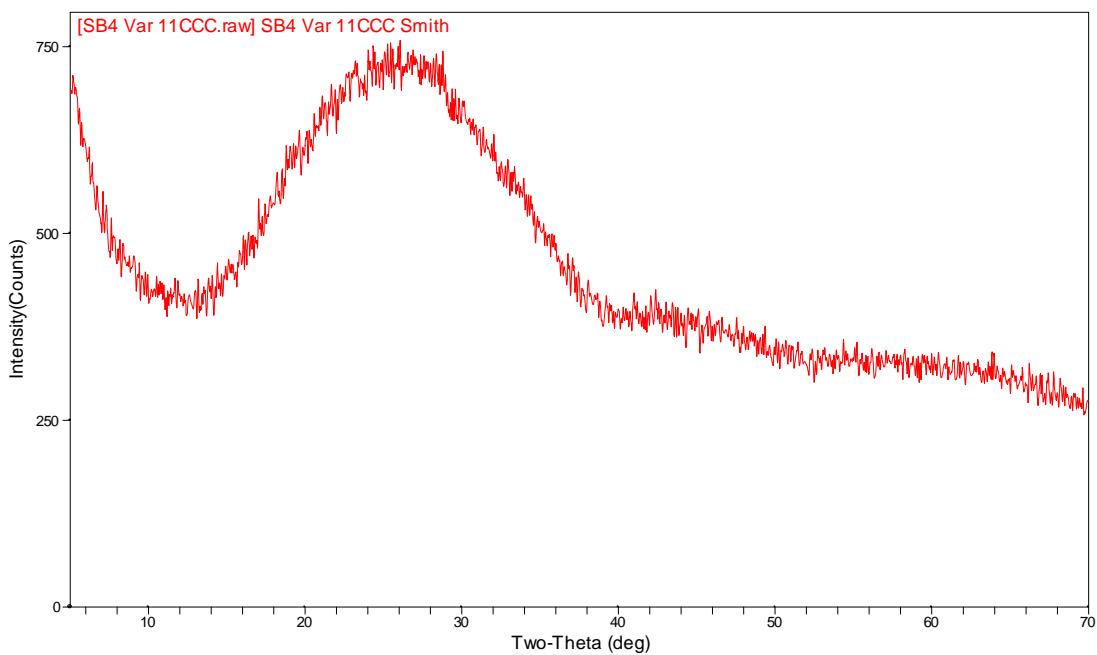
Each of the quenched glasses is amorphous (within the detection limit of the instrument), which corresponds to the visual observations (Section 4.2.1). Two of the ccc samples contain crystalline material, while all others are amorphous (within the detection limit of the instrument). Both nepheline and trevorite were detected in samples SB4VAR13ccc (Case #1 at 42% WL) and SB4VAR24ccc (Case #2 at 41% WL). A representative pattern<sup>c</sup> of an amorphous sample is shown in Figure 1, while the XRD patterns of the glasses containing nepheline and trevorite are shown in Figure 2 and Figure 3. The presence of nepheline was not expected in SB4VAR13ccc or SB4VAR24ccc. The MAR assessments suggest that the nepheline discriminator values of these glasses are well above the 0.62 value currently being used to delineate compositions that are prone to nepheline formation from those that are not. These data are the initial results that suggest that the current nepheline discriminator and the use of the 0.62 values may not be conservative for specific compositional regions. As nepheline is present in these two glasses, a negative impact on the PCT response is anticipated.

---

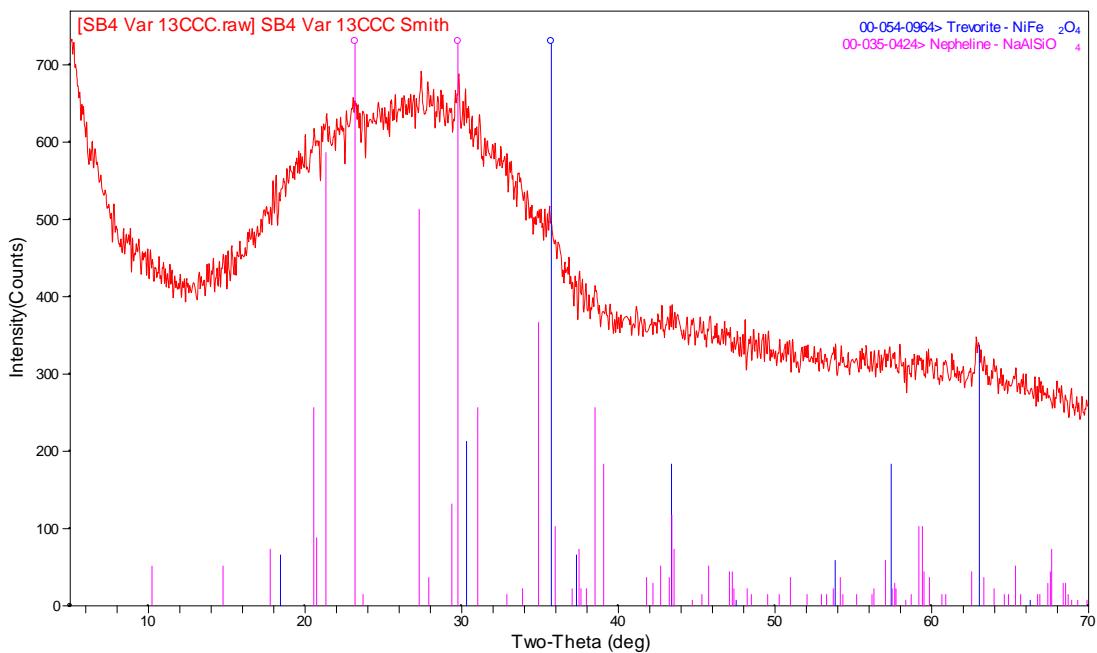
<sup>c</sup> The remainder of the XRD patterns (quenched and ccc) can be viewed in the laboratory notebook for the SB4 variability study on pages 116-118 (WSRC-NB-2006-00168).

**Table 3. Visual Observations of the CCC Glasses**

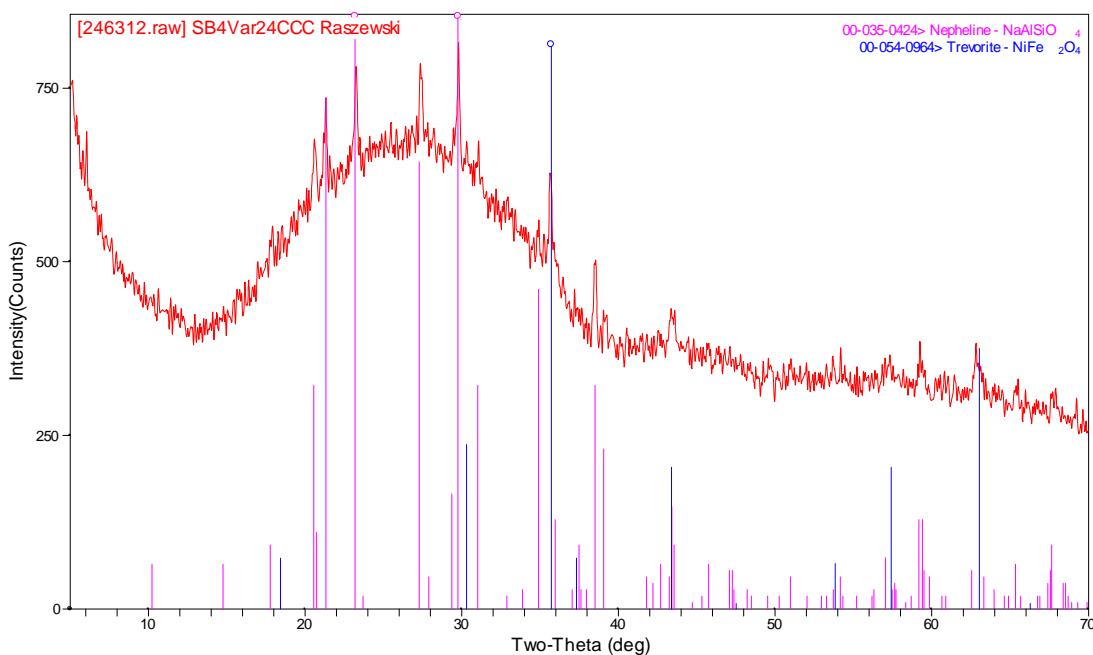
Glass ID	Frit	WL	Visual Observations		XRD
			Surface	Bulk	
SB4VAR11	510	34	Light haze	Clean	Amorphous
SB4VAR12		38	Light/shiny haze, three silver/metallic patches of crystals	Clean	Amorphous
SB4VAR13		42	Haze, large patches of silver/metallic crystals	Clean	Nepheline and Trevorite
SB4VAR21		32	Very light crystals	Clean	Amorphous
SB4VAR22		35	Silver haze with crystals	Clean	Amorphous
SB4VAR23		38	Silver haze, several patches of silver/metallic patches	Clean	Amorphous
SB4VAR24		41	Crystals, large patches of silver/metallic crystals	Crystal patches extend $\frac{1}{8}$ " into bulk	Nepheline and Trevorite
SB4VAR31		32	Black and shiny	Clean	Amorphous
SB4VAR32		36	Shiny, silver metallic haze	Clean	Amorphous
SB4VAR33		40	Haze, several silver/metallic patches of crystals	Clean	Amorphous
SB4VAR41		32	Black and shiny	Clean	Amorphous
SB4VAR42		35	Silver haze, few patches of silver crystals	Clean	Amorphous
SB4VAR43		38	Silver haze, few patches of silver crystals	Clean	Amorphous
SB4VAR44		41	Silver haze, few patches of silver crystals	Clean	Amorphous
SB4VAR51		32	Black and shiny	Clean	Amorphous
SB4VAR52		35	Silver haze	Clean	Amorphous
SB4VAR53		38	Silver haze, few patches of silver crystals	Clean	Amorphous
SB4VAR54		41	Large patches of silver crystals	Clean	Amorphous



**Figure 1.** XRD pattern of the ccc version of the SB4VAR11 glass (Case #1 at 34% WL).



**Figure 2.** XRD pattern of the ccc version of the SB4VAR13 glass (Case #1 at 42% WL).



**Figure 3. XRD pattern of the ccc version of the SB4VAR24 glass (Case #2 at 41% WL).**

#### 4.3 Statistical Review of PCT Results

Table B1 in Appendix B provides the elemental leachate concentration measurements determined by the PSAL for the solution samples generated by the PCTs. One of the quality control checkpoints for the PCT procedure is solution-weight loss over the course of the 7-day test. None of these PCT results indicated a solution-weight loss problem. Any measurement in Table B1 below the detection limit of the analytical procedure (indicated by a "<") was replaced by  $\frac{1}{2}$  of the detection limit in subsequent analyses. In addition to adjustments for detection limits, the values were adjusted for the dilution factors: the values for the study glasses, the blanks, and the ARM glass in Table B1 were multiplied by 1.6667 to determine the values in parts per million (ppm) and the values for EA were multiplied by 16.6667. Table B2 in Appendix B provides the resulting measurements.

In the following sections, the analytical sequence of the measurements is explored, the measurements of the standards are investigated and used to assess the overall accuracy of the ICP measurement process, the measurements for each glass are reviewed, plots are provided that explore the effects of heat treatment on the PCTs for these glasses, the PCTs are normalized using the compositions (targeted, measured, and bias-corrected) presented in Table A4, and the normalized PCTs are compared to durability predictions for these compositions generated from the current DWPF models.<sup>14</sup>

##### 4.3.1 Measurements in Analytical Sequence

Exhibit B1 in Appendix B provides plots of the leachate (ppm) concentrations in analytical sequence as generated by the PSAL for all of the data and for the data from only the study glasses. A different

color and symbol are used for each study glass or standard. No issues are observed in these plots.

#### ***4.3.2 Results for the Samples of the Multi–Element Solution Standard***

Exhibit B2 in Appendix B provides analyses of the PSAL measurements of the samples of the multi–element solution standard by analytical set and ICP calibration block. An ANOVA investigating for statistically significant differences among the block averages for these samples for each element of interest is included in these exhibits. There was no indication of a statistically significant (at a 5% level) difference among the averages of these measurements for any of the elements of interest. Averaging the measured concentrations for each set of triplicates helps to minimize the impact of any potential ICP–AES effects.

Table 4 summarizes the average measurements and the reference values for the 4 primary elements of interest. The results indicate consistent and accurate measurements from the PSAL processes used to conduct these analyses.

**Table 4. Results from Samples of the Multi–Element Solution Standard**

Analytical Set/Block	Avg B (ppm)	Avg Li (ppm)	Avg Na (ppm)	Avg Si (ppm)
<b>q/1</b>	20.2	10.0	81.2	49.4
<b>q/2</b>	20.3	9.8	80.1	50.6
<b>q/3</b>	19.4	9.9	80.4	50.4
<b>r/1</b>	20.1	9.8	79.3	50.0
<b>r/2</b>	20.4	9.8	80.1	52.0
<b>r/3</b>	20.8	10.0	80.7	51.5
<b>Grand Average</b>	20.2	9.9	80.3	50.7
<b>Reference Value</b>	20	10	81	50
<b>% difference</b>	1.03%	-1.22%	-0.85%	1.30%

#### ***4.3.3 Measurements by Glass Identifier***

Exhibit B3 in Appendix B provides plots (grouped by analytical set) of the leachate concentrations for each type of submitted sample: the study glasses by heat treatment and the standards (EA, ARM, the multi–element solution standard, and blanks). Exhibit B4 in Appendix B provide plots of the leachate concentrations for the PCT results of just the study glasses by heat treatment. These plots allow for the assessment of the repeatability of the measurements, which suggests some scatter in the triplicate values for some analytes for some of the glasses. Also, note that some differences between the values for the two heat treatments for some glasses are evident. More will be said regarding comparisons between the heat treatments in the discussions that follow.

#### ***4.3.4 Normalized PCT Results***

PCT leachate concentrations are typically normalized using the cation composition (expressed as a weight percent) in the glass to obtain a grams per liter (g/L) leachate concentration. The normalization of the PCTs is usually conducted using the measured compositions of the glasses. This is the preferred normalization process for the PCTs. For completeness, the targeted cation and the bias–corrected cation compositions were also used to conduct this normalization.

As is the usual convention, the common logarithm of the normalized PCT (normalized leachate, NL) for each element of interest was determined and used for comparison. To accomplish this computation, one must

- 1.) Determine the common logarithm of the elemental parts per million (ppm) leachate concentration for each of the triplicates and each of the elements of interest (these values are provided in Table B2 of Appendix B),
- 2.) Average the common logarithms over the triplicates for each element of interest, and then

Normalizing Using Measured Composition (preferred method)

- 3a.) Subtract a quantity equal to 1 plus the common logarithm of the average cation measured concentration (expressed as a weight percent of the glass) from the average computed in step 2.

Or Normalizing Using Target Composition

- 3b.) Subtract a quantity equal to 1 plus the common logarithm of the target cation concentration (expressed as a weight percent of the glass) from the average computed in step 2.

Or Normalizing Using Measured Bias-Corrected Composition

- 3c.) Subtract a quantity equal to 1 plus the common logarithm of the measured bias-corrected cation concentration (expressed as a weight percent of the glass) from the average computed in step 2.

Exhibit B5 in Appendix B provides scatter plots for these results and offers an opportunity to investigate the consistency in the leaching across the elements for the glasses of this study. All combinations of the normalizations of the PCTs (i.e., those generated using the targeted, measured, and bias-corrected compositional views) and both heat treatments are represented in the series of scatter plots. Consistency in the leaching across the elements is typically demonstrated by a high degree of linear correlation among the values for pairs of these elements. The smallest correlation in this plot is that for Li and Si, with a value of ~95%.

Table 5 summarizes the normalized PCTs for the glasses of this study, which are listed by glass identifier. The following sections discuss the two primary objectives of the variability study: (1) acceptability of the glasses with respect to the EA glass and (2) applicability of the current PCCS durability models for the measured PCT responses.

**Table 5. Normalized PCTs by Glass ID/Compositional View**

Glass ID	WL (%)	Sludge Case	Heat Treatment	Compositional View	Nepheline Assessment	log NL[B] (g/L)	log NL[Li] (g/L)	log NL[Na] (g/L)	log NL [Si(g/L)] (g/L)	NL[B] (g/L)	NL[Li] (g/L)	NL[Na] (g/L)	NL[Si] (g/L)
ARM	.			reference	0.753	-0.276	-0.208	-0.270	-0.537	0.53	0.62	0.54	0.29
ARM	.			reference	0.753	-0.324	-0.249	-0.300	-0.565	0.47	0.56	0.50	0.27
EA	.			reference	0.704	-1.243	0.973	1.116	0.597	17.52	9.40	13.05	3.96
EA	.			reference	0.704	1.241	0.959	1.108	0.597	17.41	9.10	12.83	3.95
SB4VAR11	34	Case 1	ccc	measured	0.694	-0.157	-0.143	-0.199	-0.344	0.70	0.72	0.63	0.45
SB4VAR11	34	Case 1	ccc	measured bc	0.695	-0.166	-0.164	-0.199	-0.350	0.68	0.69	0.63	0.45
SB4VAR11	34	Case 1	ccc	targeted	0.694	-0.164	-0.159	-0.199	-0.344	0.69	0.69	0.63	0.45
SB4VAR11	34	Case 1	ccc	quenched	0.694	-0.144	-0.140	-0.175	-0.346	0.72	0.72	0.67	0.45
SB4VAR11	34	Case 1	ccc	measured bc	0.695	-0.154	-0.161	-0.175	-0.352	0.70	0.69	0.67	0.45
SB4VAR12	38	Case 1	ccc	targeted	0.694	-0.152	-0.156	-0.175	-0.346	0.70	0.70	0.67	0.45
SB4VAR12	38	Case 1	ccc	measured	0.673	-0.128	-0.126	-0.124	-0.342	0.74	0.75	0.75	0.45
SB4VAR12	38	Case 1	ccc	measured bc	0.673	-0.138	-0.147	-0.126	-0.347	0.73	0.71	0.75	0.45
SB4VAR12	38	Case 1	ccc	targeted	0.667	-0.132	-0.135	-0.132	-0.334	0.74	0.73	0.74	0.46
SB4VAR12	38	Case 1	ccc	quenched	0.673	-0.101	-0.116	-0.120	-0.325	0.79	0.77	0.76	0.47
SB4VAR12	38	Case 1	ccc	measured	0.673	-0.110	-0.137	-0.123	-0.330	0.78	0.73	0.75	0.47
SB4VAR12	38	Case 1	ccc	measured bc	0.673	-0.105	-0.125	-0.129	-0.316	0.79	0.75	0.74	0.48
SB4VAR13	42	Case 1	ccc	measured	0.651	0.175	0.132	0.042	-0.244	1.49	1.36	1.10	0.57
SB4VAR13	42	Case 1	ccc	measured bc	0.644	0.188	0.123	0.042	-0.233	1.54	1.33	1.10	0.58
SB4VAR13	42	Case 1	ccc	targeted	0.638	0.189	0.131	0.037	-0.221	1.55	1.35	1.09	0.60
SB4VAR13	42	Case 1	ccc	quenched	0.651	-0.094	-0.098	-0.071	-0.349	0.80	0.80	0.85	0.45
SB4VAR13	42	Case 1	ccc	measured bc	0.644	-0.081	-0.106	-0.071	-0.339	0.83	0.78	0.85	0.46
SB4VAR13	42	Case 1	ccc	quenched	0.638	-0.080	-0.099	-0.076	-0.327	0.83	0.80	0.84	0.47
SB4VAR21	32	Case 2	ccc	measured	0.723	-0.200	-0.152	-0.218	-0.365	0.63	0.70	0.61	0.43
SB4VAR21	32	Case 2	ccc	measured bc	0.717	-0.187	-0.161	-0.217	-0.355	0.65	0.69	0.61	0.44
SB4VAR21	32	Case 2	ccc	targeted	0.715	-0.190	-0.151	-0.225	-0.351	0.65	0.71	0.60	0.45
SB4VAR21	32	Case 2	ccc	quenched	0.723	-0.198	-0.142	-0.208	-0.366	0.63	0.72	0.62	0.43
SB4VAR21	32	Case 2	ccc	measured bc	0.717	-0.184	-0.150	-0.207	-0.355	0.65	0.71	0.62	0.44
SB4VAR21	32	Case 2	ccc	targeted	0.715	-0.188	-0.141	-0.215	-0.351	0.65	0.72	0.61	0.45
SB4VAR22	35	Case 2	ccc	measured	0.706	-0.186	-0.136	-0.184	-0.365	0.65	0.73	0.65	0.43
SB4VAR22	35	Case 2	ccc	measured bc	0.698	-0.173	-0.145	-0.187	-0.354	0.67	0.72	0.65	0.44
SB4VAR22	35	Case 2	ccc	targeted	0.696	-0.173	-0.139	-0.191	-0.347	0.67	0.73	0.64	0.45
SB4VAR22	35	Case 2	ccc	quenched	0.706	-0.170	-0.125	-0.192	-0.360	0.68	0.75	0.64	0.44
SB4VAR22	35	Case 2	ccc	measured bc	0.698	-0.157	-0.134	-0.195	-0.350	0.70	0.73	0.64	0.45
SB4VAR22	35	Case 2	ccc	targeted	0.696	-0.157	-0.128	-0.200	-0.343	0.70	0.75	0.63	0.45
SB4VAR23	38	Case 2	ccc	measured	0.676	-0.140	-0.104	-0.163	-0.347	0.73	0.79	0.69	0.45
SB4VAR23	38	Case 2	ccc	measured bc	0.669	-0.126	-0.112	-0.162	-0.337	0.75	0.77	0.69	0.46
SB4VAR23	38	Case 2	ccc	targeted	0.675	-0.138	-0.117	-0.170	-0.340	0.73	0.76	0.68	0.46
SB4VAR23	38	Case 2	ccc	quenched	0.676	-0.156	-0.112	-0.168	-0.360	0.70	0.77	0.68	0.44
SB4VAR23	38	Case 2	ccc	measured bc	0.669	-0.142	-0.121	-0.168	-0.350	0.72	0.76	0.68	0.45
SB4VAR23	38	Case 2	ccc	targeted	0.675	-0.154	-0.125	-0.175	-0.353	0.70	0.75	0.67	0.44

**Table 4 cont. Normalized PCTs by Glass ID/Compositional View**

Glass ID	WL (%)	Sludge Case	Heat Treatment	Compositional View	Nepheline Assessment	$\log \text{NL[B]} (\text{g/L})$	$\log \text{NL[Li]} (\text{g/L})$	$\log \text{NL[Na]} (\text{g/L})$	$\log \text{NL[Si]} (\text{g/L})$	$\text{NL[B]} (\text{g/L})$	$\text{NL[Li]} (\text{g/L})$	$\text{NL[Na]} (\text{g/L})$	$\text{NL[Si]} (\text{g/L})$
SB4VAR24	41	Case 2	ecc	measured	0.659	0.257	0.230	0.054	-0.223	1.81	1.70	1.13	0.60
SB4VAR24	41	Case 2	ccc	measured bc	0.660	0.247	0.209	0.055	-0.228	1.77	1.62	1.13	0.59
SB4VAR24	41	Case 2	ccc	targeted	0.654	0.251	0.218	0.049	-0.217	1.78	1.65	1.12	0.61
SB4VAR24	41	Case 2	quenched	measured	0.659	-0.109	-0.090	-0.140	-0.341	0.78	0.81	0.72	0.46
SB4VAR24	41	Case 2	quenched	measured bc	0.660	-0.118	-0.111	-0.140	-0.346	0.76	0.77	0.72	0.45
SB4VAR24	41	Case 2	quenched	targeted	0.654	-0.115	-0.102	-0.146	-0.335	0.77	0.79	0.71	0.46
SB4VAR31	32	Case 3	ccc	measured	0.708	-0.175	-0.153	-0.196	-0.343	0.67	0.70	0.64	0.45
SB4VAR31	32	Case 3	ccc	measured bc	0.706	-0.170	-0.168	-0.188	-0.334	0.68	0.68	0.65	0.46
SB4VAR31	32	Case 3	ccc	targeted	0.709	-0.170	-0.156	-0.198	-0.343	0.68	0.70	0.63	0.45
SB4VAR31	32	Case 3	quenched	measured	0.708	-0.143	-0.138	-0.180	-0.328	0.72	0.73	0.66	0.47
SB4VAR31	32	Case 3	quenched	measured bc	0.706	-0.137	-0.153	-0.172	-0.319	0.73	0.70	0.67	0.48
SB4VAR31	32	Case 3	quenched	targeted	0.709	-0.137	-0.141	-0.182	-0.328	0.73	0.72	0.66	0.47
SB4VAR32	36	Case 3	ccc	measured	0.682	-0.134	-0.123	-0.153	-0.330	0.73	0.75	0.70	0.47
SB4VAR32	36	Case 3	ccc	measured bc	0.680	-0.136	-0.145	-0.145	-0.321	0.73	0.72	0.72	0.48
SB4VAR32	36	Case 3	ccc	targeted	0.681	-0.132	-0.132	-0.154	-0.327	0.74	0.74	0.70	0.47
SB4VAR32	36	Case 3	quenched	measured	0.682	-0.137	-0.136	-0.162	-0.333	0.73	0.73	0.69	0.46
SB4VAR32	36	Case 3	quenched	measured bc	0.680	-0.140	-0.158	-0.154	-0.324	0.73	0.69	0.70	0.47
SB4VAR32	36	Case 3	quenched	targeted	0.681	-0.135	-0.144	-0.163	-0.330	0.73	0.72	0.69	0.47
SB4VAR33	40	Case 3	ccc	measured	0.655	-0.088	-0.101	-0.071	-0.304	0.82	0.79	0.85	0.50
SB4VAR33	40	Case 3	ccc	measured bc	0.646	-0.083	-0.116	-0.080	-0.299	0.83	0.77	0.83	0.50
SB4VAR33	40	Case 3	ccc	targeted	0.653	-0.084	-0.103	-0.086	-0.312	0.83	0.79	0.82	0.49
SB4VAR33	40	Case 3	quenched	measured	0.655	-0.108	-0.109	-0.083	-0.314	0.78	0.78	0.83	0.49
SB4VAR33	40	Case 3	quenched	measured bc	0.646	-0.103	-0.125	-0.091	-0.309	0.79	0.75	0.81	0.49
SB4VAR33	40	Case 3	quenched	targeted	0.653	-0.104	-0.111	-0.097	-0.322	0.79	0.77	0.80	0.48
SB4VAR41	32	Case 4	ccc	measured	0.721	-0.170	-0.119	-0.196	-0.338	0.68	0.76	0.64	0.46
SB4VAR41	32	Case 4	ccc	measured bc	0.714	-0.157	-0.128	-0.199	-0.328	0.70	0.75	0.63	0.47
SB4VAR41	32	Case 4	ccc	targeted	0.715	-0.159	-0.118	-0.195	-0.320	0.69	0.76	0.64	0.48
SB4VAR41	32	Case 4	quenched	measured	0.721	-0.191	-0.139	-0.197	-0.364	0.64	0.73	0.63	0.43
SB4VAR41	32	Case 4	quenched	measured bc	0.714	-0.178	-0.148	-0.200	-0.354	0.66	0.71	0.63	0.44
SB4VAR41	32	Case 4	quenched	targeted	0.715	-0.181	-0.138	-0.196	-0.346	0.66	0.73	0.64	0.45
SB4VAR42	35	Case 4	ccc	measured	0.703	-0.161	-0.122	-0.166	-0.348	0.69	0.75	0.68	0.45
SB4VAR42	35	Case 4	quenched	measured	0.695	-0.148	-0.131	-0.169	-0.337	0.71	0.74	0.68	0.46
SB4VAR42	35	Case 4	quenched	targeted	0.695	-0.159	-0.132	-0.177	-0.339	0.69	0.74	0.67	0.46
SB4VAR42	35	Case 4	ccc	measured	0.684	-0.160	-0.124	-0.165	-0.356	0.69	0.75	0.68	0.44
SB4VAR43	38	Case 4	ccc	measured bc	0.684	-0.169	-0.145	-0.168	-0.361	0.68	0.72	0.68	0.44
SB4VAR43	38	Case 4	ccc	targeted	0.674	-0.162	-0.133	-0.178	-0.345	0.69	0.74	0.66	0.45
SB4VAR43	38	Case 4	quenched	measured	0.684	-0.144	-0.113	-0.139	-0.340	0.72	0.77	0.73	0.46
SB4VAR43	38	Case 4	quenched	measured bc	0.684	-0.154	-0.134	-0.142	-0.345	0.70	0.73	0.72	0.45

**Table 4 cont. Normalized PCTs by Glass ID/Compositional View**

Glass ID	WL (%)	Sludge Case	Heat Treatment	Compositional View	Nepheline Assessment	log NL[B] (g/L)	log NL[Li] (g/L)	log NL[Na] (g/L)	log NL [Si(g/L)]	NL[B] (g/L)	NL[Li] (g/L)	NL[Na] (g/L)	NL[Si] (g/L)
SR4VAR43	38	Case 4	quenched	targeted	0.674	-0.147	-0.122	-0.152	-0.330	0.71	0.75	0.71	0.47
SR4VAR44	41	Case 4	ccc	measured	0.659	-0.062	-0.037	-0.108	-0.325	0.87	0.92	0.78	0.47
SR4VAR44	41	Case 4	ccc	measured bc	0.660	-0.072	-0.058	-0.108	-0.330	0.85	0.88	0.78	0.47
SR4VAR44	41	Case 4	ccc	targeted	0.653	-0.062	-0.050	-0.112	-0.316	0.87	0.89	0.77	0.48
SR4VAR44	41	Case 4	quenched	measured	0.659	-0.140	-0.111	-0.143	-0.351	0.72	0.78	0.72	0.45
SR4VAR44	41	Case 4	quenched	measured bc	0.660	-0.150	-0.132	-0.143	-0.357	0.71	0.74	0.72	0.44
SR4VAR44	41	Case 4	quenched	targeted	0.653	-0.140	-0.124	-0.147	-0.343	0.72	0.75	0.71	0.45
SR4VAR51	32	Case 5	ccc	measured	0.708	-0.163	-0.115	-0.172	-0.329	0.69	0.77	0.67	0.47
SR4VAR51	32	Case 5	ccc	measured bc	0.707	-0.172	-0.136	-0.175	-0.334	0.67	0.73	0.67	0.46
SR4VAR51	32	Case 5	ccc	targeted	0.708	-0.169	-0.128	-0.175	-0.330	0.68	0.75	0.67	0.47
SR4VAR51	32	Case 5	quenched	measured	0.708	-0.162	-0.131	-0.169	-0.340	0.69	0.74	0.68	0.46
SR4VAR51	32	Case 5	quenched	measured bc	0.707	-0.171	-0.152	-0.172	-0.345	0.67	0.70	0.67	0.45
SR4VAR51	32	Case 5	quenched	targeted	0.708	-0.168	-0.143	-0.172	-0.341	0.68	0.72	0.67	0.46
SR4VAR52	35	Case 5	ccc	measured	0.688	-0.143	-0.115	-0.148	-0.331	0.72	0.77	0.71	0.47
SR4VAR52	35	Case 5	ccc	measured bc	0.690	-0.153	-0.136	-0.147	-0.336	0.70	0.73	0.71	0.46
SR4VAR52	35	Case 5	ccc	targeted	0.688	-0.147	-0.128	-0.150	-0.328	0.71	0.74	0.71	0.47
SR4VAR52	35	Case 5	quenched	measured	0.688	-0.144	-0.119	-0.144	-0.337	0.72	0.76	0.72	0.46
SR4VAR52	35	Case 5	quenched	measured bc	0.690	-0.154	-0.140	-0.144	-0.342	0.70	0.72	0.72	0.46
SR4VAR52	35	Case 5	quenched	targeted	0.688	-0.148	-0.132	-0.147	-0.333	0.71	0.74	0.71	0.46
SR4VAR53	38	Case 5	ccc	measured	0.674	-0.152	-0.118	-0.135	-0.341	0.70	0.76	0.73	0.46
SR4VAR53	38	Case 5	ccc	measured bc	0.667	-0.138	-0.127	-0.134	-0.331	0.73	0.75	0.73	0.47
SR4VAR53	38	Case 5	ccc	targeted	0.667	-0.136	-0.120	-0.134	-0.326	0.73	0.76	0.73	0.47
SR4VAR53	38	Case 5	quenched	measured	0.674	-0.147	-0.120	-0.104	-0.343	0.71	0.76	0.79	0.45
SR4VAR53	38	Case 5	quenched	measured bc	0.667	-0.133	-0.128	-0.103	-0.332	0.74	0.74	0.79	0.47
SR4VAR53	38	Case 5	quenched	targeted	0.667	-0.131	-0.121	-0.103	-0.328	0.74	0.76	0.79	0.47
SR4VAR54	41	Case 5	ccc	measured	0.649	0.009	0.003	-0.049	-0.286	1.02	1.01	0.89	0.52
SR4VAR54	41	Case 5	ccc	measured bc	0.640	0.022	-0.006	-0.052	-0.275	1.05	0.99	0.89	0.53
SR4VAR54	41	Case 5	ccc	targeted	0.645	0.003	-0.006	-0.054	-0.282	1.02	0.99	0.88	0.52
SR4VAR54	41	Case 5	quenched	measured	0.649	-0.106	-0.102	-0.086	-0.323	0.78	0.79	0.82	0.47
SR4VAR54	41	Case 5	quenched	measured bc	0.640	-0.092	-0.111	-0.089	-0.313	0.81	0.77	0.81	0.49
SR4VAR54	41	Case 5	quenched	targeted	0.645	-0.106	-0.111	-0.092	-0.320	0.78	0.77	0.81	0.48

### **4.3.5 Acceptability of the SB4 VS Glasses**

The NL [B] for each quenched and ccc glass is well below that of the reference EA glass (16.695 g/L).<sup>12</sup> For the quenched glasses, the NL [B] (based on measured bc compositions) ranges from 0.65 g/L (SB4VAR21) to 0.83 g/L (SB4VAR13). Within each SB4 post-decant option, the general trend observed for the quenched glasses is a gradual decrease in durability with increasing WL. For example, in Case #1 (SB4 nominal pre-decant) the NL [B] for glasses targeting 34, 38, and 42% WL are 0.70, 0.78, and 0.83 g/L, respectively and in Case #2 (SB4 after the 100K decant), the NL [B] for glasses targeting 32, 35, 38, 41% WL are 0.65, 0.70, 0.72, and 0.76 g/L, respectively. Similar trends are also observed for Cases #3, #4, and #5. Regardless of the SB4 option or targeted WL, the durabilities of the quenched Frit 510-based glasses are very acceptable.

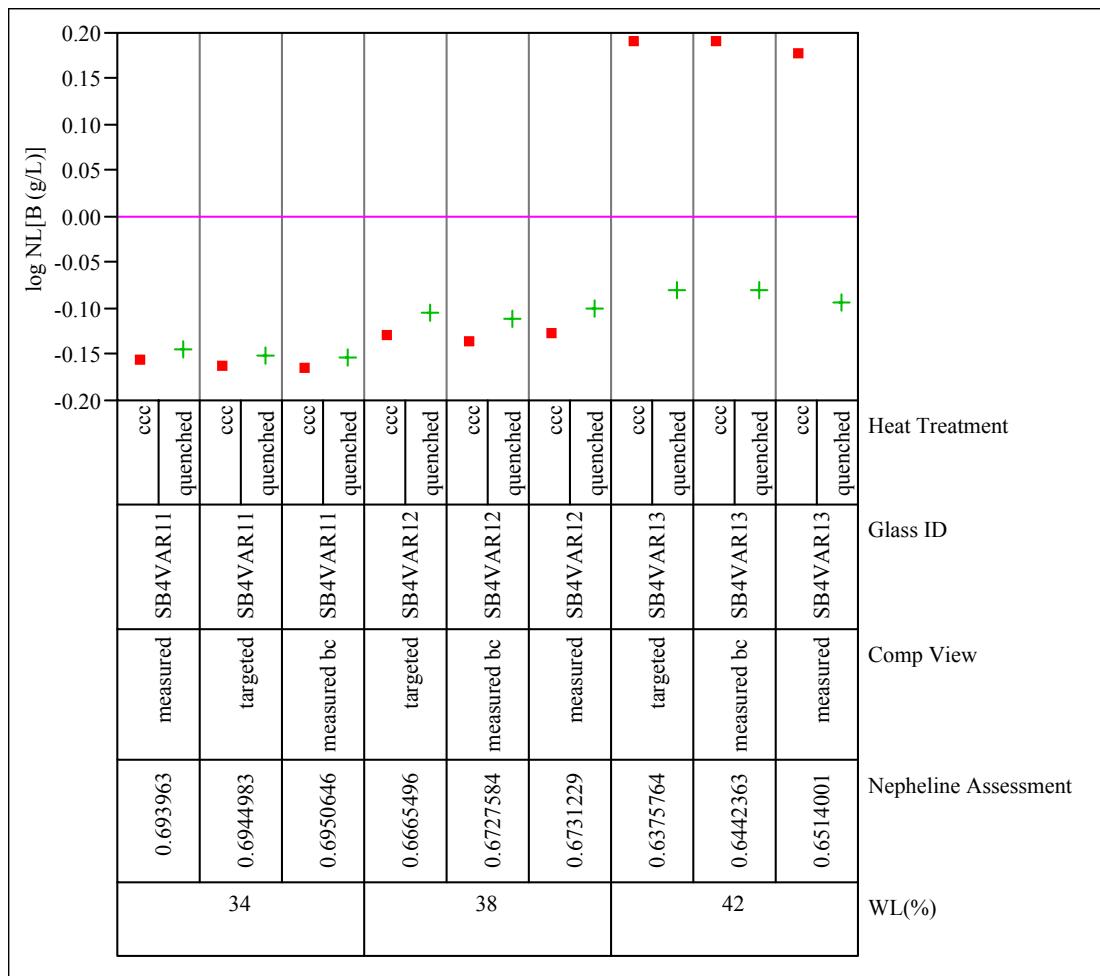
With respect to the ccc versions of the variability study glasses, the NL [B] (based on measured bc compositions) range from 0.65 g/L (SB4VAR21ccc) to 1.77 g/L (SB4VAR24ccc). As in the quenched glasses, the PCT responses for all of the ccc glasses are acceptable relative to the EA reference glass (16.695 g/L). A gradual decrease in durability with increasing WL (within a specific option) is observed. For example, the NL [B] of the Case #1 ccc glasses are 0.68, 0.73, and 1.54 g/L for the 34, 38, and 41% WL targets and for Case #2, the NL [B] of the 32, 35, 38, and 41% WL glasses are 0.65, 0.67, 0.75, and 1.77 g/L. Again, all of the NL [B] values are very acceptable relative to EA and the durability trend as a function of WL is consistent for both quenched and ccc glasses.

One primary difference is observed for two of the ccc glasses, specifically SB4VAR13ccc (Case #1 at 42% WL) and SB4VAR24ccc (Case #2 at 41% WL). Although the PCT responses are acceptable, there is a considerable increase (a factor of approximately 2) in the PCT response as the WL is raised to the maximum level considered in this study. Consider Figure 4 which shows the log NL [B] for the Case #1 (Frit 510-SB4 nominal (pre-decant)) glasses as a function of WL, compositional view, and thermal treatment (quenched and ccc). There is very little difference (no practical significance) between the quenched and ccc glasses targeting 34 and 38% WL; however, a significant and potentially practical difference exists between the quenched and ccc versions of the glass at 42% WL. More specifically, the NL [B] of the SB4VAR12ccc (Case #1 at 38% WL) is 0.73 g/L, while SB4VAR13ccc (Case #1 at 42% WL) has a NL [B] of 1.54 g/L. This same trend is observed for Case #2 (post 100K decant) as the NL [B] of the ccc glasses at 38 and 41% WL are 0.75 and 1.77 g/L, respectively. The magnitude of the decrease in durability for these two glasses is inconsistent with the general differences of the lower WL glasses within their respective options. Such a trend in NL [B] would suggest that nepheline formation may be responsible for the lower durabilities of these glasses. In fact, nepheline formation was observed in both SB4VAR13ccc and SB4VAR24ccc (refer to Section 4.2.2). While the increased NL [B] of SB4VAR44ccc (Case #4 at 41% WL) and SB4VAR54ccc (Case #5 at 41%) would suggest the presence of nepheline, none was detected with XRD. Due to the detection limit of the instrument, these results indicate that the PCT response of a sample may be more sensitive to the presence of nepheline than XRD.

Although not an issue in terms of acceptability, the fact that nepheline was detected in two of the study glasses are the first results which indicate that the current nepheline discriminator value of 0.62 is not conservative. The nepheline discriminator was implemented into PCCS for SB4 based on the fact that all of the historical glasses evaluated with nepheline values of 0.62 or greater did not contain nepheline via XRD analysis.<sup>15</sup> During that assessment, glasses were identified with nepheline discriminator values less than 0.62 that were not characterized by the formation of nepheline upon slow cooling. These results suggest that there was either a compositional or thermal (kinetic) effect not fully captured in the discriminator but at that point the 0.62 value was deemed to be conservative. The current results (XRD patterns and PCT response for SB4VAR13 and SB4VAR24) suggest that

the discriminator is not conservative within this glass compositional region. These results have altered concurrent experimental studies that continue to focus on both compositional and heat treatment effects for nepheline formation in an attempt to gain a more fundamental understanding of its formation and impacts to DWPF type glasses.

Although these two glasses do cause some concern over the continued use of the 0.62 nepheline value to predict nepheline in ccc glasses for future DWPF glass systems, the impact on the current DWPF operating window for the SB4 system is of little concern. Nepheline was only observed in glasses targeting 41 or 42% WL. Current processing of the Frit 510–SB4 system in DWPF has nominally targeted 34% WL. For those SB4 variability study glasses targeting these lower WLs, nepheline formation was not observed and the minimal difference in PCT response between quenched and ccc versions supported its absence. It should also be noted that the glasses targeting the higher WLs in the two “post decanted” systems (Case #3 and Case #4) did not formally show nepheline formation via XRD results, but a comparison of the quenched and ccc PCT response do suggest crystallization may be present below the detection limit of the X-ray diffractometer.



**Figure 4. Effect of heat treatment on  $\log NL[B \text{ (g/L)}]$  for Case #1.**

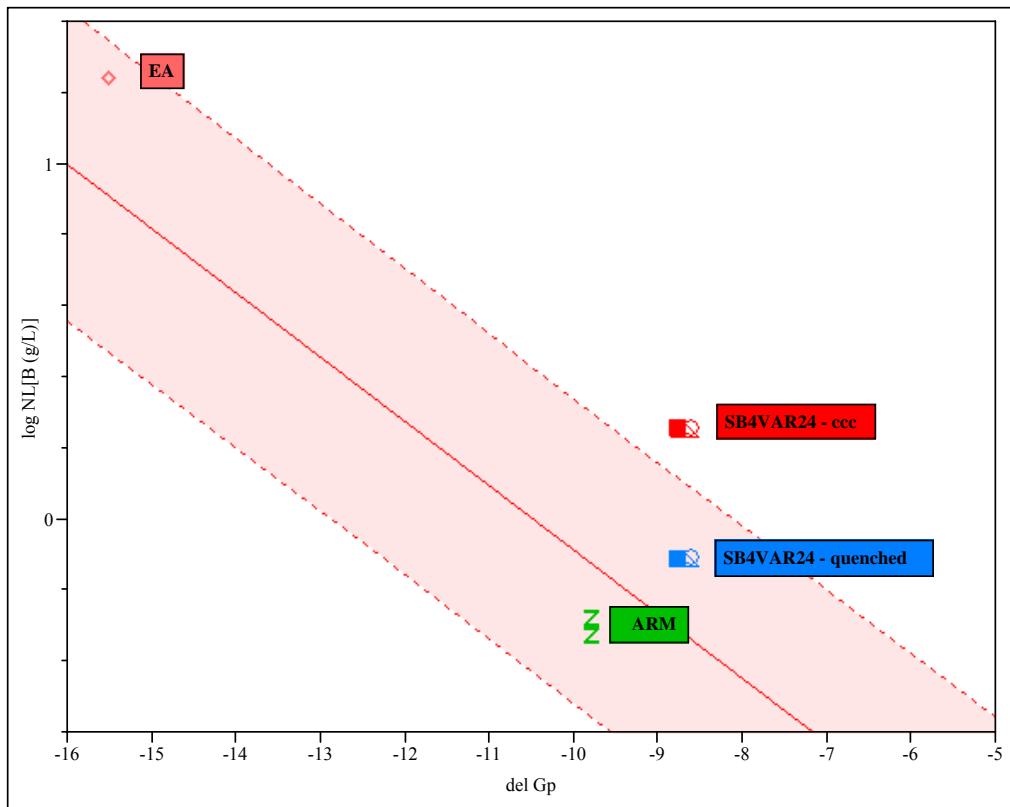
#### **4.3.6 Predicted versus Measured PCTs**

As discussed in Section 4.3.5 and shown in Table 5, the durabilities of the SB4/Decant VS glasses are all very acceptable when compared to the durability of EA, which meets one objective of the variability study. The second objective is to evaluate the applicability of the current durability model to the compositional region of interest. The term applicability refers to the ability of the current durability model to predict the PCT response of the study glasses. Note that the current durability model is only valid for homogeneous glasses and is not expected to predict the PCT response of glasses containing crystallization that would significantly alter the response (i.e., nepheline). Non-homogeneous glasses (based on XRD analysis) in this study include SB4VAR13ccc (Case #1 at 42% WL) and SB4VAR24ccc (Case #2 at 41% WL).

Exhibit B8 in Appendix B provides plots of the DWPF models that relate the logarithm of the normalized PCT (for each element of interest) to a linear function of a free energy of hydration term ( $\Delta G_p$ , kcal/100g glass) derived for all of the glass compositional views and heat treatments.<sup>14</sup> Prediction limits (at a 95% confidence) for an individual PCT result are also plotted along with the linear fit. The EA and ARM results are also indicated on these plots. Exhibit B9 in Appendix B provides a version of these plots for the quenched glasses only and Exhibit B10 in Appendix B provides a version for ccc glasses only. While all of these glasses show acceptable PCT responses, some points fall above the confidence limits for the ccc versions of the study glasses.

Figure 5 provides a closer look at the PCT response that falls above the confidence interval, which is the ccc version of glass SB4VAR24. The PCT response for the quenched version of this glass is also included on the plot along with the EA and ARM results. The points lying above the 95% confidence interval are associated with the three compositional views (target, measured and measured bc) of SB4VAR24ccc. As previously mentioned, SB4VAR24ccc contains nepheline, which is the cause for the higher PCT response and the inability of the  $\Delta G_p$  model to predict the NL [B]. Implementation of the nepheline discriminator in DWPF's PCCS is the primary mechanism to avoid the production of a glass that precipitates nepheline upon slow cooling, thus creating a potentially unacceptable glass.

Although the PCT response for the SB4VAR24ccc glass is acceptable, there is currently no tool or model within the DWPF's process control system that would have prevented this glass (as well as SB4VAR13) from being processed. As previously mentioned, targeted WLs for the Frit 510-SB4 system have been approximately 34%, so a comfortable processing margin exists for the operating window since nepheline formed only in glasses targeting a WL of either 41 or 42% WL. These data do identify the need for a better understanding of the current nepheline discriminator over DWPF compositions of interest.



**Figure 5. Log NL[B (g/L)] versus B Del Gp model with a 95% confidence interval for individual PCTs.**

#### 4.4 A Review of the Nepheline Assessments for DWPF's SB4 Process Batches

In order to evaluate the potential impacts of the two non-conservative data points from this study on DWPF operations with SB4 (pre-Tank 40 decant), values of the nepheline discriminator for the SB4 SME batches 402 through 436 that have been processed by the DWPF were assessed. These values were obtained from the Sample\_Date Folder maintained by the DWPF Chem Group on the WG09 server and are shown in Table 6. The smallest nepheline discriminator value the DWPF has recorded as part of the SB4 processing to date is 0.704, which is well above the 0.62 nominal limit for this constraint as well as being above the 0.654 value of the SB4VAR24 glass of this study.

**Table 6. Nepheline Discriminator Values Recorded by DWPF during the Processing of SB4**

SME Batch	402	403	404	405	406	407	408	409	410	411	412	413
Nepheline Value	0.719	0.743	0.727	0.742	0.726	0.735	0.723	0.722	0.725	0.719	0.717	0.723
SME Batch	414	415	416	417	418	419	420	421	422	423	424	425
Nepheline Value	0.721	0.752	0.729	0.728	0.730	0.712	0.720	0.732	0.731	0.724	0.711	0.707
SME Batch	426	427	428	429	430	431	432	433	434	435	436	
Nepheline Value	0.723	0.717	0.704	0.722	0.722	0.709	0.719	0.721	0.722	0.727	0.735	

The nepheline values predicted by the actual DWPF SME analytical data in combination with the data of the study glasses provide no indication that the production glasses within the Frit 510–SB4 are not acceptable. To support this statement, SRNL fabricated five supplemental glasses based on the specific SB4 SME batch information from WG09. Specifically, elemental compositional information from SME batches 434 and 435<sup>d</sup> were obtained from WG09, converted to oxides, and normalized. The SME data suggested that the WLs for these two Frit 510–SB4 nominal (pre-Tank 40 decant) glasses were approximately 33 and 32%, respectively. In addition to these two specific glasses three other glasses were made using the nominal Case #1 variability study composition coupled with Frit 510 at WLs of ~32, 33, and 34% WL.<sup>e</sup> The target and measured compositions of these five supplemental glasses are shown in Table 7 and Table 8.<sup>f</sup> The nomenclature for these pre-decant glasses can be summarized as follows:

- 1.) SB4PS1: Nominal glass targeting the measured composition of SME batch 434 (normalized)
- 2.) SB4PS2: Nominal glass targeting the measured composition of SME batch 435 (normalized)
- 3.) SB4PS3: Nominal glass targeting a Frit 510 – SB4 Case #1 glass at 32% WL
- 4.) SB4PS4: Nominal glass targeting a Frit 510 – SB4 Case #1 glass at 33% WL
- 5.) SB4PS5: Nominal glass targeting a Frit 510 – SB4 Case #1 glass at 34% WL

Table 9 summarizes the PCT results (normalized to the target compositions) of both the quenched and ccc versions of these five supplemental glasses. The results indicate that all of the glasses are acceptable and predictable<sup>g</sup> regardless of thermal history (quenched or ccc). The NL [B] ranges from 0.41 g/L (SB4PS1ccc) to 0.52 g/L (SB4PS3 quenched and SB4PS4 ccc). When comparing the quenched glasses to their ccc counterparts, there is very little (if any) difference between the PCT response, which suggests that the ccc glasses are void of nepheline. These results have also been confirmed by XRD.<sup>h,i</sup> The PCT responses of these supplemental glasses are comparable to the lower WL glasses of the initial 18 variability study glasses. More specifically, the PCT responses of the quenched and ccc SB4VAR11 (Case #1, pre-Tank 40 decant glass at 34% WL) are 0.70 and 0.68 NL [B], respectively. Again, these data coupled with nepheline values predicted by the actual SME analytical data and the measured PCT response from the study glasses indicate that the production glasses are void of nepheline and are very acceptable regardless of the thermal history. Even though the PCT responses for the higher WL post-Tank 40 decant study glasses are acceptable and no nepheline was observed via XRD, it is recommended that DWPF continue to target lower WLs during processing of SB4.

---

<sup>d</sup> It should be noted that SB4 pour stream samples were also pulled during processing of these two SME batches. The first pour stream sample was pulled on 3/12/08 during the processing SME 434. The second pour stream sample was pulled on 3/18/08 during the processing SME 435. The two pour stream samples have been transported to SRNL, but have not been characterized.

<sup>e</sup> The Al<sub>2</sub>O<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub>, Na<sub>2</sub>O and U<sub>3</sub>O<sub>8</sub> content of each SME batch were compared. All of the variability study glasses and supplemental glasses have compositions that are within the bounds of the SME batch compositions, with the exception of 2 glasses (SB4VAR24 and SB4VAR54). Both of these glasses targeted higher WLs (41%), so they are not expected to fall within the bounds of the SME batches. A comparison of the data is shown in Appendix C, Table C1.

<sup>f</sup> No analytical plan was used as guidance for the chemical composition measurements, so there are no measured bc values. The measured compositions in Table 8 are an average of the values obtained by the LM and PF methods.

<sup>g</sup> For more information see page 135 of WSRC-NB-2006-00168.

<sup>h</sup> The XRD patterns of the supplemental glasses (ccc) can be viewed in the laboratory notebook for the SB4 variability study on page 132 (WSRC-NB-2006-00168).

<sup>i</sup> During the testing of the supplemental glasses, replicates of SB4VAR13ccc (Case #1 at 42% WL) and SB4VAR24ccc (Case #2 at 41% WL) were fabricated and tested to confirm reproducibility. While the composition and PCT results correspond to the previous values, the XRD patterns *do not* indicate the presence of nepheline (see pages 132 and 134 of WSRC-SB-2006-00168 for the PCT and XRD results). We have recognized the issues and will integrate these results into future nepheline testing.

Table 7. Target Compositions of the SB4PS Glasses

Glass ID	SB4PS1	SB4PS2	SB4PS3	SB4PS4	SB4PS5
Frit					
SME 434	SME 435	31.7	33.2	34	
WL					
Al <sub>2</sub> O <sub>3</sub>	7.61	7.37	7.92	8.29	8.49
B <sub>2</sub> O <sub>3</sub>	8.53	8.77	9.56	9.35	9.24
CaO	0.84	0.79	0.87	0.91	0.93
Cr <sub>2</sub> O <sub>3</sub>	0.05	0.04	0.05	0.05	0.05
CuO	0.01	0.00	0.02	0.02	0.02
Fe <sub>2</sub> O <sub>3</sub>	8.07	8.03	9.00	9.42	9.65
K <sub>2</sub> O	0.08	0.02	0.11	0.12	0.12
Li <sub>2</sub> O	5.19	5.31	5.46	5.34	5.28
MgO	0.79	0.85	0.85	0.89	0.92
MnO	1.43	1.57	1.81	1.89	1.94
Na <sub>2</sub> O	12.12	11.98	11.99	12.18	12.28
NiO	0.45	0.46	0.50	0.52	0.54
SO <sub>4</sub>	0.44	0.42	0.42	0.44	0.45
SiO <sub>2</sub>	51.37	51.48	48.66	47.65	47.11
TiO <sub>2</sub>	0.09	0.07	0.01	0.01	0.01
U <sub>3</sub> O <sub>8</sub>	2.73	2.68	2.75	2.88	2.94
ZrO <sub>2</sub>	0.19	0.15	0.03	0.03	0.03

Table 8. Measured Compositions of the SB4PS Glasses

Glass ID	SB4PS1	SB4PS2	SB4PS3	SB4PS4	SB4PS5
Frit					
WL					
SME 434	SME 435	31.7	33.2	34	
Al <sub>2</sub> O <sub>3</sub>	7.69	7.41	7.89	8.61	8.51
B <sub>2</sub> O <sub>3</sub>	8.87	9.29	9.71	9.60	9.42
CaO	0.82	0.77	0.85	0.91	0.89
Cr <sub>2</sub> O <sub>3</sub>	0.07	0.05	0.05	0.06	0.06
CuO	0.02	0.01	0.02	0.03	0.03
Fe <sub>2</sub> O <sub>3</sub>	7.80	7.91	8.66	9.47	9.33
K <sub>2</sub> O	0.08	0.02	0.12	0.12	0.11
Li <sub>2</sub> O	5.19	5.46	5.49	5.43	5.27
MgO	0.78	0.83	0.83	0.91	0.91
MnO	1.43	1.58	1.80	1.96	1.94
Na <sub>2</sub> O	12.47	12.30	12.40	13.00	12.39
NiO	0.41	0.43	0.45	0.49	0.50
SO <sub>4</sub>	0.39	0.39	0.39	0.40	0.41
SiO <sub>2</sub>	51.25	51.93	48.72	47.94	46.87
TiO <sub>2</sub>	0.09	0.07	0.02	0.02	0.02
U <sub>3</sub> O <sub>8</sub>	2.73	2.67	2.68	2.94	2.92
ZrO <sub>2</sub>	0.00	0.14	0.02	0.02	0.02

**Table 9. Normalized\* PCT Responses of the Frit 510 – SB4 Supplemental Glasses (quenched and ccc)**

Sample	NL (g/L)			
	B	Li	Na	Si
<b>SB4PS-1</b>	0.44	0.43	0.62	0.46
<b>SB4PS-1-ccc</b>	0.41	0.41	0.61	0.45
<b>SB4PS-2</b>	0.44	0.43	0.63	0.46
<b>SB4PS-2-ccc</b>	0.42	0.42	0.61	0.45
<b>SB4PS-3</b>	0.52	0.45	0.69	0.48
<b>SB4PS-3-ccc</b>	0.49	0.44	0.66	0.48
<b>SB4PS-4</b>	0.49	0.43	0.66	0.47
<b>SB4PS-4-ccc</b>	0.52	0.45	0.70	0.50
<b>SB4PS-5</b>	0.50	0.44	0.74	0.48
<b>SB4PS-5-ccc</b>	0.50	0.44	0.71	0.49

\*Based on measured compositions

## 5.0 Conclusions

Frit 510 is a viable option for the processing of SB4 after a Tank 40 decant and the addition of products from the Actinide Removal Process (ARP). The addition of ARP did not have any negative impacts on the acceptability and predictability of the variability study glasses.

The durabilities of all of the study glasses (both quenched and ccc) are well below that of the NL [B] reference EA glass (16.695 g/L). For the quenched glasses, the NL [B] (based on measured bc compositions) ranges from 0.65 g/L (SB4VAR21) to 0.83 g/L (SB4VAR13). With respect to the ccc versions of the variability study glasses, the NL [B] (based on measured bc compositions) range from 0.65 g/L (SB4VAR21ccc) to 1.77 g/L (SB4VAR24ccc). A gradual decrease in durability is observed with increasing WL for the quenched glasses. Although a similar trend is observed for the ccc glasses, the primary distinction is the magnitude of the difference at higher WLs. The durabilities of all of the study glasses are predictable using the current Product Composition Control System (PCCS) durability models with the exception of SB4VAR24ccc (Case #2 at 41%). PCCS is not applicable to non-homogeneous glasses (i.e. glasses containing crystals such as acmite and nepheline), thus SB4VAR24ccc should not be predictable as it contains nepheline.

The presence of nepheline has been confirmed in both SB4VAR13ccc and SB4VAR24ccc by X-ray diffraction (XRD). These two glasses are the first results which indicate that the current nepheline discriminator value of 0.62 is not conservative. The nepheline discriminator was implemented into PCCS for SB4 based on the fact that all of the historical glasses evaluated with nepheline values of 0.62 or greater did not contain nepheline via XRD analysis. Although these two glasses do cause some concern over the use of the 0.62 nepheline value for future DWPF glass systems, the impact to the current SB4 system is of little concern. Specifically, the formation of nepheline was observed in glasses targeting 41 or 42% WL. Current processing of the Frit 510–SB4 system in DWPF has nominally targeted 34% WL. For the SB4 variability study glasses targeting these lower WLs, nepheline formation was not observed and the minimal difference in PCT response between quenched

and ccc versions supported its absence.

## 6.0 References

1. M.E. Stone, F.C. Raszewski, B.R. Pickenheim, T.B. Edwards, and D.K. Peeler, "Impacts of a Tank 40 Supernate Decant to DWPF Glass Formulation and CPC Processing: A Preliminary Assessment for SB4," Savannah River National Laboratory, Aiken, SC, Report No. SRNL-PSE-2007-00257, 2007.
2. B.A. Davis, "SB4 Flowsheet and Variability Studies for Tank 40H 100,000 Gallon Decant Technical Task Request," Liquid Waste Organization, Aiken, SC, Report No. HLW-DWPF-TTR-2008-0009, Rev. 0, 2007.
3. F.C. Raszewski, T.B. Edwards, and D.K. Peeler, "The Impact of a Tank 40H Decant on the Projected Operating Windows for SB4 and Glass Selection Strategy in Support of the Variability Study," Savannah River National Laboratory, Aiken, SC, Report No. WSRC-STI-2008-00017, 2008.
4. A.S. Taylor, T.B. Edwards, J.C. George, T.K. Snyder, and D.K. Peeler, "The SRNL Composition - Properties (ComPro<sup>TM</sup>) Database," Westinghouse Savannah River Company, Aiken, SC, Report No. WSRC-RP-2004-00704, Revision 0, 2004.
5. K.M. Fox, T.B. Edwards, D.K. Peeler, D.R. Best, I.A. Reamer, and R.J. Workman, "High Level Waste (HLW) Sludge Batch 4 (SB4) Variability Study," Washington Savannah River Company, Aiken, SC, Report No. WSRC-STI-2006-00204, Revision 0, 2006.
6. K.M. Fox, T.B. Edwards, D.K. Peeler, D.R. Best, I.A. Reamer, and R.J. Workman, "High Level Waste (HLW) Sludge Batch 4 (SB4) with Frit 418: Results of a Phase II Variability Study," Washington Savannah River Company, Aiken, SC, Report No. WSRC-STI-2006-00329, Revision 0, 2006.
7. S.L. Marra and C.M. Jantzen, "Characterization of Projected DWPF Glass Heat Treated to Simulate Canister Centerline Cooling," Westinghouse Savannah River Company, Aiken, SC, Report No. WSRC-TR-92-142, Rev. 1, 1993.
8. "Glass Batching," Savannah River National Laboratory, Aiken, SC, Report No. ITS-0001, Rev. 1, 2007.
9. "Glass Melting," Savannah River National Laboratory, Aiken, SC, Report No. ITS-0003, Rev. 2, 2007.
10. T.B. Edwards, "Analytical Plans for Measuring the Chemical Compositions of Glasses from an EM-20 Study and Glasses from Two DWPF Studies," Savannah River National Laboratory, Aiken, SC, Report No. SRNL-SCS-2008-00003, 2008.
11. "Standard Test Methods for Determining Chemical Durability of Nuclear, Hazardous, and Mixed Waste Glasses and Multiphase Glass Ceramics: The Product Consistency Test (PCT)," ASTM International, West Conshohocken, PA, Report No. ASTM C 1285-02, 2002.

12. C.M. Jantzen, N.E. Bibler, D.C. Beam, C.L. Crawford, and M.A. Pickett, "Characterization of the Defense Waste Processing Facility (DWPF) Environmental Assessment (EA) Glass Standard Reference Material," Westinghouse Savannah River Company, Aiken, SC, Report No. WSRC-TR-92-346, Rev. 1, 1993.
13. T.B. Edwards, "Analytical Plans for Measuring the PCT Solutions of Glasses from an EM-20 Study and Glasses from Two DWPF Studies," Savannah River National Laboratory, Aiken, SC, Report No. SRNL-SCS-2008-00005, 2008.
14. C.M. Jantzen, J.B. Picket, K.G. Brown, T.B. Edwards, and D.C. Beam, "Process/Product Models for the Defense Waste Processing Facility (DWPF): Part I. Predicting Glass Durability from Composition Using a Thermodynamic Hydration Energy Reaction Model (THERMO)," Westinghouse Savannah River Company, Aiken, SC, Report No. WSRC-TR-93-672, Rev. 1, 1995.
15. T.B. Edwards, D.K. Peeler, and K.M. Fox, "The Nepheline Discriminator: Justification and DWPF PCCS Implementation Details," Washington Savannah River Company, Aiken, SC, Report No. WSRC-STI-2006-00014, Revision 0, 2006.

## **APPENDIX A**

### **TABLES AND EXHIBITS SUPPORTING THE ANALYSIS OF THE CHEMICAL COMPOSITION MEASUREMENTS OF THE SB4/DECANT VARIABILITY STUDY GLASSES**

*This page intentionally left blank.*







**Table A1. Measured Elemental Concentrations (wt%) for Samples Prepared Using Lithium Metaborate (part 1)**

Set	Glass ID	Block	Sub-Block	Sequence	Lab ID	Ag <sup>b</sup> (wt%)	Al (wt%)	Ba (wt%)	Ca (wt%)	Cd (wt%)	Ce (wt%)	Co (wt%)	Cr (wt%)	Cu (wt%)	Fe (wt%)	K (wt%)	La (wt%)	Mg (wt%)	Mn (wt%)
2	SB5.08	2	2	9	N10LM12	5.27	0.037	0.541	0.014	0.052	<0.010	0.092	<0.010	0.73	0.073	<0.100	0.314	1.59	
2	Batch1	2	2	10	BCHLM2-222	2.66	0.128	0.859	<0.010	0.01	<0.010	0.073	0.304	8.91	2.53	<0.100	0.843	1.31	
2	U std	2	2	11	UsdlM2-222	2.2	<0.010	0.928	<0.010	0.010	0.164	<0.010	9.39	2.26	<0.100	0.731	2.2		
2	SB5.03	2	2	12	N09LM12	6.14	0.032	1.55	0.012	0.086	<0.010	0.081	<0.010	5.85	0.008	<0.100	0.282	1.41	
2	SB5.10	2	2	13	N08LM22	4.41	0.037	1.62	0.016	0.122	<0.010	0.085	<0.010	6.99	0.015	<0.100	0.33	1.71	
2	SB5.09	2	2	14	N04LM22	4.34	0.038	2.58	0.014	0.085	<0.010	0.096	<0.010	6.63	0.014	<0.100	0.348	1.57	
2	SB5.03	2	2	15	N09LM22	5.96	0.034	1.51	0.013	0.089	<0.010	0.085	<0.010	5.59	0.007	<0.100	0.298	1.36	
2	SB5.08	2	2	16	N10LM22	5.01	0.037	0.513	0.012	0.054	<0.010	0.089	<0.010	6.59	0.01	<0.100	0.314	1.48	
2	SB5.06	2	2	17	N01LM12	5.19	0.036	1.56	0.012	0.092	<0.010	0.083	<0.010	6.51	0.012	<0.100	0.315	1.56	
2	SBAVAR32	2	2	18	N11LM12	4.92	0.021	0.677	<0.010	0.016	<0.010	0.046	0.018	6.72	0.106	<0.100	0.6	1.55	
2	Batch1	2	2	19	BCHLM2-223	2.62	0.134	0.833	<0.010	0.011	<0.010	0.077	0.304	8.91	2.48	<0.100	0.888	1.34	
2	U std	2	2	20	UsdlM2-223	2.2	<0.010	0.881	<0.010	0.173	<0.010	9.16	2.17	<0.100	0.767	2.18			







**Table A2. Measured Elemental Concentrations (wt%) for Samples Prepared Using Lithium Metaborate (part 2)**

Set	Glass ID	Block	Sub-Block	Sequence	Lab ID	Na (wt%)	Nb (wt%)	Ni (wt%)	P (wt%)	Pb (wt%)	S (wt%)	Si (wt%)	Sr (wt%)	Ti (wt%)	U (wt%)	Zn (wt%)	Zr (wt%)	
2	SB4VAR31	2	1	14	N06LM21	8.69	<0.010	0.362	<0.100	<0.020	0.103	22.8	<0.010	<0.100	0.015	2.26	<0.010	0.017
2	SB5-10	2	1	15	N08LM21	9.8	<0.010	0.86	<0.100	<0.020	0.107	21.4	0.121	<0.100	0.012	2.69	<0.010	0.081
2	SB5-08	2	1	16	N10LM11	10.4	<0.010	0.877	<0.100	<0.020	0.105	20.7	0.11	<0.100	0.012	2.56	<0.010	0.075
2	SB5-09	2	1	17	N04LM21	9.8	<0.010	0.89	<0.100	<0.020	0.107	20.7	0.118	<0.100	0.012	2.68	<0.010	0.089
2	SB5-06	2	1	18	N01LM21	10.2	<0.010	0.74	<0.100	<0.020	<0.100	21.7	0.106	<0.100	0.01	2.65	<0.010	0.071
2	Batch 1	2	1	19	BCHLM2-213	6.66	0.031	0.558	<0.100	<0.020	<0.100	24.2	<0.010	<0.100	0.399	<0.100	0.010	0.066
2	U std	2	1	20	UsdlM2-213	8.49	0.051	0.81	<0.100	<0.020	<0.100	21.7	<0.010	<0.100	0.578	1.96	<0.010	<0.010
2	Batch 1	2	2	1	BCHLM2-221	6.91	0.028	0.557	<0.100	<0.020	<0.100	23.7	<0.010	<0.100	0.394	<0.100	<0.010	0.062
2	U std	2	2	2	UsdlM2-221	9.13	0.047	0.805	<0.100	<0.020	<0.100	22	<0.010	<0.100	0.575	2.11	<0.010	<0.010
2	SB4VAR31	2	2	3	N06LM22	9.02	<0.010	0.357	<0.100	<0.020	0.100	22.9	<0.010	<0.100	0.012	2.41	<0.010	0.014
2	SB4VAR32	2	2	4	N11LM22	9.24	<0.010	0.405	<0.100	<0.020	0.115	21.9	<0.010	<0.100	0.01	2.71	<0.010	0.016
2	SB5-10	2	2	5	N08LM12	10.1	<0.010	0.839	<0.100	<0.020	0.107	22.1	0.118	<0.100	0.010	2.88	<0.010	0.077
2	SB5-06	2	2	6	N01LM22	10.2	<0.010	0.789	<0.100	<0.020	<0.100	21.7	0.107	<0.100	0.010	2.69	<0.010	0.072
2	SB4VAR31	2	2	7	N06LM12	8.97	<0.010	0.38	<0.100	<0.020	0.104	22.9	<0.010	<0.100	0.012	2.38	<0.010	0.016
2	SB5-09	2	2	8	N04LM12	10.4	<0.010	0.843	<0.100	<0.020	0.107	21.6	0.12	<0.100	<0.010	2.87	<0.010	0.083
2	SB5-08	2	2	9	N10LM12	10.9	<0.010	0.881	<0.100	<0.020	0.101	21.3	0.105	<0.100	<0.010	2.71	<0.010	0.073
2	Batch 1	2	2	10	BCHLM2-222	7.1	0.027	0.562	<0.100	<0.020	<0.100	24.2	<0.010	<0.100	0.396	<0.100	<0.010	0.063
2	U std	2	2	11	UsdlM2-222	9.17	0.047	0.812	<0.100	<0.020	<0.100	22.1	<0.010	<0.100	0.579	2.08	<0.010	<0.010
2	SB5-03	2	2	12	N09LM12	10.7	<0.010	0.747	<0.100	<0.020	<0.100	21.5	0.093	<0.100	<0.010	2.46	<0.010	0.068
2	SB5-10	2	2	13	N08LM22	10.4	<0.010	0.877	<0.100	<0.020	0.104	22.1	0.111	<0.100	<0.010	2.86	<0.010	0.078
2	SB5-09	2	2	14	N04LM22	10.3	<0.010	0.926	<0.100	<0.020	0.108	20.7	0.112	<0.100	<0.010	2.82	<0.010	0.088
2	SB5-03	2	2	15	N09LM22	10.4	<0.010	0.796	<0.100	<0.020	<0.100	20.8	0.092	<0.100	<0.010	2.42	<0.010	0.071
2	SB5-08	2	2	16	N10LM22	10.4	<0.010	0.838	<0.100	<0.020	<0.100	21.3	0.098	<0.100	<0.010	2.57	<0.010	0.071
2	SB5-06	2	2	17	N01LM12	10.4	<0.010	0.84	<0.100	<0.020	0.103	21.4	0.106	<0.100	<0.010	2.65	<0.010	0.075
2	SB4VAR32	2	2	18	N11LM12	9.61	<0.010	0.419	<0.100	<0.020	0.118	21.4	<0.010	<0.100	0.01	2.66	<0.010	0.017
2	Batch 1	2	2	19	BCHLM2-223	6.93	0.028	0.586	<0.100	<0.020	<0.100	24.1	<0.010	<0.100	0.407	<0.100	<0.010	0.064
2	U std	2	2	20	UsdlM2-223	9.21	0.048	0.851	<0.100	<0.020	<0.100	22	<0.010	<0.100	0.592	2.09	<0.010	<0.010

**Table A3. Measured Elemental Concentrations (wt%)  
for Samples Prepared Using Peroxide Fusion**

Set	Glass ID	Block	Sub-Block	Sequence	Lab ID	B (wt%)	Li (wt%)	Si (wt%)
1	Batch 1	1	1	1	BCHPF1-111	2.57	2.03	24.1
1	U std	1	1	2	UstdPF1-111	2.86	1.37	21.3
1	SB4VAR54	1	1	3	M03PF11	2.55	2.17	19.6
1	SB4VAR41	1	1	4	M01PF21	2.84	2.51	22.9
1	SB4VAR21	1	1	5	M13PF11	2.95	2.52	22.9
1	SB4VAR54	1	1	6	M03PF21	2.5	2.12	20
1	SB4VAR53	1	1	7	M11PF21	2.69	2.26	20.8
1	SB4VAR22	1	1	8	M12PF21	2.75	2.35	21.7
1	SB4VAR42	1	1	9	M05PF21	2.83	2.4	22.3
1	SB4VAR23	1	1	10	M10PF21	2.65	2.23	20.8
1	Batch 1	1	1	11	BCHPF1-112	2.33	1.97	23.1
1	U std	1	1	12	UstdPF1-112	2.73	1.36	20.5
1	SB4VAR13	1	1	13	M14PF21	2.54	2.14	19.9
1	SB4VAR13	1	1	14	M14PF11	2.55	2.11	20.3
1	SB4VAR42	1	1	15	M05PF11	2.7	2.28	21.1
1	SB4VAR23	1	1	16	M10PF11	2.58	2.19	20.5
1	SB4VAR53	1	1	17	M11PF11	2.7	2.29	21.2
1	SB4VAR22	1	1	18	M12PF11	2.9	2.41	22.7
1	SB4VAR21	1	1	19	M13PF21	3.08	2.55	23.8
1	SB4VAR41	1	1	20	M01PF11	3.14	2.55	24.2
1	Batch 1	1	1	21	BCHPF1-113	2.52	2.04	24.6
1	U std	1	1	22	UstdPF1-113	2.96	1.41	22.3
1	Batch 1	1	2	1	BCHPF1-121	2.53	2.02	23.9
1	U std	1	2	2	UstdPF1-121	2.86	1.37	20.8
1	SB4VAR54	1	2	3	M03PF22	2.58	2.13	20.1
1	SB4VAR42	1	2	4	M05PF12	2.9	2.35	22.2
1	SB4VAR41	1	2	5	M01PF12	3.05	2.5	23.4
1	SB4VAR54	1	2	6	M03PF12	2.62	2.17	20.2
1	SB4VAR21	1	2	7	M13PF22	3.01	2.52	23.5
1	SB4VAR23	1	2	8	M10PF12	2.74	2.25	21.4
1	SB4VAR21	1	2	9	M13PF12	3.06	2.54	23.5
1	SB4VAR42	1	2	10	M05PF22	2.94	2.42	23
1	Batch 1	1	2	11	BCHPF1-122	2.48	2	23.9
1	U std	1	2	12	UstdPF1-122	2.86	1.38	21.3
1	SB4VAR23	1	2	13	M10PF22	2.86	2.27	21.8
1	SB4VAR53	1	2	14	M11PF12	2.9	2.33	22.3
1	SB4VAR41	1	2	15	M01PF22	3.09	2.57	24
1	SB4VAR13	1	2	16	M14PF22	2.63	2.17	20.8
1	SB4VAR53	1	2	17	M11PF22	2.89	2.31	21.6
1	SB4VAR22	1	2	18	M12PF12	3.06	2.44	23.5
1	SB4VAR13	1	2	19	M14PF12	2.71	2.18	21.1
1	SB4VAR22	1	2	20	M12PF22	2.96	2.41	22.5
1	Batch 1	1	2	21	BCHPF1-123	2.52	2.04	24.7
1	U std	1	2	22	UstdPF1-123	2.95	1.4	21.8
1	Batch 1	2	1	1	BCHPF1-211	2.43	1.97	23.3
1	U std	2	1	2	UstdPF1-211	2.75	1.35	20.9
1	SB4VAR12	2	1	3	M15PF21	2.7	2.26	21.4
1	SB4VAR52	2	1	4	M09PF11	2.79	2.34	22
1	SB4VAR43	2	1	5	M06PF21	2.69	2.25	21.4
1	SB4VAR51	2	1	6	M04PF11	2.89	2.45	23
1	SB4VAR52	2	1	7	M09PF21	2.8	2.35	21.9
1	SB4VAR44	2	1	8	M08PF21	2.56	2.14	20.4
1	SB4VAR24	2	1	9	M07PF21	2.58	2.14	20.5
1	Batch 1	2	1	10	BCHPF1-212	2.31	1.96	23.2
1	U std	2	1	11	UstdPF1-212	2.75	1.36	20.8
1	SB4VAR44	2	1	12	M08PF11	2.54	2.11	19.9
1	SB4VAR24	2	1	13	M07PF11	2.54	2.14	20.3
1	SB4VAR11	2	1	14	M02PF11	2.81	2.34	22
1	SB4VAR11	2	1	15	M02PF21	2.81	2.4	22.4
1	SB4VAR51	2	1	16	M04PF21	2.92	2.47	22.5
1	SB4VAR12	2	1	17	M15PF11	2.71	2.26	21.6
1	SB4VAR43	2	1	18	M06PF11	2.63	2.25	21.3
1	Batch 1	2	1	19	BCHPF1-213	2.35	1.97	23.6
1	U std	2	1	20	UstdPF1-213	2.73	1.35	21
1	Batch 1	2	2	1	BCHPF1-221	2.46	1.97	23.3
1	U std	2	2	2	UstdPF1-221	2.79	1.35	20.4
1	SB4VAR43	2	2	3	M06PF22	2.69	2.26	21
1	SB4VAR43	2	2	4	M06PF12	2.71	2.26	21.4

**Table A3. Measured Elemental Concentrations (wt%)  
for Samples Prepared Using Peroxide Fusion**

Set	Glass ID	Block	Sub-Block	Sequence	Lab ID	B (wt%)	Li (wt%)	Si (wt%)
1	SB4VAR52	2	2	5	M09PF12	2.82	2.34	21.9
1	SB4VAR51	2	2	6	M04PF22	2.95	2.46	22.3
1	SB4VAR44	2	2	7	M08PF22	2.59	2.14	20.4
1	SB4VAR52	2	2	8	M09PF22	2.79	2.35	21.6
1	SB4VAR24	2	2	9	M07PF22	2.52	2.14	20
1	Batch 1	2	2	10	BCHPF1-222	2.29	1.94	22.7
1	U std	2	2	11	UstdPF1-222	2.74	1.35	20.5
1	SB4VAR11	2	2	12	M02PF12	2.87	2.34	22
1	SB4VAR44	2	2	13	M08PF12	2.57	2.12	20.2
1	SB4VAR12	2	2	14	M15PF12	2.67	2.27	21.1
1	SB4VAR24	2	2	15	M07PF12	2.48	2.11	19.8
1	SB4VAR12	2	2	16	M15PF22	2.61	2.24	20.6
1	SB4VAR11	2	2	17	M02PF22	2.79	2.37	21.8
1	SB4VAR51	2	2	18	M04PF12	2.9	2.44	22.5
1	Batch 1	2	2	19	BCHPF1-223	2.34	1.95	23.1
1	U std	2	2	20	UstdPF1-223	2.7	1.35	20.3
2	Batch 1	1	1	1	BCHPF2-111	2.45	1.97	
2	U std	1	1	2	UstdPF2-111	2.8	1.35	
2	SB5-04	1	1	3	N03PF11	3.13	1.46	
2	SB5-09	1	1	4	N04PF21	2.02	1.98	
2	SB5-08	1	1	5	N10PF21	3.12	1.42	
2	SB5-09	1	1	6	N04PF11	1.99	1.98	
2	SB5-04	1	1	7	N03PF21	3.26	1.43	
2	SB5-08	1	1	8	N10PF11	3.14	1.42	
2	SB5-03	1	1	9	N09PF11	2.56	1.6	
2	Batch 1	1	1	10	BCHPF2-112	2.3	1.91	
2	U std	1	1	11	UstdPF2-112	2.78	1.35	
2	SB4VAR32	1	1	12	N11PF11	2.86	2.32	
2	SB5-12	1	1	13	N13PF21	3.15	1.45	
2	SB5-11	1	1	14	N14PF11	2.68	1.68	
2	SB5-12	1	1	15	N13PF11	3.11	1.43	
2	SB5-03	1	1	16	N09PF21	2.65	1.68	
2	SB4VAR32	1	1	17	N11PF21	2.7	2.32	
2	SB5-11	1	1	18	N14PF21	2.62	1.69	
2	Batch 1	1	1	19	BCHPF2-113	2.36	1.95	
2	U std	1	1	20	UstdPF2-113	2.71	1.34	
2	Batch 1	1	2	1	BCHPF1-121	2.5	1.98	
2	U std	1	2	2	UstdPF1-121	2.85	1.36	
2	SB5-12	1	2	3	N13PF22	3.16	1.45	
2	SB5-11	1	2	4	N14PF12	2.72	1.7	
2	SB5-03	1	2	5	N09PF22	2.76	1.72	
2	SB5-11	1	2	6	N14PF22	2.74	1.7	
2	SB5-03	1	2	7	N09PF12	2.6	1.62	
2	SB5-08	1	2	8	N10PF12	3.18	1.45	
2	SB4VAR32	1	2	9	N11PF12	2.84	2.32	
2	Batch 1	1	2	10	BCHPF1-122	2.44	1.97	
2	U std	1	2	11	UstdPF1-122	2.83	1.36	
2	SB5-08	1	2	12	N10PF22	3.17	1.44	
2	SB4VAR32	1	2	13	N11PF22	2.79	2.36	
2	SB5-04	1	2	14	N03PF12	3.19	1.45	
2	SB5-04	1	2	15	N03PF22	3.22	1.45	
2	SB5-09	1	2	16	N04PF22	1.98	2	
2	SB5-12	1	2	17	N13PF12	3.06	1.45	
2	SB5-09	1	2	18	N04PF12	2	2	
2	Batch 1	1	2	19	BCHPF2-123	2.37	1.94	
2	U std	1	2	20	UstdPF1-123	2.79	1.36	
2	Batch 1	2	1	1	BCHPF2-211	2.5	1.98	
2	U std	2	1	2	UstdPF2-211	2.84	1.37	
2	SB5-06	2	1	3	N01PF21	2.19	2	
2	SB5-05	2	1	4	N07PF11	2.01	2.02	
2	SB4VAR33	2	1	5	N05PF11	2.67	2.23	
2	SB5-10	2	1	6	N08PF21	2.17	2	
2	SB5-02	2	1	7	N12PF11	2.15	2.01	
2	SB5-07	2	1	8	N15PF21	2.62	1.7	
2	SB5-01	2	1	9	N02PF11	1.89	1.96	
2	SB5-02	2	1	10	N12PF21	2.12	2	
2	Batch 1	2	1	11	BCHPF2-212	2.35	1.97	
2	U std	2	1	12	UstdPF2-212	2.77	1.37	
2	SB4VAR31	2	1	13	N06PF21	2.96	2.48	

**Table A3. Measured Elemental Concentrations (wt%)  
for Samples Prepared Using Peroxide Fusion**

Set	Glass ID	Block	Sub-Block	Sequence	Lab ID	B (wt%)	Li (wt%)	Si (wt%)
2	SB5-05	2	1	14	N07PF21	1.97	1.99	
2	SB4VAR33	2	1	15	N05PF21	2.57	2.2	
2	SB5-01	2	1	16	N02PF21	1.9	1.96	
2	SB5-10	2	1	17	N08PF11	2.05	2	
2	SB4VAR31	2	1	18	N06PF11	2.91	2.5	
2	SB5-06	2	1	19	N01PF11	2.16	1.97	
2	SB5-07	2	1	20	N15PF11	2.68	1.71	
2	Batch 1	2	1	21	BCHPF2-213	2.37	1.99	
2	U std	2	1	22	UstdPF2-213	2.72	1.36	
2	Batch 1	2	2	1	BCHPF2-221	2.5	1.98	
2	U std	2	2	2	UstdPF2-221	2.83	1.38	
2	SB5-06	2	2	3	N01PF12	2.27	2.01	
2	SB4VAR33	2	2	4	N05PF22	2.66	2.23	
2	SB5-01	2	2	5	N02PF22	1.93	1.95	
2	SB5-10	2	2	6	N08PF22	2.19	2.02	
2	SB5-05	2	2	7	N07PF22	2	2.02	
2	SB4VAR31	2	2	8	N06PF22	3.03	2.48	
2	SB5-07	2	2	9	N15PF12	2.78	1.73	
2	SB4VAR33	2	2	10	N05PF12	2.64	2.23	
2	Batch 1	2	2	11	BCHPF2-222	2.43	1.98	
2	U std	2	2	12	UstdPF2-222	2.79	1.38	
2	SB5-05	2	2	13	N07PF12	2.09	2.04	
2	SB5-01	2	2	14	N02PF12	1.99	1.98	
2	SB5-06	2	2	15	N01PF22	2.18	2.01	
2	SB5-10	2	2	16	N08PF12	2.14	2.03	
2	SB5-02	2	2	17	N12PF22	2.18	2.03	
2	SB5-07	2	2	18	N15PF22	2.65	1.72	
2	SB5-02	2	2	19	N12PF12	2.26	2.06	
2	SB4VAR31	2	2	20	N06PF12	3.08	2.58	
2	Batch 1	2	2	21	BCHPF2-223	2.52	2.02	
2	U std	2	2	22	UstdPF2-223	2.88	1.4	

**Table A4. Average Measured and Bias-Corrected Chemical Compositions Versus Targeted Compositions by Oxide by SB4-Decant Variability Study Glass**

Set	Glass ID	Oxide	Measured		Targeted	Diff of Measured	Diff of Meas BC	% Diff of Measured	% Diff of BC
			Measured (wt%)	Bias-Corrected (BC) (wt%)					
1	Batch 1	Al <sub>2</sub> O <sub>3</sub>	4.7820	4.8770	4.8770	-0.0950	0.0000	-1.9%	0.0%
1	Batch 1	B <sub>2</sub> O <sub>3</sub>	7.8163	7.7770	7.7770	0.0393	0.0000	0.5%	0.0%
1	Batch 1	BaO	0.1411	0.1510	0.1510	-0.0099	0.0000	-6.5%	0.0%
1	Batch 1	CaO	1.1838	1.2200	1.2200	-0.0362	0.0000	-3.0%	0.0%
1	Batch 1	Ce <sub>2</sub> O <sub>3</sub>	0.0224	0.0224	0.0000	0.0224	0.0224		
1	Batch 1	Cr <sub>2</sub> O <sub>3</sub>	0.1056	0.1070	0.1070	-0.0014	0.0000	-1.3%	0.0%
1	Batch 1	CuO	0.3755	0.3990	0.3990	-0.0235	0.0000	-5.9%	0.0%
1	Batch 1	Fe <sub>2</sub> O <sub>3</sub>	12.6636	12.8390	12.8390	-0.1754	0.0000	-1.4%	0.0%
1	Batch 1	K <sub>2</sub> O	3.5967	3.3270	3.3270	0.2697	0.0000	8.1%	0.0%
1	Batch 1	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0000	0.0586	0.0586		
1	Batch 1	Li <sub>2</sub> O	4.2807	4.4290	4.4290	-0.1483	0.0000	-3.3%	0.0%
1	Batch 1	MgO	1.3649	1.4190	1.4190	-0.0541	0.0000	-3.8%	0.0%
1	Batch 1	MnO	1.7173	1.7260	1.7260	-0.0087	0.0000	-0.5%	0.0%
1	Batch 1	Na <sub>2</sub> O	8.9788	9.0030	9.0030	-0.0242	0.0000	-0.3%	0.0%
1	Batch 1	NiO	0.7007	0.7510	0.7510	-0.0503	0.0000	-6.7%	0.0%
1	Batch 1	PbO	0.0108	0.0108	0.0000	0.0108	0.0108		
1	Batch 1	SiO <sub>2</sub>	50.5410	50.2200	50.2200	0.3210	0.0000	0.6%	0.0%
1	Batch 1	SO <sub>4</sub>	0.1498	0.1498	0.0000	0.1498	0.1498		
1	Batch 1	TiO <sub>2</sub>	0.6465	0.6770	0.6770	-0.0305	0.0000	-4.5%	0.0%
1	Batch 1	U <sub>3</sub> O <sub>8</sub>	0.0590	0.0615	0.0000	0.0590	0.0615		
1	Batch 1	ZnO	0.0062	0.0062	0.0000	0.0062	0.0062		
1	Batch 1	ZrO <sub>2</sub>	0.0858	0.0858	0.0980	-0.0122	-0.0122	-12.5%	-12.5%
1	Batch 1	Sum	99.2872	99.3172	99.0200	0.2672	0.2972	0.3%	0.3%
1	SB4VAR11	Al <sub>2</sub> O <sub>3</sub>	8.5358	8.6855	8.4639	0.0719	0.2216	0.8%	2.6%
1	SB4VAR11	B <sub>2</sub> O <sub>3</sub>	9.0801	9.2797	9.2400	-0.1599	0.0397	-1.7%	0.4%
1	SB4VAR11	BaO	0.0229	0.0244	0.0252	-0.0023	-0.0008	-9.2%	-3.1%
1	SB4VAR11	CaO	0.8825	0.9058	0.9283	-0.0458	-0.0225	-4.9%	-2.4%
1	SB4VAR11	Ce <sub>2</sub> O <sub>3</sub>	0.0190	0.0190	0.0221	-0.0031	-0.0031	-13.9%	-13.9%
1	SB4VAR11	Cr <sub>2</sub> O <sub>3</sub>	0.0570	0.0577	0.0527	0.0043	0.0050	8.2%	9.5%
1	SB4VAR11	CuO	0.0244	0.0259	0.0195	0.0049	0.0064	25.2%	32.8%
1	SB4VAR11	Fe <sub>2</sub> O <sub>3</sub>	9.0214	9.4768	9.6198	-0.5984	-0.1430	-6.2%	-1.5%
1	SB4VAR11	K <sub>2</sub> O	0.1262	0.1171	0.1190	0.0071	-0.0020	6.0%	-1.6%
1	SB4VAR11	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0166	0.0420	0.0420	253.3%	253.3%
1	SB4VAR11	Li <sub>2</sub> O	5.0862	5.3385	5.2800	-0.1938	0.0585	-3.7%	1.1%
1	SB4VAR11	MgO	0.8777	0.9221	0.9129	-0.0352	0.0092	-3.9%	1.0%
1	SB4VAR11	MnO	1.8722	1.9275	1.9320	-0.0598	-0.0045	-3.1%	-0.2%
1	SB4VAR11	Na <sub>2</sub> O	12.2668	12.2547	12.2570	0.0098	-0.0023	0.1%	0.0%
1	SB4VAR11	NiO	0.4826	0.5220	0.5353	-0.0527	-0.0133	-9.8%	-2.5%
1	SB4VAR11	PbO	0.0232	0.0232	0.0211	0.0021	0.0021	9.8%	9.8%
1	SB4VAR11	SiO <sub>2</sub>	47.1716	47.7308	47.1049	0.0667	0.6259	0.1%	1.3%
1	SB4VAR11	SO <sub>4</sub>	0.4127	0.4127	0.4483	-0.0356	-0.0356	-7.9%	-7.9%
1	SB4VAR11	TiO <sub>2</sub>	0.0171	0.0180	0.0130	0.0041	0.0050	31.5%	38.6%
1	SB4VAR11	U <sub>3</sub> O <sub>8</sub>	2.8271	2.9482	2.9352	-0.1081	0.0130	-3.7%	0.4%
1	SB4VAR11	ZnO	0.0218	0.0218	0.0263	-0.0045	-0.0045	-17.2%	-17.2%
1	SB4VAR11	ZrO <sub>2</sub>	0.0257	0.0257	0.0268	-0.0011	-0.0011	-4.2%	-4.2%
1	SB4VAR11	Sum	98.9126	100.7958	100.0000	-1.0873	0.7958	-1.1%	0.8%
1	SB4VAR12	Al <sub>2</sub> O <sub>3</sub>	9.4853	9.6987	9.4596	0.0257	0.2391	0.3%	2.5%
1	SB4VAR12	B <sub>2</sub> O <sub>3</sub>	8.6052	8.7944	8.6800	-0.0748	0.1144	-0.9%	1.3%
1	SB4VAR12	BaO	0.0232	0.0248	0.0281	-0.0049	-0.0033	-17.6%	-11.6%
1	SB4VAR12	CaO	0.9798	1.0138	1.0375	-0.0577	-0.0237	-5.6%	-2.3%
1	SB4VAR12	Ce <sub>2</sub> O <sub>3</sub>	0.0193	0.0193	0.0247	-0.0054	-0.0054	-21.8%	-21.8%
1	SB4VAR12	Cr <sub>2</sub> O <sub>3</sub>	0.0607	0.0615	0.0589	0.0018	0.0026	3.0%	4.5%
1	SB4VAR12	CuO	0.0275	0.0293	0.0218	0.0057	0.0075	26.3%	34.4%
1	SB4VAR12	Fe <sub>2</sub> O <sub>3</sub>	10.8800	10.6604	10.7516	0.1284	-0.0912	1.2%	-0.8%
1	SB4VAR12	K <sub>2</sub> O	0.1430	0.1319	0.1330	0.0100	-0.0011	7.5%	-0.8%
1	SB4VAR12	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0185	0.0401	0.0401	217.0%	217.0%
1	SB4VAR12	Li <sub>2</sub> O	4.8602	5.1013	4.9600	-0.0998	0.1413	-2.0%	2.8%
1	SB4VAR12	MgO	0.9950	1.0236	1.0203	-0.0253	0.0033	-2.5%	0.3%

**Table A4. Average Measured and Bias-Corrected Chemical Compositions Versus Targeted Compositions by Oxide by SB4-Decant Variability Study Glass**

Set	Glass ID	Oxide	Measured		Diff of Measured	Diff of Meas BC	% Diff of Measured	% Diff of BC
			Measured (wt%)	Bias-Corrected (BC) (wt%)				
1	SB4VAR12	MnO	2.2305	2.1919	2.1593	0.0712	0.0326	3.3% 1.5%
1	SB4VAR12	Na <sub>2</sub> O	12.5128	12.5957	12.7578	-0.2450	-0.1621	-1.9% -1.3%
1	SB4VAR12	NiO	0.5402	0.5737	0.5983	-0.0581	-0.0246	-9.7% -4.1%
1	SB4VAR12	PbO	0.0191	0.0191	0.0236	-0.0045	-0.0045	-19.0% -19.0%
1	SB4VAR12	SiO <sub>2</sub>	45.2997	45.8339	44.4114	0.8883	1.4225	2.0% 3.2%
1	SB4VAR12	SO <sub>4</sub>	0.4441	0.4441	0.5011	-0.0569	-0.0569	-11.4% -11.4%
1	SB4VAR12	TiO <sub>2</sub>	0.0229	0.0239	0.0146	0.0083	0.0093	57.1% 63.6%
1	SB4VAR12	U <sub>3</sub> O <sub>8</sub>	3.1573	3.2923	3.2805	-0.1232	0.0118	-3.8% 0.4%
1	SB4VAR12	ZnO	0.0215	0.0215	0.0294	-0.0079	-0.0079	-27.0% -27.0%
1	SB4VAR12	ZrO <sub>2</sub>	0.0277	0.0277	0.0300	-0.0023	-0.0023	-7.7% -7.7%
1	SB4VAR12	Sum	100.4137	101.6415	100.0000	0.4137	1.6415	0.4% 1.6%
1	SB4VAR13	Al <sub>2</sub> O <sub>3</sub>	10.3923	10.5745	10.4554	-0.0631	0.1191	-0.6% 1.1%
1	SB4VAR13	B <sub>2</sub> O <sub>3</sub>	8.3959	8.1375	8.1200	0.2759	0.0175	3.4% 0.2%
1	SB4VAR13	BaO	0.0299	0.0319	0.0311	-0.0012	0.0008	-4.0% 2.5%
1	SB4VAR13	CaO	1.0861	1.1148	1.1467	-0.0606	-0.0319	-5.3% -2.8%
1	SB4VAR13	Ce <sub>2</sub> O <sub>3</sub>	0.0237	0.0237	0.0273	-0.0036	-0.0036	-13.1% -13.1%
1	SB4VAR13	Cr <sub>2</sub> O <sub>3</sub>	0.0614	0.0621	0.0651	-0.0037	-0.0030	-5.7% -4.6%
1	SB4VAR13	CuO	0.0304	0.0322	0.0241	0.0063	0.0081	26.0% 33.6%
1	SB4VAR13	Fe <sub>2</sub> O <sub>3</sub>	11.0980	11.6585	11.8833	-0.7853	-0.2248	-6.6% -1.9%
1	SB4VAR13	K <sub>2</sub> O	0.1391	0.1291	0.1470	-0.0079	-0.0179	-5.4% -12.2%
1	SB4VAR13	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0205	0.0381	0.0381	186.0% 186.0%
1	SB4VAR13	Li <sub>2</sub> O	4.6287	4.7217	4.6400	-0.0113	0.0817	-0.2% 1.8%
1	SB4VAR13	MgO	1.1111	1.1673	1.1277	-0.0166	0.0396	-1.5% 3.5%
1	SB4VAR13	MnO	2.3209	2.3896	2.3866	-0.0657	0.0030	-2.8% 0.1%
1	SB4VAR13	Na <sub>2</sub> O	13.1059	13.0917	13.2587	-0.1528	-0.1670	-1.2% -1.3%
1	SB4VAR13	NiO	0.5917	0.6400	0.6612	-0.0695	-0.0212	-10.5% -3.2%
1	SB4VAR13	PbO	0.0304	0.0304	0.0261	0.0043	0.0043	16.6% 16.6%
1	SB4VAR13	SiO <sub>2</sub>	43.9091	42.8560	41.7179	2.1912	1.1381	5.3% 2.7%
1	SB4VAR13	SO <sub>4</sub>	0.5048	0.5048	0.5538	-0.0490	-0.0490	-8.8% -8.8%
1	SB4VAR13	TiO <sub>2</sub>	0.0229	0.0242	0.0161	0.0068	0.0081	42.5% 50.2%
1	SB4VAR13	U <sub>3</sub> O <sub>8</sub>	3.4875	3.6368	3.6258	-0.1383	0.0110	-3.8% 0.3%
1	SB4VAR13	ZnO	0.0274	0.0274	0.0325	-0.0051	-0.0051	-15.7% -15.7%
1	SB4VAR13	ZrO <sub>2</sub>	0.0317	0.0317	0.0331	-0.0014	-0.0014	-4.1% -4.1%
1	SB4VAR13	Sum	101.0877	100.9447	100.0001	1.0877	0.9447	1.1% 0.9%
1	SB4VAR21	Al <sub>2</sub> O <sub>3</sub>	8.3658	8.5123	8.3067	0.0591	0.2056	0.7% 2.5%
1	SB4VAR21	B <sub>2</sub> O <sub>3</sub>	9.7402	9.4419	9.5200	0.2202	-0.0781	2.3% -0.8%
1	SB4VAR21	BaO	0.0246	0.0262	0.0248	-0.0002	0.0014	-1.0% 5.7%
1	SB4VAR21	CaO	0.8755	0.8987	0.9141	-0.0386	-0.0154	-4.2% -1.7%
1	SB4VAR21	Ce <sub>2</sub> O <sub>3</sub>	0.0170	0.0170	0.0218	-0.0048	-0.0048	-21.9% -21.9%
1	SB4VAR21	Cr <sub>2</sub> O <sub>3</sub>	0.0555	0.0562	0.0519	0.0036	0.0043	7.0% 8.3%
1	SB4VAR21	CuO	0.0250	0.0266	0.0192	0.0058	0.0074	30.4% 38.3%
1	SB4VAR21	Fe <sub>2</sub> O <sub>3</sub>	8.7712	9.2133	9.4727	-0.7015	-0.2594	-7.4% -2.7%
1	SB4VAR21	K <sub>2</sub> O	0.1168	0.1084	0.1172	-0.0004	-0.0088	-0.3% -7.5%
1	SB4VAR21	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0163	0.0423	0.0423	259.8% 259.8%
1	SB4VAR21	Li <sub>2</sub> O	5.4522	5.5619	5.4400	0.0122	0.1219	0.2% 2.2%
1	SB4VAR21	MgO	0.8735	0.9177	0.8989	-0.0254	0.0188	-2.8% 2.1%
1	SB4VAR21	MnO	1.8335	1.8875	1.9024	-0.0689	-0.0149	-3.6% -0.8%
1	SB4VAR21	Na <sub>2</sub> O	10.8042	10.7917	10.9820	-0.1778	-0.1903	-1.6% -1.7%
1	SB4VAR21	NiO	0.4801	0.5192	0.5271	-0.0470	-0.0079	-8.9% -1.5%
1	SB4VAR21	PbO	0.0232	0.0232	0.0208	0.0024	0.0024	11.3% 11.3%
1	SB4VAR21	SiO <sub>2</sub>	50.1131	48.9153	48.4911	1.6220	0.4242	3.3% 0.9%
1	SB4VAR21	SO <sub>4</sub>	0.1498	0.1498	0.3175	-0.1677	-0.1677	-52.8% -52.8%
1	SB4VAR21	TiO <sub>2</sub>	0.0200	0.0211	0.0128	0.0072	0.0083	56.4% 64.9%
1	SB4VAR21	U <sub>3</sub> O <sub>8</sub>	2.7652	2.8834	2.8902	-0.1250	-0.0068	-4.3% -0.2%
1	SB4VAR21	ZnO	0.0205	0.0205	0.0259	-0.0054	-0.0054	-20.7% -20.7%
1	SB4VAR21	ZrO <sub>2</sub>	0.0253	0.0253	0.0264	-0.0011	-0.0011	-4.1% -4.1%
1	SB4VAR21	Sum	100.6110	100.0758	99.9998	0.6112	0.0760	0.6% 0.1%
1	SB4VAR22	Al <sub>2</sub> O <sub>3</sub>	9.0507	9.2565	9.0855	-0.0348	0.1710	-0.4% 1.9%

**Table A4. Average Measured and Bias-Corrected Chemical Compositions Versus Targeted Compositions by Oxide by SB4-Decant Variability Study Glass**

Set	Glass ID	Oxide	Measured		Targeted	Diff of Measured	Diff of Meas BC	% Diff of Measured	% Diff of BC
			Measured (wt%)	Bias-Corrected (BC) (wt%)					
1	SB4VAR22	B <sub>2</sub> O <sub>3</sub>	9.3941	9.1045	9.1000	0.2941	0.0045	3.2%	0.0%
1	SB4VAR22	BaO	0.0257	0.0275	0.0271	-0.0014	0.0004	-5.2%	1.6%
1	SB4VAR22	CaO	0.9466	0.9794	0.9998	-0.0532	-0.0204	-5.3%	-2.0%
1	SB4VAR22	Ce <sub>2</sub> O <sub>3</sub>	0.0179	0.0179	0.0238	-0.0059	-0.0059	-24.9%	-24.9%
1	SB4VAR22	Cr <sub>2</sub> O <sub>3</sub>	0.0643	0.0652	0.0568	0.0075	0.0084	13.2%	14.9%
1	SB4VAR22	CuO	0.0269	0.0286	0.0210	0.0059	0.0076	28.2%	36.4%
1	SB4VAR22	Fe <sub>2</sub> O <sub>3</sub>	10.1973	9.9915	10.3607	-0.1634	-0.3692	-1.6%	-3.6%
1	SB4VAR22	K <sub>2</sub> O	0.1283	0.1183	0.1282	0.0001	-0.0099	0.1%	-7.7%
1	SB4VAR22	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0178	0.0408	0.0408	229.4%	229.4%
1	SB4VAR22	Li <sub>2</sub> O	5.1723	5.2763	5.2000	-0.0277	0.0763	-0.5%	1.5%
1	SB4VAR22	MgO	0.9888	1.0172	0.9832	0.0056	0.0340	0.6%	3.5%
1	SB4VAR22	MnO	2.1047	2.0681	2.0808	0.0239	-0.0127	1.1%	-0.6%
1	SB4VAR22	Na <sub>2</sub> O	11.0772	11.1544	11.2616	-0.1844	-0.1072	-1.6%	-1.0%
1	SB4VAR22	NiO	0.5386	0.5720	0.5765	-0.0379	-0.0045	-6.6%	-0.8%
1	SB4VAR22	PbO	0.0240	0.0240	0.0228	0.0012	0.0012	5.1%	5.1%
1	SB4VAR22	SiO <sub>2</sub>	48.3482	47.1892	46.4746	1.8736	0.7146	4.0%	1.5%
1	SB4VAR22	SO <sub>4</sub>	0.3438	0.3438	0.3473	-0.0035	-0.0035	-1.0%	-1.0%
1	SB4VAR22	TiO <sub>2</sub>	0.0267	0.0278	0.0140	0.0127	0.0138	90.6%	98.5%
1	SB4VAR22	U <sub>3</sub> O <sub>8</sub>	3.0423	3.1734	3.1612	-0.1189	0.0122	-3.8%	0.4%
1	SB4VAR22	ZnO	0.0212	0.0212	0.0283	-0.0071	-0.0071	-25.2%	-25.2%
1	SB4VAR22	ZrO <sub>2</sub>	0.0216	0.0216	0.0289	-0.0073	-0.0073	-25.2%	-25.2%
1	SB4VAR22	Sum	101.6196	100.5370	99.9999	1.6197	0.5371	1.6%	0.5%
1	SB4VAR23	Al <sub>2</sub> O <sub>3</sub>	10.2931	10.4731	9.8642	0.4289	0.6089	4.3%	6.2%
1	SB4VAR23	B <sub>2</sub> O <sub>3</sub>	8.7179	8.4490	8.6800	0.0379	-0.2310	0.4%	-2.7%
1	SB4VAR23	BaO	0.0268	0.0286	0.0294	-0.0026	-0.0008	-8.9%	-2.7%
1	SB4VAR23	CaO	1.0323	1.0595	1.0855	-0.0532	-0.0260	-4.9%	-2.4%
1	SB4VAR23	Ce <sub>2</sub> O <sub>3</sub>	0.0199	0.0199	0.0258	-0.0059	-0.0059	-22.9%	-22.9%
1	SB4VAR23	Cr <sub>2</sub> O <sub>3</sub>	0.0552	0.0558	0.0617	-0.0065	-0.0059	-10.6%	-9.5%
1	SB4VAR23	CuO	0.0300	0.0319	0.0228	0.0072	0.0091	31.8%	39.8%
1	SB4VAR23	Fe <sub>2</sub> O <sub>3</sub>	10.4404	10.9679	11.2488	-0.8084	-0.2809	-7.2%	-2.5%
1	SB4VAR23	K <sub>2</sub> O	0.1436	0.1333	0.1392	0.0045	-0.0059	3.2%	-4.2%
1	SB4VAR23	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0193	0.0393	0.0393	203.8%	203.8%
1	SB4VAR23	Li <sub>2</sub> O	4.8117	4.9084	4.9600	-0.1483	-0.0516	-3.0%	-1.0%
1	SB4VAR23	MgO	1.0215	1.0732	1.0675	-0.0460	0.0057	-4.3%	0.5%
1	SB4VAR23	MnO	2.2047	2.2700	2.2591	-0.0544	0.0109	-2.4%	0.5%
1	SB4VAR23	Na <sub>2</sub> O	11.3603	11.3469	11.5412	-0.1809	-0.1943	-1.6%	-1.7%
1	SB4VAR23	NiO	0.5437	0.5880	0.6259	-0.0822	-0.0379	-13.1%	-6.1%
1	SB4VAR23	PbO	0.0259	0.0259	0.0247	0.0012	0.0012	4.7%	4.7%
1	SB4VAR23	SiO <sub>2</sub>	45.1927	44.1084	44.4582	0.7345	-0.3498	1.7%	-0.8%
1	SB4VAR23	SO <sub>4</sub>	0.3505	0.3505	0.3770	-0.0265	-0.0265	-7.0%	-7.0%
1	SB4VAR23	TiO <sub>2</sub>	0.0229	0.0242	0.0152	0.0077	0.0090	50.9%	59.1%
1	SB4VAR23	U <sub>3</sub> O <sub>8</sub>	3.2575	3.3968	3.4322	-0.1747	-0.0354	-5.1%	-1.0%
1	SB4VAR23	ZnO	0.0255	0.0255	0.0307	-0.0052	-0.0052	-16.9%	-16.9%
1	SB4VAR23	ZrO <sub>2</sub>	0.0277	0.0277	0.0314	-0.0037	-0.0037	-11.8%	-11.8%
1	SB4VAR23	Sum	99.6625	99.4231	99.9999	-0.3374	-0.5767	-0.3%	-0.6%
1	SB4VAR24	Al <sub>2</sub> O <sub>3</sub>	10.6284	10.8147	10.6430	-0.0146	0.1717	-0.1%	1.6%
1	SB4VAR24	B <sub>2</sub> O <sub>3</sub>	8.1463	8.3254	8.2600	-0.1137	0.0654	-1.4%	0.8%
1	SB4VAR24	BaO	0.0287	0.0307	0.0317	-0.0030	-0.0010	-9.3%	-3.2%
1	SB4VAR24	CaO	1.1362	1.1661	1.1712	-0.0350	-0.0051	-3.0%	-0.4%
1	SB4VAR24	Ce <sub>2</sub> O <sub>3</sub>	0.0246	0.0246	0.0279	-0.0033	-0.0033	-11.8%	-11.8%
1	SB4VAR24	Cr <sub>2</sub> O <sub>3</sub>	0.0607	0.0614	0.0665	-0.0058	-0.0051	-8.8%	-7.7%
1	SB4VAR24	CuO	0.0310	0.0329	0.0246	0.0064	0.0083	25.9%	33.6%
1	SB4VAR24	Fe <sub>2</sub> O <sub>3</sub>	11.1409	11.7035	12.1369	-0.9960	-0.4334	-8.2%	-3.6%
1	SB4VAR24	K <sub>2</sub> O	0.1991	0.1847	0.1502	0.0489	0.0345	32.5%	23.0%
1	SB4VAR24	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0209	0.0377	0.0377	180.6%	180.6%
1	SB4VAR24	Li <sub>2</sub> O	4.5911	4.8188	4.7200	-0.1289	0.0988	-2.7%	2.1%
1	SB4VAR24	MgO	1.0820	1.1368	1.1518	-0.0698	-0.0150	-6.1%	-1.3%
1	SB4VAR24	MnO	2.4016	2.4726	2.4375	-0.0359	0.0351	-1.5%	1.4%

**Table A4. Average Measured and Bias-Corrected Chemical Compositions Versus Targeted Compositions by Oxide by SB4-Decant Variability Study Glass**

Set	Glass ID	Oxide	Measured		Targeted	Diff of Measured	Diff of Meas BC	% Diff of Measured	% Diff of BC
			Measured (wt%)	Bias-Corrected (BC) (wt%)					
1	SB4VAR24	Na <sub>2</sub> O	11.6669	11.6534	11.8207	-0.1538	-0.1673	-1.3%	-1.4%
1	SB4VAR24	NiO	0.5500	0.5949	0.6754	-0.1254	-0.0805	-18.6%	-11.9%
1	SB4VAR24	PbO	0.0302	0.0302	0.0267	0.0035	0.0035	13.0%	13.0%
1	SB4VAR24	SiO <sub>2</sub>	43.1069	43.6162	42.4417	0.6652	1.1745	1.6%	2.8%
1	SB4VAR24	SO <sub>4</sub>	0.3790	0.3790	0.4068	-0.0278	-0.0278	-6.8%	-6.8%
1	SB4VAR24	TiO <sub>2</sub>	0.0225	0.0237	0.0164	0.0061	0.0073	37.3%	44.7%
1	SB4VAR24	U <sub>3</sub> O <sub>8</sub>	3.5405	3.6919	3.7031	-0.1626	-0.0112	-4.4%	-0.3%
1	SB4VAR24	ZnO	0.0268	0.0268	0.0332	-0.0064	-0.0064	-19.4%	-19.4%
1	SB4VAR24	ZrO <sub>2</sub>	0.0317	0.0317	0.0338	-0.0021	-0.0021	-6.1%	-6.1%
1	SB4VAR24	Sum	98.8839	100.8786	100.0000	-1.1161	0.8786	-1.1%	0.9%
1	SB4VAR41	Al <sub>2</sub> O <sub>3</sub>	8.1390	8.3219	7.9963	0.1427	0.3256	1.8%	4.1%
1	SB4VAR41	B <sub>2</sub> O <sub>3</sub>	9.7563	9.4568	9.5200	0.2363	-0.0632	2.5%	-0.7%
1	SB4VAR41	BaO	0.0212	0.0227	0.0249	-0.0037	-0.0022	-14.8%	-8.7%
1	SB4VAR41	CaO	0.8546	0.8842	0.8848	-0.0302	-0.0006	-3.4%	-0.1%
1	SB4VAR41	Ce <sub>2</sub> O <sub>3</sub>	0.0214	0.0214	0.0233	-0.0019	-0.0019	-8.2%	-8.2%
1	SB4VAR41	Cr <sub>2</sub> O <sub>3</sub>	0.0548	0.0556	0.0510	0.0038	0.0046	7.5%	9.0%
1	SB4VAR41	CuO	0.0238	0.0253	0.0190	0.0048	0.0063	25.2%	33.2%
1	SB4VAR41	Fe <sub>2</sub> O <sub>3</sub>	9.2502	9.0625	9.1990	0.0512	-0.1365	0.6%	-1.5%
1	SB4VAR41	K <sub>2</sub> O	0.1274	0.1175	0.1133	0.0141	0.0042	12.5%	3.7%
1	SB4VAR41	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0165	0.0421	0.0421	255.4%	255.4%
1	SB4VAR41	Li <sub>2</sub> O	5.4522	5.5619	5.4400	0.0122	0.1219	0.2%	2.2%
1	SB4VAR41	MgO	0.8354	0.8595	0.8564	-0.0210	0.0031	-2.5%	0.4%
1	SB4VAR41	MnO	1.9626	1.9275	1.8810	0.0816	0.0465	4.3%	2.5%
1	SB4VAR41	Na <sub>2</sub> O	11.3839	11.4605	11.3434	0.0405	0.1171	0.4%	1.0%
1	SB4VAR41	NiO	0.4629	0.4916	0.5227	-0.0598	-0.0311	-11.4%	-6.0%
1	SB4VAR41	PbO	0.0218	0.0218	0.0217	0.0001	0.0001	0.5%	0.5%
1	SB4VAR41	SiO <sub>2</sub>	50.5410	49.3329	48.4580	2.0830	0.8749	4.3%	1.8%
1	SB4VAR41	SO <sub>4</sub>	0.3303	0.3303	0.3475	-0.0172	-0.0172	-5.0%	-5.0%
1	SB4VAR41	TiO <sub>2</sub>	0.3962	0.4121	0.4279	-0.0318	-0.0158	-7.4%	-3.7%
1	SB4VAR41	U <sub>3</sub> O <sub>8</sub>	2.7416	2.8590	2.7991	-0.0575	0.0599	-2.1%	2.1%
1	SB4VAR41	ZnO	0.0180	0.0180	0.0258	-0.0078	-0.0078	-30.0%	-30.0%
1	SB4VAR41	ZrO <sub>2</sub>	0.0257	0.0257	0.0283	-0.0026	-0.0026	-9.3%	-9.3%
1	SB4VAR41	Sum	102.4788	101.3274	99.9999	2.4789	1.3275	2.5%	1.3%
1	SB4VAR42	Al <sub>2</sub> O <sub>3</sub>	8.6775	8.8748	8.7460	-0.0685	0.1288	-0.8%	1.5%
1	SB4VAR42	B <sub>2</sub> O <sub>3</sub>	9.1526	8.8707	9.1000	0.0526	-0.2293	0.6%	-2.5%
1	SB4VAR42	BaO	0.0232	0.0248	0.0273	-0.0041	-0.0025	-15.1%	-9.0%
1	SB4VAR42	CaO	0.9193	0.9512	0.9678	-0.0485	-0.0166	-5.0%	-1.7%
1	SB4VAR42	Ce <sub>2</sub> O <sub>3</sub>	0.0228	0.0228	0.0255	-0.0026	-0.0026	-10.4%	-10.4%
1	SB4VAR42	Cr <sub>2</sub> O <sub>3</sub>	0.0555	0.0563	0.0558	-0.0003	0.0005	-0.5%	1.0%
1	SB4VAR42	CuO	0.0272	0.0290	0.0208	0.0064	0.0082	30.9%	39.3%
1	SB4VAR42	Fe <sub>2</sub> O <sub>3</sub>	10.1080	9.9032	10.0615	0.0465	-0.1583	0.5%	-1.6%
1	SB4VAR42	K <sub>2</sub> O	0.1310	0.1208	0.1239	0.0071	-0.0031	5.7%	-2.5%
1	SB4VAR42	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0181	0.0405	0.0405	224.0%	224.0%
1	SB4VAR42	Li <sub>2</sub> O	5.0862	5.1885	5.2000	-0.1138	-0.0115	-2.2%	-0.2%
1	SB4VAR42	MgO	0.9270	0.9538	0.9367	-0.0097	0.0171	-1.0%	1.8%
1	SB4VAR42	MnO	2.1240	2.0863	2.0573	0.0667	0.0290	3.2%	1.4%
1	SB4VAR42	Na <sub>2</sub> O	11.3738	11.4551	11.6568	-0.2831	-0.2017	-2.4%	-1.7%
1	SB4VAR42	NiO	0.5192	0.5514	0.5717	-0.0525	-0.0203	-9.2%	-3.6%
1	SB4VAR42	PbO	0.0248	0.0248	0.0237	0.0011	0.0011	4.5%	4.5%
1	SB4VAR42	SiO <sub>2</sub>	47.3855	46.2490	46.4385	0.9470	-0.1895	2.0%	-0.4%
1	SB4VAR42	SO <sub>4</sub>	0.3505	0.3505	0.3801	-0.0296	-0.0296	-7.8%	-7.8%
1	SB4VAR42	TiO <sub>2</sub>	0.4474	0.4655	0.4680	-0.0206	-0.0025	-4.4%	-0.5%
1	SB4VAR42	U <sub>3</sub> O <sub>8</sub>	2.9244	3.0501	3.0615	-0.1371	-0.0114	-4.5%	-0.4%
1	SB4VAR42	ZnO	0.0224	0.0224	0.0282	-0.0058	-0.0058	-20.5%	-20.5%
1	SB4VAR42	ZrO <sub>2</sub>	0.0263	0.0263	0.0309	-0.0046	-0.0046	-14.8%	-14.8%
1	SB4VAR42	Sum	100.3873	99.3361	100.0001	0.3872	-0.6640	0.4%	-0.7%
1	SB4VAR43	Al <sub>2</sub> O <sub>3</sub>	9.4144	9.6252	9.4956	-0.0812	0.1296	-0.9%	1.4%
1	SB4VAR43	B <sub>2</sub> O <sub>3</sub>	8.6293	8.8191	8.6800	-0.0507	0.1391	-0.6%	1.6%

**Table A4. Average Measured and Bias-Corrected Chemical Compositions Versus Targeted Compositions by Oxide by SB4-Decant Variability Study Glass**

Set	Glass ID	Oxide	Measured		Targeted	Diff of Measured	Diff of Meas BC	% Diff of Measured	% Diff of BC
			Measured (wt%)	Bias-Corrected (BC) (wt%)					
1	SB4VAR43	BaO	0.0290	0.0311	0.0296	-0.0006	0.0015	-1.9%	5.1%
1	SB4VAR43	CaO	0.9903	1.0246	1.0507	-0.0604	-0.0261	-5.8%	-2.5%
1	SB4VAR43	Ce <sub>2</sub> O <sub>3</sub>	0.0252	0.0252	0.0277	-0.0025	-0.0025	-9.0%	-9.0%
1	SB4VAR43	Cr <sub>2</sub> O <sub>3</sub>	0.0515	0.0523	0.0606	-0.0091	-0.0083	-15.0%	-13.8%
1	SB4VAR43	CuO	0.0300	0.0320	0.0225	0.0075	0.0095	33.5%	42.1%
1	SB4VAR43	Fe <sub>2</sub> O <sub>3</sub>	11.2339	11.0068	10.9239	0.3100	0.0829	2.8%	0.8%
1	SB4VAR43	K <sub>2</sub> O	0.1705	0.1572	0.1345	0.0359	0.0227	26.7%	16.8%
1	SB4VAR43	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0196	0.0390	0.0390	199.2%	199.2%
1	SB4VAR43	Li <sub>2</sub> O	4.8548	5.0957	4.9600	-0.1052	0.1357	-2.1%	2.7%
1	SB4VAR43	MgO	1.0070	1.0361	1.0170	-0.0100	0.0191	-1.0%	1.9%
1	SB4VAR43	MnO	2.3758	2.3344	2.2337	0.1421	0.1007	6.4%	4.5%
1	SB4VAR43	Na <sub>2</sub> O	11.6198	11.6971	11.9703	-0.3505	-0.2732	-2.9%	-2.3%
1	SB4VAR43	NiO	0.5685	0.6038	0.6207	-0.0522	-0.0169	-8.4%	-2.7%
1	SB4VAR43	PbO	0.0264	0.0264	0.0258	0.0006	0.0006	2.3%	2.3%
1	SB4VAR43	SiO <sub>2</sub>	45.5136	46.0542	44.4189	1.0947	1.6353	2.5%	3.7%
1	SB4VAR43	SO <sub>4</sub>	0.4000	0.4000	0.4127	-0.0127	-0.0127	-3.1%	-3.1%
1	SB4VAR43	TiO <sub>2</sub>	0.5158	0.5366	0.5081	0.0077	0.0285	1.5%	5.6%
1	SB4VAR43	U <sub>3</sub> O <sub>8</sub>	3.2074	3.3446	3.3239	-0.1165	0.0207	-3.5%	0.6%
1	SB4VAR43	ZnO	0.0249	0.0249	0.0307	-0.0058	-0.0058	-18.9%	-18.9%
1	SB4VAR43	ZrO <sub>2</sub>	0.0277	0.0277	0.0336	-0.0059	-0.0059	-17.6%	-17.6%
1	SB4VAR43	Sum	100.7744	102.0135	100.0001	0.7744	2.0134	0.8%	2.0%
1	SB4VAR44	Al <sub>2</sub> O <sub>3</sub>	10.2553	10.4345	10.2453	0.0100	0.1892	0.1%	1.8%
1	SB4VAR44	B <sub>2</sub> O <sub>3</sub>	8.2590	8.4406	8.2600	-0.0010	0.1806	0.0%	2.2%
1	SB4VAR44	BaO	0.0299	0.0319	0.0319	-0.0020	0.0000	-6.4%	-0.1%
1	SB4VAR44	CaO	1.0756	1.1040	1.1337	-0.0581	-0.0297	-5.1%	-2.6%
1	SB4VAR44	Ce <sub>2</sub> O <sub>3</sub>	0.0258	0.0258	0.0298	-0.0041	-0.0041	-13.7%	-13.7%
1	SB4VAR44	Cr <sub>2</sub> O <sub>3</sub>	0.0661	0.0669	0.0654	0.0007	0.0015	1.1%	2.3%
1	SB4VAR44	CuO	0.0307	0.0325	0.0243	0.0064	0.0082	26.2%	33.9%
1	SB4VAR44	Fe <sub>2</sub> O <sub>3</sub>	10.5691	11.1031	11.7863	-1.2172	-0.6832	-10.3%	-5.8%
1	SB4VAR44	K <sub>2</sub> O	0.1482	0.1375	0.1451	0.0030	-0.0077	2.1%	-5.3%
1	SB4VAR44	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0212	0.0374	0.0374	176.6%	176.6%
1	SB4VAR44	Li <sub>2</sub> O	4.5803	4.8076	4.7200	-0.1397	0.0876	-3.0%	1.9%
1	SB4VAR44	MgO	1.0601	1.1137	1.0972	-0.0371	0.0165	-3.4%	1.5%
1	SB4VAR44	MnO	2.3112	2.3796	2.4100	-0.0988	-0.0304	-4.1%	-1.3%
1	SB4VAR44	Na <sub>2</sub> O	12.1758	12.1614	12.2837	-0.1079	-0.1223	-0.9%	-1.0%
1	SB4VAR44	NiO	0.5704	0.6169	0.6697	-0.0993	-0.0528	-14.8%	-7.9%
1	SB4VAR44	PbO	0.0307	0.0307	0.0278	0.0029	0.0029	10.4%	10.4%
1	SB4VAR44	SiO <sub>2</sub>	43.2673	43.7836	42.3993	0.8680	1.3843	2.0%	3.3%
1	SB4VAR44	SO <sub>4</sub>	0.4104	0.4104	0.4453	-0.0348	-0.0348	-7.8%	-7.8%
1	SB4VAR44	TiO <sub>2</sub>	0.5029	0.5302	0.5482	-0.0453	-0.0180	-8.3%	-3.3%
1	SB4VAR44	U <sub>3</sub> O <sub>8</sub>	3.4079	3.5535	3.5863	-0.1784	-0.0328	-5.0%	-0.9%
1	SB4VAR44	ZnO	0.0296	0.0296	0.0331	-0.0035	-0.0035	-10.7%	-10.7%
1	SB4VAR44	ZrO <sub>2</sub>	0.0317	0.0317	0.0362	-0.0045	-0.0045	-12.3%	-12.3%
1	SB4VAR44	Sum	98.8966	100.8844	99.9998	-1.1032	0.8846	-1.1%	0.9%
1	SB4VAR51	Al <sub>2</sub> O <sub>3</sub>	7.7847	7.9605	7.7091	0.0756	0.2514	1.0%	3.3%
1	SB4VAR51	B <sub>2</sub> O <sub>3</sub>	9.3860	9.5924	9.5200	-0.1340	0.0724	-1.4%	0.8%
1	SB4VAR51	BaO	0.0207	0.0221	0.0241	-0.0034	-0.0020	-14.3%	-8.1%
1	SB4VAR51	CaO	0.8101	0.8383	0.8532	-0.0431	-0.0149	-5.0%	-1.7%
1	SB4VAR51	Ce <sub>2</sub> O <sub>3</sub>	0.0202	0.0202	0.0225	-0.0023	-0.0023	-10.3%	-10.3%
1	SB4VAR51	Cr <sub>2</sub> O <sub>3</sub>	0.0512	0.0519	0.0492	0.0020	0.0027	4.0%	5.5%
1	SB4VAR51	CuO	0.0272	0.0290	0.0183	0.0089	0.0107	48.8%	58.3%
1	SB4VAR51	Fe <sub>2</sub> O <sub>3</sub>	8.7140	8.5366	8.8716	-0.1576	-0.3350	-1.8%	-3.8%
1	SB4VAR51	K <sub>2</sub> O	0.1177	0.1086	0.1092	0.0085	-0.0006	7.8%	-0.6%
1	SB4VAR51	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0160	0.0426	0.0426	266.5%	266.5%
1	SB4VAR51	Li <sub>2</sub> O	5.2854	5.5476	5.4400	-0.1546	0.1076	-2.8%	2.0%
1	SB4VAR51	MgO	0.7964	0.8194	0.8253	-0.0289	-0.0059	-3.5%	-0.7%
1	SB4VAR51	MnO	1.8432	1.8094	1.8152	0.0280	-0.0058	1.5%	-0.3%
1	SB4VAR51	Na <sub>2</sub> O	12.1657	12.2525	12.2471	-0.0814	0.0054	-0.7%	0.0%



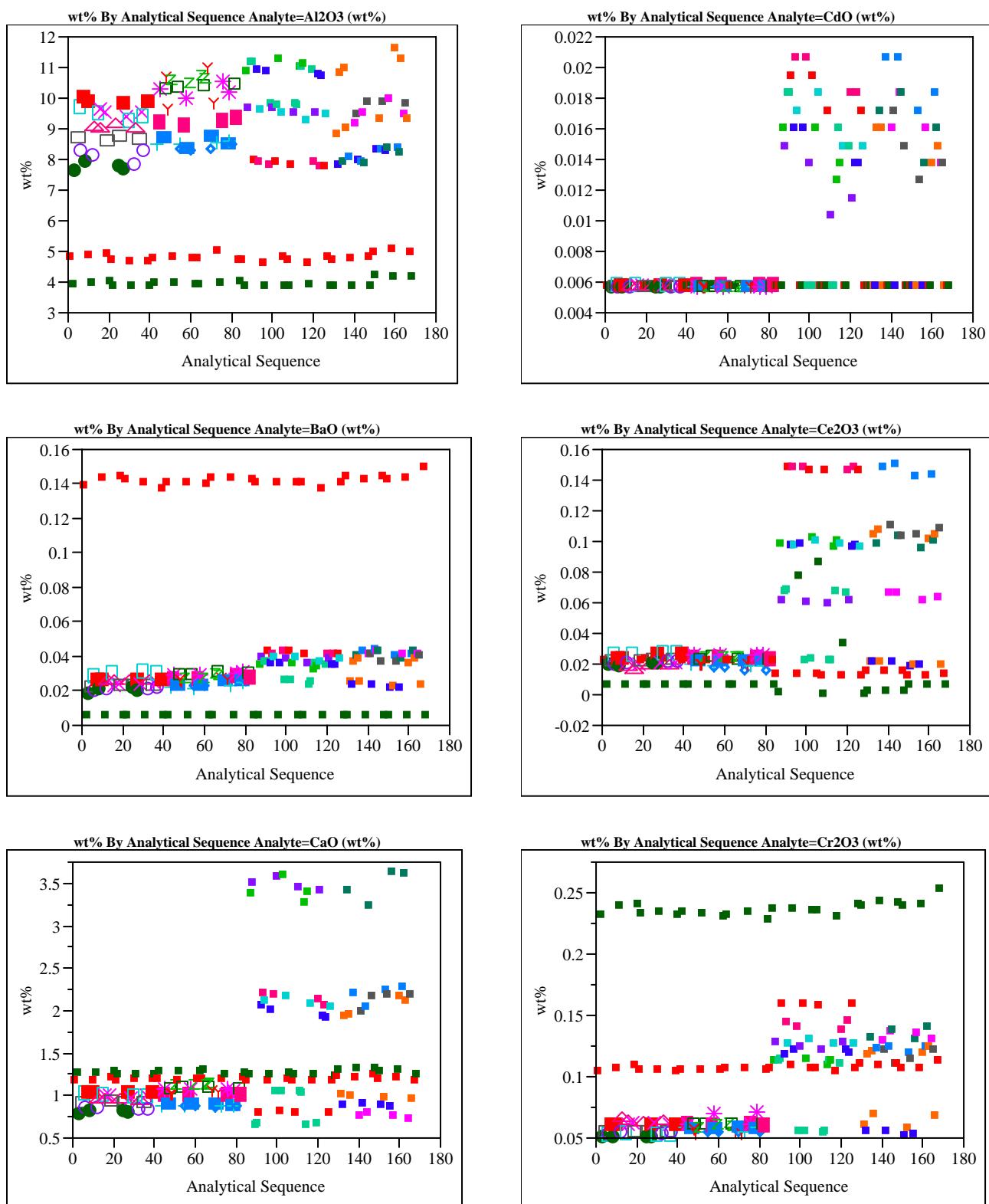




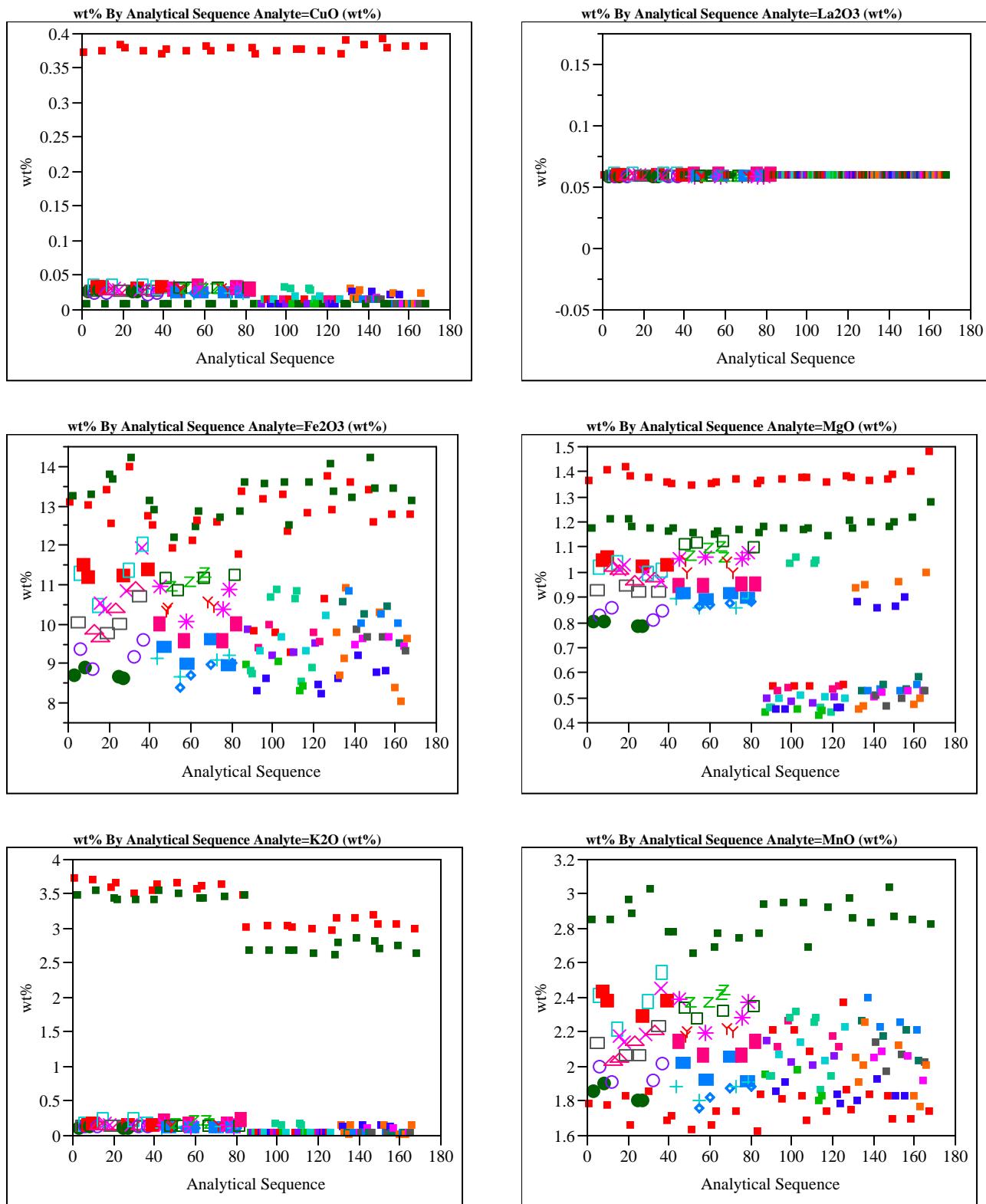
**Table A4. Average Measured and Bias-Corrected Chemical Compositions Versus Targeted Compositions by Oxide by SB4-Decant Variability Study Glass**

Set	Glass ID	Oxide	Measured		Targeted	Diff of Measured	Diff of Meas BC	% Diff of Measured	% Diff of BC
			Measured (wt%)	Bias-Corrected (BC) (wt%)					
2	SB4VAR33	Ce <sub>2</sub> O <sub>3</sub>	0.0225	0.0225	0.0262	-0.0037	-0.0037	-13.9%	-13.9%
2	SB4VAR33	Cr <sub>2</sub> O <sub>3</sub>	0.0552	0.0555	0.0626	-0.0074	-0.0071	-11.9%	-11.4%
2	SB4VAR33	CuO	0.0288	0.0308	0.0231	0.0057	0.0077	24.6%	33.5%
2	SB4VAR33	Fe <sub>2</sub> O <sub>3</sub>	10.7299	10.5166	11.4103	-0.6804	-0.8937	-6.0%	-7.8%
2	SB4VAR33	K <sub>2</sub> O	0.1458	0.1619	0.1412	0.0046	0.0207	3.2%	14.7%
2	SB4VAR33	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0196	0.0390	0.0390	199.2%	199.2%
2	SB4VAR33	Li <sub>2</sub> O	4.7848	4.9548	4.8000	-0.0152	0.1548	-0.3%	3.2%
2	SB4VAR33	MgO	1.0377	1.0769	1.0828	-0.0451	-0.0059	-4.2%	-0.5%
2	SB4VAR33	MnO	2.2757	2.1969	2.2916	-0.0159	-0.0947	-0.7%	-4.1%
2	SB4VAR33	Na <sub>2</sub> O	12.4926	12.7415	12.9157	-0.4231	-0.1742	-3.3%	-1.3%
2	SB4VAR33	NiO	0.5574	0.5966	0.6349	-0.0775	-0.0383	-12.2%	-6.0%
2	SB4VAR33	PbO	0.0272	0.0272	0.0251	0.0021	0.0021	8.4%	8.4%
2	SB4VAR33	SiO <sub>2</sub>	42.2512	41.7624	43.0734	-0.8222	-1.3110	-1.9%	-3.0%
2	SB4VAR33	SO <sub>4</sub>	0.3715	0.3715	0.3969	-0.0254	-0.0254	-6.4%	-6.4%
2	SB4VAR33	TiO <sub>2</sub>	0.0217	0.0228	0.0154	0.0063	0.0074	40.8%	47.7%
2	SB4VAR33	U <sub>3</sub> O <sub>8</sub>	3.3018	3.4637	3.4814	-0.1796	-0.0177	-5.2%	-0.5%
2	SB4VAR33	ZnO	0.0062	0.0062	0.0312	-0.0250	-0.0250	-80.1%	-80.1%
2	SB4VAR33	ZrO <sub>2</sub>	0.0270	0.0270	0.0318	-0.0048	-0.0048	-15.0%	-15.0%
2	SB4VAR33	Sum	97.5277	97.7396	99.9999	-2.4722	-2.2603	-2.5%	-2.3%
2	U std	Al <sub>2</sub> O <sub>3</sub>	3.9365	4.0138	4.1000	-0.1635	-0.0862	-4.0%	-2.1%
2	U std	B <sub>2</sub> O <sub>3</sub>	9.0130	8.9811	9.2090	-0.1960	-0.2279	-2.1%	-2.5%
2	U std	BaO	0.0056	0.0059	0.0000	0.0056	0.0059		
2	U std	CaO	1.2649	1.2983	1.3010	-0.0361	-0.0027	-2.8%	-0.2%
2	U std	Ce <sub>2</sub> O <sub>3</sub>	0.0184	0.0184	0.0000	0.0184	0.0184		
2	U std	Cr <sub>2</sub> O <sub>3</sub>	0.2388	0.2374	0.0000	0.2388	0.2374		
2	U std	CuO	0.0063	0.0066	0.0000	0.0063	0.0066		
2	U std	Fe <sub>2</sub> O <sub>3</sub>	13.4511	13.2525	13.1960	0.2551	0.0565	1.9%	0.4%
2	U std	K <sub>2</sub> O	2.6973	2.9511	2.9990	-0.3017	-0.0479	-10.1%	-1.6%
2	U std	La <sub>2</sub> O <sub>3</sub>	0.0586	0.0586	0.0000	0.0586	0.0586		
2	U std	Li <sub>2</sub> O	2.9387	3.0688	3.0570	-0.1183	0.0118	-3.9%	0.4%
2	U std	MgO	1.1868	1.2208	1.2100	-0.0232	0.0108	-1.9%	0.9%
2	U std	MnO	2.8858	2.8149	2.8920	-0.0062	-0.0771	-0.2%	-2.7%
2	U std	Na <sub>2</sub> O	11.6624	11.6666	11.7950	-0.1326	-0.1284	-1.1%	-1.1%
2	U std	NiO	0.9483	1.0044	1.1200	-0.1717	-0.1156	-15.3%	-10.3%
2	U std	PbO	0.0108	0.0108	0.0000	0.0108	0.0108		
2	U std	SiO <sub>2</sub>	46.0841	45.3438	45.3530	0.7311	-0.0092	1.6%	0.0%
2	U std	SO <sub>4</sub>	0.1498	0.1498	0.0000	0.1498	0.1498		
2	U std	TiO <sub>2</sub>	0.9517	0.9847	1.0490	-0.0973	-0.0643	-9.3%	-6.1%
2	U std	U <sub>3</sub> O <sub>8</sub>	2.3378	2.4060	2.4060	-0.0682	0.0000	-2.8%	0.0%
2	U std	ZnO	0.0062	0.0062	0.0000	0.0062	0.0062		
2	U std	ZrO <sub>2</sub>	0.0068	0.0068	0.0000	0.0068	0.0068		
2	U std	Sum	99.8598	99.5075	99.6870	0.1728	-0.1795	0.2%	-0.2%

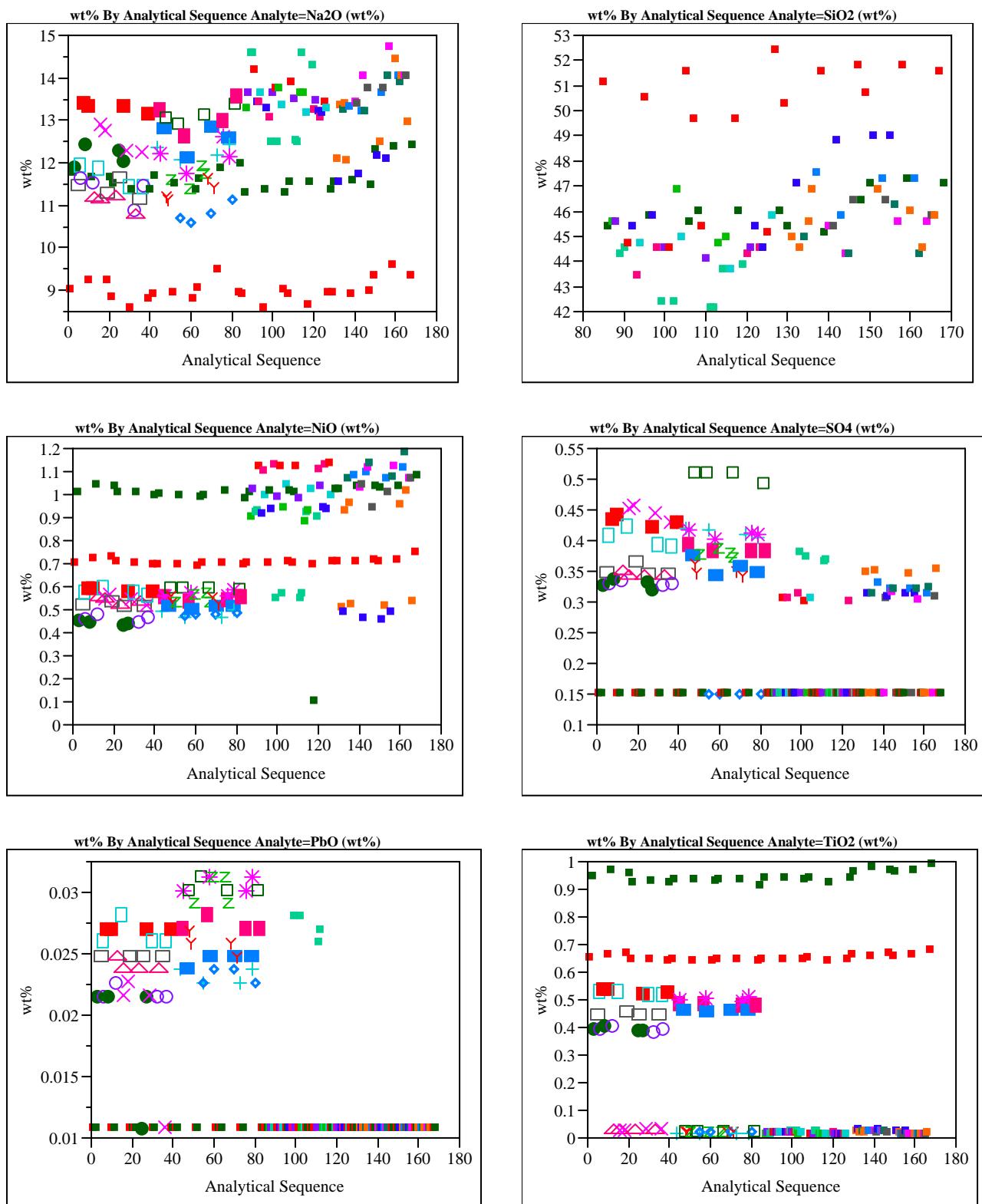
**Exhibit A1. Oxide Measurements in Analytical Sequence for  
Samples Prepared Using the LM Method**



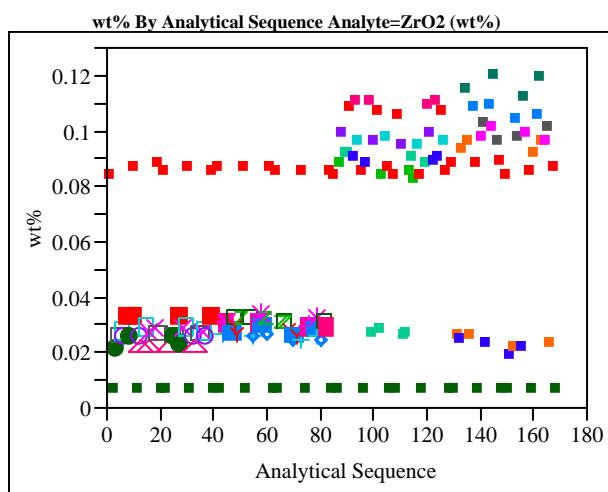
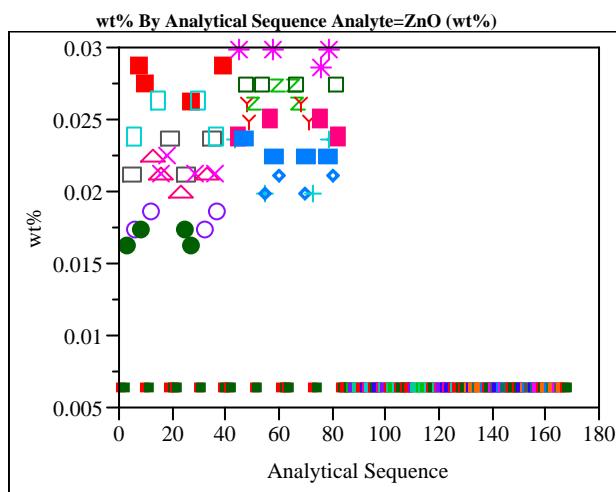
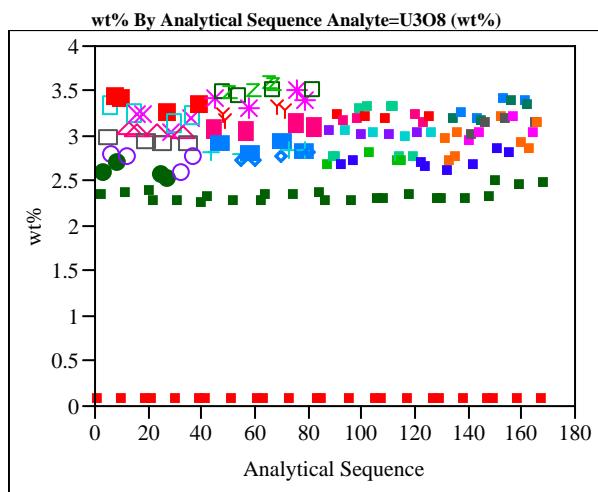
**Exhibit A1. Oxide Measurements in Analytical Sequence for  
Samples Prepared Using the LM Method**



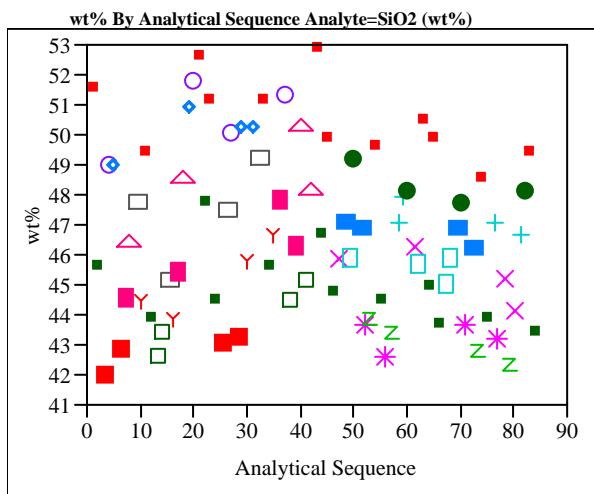
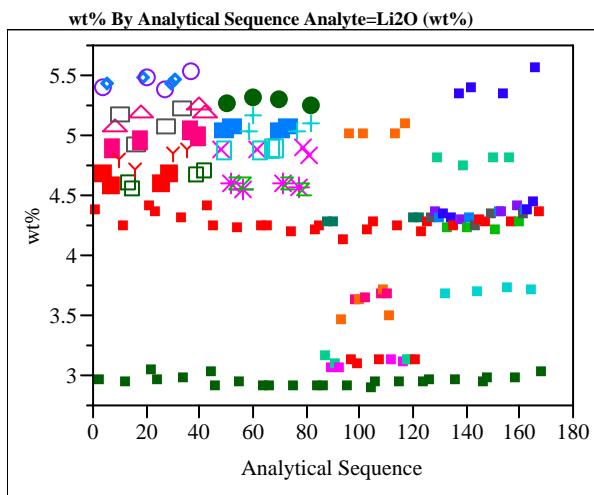
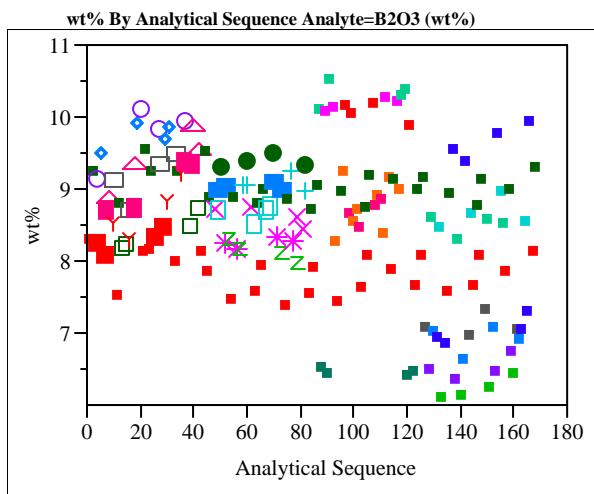
**Exhibit A1. Oxide Measurements in Analytical Sequence for  
Samples Prepared Using the LM Method**



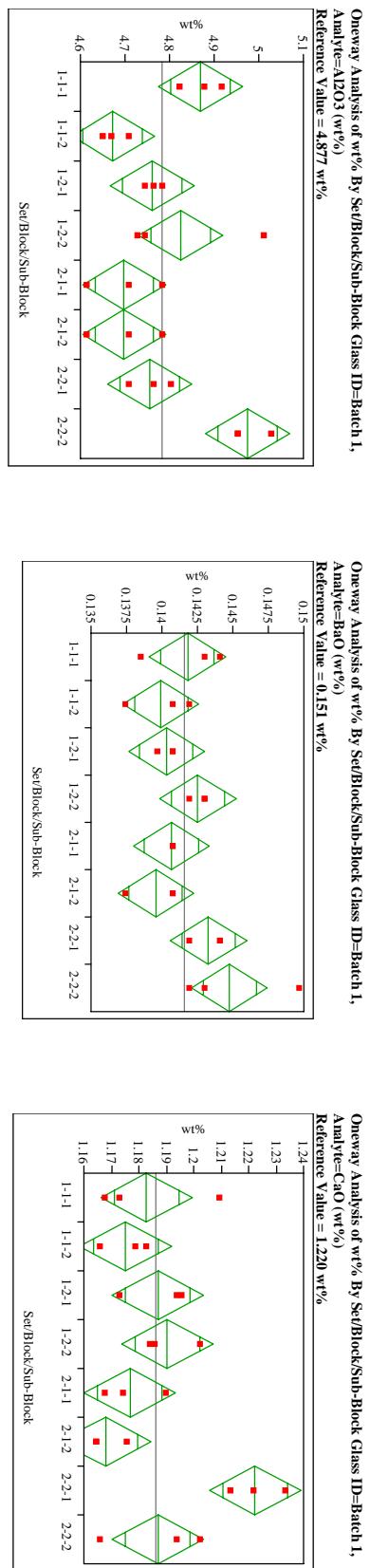
**Exhibit A1. Oxide Measurements in Analytical Sequence for  
Samples Prepared Using the LM Method**



**Exhibit A2. Oxide Measurements in Analytical Sequence for Samples Prepared Using the PF Method**



## Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



One-way Anova Summary of Fit						
Source	0.700547					
R Square	0.569536					
Adj R Square	0.24858					
Root Mean Square Error	0.076849					
Mean of Response	4.78201					
Observations (or Sum Wgts)	24					

Analysis of Variance						
Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F	
Set/Block/Sub-Block	7	0.2210552	0.031579	5.3472	0.0027	
Error	16	0.09449156	0.005906			
C. Total	23	0.31554708				

Means for One-way Anova						
Level	Number	Mean	Std Error	Lower 95%	Upper 95%	
1-1-1	3	4.1796	0.00126	0.13912	0.14447	
1-1-1	3	4.86861	0.04437	4.7746	4.9627	
1-1-2	3	4.67336	0.04437	4.5793	4.7674	
1-2-1	3	4.76154	0.04437	4.6675	4.8556	
1-2-2	3	4.82452	0.04437	4.7305	4.9186	
2-1-1	3	4.69856	0.04437	4.6045	4.7926	
2-1-2	3	4.69856	0.04437	4.6045	4.7926	
2-2-1	3	4.7524	0.04437	4.6612	4.8493	
2-2-2	3	4.97568	0.04437	4.8816	5.0097	

One-way Anova Summary of Fit						
Source	0.477273					
R Square	0.504591					
Adj R Square	0.24858					
Root Mean Square Error	0.013638					
Mean of Response	1.186172					
Observations (or Sum Wgts)	24					

Analysis of Variance						
Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F	
Set/Block/Sub-Block	7	0.00565891	0.000808	4.3466	0.0071	
Error	16	0.00297580				
C. Total	23	0.00863470				

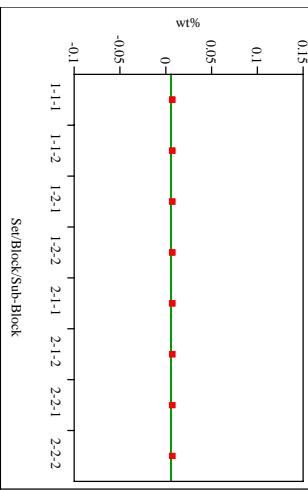
  

Means for One-way Anova						
Level	Number	Mean	Std Error	Lower 95%	Upper 95%	
1-1-1	3	1.18279	0.00757	1.1661	1.1995	
1-1-2	3	1.17533	0.00787	1.1586	1.1920	
1-2-1	3	1.18699	0.00787	1.1703	1.2037	
1-2-2	3	1.19025	0.00787	1.1736	1.2069	
2-1-1	3	1.17673	0.00787	1.1600	1.1934	
2-1-2	3	1.16787	0.00787	1.1512	1.1846	
2-2-1	3	1.22233	0.00787	1.2057	1.2391	
2-2-2	3	1.18699	0.00787	1.1703	1.2037	

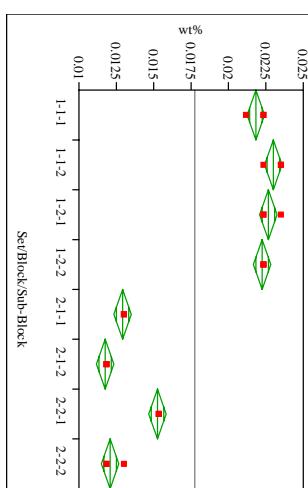
Std Error uses a pooled estimate of error variance

## Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method

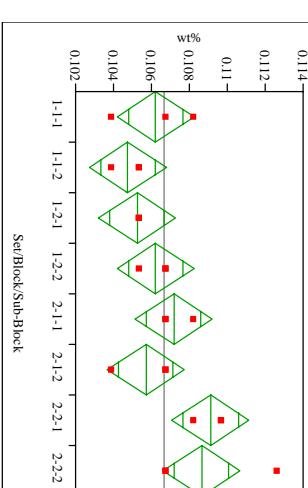
One-way Analysis of wt% By Set/Block/Sub-Block Glass ID=Batch 1,  
Analyte=CdO (wt%)  
Reference Value = 0.0 wt%



One-way Analysis of wt% By Set/Block/Sub-Block Glass ID=Batch 1,  
Analyte=CeO3 (wt%)  
Reference Value = 0.0 wt%



One-way Analysis of wt% By Set/Block/Sub-Block Glass ID=Batch 1,  
Analyte=C (wt%)  
Reference Value = 0.107 wt%



One-way Anova  
Summary of Fit

One-way Anova  
Summary of Fit

One-way Anova  
Summary of Fit

Source DF Sum of Squares Mean Square F Ratio Prob > F  
Resquare . 0.993537  
Adj Resquare 0.99071  
Root Mean Square Error 0.000478  
Mean of Response 0.005712  
Observations (or Sum Wgts) 24

Source DF Sum of Squares Mean Square F Ratio Prob > F  
Resquare . 0.993537  
Adj Resquare 0.99071  
Root Mean Square Error 0.000478  
Mean of Response 0.005712  
Observations (or Sum Wgts) 24

Source DF Sum of Squares Mean Square F Ratio Prob > F  
Resquare . 0.993537  
Adj Resquare 0.99071  
Root Mean Square Error 0.000478  
Mean of Response 0.005712  
Observations (or Sum Wgts) 24

Analysis of Variance

Analysis of Variance

Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block/Sub-Block	7	0.00056244	0.000080	351.3929	<.0001
Error	16	0.00000366	2.287e-7		
C. Total	23	0.00056610			

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block/Sub-Block	7	0.0005189	7.4134e-6	2.6866	0.0482
Error	16	0.00004415	2.7594e-6		
C. Total	23	0.00056604			

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block/Sub-Block	7	0.0005189	7.4134e-6	2.6866	0.0482
Error	16	0.00004415	2.7594e-6		
C. Total	23	0.00056604			

Means for One-way Anova

Means for One-way Anova

Means for One-way Anova

Level Number	Mean	Std Error	Lower 95%	Upper 95%
1-1-1	0.005712	0	0.00571	0.00571
1-1-2	0	0.00571	0.00571	0.00571
1-2-1	0	0.00571	0.00571	0.00571
1-2-2	0	0.00571	0.00571	0.00571
2-1-1	0	0.00571	0.00571	0.00571
2-1-2	0	0.00571	0.00571	0.00571
2-2-1	0	0.00571	0.00571	0.00571
2-2-2	0	0.00571	0.00571	0.00571

Level Number	Mean	Std Error	Lower 95%	Upper 95%
1-1-1	0.005712	0	0.00571	0.00571
1-1-2	0	0.00571	0.00571	0.00571
1-2-1	0	0.00571	0.00571	0.00571
1-2-2	0	0.00571	0.00571	0.00571
2-1-1	0	0.00571	0.00571	0.00571
2-1-2	0	0.00571	0.00571	0.00571
2-2-1	0	0.00571	0.00571	0.00571
2-2-2	0	0.00571	0.00571	0.00571

Level Number	Mean	Std Error	Lower 95%	Upper 95%
1-1-1	0.005712	0	0.00571	0.00571
1-1-2	0	0.00571	0.00571	0.00571
1-2-1	0	0.00571	0.00571	0.00571
1-2-2	0	0.00571	0.00571	0.00571
2-1-1	0	0.00571	0.00571	0.00571
2-1-2	0	0.00571	0.00571	0.00571
2-2-1	0	0.00571	0.00571	0.00571
2-2-2	0	0.00571	0.00571	0.00571

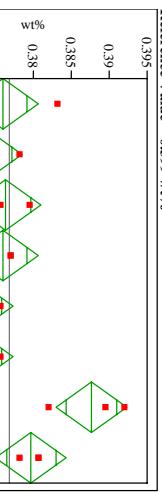
Std Error uses a pooled estimate of error variance

Std Error uses a pooled estimate of error variance

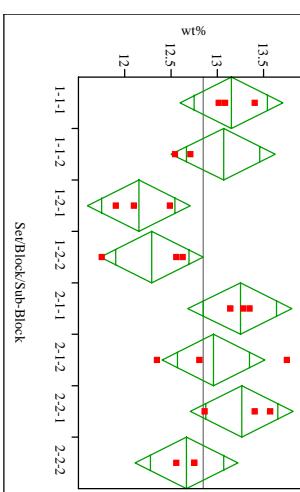
Std Error uses a pooled estimate of error variance

### Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method

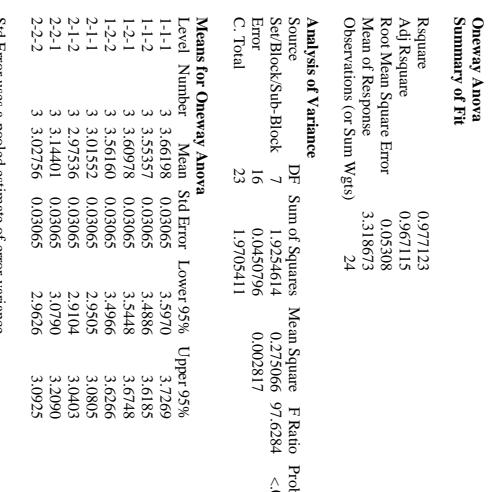
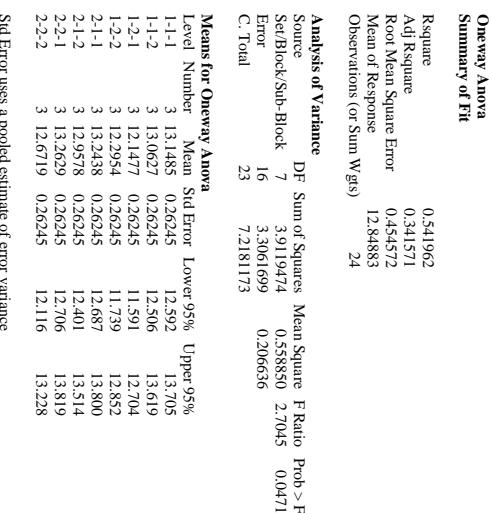
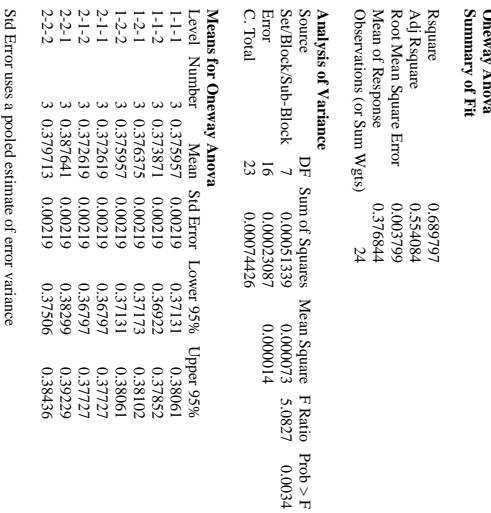
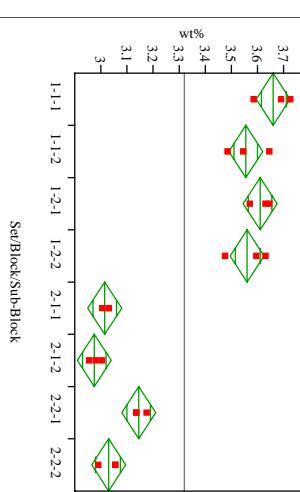
Oneway Analysis of wt% By Set/Block/Sub-Block Glass ID=Batch 1,  
Analyte=CuO (wt%)  
Reference Value = 0.399 wt%



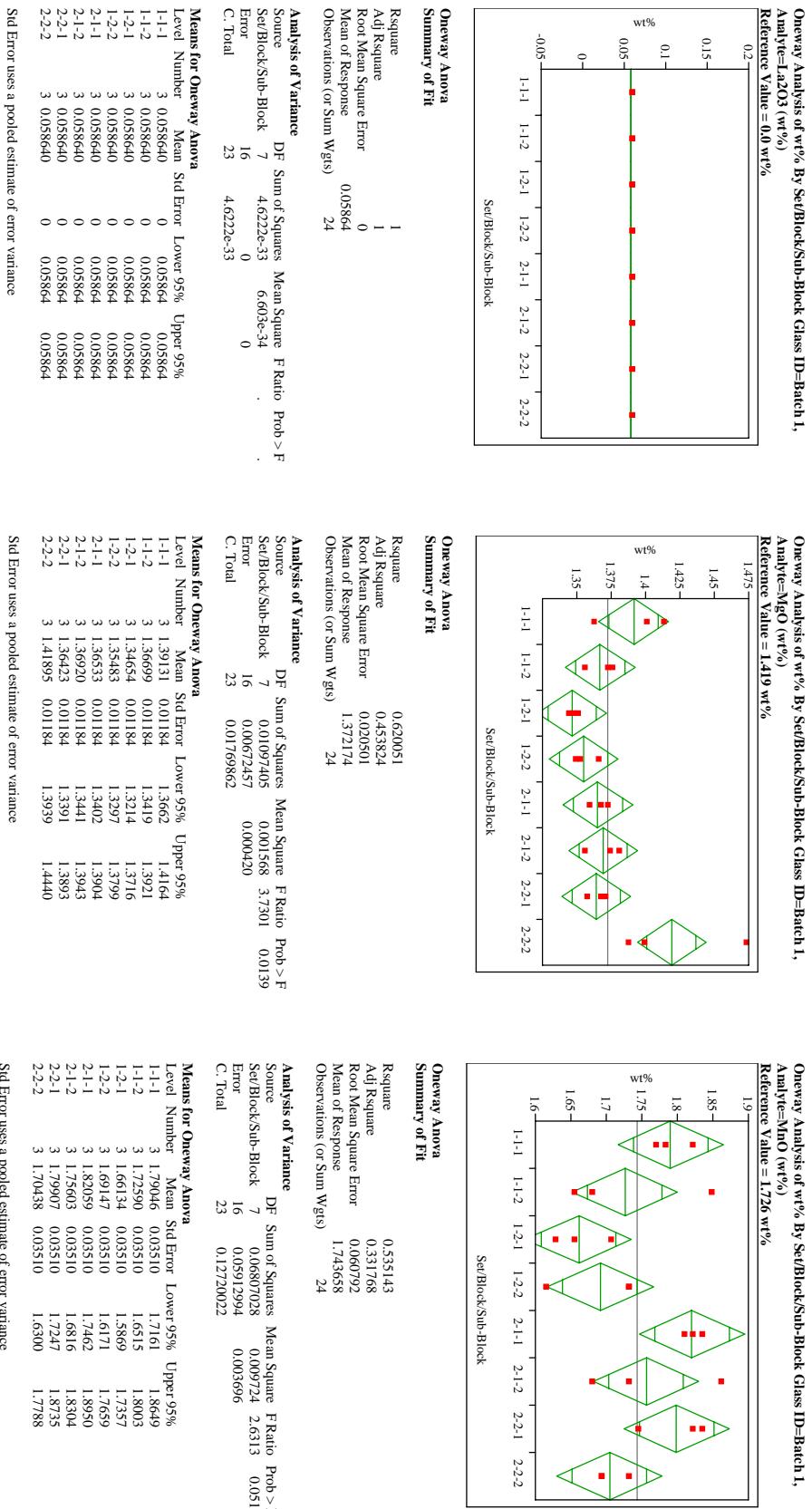
Oneway Analysis of wt% By Set/Block/Sub-Block Glass ID=Batch 1,  
Analyte=F2CO3 (wt%)  
Reference Value = 12.839 wt%



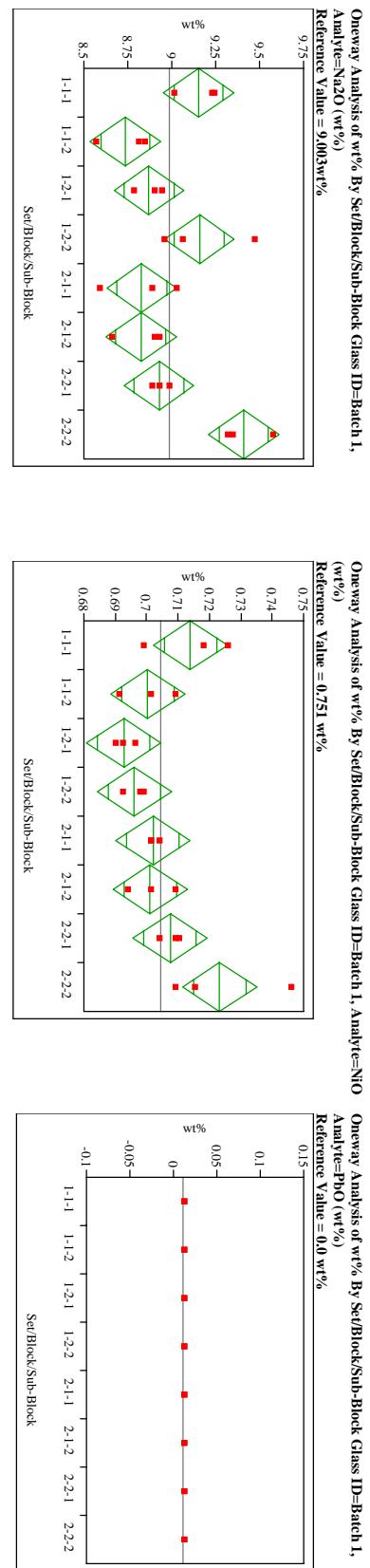
Oneway Analysis of wt% By Set/Block/Sub-Block Glass ID=Batch 1,  
Analyte=K2O (wt%)  
Reference Value = 3.327 wt%



### Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



## Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



Oneway Analysis of wt% By Set/Block/Sub-Block Glass ID=Batch 1,  
Analyte=Na<sub>2</sub>O (wt%)  
Reference Value = 9.003wt%

Oneway Analysis of wt% By Set/Block/Sub-Block Glass ID=Batch 1, Analyte=NiO  
(wt%)  
Reference Value = 0.751 wt%

Oneway Analysis of wt% By Set/Block/Sub-Block Glass ID=Batch 1,  
Analyte=PbO (wt%)  
Reference Value = 0.0 wt%

**Oneway Anova Summary of Fit**

Resquare	0.720923
Adj Rsquare	0.598827
Root Mean Square Error	0.163089
Mean of Response	8.988532
Observations (or Sum Wgts)	24

**Oneway Anova Summary of Fit**

Resquare	0.580351
Adj Rsquare	0.396754
Root Mean Square Error	0.099695
Mean of Response	0.704594
Observations (or Sum Wgts)	24

**Oneway Anova Summary of Fit**

Resquare	5.3125
Adj Rsquare	-
Root Mean Square Error	0.010772
Mean of Response	-
Observations (or Sum Wgts)	24

**Analysis of Variance**

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob>F
Set/Block/Sub-Block	7	1.0993403	0.157049	5.59046	0.00016
Error	16	0.4255058	0.026598		
C. Total	23	1.5249061			

**Analysis of Variance**

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob>F
Set/Block/Sub-Block	7	0.000207960	0.000297	3.1610	0.0268
Error	16	0.00150375	0.000094		
C. Total	23	0.00358335			

**Analysis of Variance**

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob>F
Set/Block/Sub-Block	7	2.88889e-34	4.127e-35	-	-3.0476
Error	16	-2.167e-34	-	-	0.0000
C. Total	23	7.2222e-35	-1.35e-35	-	

**Means for One-way Anova**

Level Number	Mean	Sd Error	Lower 95%	Upper 95%
1-1-1	9.15292	0.09416	8.9533	9.3525
1-1-2	8.73504	0.09416	8.5354	8.9346
1-2-1	8.86984	0.09416	8.6702	9.0694
1-2-2	9.15741	0.09416	8.9578	9.3570
2-1-1	8.82940	0.09416	8.6298	9.0290
2-1-2	8.83491	0.09416	8.6353	9.0245
2-2-1	8.92825	0.09416	8.7286	9.1279
2-2-2	9.40904	0.09416	9.2094	9.6086

Level Number	Mean	Sd Error	Lower 95%	Upper 95%
1-1-1	9.13873	0.00560	9.0201	9.2574
1-1-2	9.07029	0.00560	8.68843	9.71216
1-2-1	9.09264	0.00560	8.68080	9.70453
1-2-2	9.06956	0.00560	8.68419	9.70792
2-1-1	9.07196	0.00560	8.69013	9.71386
2-1-2	9.071148	0.00560	8.68928	9.71301
2-2-1	9.0707510	0.00560	8.69564	9.71938
2-2-2	9.0723204	0.00560	8.71134	9.73507

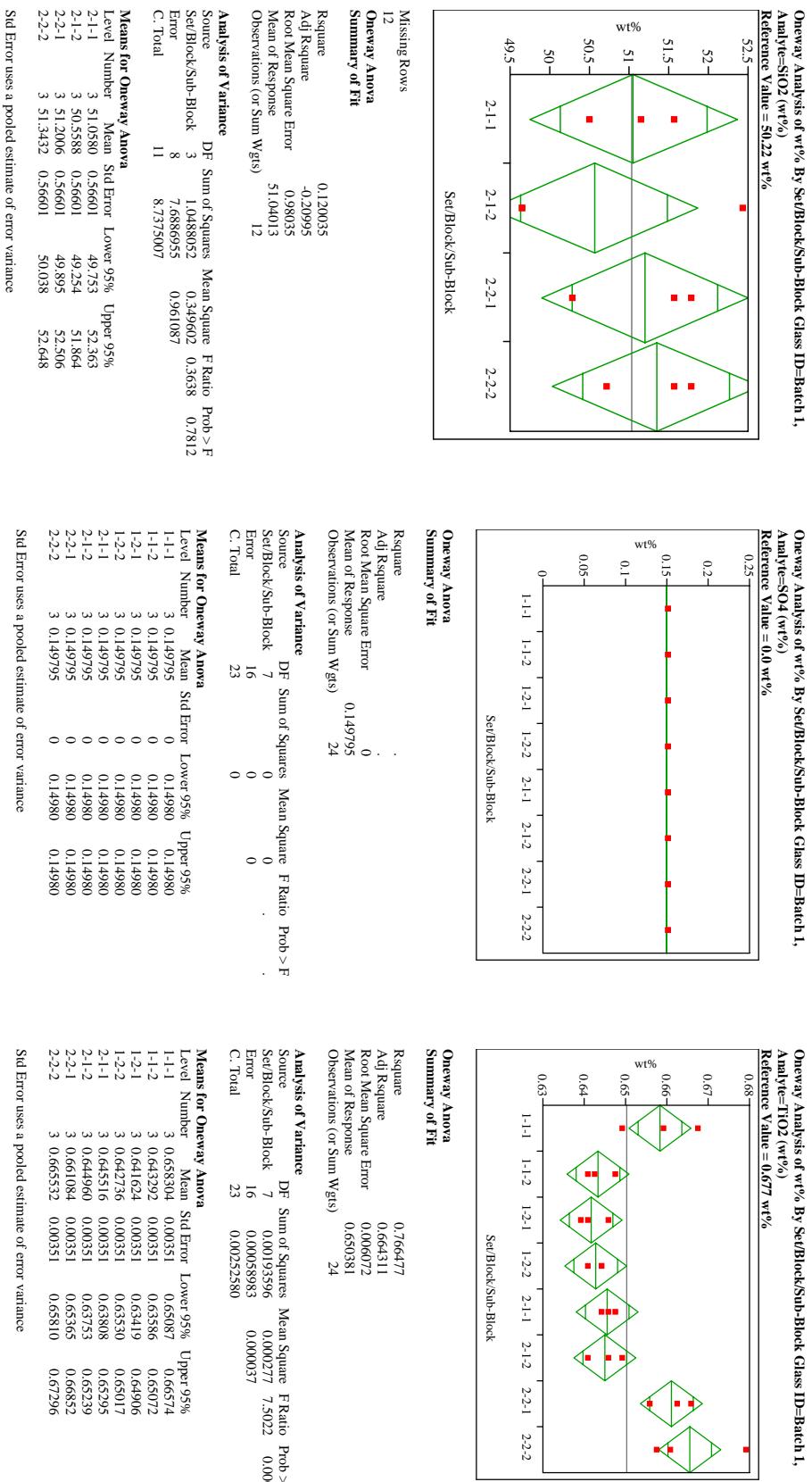
Level Number	Mean	Sd Error	Lower 95%	Upper 95%
1-1-1	0.010772	-	-	-
1-1-2	0.010772	-	-	-
1-2-1	0.010772	-	-	-
1-2-2	0.010772	-	-	-
2-1-1	0.010772	-	-	-
2-1-2	0.010772	-	-	-
2-2-1	0.010772	-	-	-
2-2-2	0.010772	-	-	-

Std Error uses a pooled estimate of error variance

Std Error uses a pooled estimate of error variance

Std Error uses a pooled estimate of error variance

### Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



## Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



**Oneway Anova Summary of Fit**

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block/Sub-Block	7	4.6222e-33	6.603e-34	.	.
Error	16	0	0	.	.
C. Total	23	4.6222e-33			

**Oneway Anova Summary of Fit**

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block/Sub-Block	7	0	0	.	.
Error	16	0	0	.	.
C. Total	23	0			

**Oneway Anova Summary of Fit**

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block/Sub-Block	7	0.00003155	4.5073e-6	3.7054	0.0142
Error	16	0.00001946	1.2164e-6		
C. Total	23	0.00005101			

### Means for Oneway Anova

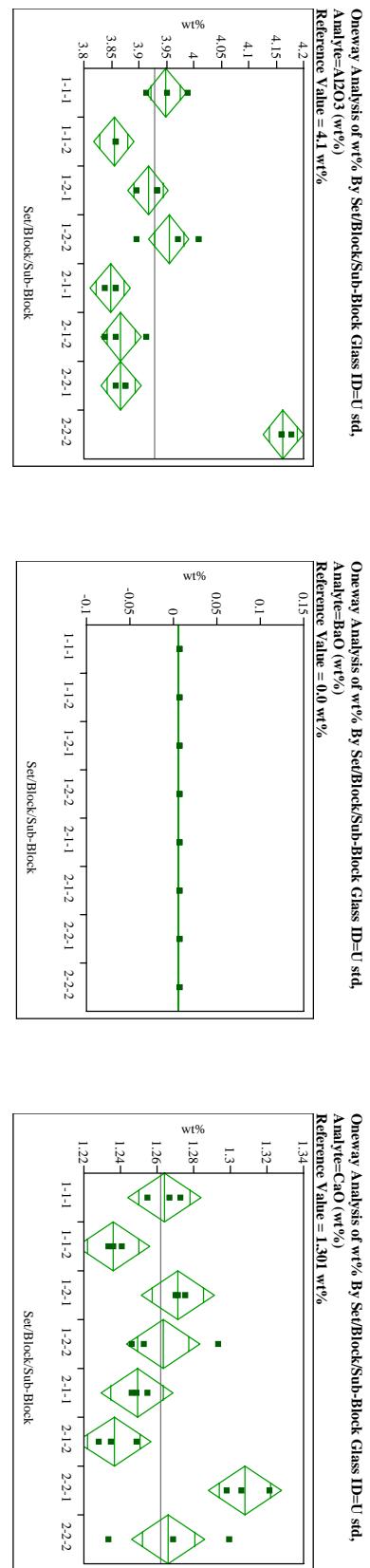
Level Number	Mean	Sd Error	Lower 95%	Upper 95%
1-1-1	0.058960	0.05896	0.05896	0.05896
1-1-2	0.058960	0.05896	0.05896	0.05896
1-2-1	0.058960	0.05896	0.05896	0.05896
1-2-2	0.058960	0.05896	0.05896	0.05896
2-1-1	0.058960	0.05896	0.05896	0.05896
2-1-2	0.058960	0.05896	0.05896	0.05896
2-2-1	0.058960	0.05896	0.05896	0.05896
2-2-2	0.058960	0.05896	0.05896	0.05896

Std Error uses a pooled estimate of error variance

Std Error uses a pooled estimate of error variance

Std Error uses a pooled estimate of error variance

## Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



Oneway Analysis of wt% By Set/Block/Sub-Block Glass ID=U std.  
Analyte=A12O3 (wt%)  
Reference Value = 4.1 wt%

Oneway Analysis of wtr% By Set/Block/Sub-Block Glass ID=U std.  
Analyte=BaO (wt%)  
Reference Value = 0.0 wt%

Oneway Analysis of wt% By Set/Block/Sub-Block Glass ID=U std.  
Analyte=CaO (wt%)  
Reference Value = 1.301 wt%

Oneway Analysis of wt% By Set/Block/Sub-Block Glass ID=U std.  
Analyte=wtr%  
Reference Value = 4.1 wt%

**Oneway Anova Summary of Fit**

Resquare	0.940883
Adj Resquare	0.915019
Root Mean Square Error	0.029876
Mean of Response	3.927798
Observations (or Sum Wgts)	24

**Oneway Anova Summary of Fit**

Resquare	.
Adj Resquare	.
Root Mean Square Error	0
Mean of Response	0.005533
Observations (or Sum Wgts)	24

**Oneway Anova Summary of Fit**

Resquare	0.727338
Adj Resquare	0.602298
Root Mean Square Error	0.01631
Mean of Response	1.261787
Observations (or Sum Wgts)	24

**Oneway Anova Summary of Fit**

Resquare	0.024156935
Set/Block/Sub-Block	7
Error	16
C. Total	23

**Oneway Anova Summary of Fit**

Resquare	0.02425617
Adj Resquare	0.000266
Root Mean Square Error	0.000558
Mean of Response	0.00558
Observations (or Sum Wgts)	24

**Oneway Anova Summary of Fit**

Resquare	0.01112783
Adj Resquare	0.00425617
Root Mean Square Error	0.000266
Mean of Response	0.00558
Observations (or Sum Wgts)	24

**Oneway Anova Summary of Fit**

### Means for Oneway Anova

Level Number	Mean	Sd Error	Lower 95%	Upper 95%
1-1-1	3.94906	0.01725	3.9125	3.9856
1-1-2	3.85458	0.01725	3.8180	3.8911
1-2-1	3.91756	0.01725	3.8810	3.9541
1-2-2	3.95536	0.01725	3.9188	3.9919
2-1-1	3.84828	0.01725	3.8117	3.8848
2-1-2	3.86718	0.01725	3.8306	3.9037
2-2-1	3.86718	0.01725	3.8306	3.9037
2-2-2	3.416320	0.01725	4.1266	4.1998

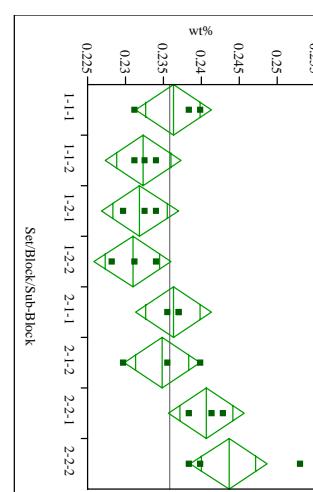
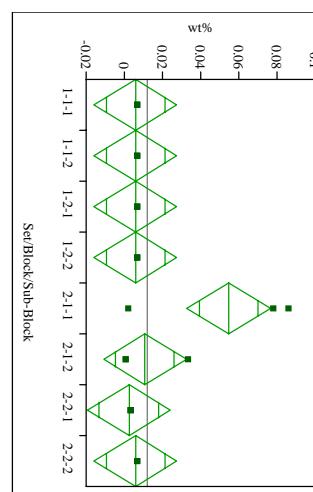
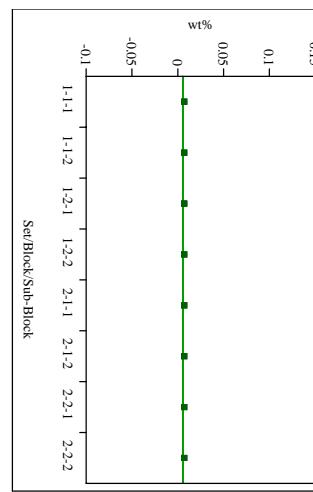
Std Error uses a pooled estimate of error variance

Std Error uses a pooled estimate of error variance

Std Error uses a pooled estimate of error variance

Std Error uses a pooled estimate of error variance

## Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



One-way Anova  
Summary of Fit

Source DF Sum of Squares Mean Square F Ratio Prob > F  
Residual 1 0.005712 0.005712  
Root Mean Square Error 0.0005712  
Mean of Response 0.0121532  
Observations (or Sum Wgts) 24

Analysis of Variance

Source DF Sum of Squares Mean Square F Ratio Prob > F  
Set/Block/Sub-Block 7 0.00630860 0.000901 2.8597 0.0387  
Error 16 0.00504235 0.000315  
C. Total 23 0.01153095

Analysis of Variance

Source DF Sum of Squares Mean Square F Ratio Prob > F  
Set/Block/Sub-Block 7 0.00040936 0.000058 3.4762 0.0185  
Error 16 0.00026917 0.000017  
C. Total 23 0.00067853

One-way Anova  
Summary of Fit

Source DF Sum of Squares Mean Square F Ratio Prob > F  
Set/Block/Sub-Block 7 0.00040936 0.000058 3.4762 0.0185  
Error 16 0.00026917 0.000017  
C. Total 23 0.00067853

One-way Anova  
Summary of Fit

Source DF Sum of Squares Mean Square F Ratio Prob > F  
Residual 1 0.005712 0.005712  
Root Mean Square Error 0.0005712  
Mean of Response 0.0121532  
Observations (or Sum Wgts) 24

Analysis of Variance

Source DF Sum of Squares Mean Square F Ratio Prob > F  
Set/Block/Sub-Block 7 0.00630860 0.000901 2.8597 0.0387  
Error 16 0.00504235 0.000315  
C. Total 23 0.01153095

Analysis of Variance

Source DF Sum of Squares Mean Square F Ratio Prob > F  
Set/Block/Sub-Block 7 0.00040936 0.000058 3.4762 0.0185  
Error 16 0.00026917 0.000017  
C. Total 23 0.00067853

Means for One-way Anova

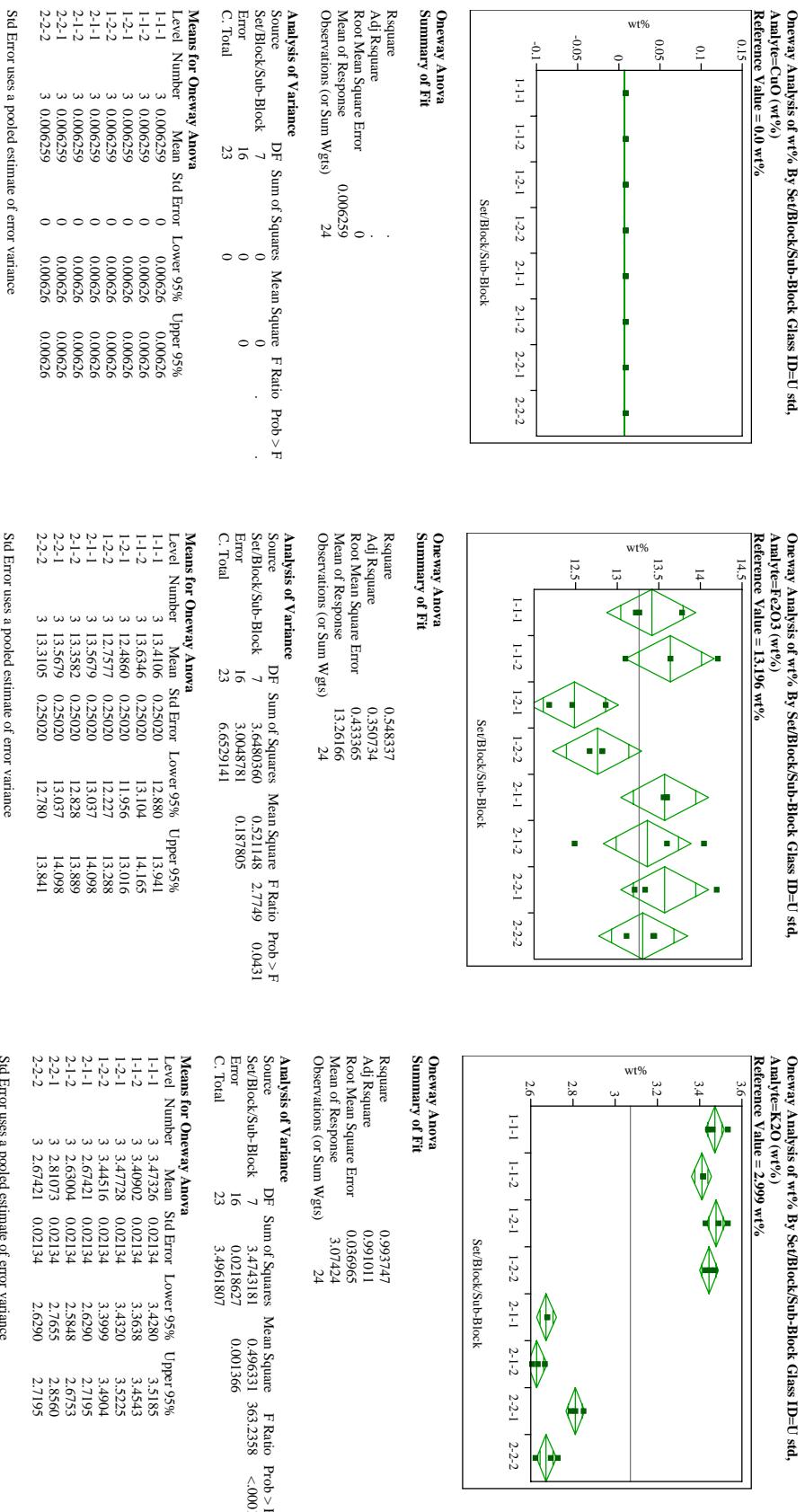
Level Number	Mean	Std Error	Lower 95%	Upper 95%
1-1-1	0.005712	0	0.00571	0.00571
1-1-2	0	0.00571	0.00571	0.00571
1-2-1	0	0.00571	0.00571	0.00571
1-2-2	0	0.00571	0.00571	0.00571
2-1-1	0	0.00571	0.00571	0.00571
2-1-2	0	0.00571	0.00571	0.00571
2-2-1	0	0.00571	0.00571	0.00571
2-2-2	0	0.00571	0.00571	0.00571

Std Error uses a pooled estimate of error variance

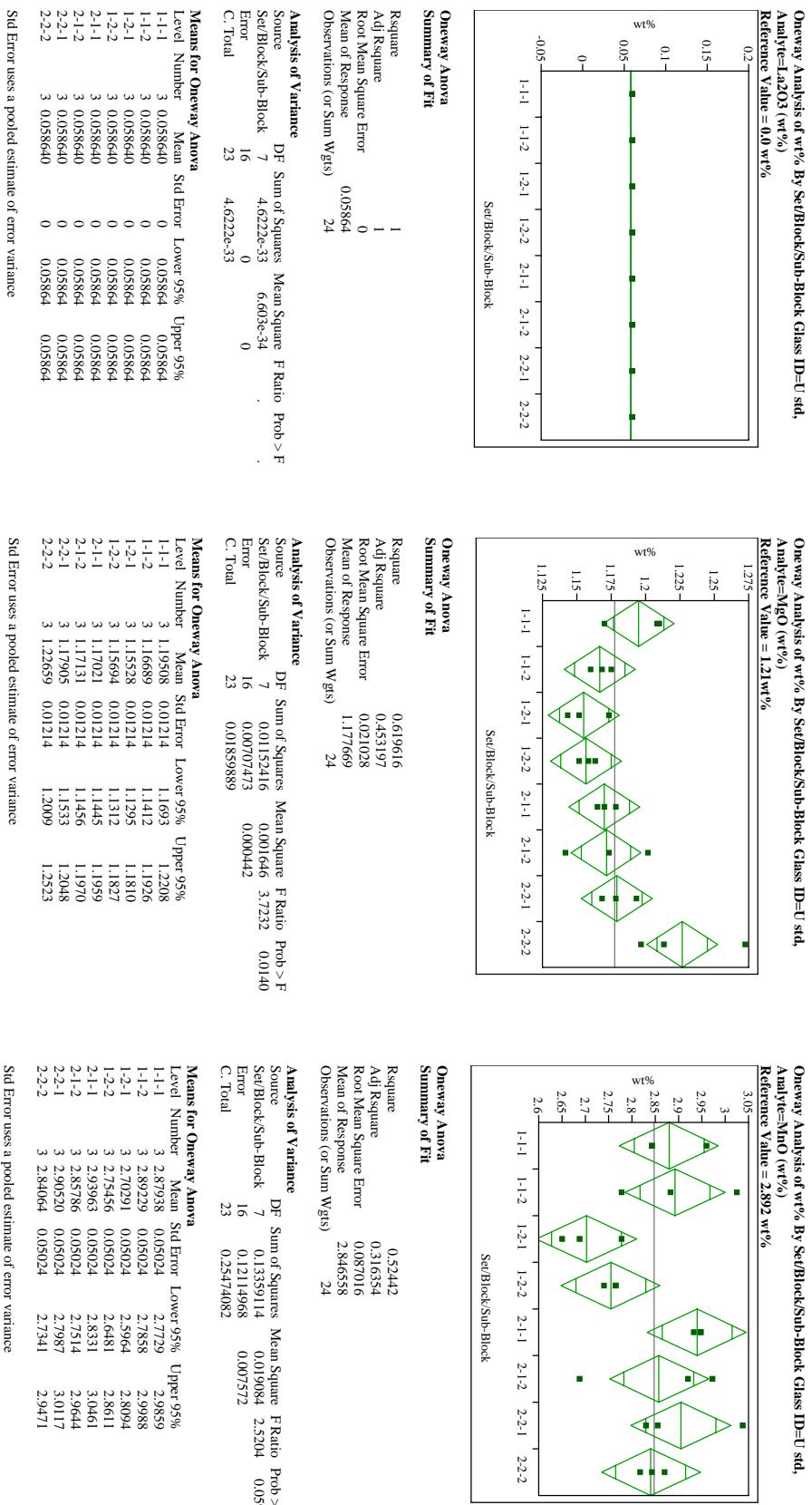
Std Error uses a pooled estimate of error variance

Std Error uses a pooled estimate of error variance

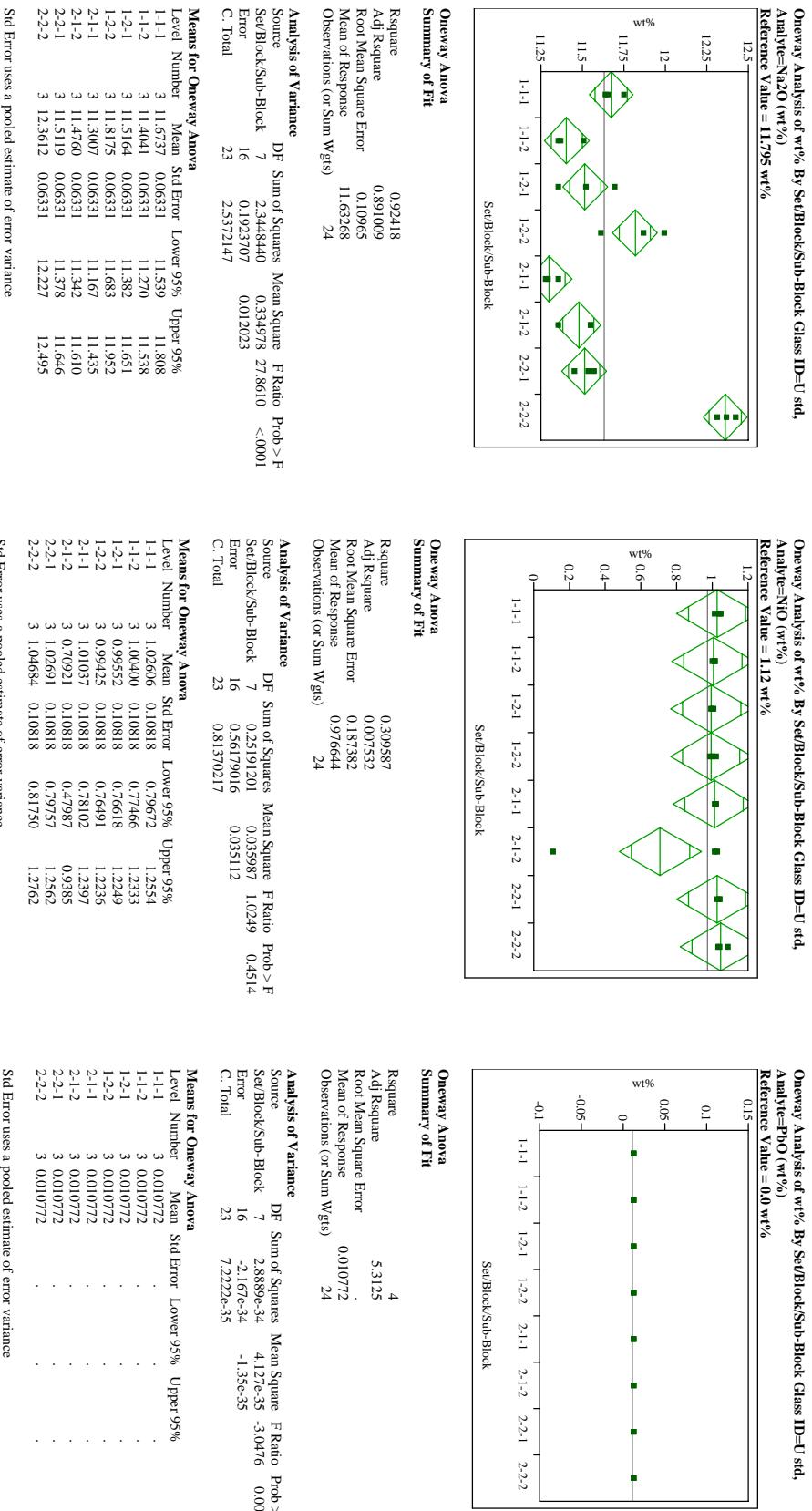
### Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



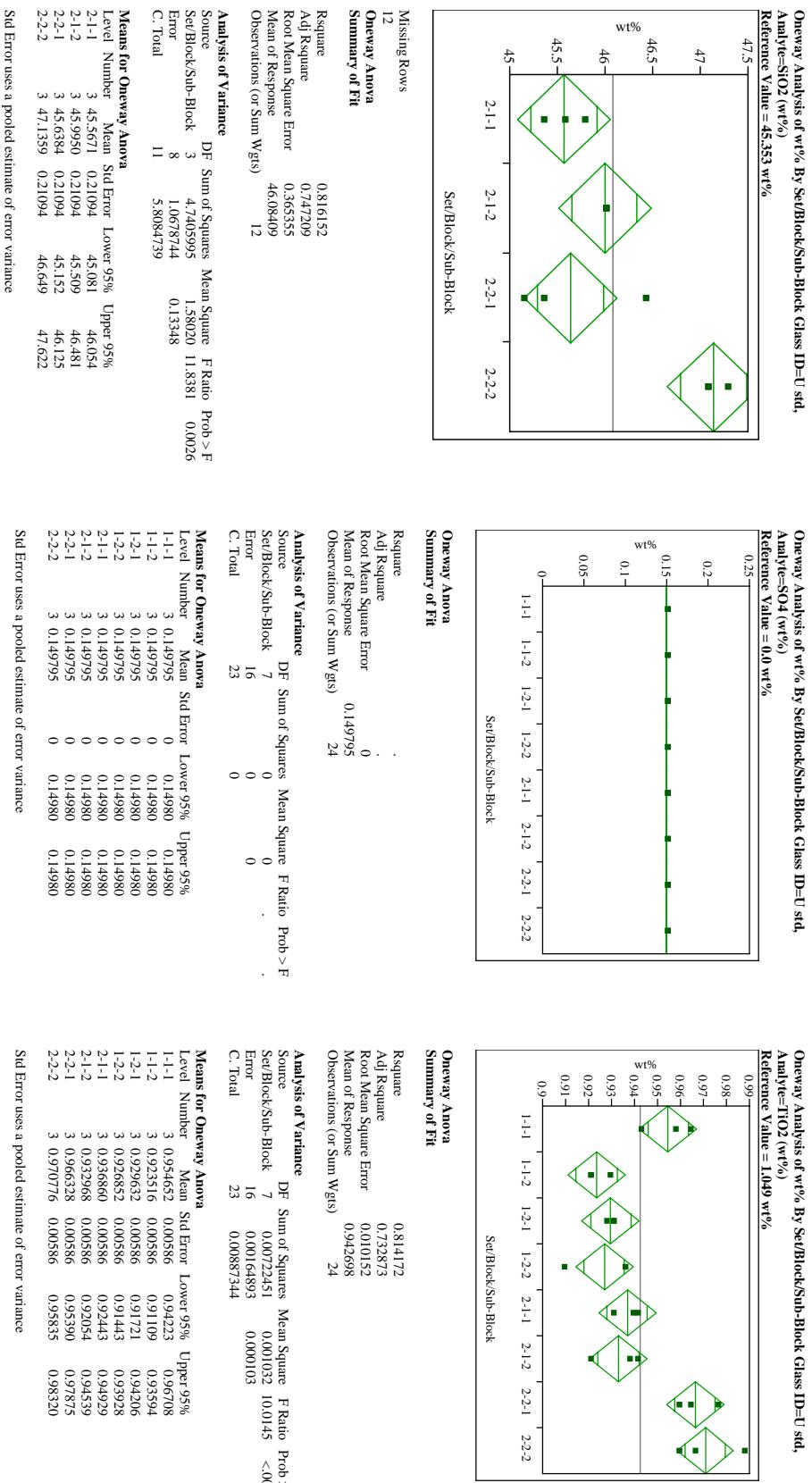
## Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



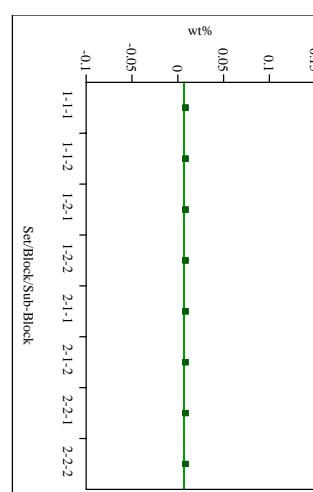
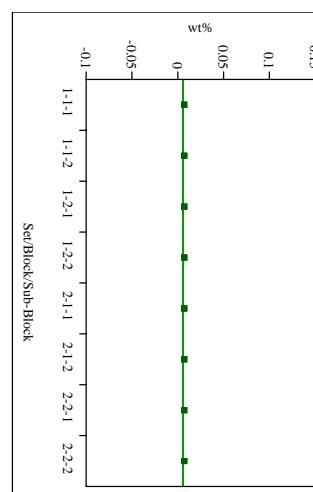
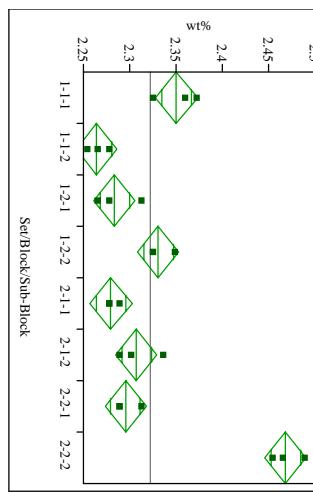
### Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



### Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



## Exhibit A3. PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the LM Method



**Oneway Anova Summary of Fit**

Resquare	0.943384
Adj Resquare	0.918614
Root Mean Square Error	0.018331
Mean of Response	2.322533
Observations (or Sum Wgts)	24

**Analysis of Variance**

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block/Sub-Block	7	0.08958957	0.012799	38.0862	<.0001
Error	16	0.00553765	0.000336		
C. Total	23	0.09496622			

**Means for Oneway Anova**

Level Number	Mean	Sd Error	Lower 95%	Upper 95%
1-1-1	3.235054	0.01058	2.3281	2.3730
1-1-2	3.226406	0.01058	2.2416	2.2865
1-2-1	3.228372	0.01058	2.2613	2.3062
1-2-2	3.233089	0.01058	2.3084	2.3533
2-1-1	3.227979	0.01058	2.2574	2.3022
2-1-2	3.230750	0.01058	2.2849	2.3297
2-2-1	3.229551	0.01058	2.2731	2.3179
2-2-2	3.246846	0.01058	2.4460	2.4909

Std Error uses a pooled estimate of error variance

**Oneway Anova Summary of Fit**

Resquare	.
Adj Resquare	.
Root Mean Square Error	0
Mean of Response	0.006224
Observations (or Sum Wgts)	24

**Analysis of Variance**

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block/Sub-Block	7	0	0	.	.
Error	16	0	0	.	.
C. Total	23	0	0	.	.

**Means for Oneway Anova**

Level Number	Mean	Sd Error	Lower 95%	Upper 95%
1-1-1	3.006224	0	0.00622	0.00622
1-1-2	3.006224	0	0.00622	0.00622
1-2-1	3.006224	0	0.00622	0.00622
1-2-2	3.006224	0	0.00622	0.00622
2-1-1	3.006224	0	0.00622	0.00622
2-1-2	3.006224	0	0.00622	0.00622
2-2-1	3.006224	0	0.00622	0.00622
2-2-2	3.006224	0	0.00622	0.00622

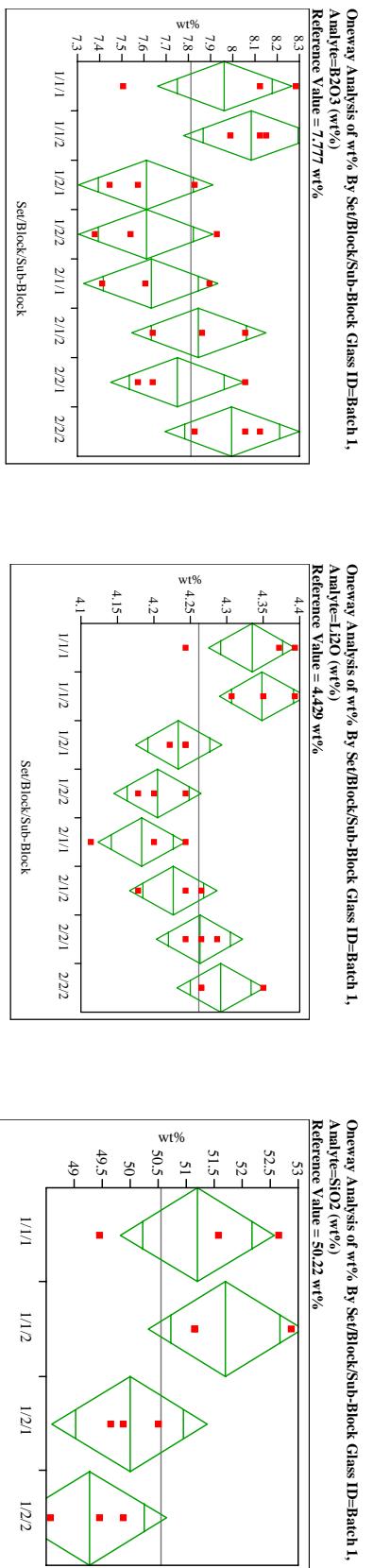
Std Error uses a pooled estimate of error variance

**Means for Oneway Anova**

Level Number	Mean	Sd Error	Lower 95%	Upper 95%
1-1-1	3.006754	0	0.00675	0.00675
1-1-2	3.006754	0	0.00675	0.00675
1-2-1	3.006754	0	0.00675	0.00675
1-2-2	3.006754	0	0.00675	0.00675
2-1-1	3.006754	0	0.00675	0.00675
2-1-2	3.006754	0	0.00675	0.00675
2-2-1	3.006754	0	0.00675	0.00675
2-2-2	3.006754	0	0.00675	0.00675

Std Error uses a pooled estimate of error variance

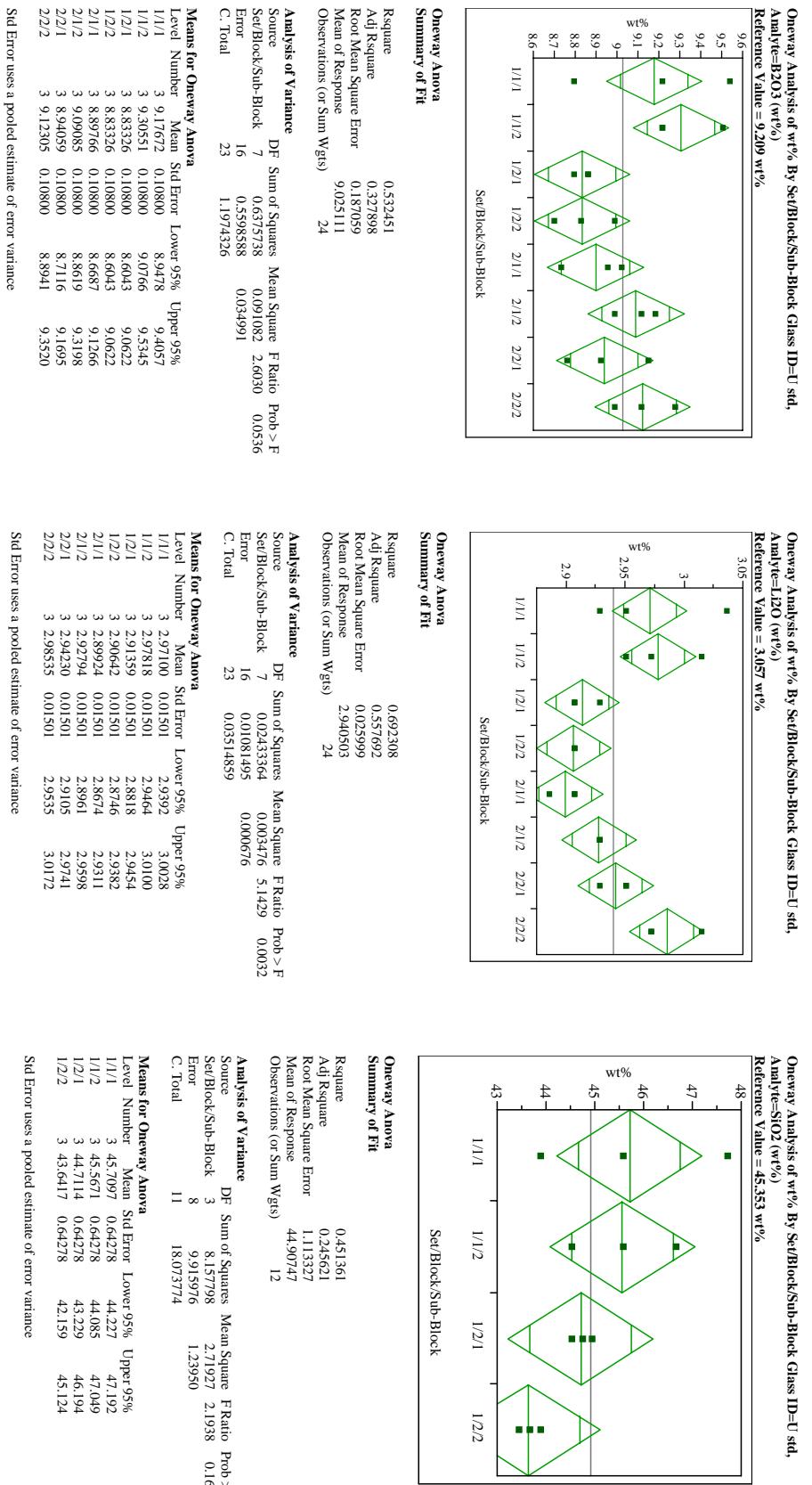
## Exhibit A4: PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the PF Method



Oneway Anova Summary of Fit								
Source	0.434883							
Rsquare	0.18764							
Adj Rsquare	0.18764							
Root Mean Square Error	0.246538							
Mean of Response	7.810941							
Observations (or Sum Wgts)	24							
Analysis of Variance								
Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F			
Set/Block/Sub-Block	7	0.7483792	0.106911	1.7590	0.1653			
Error	16	0.9724955	0.060781					
C. Total	23	1.7208747						
Means for Oneway Anova								
Level Number	Mean	Std Error	Lower 95%	Upper 95%				
1/1/1	7.96389	0.14234	7.6621	8.2656				
1/1/2	3.808195	0.14234	7.7802	8.8837				
1/2/1	3.760970	0.14234	7.3080	7.9114				
1/2/2	3.760970	0.14234	7.3080	7.9114				
2/1/1	3.763116	0.14234	7.3294	7.9114				
2/1/2	3.784582	0.14234	7.5441	8.1476				
2/2/1	3.74923	0.14234	7.4475	8.0510				
2/2/2	3.799609	0.14234	7.6943	8.2978				
Means for Oneway Anova								
Level Number	Mean	Std Error	Lower 95%	Upper 95%				
1/1/1	3.433451	0.02814	4.2749	4.3942				
1/1/2	3.434886	0.02814	4.2892	4.4085				
1/2/1	3.4223404	0.02814	4.1744	4.2937				
1/2/2	3.420533	0.02814	4.1457	4.2650				
2/1/1	3.418380	0.02814	4.1242	4.2435				
2/1/2	3.422586	0.02814	4.1672	4.2865				
2/2/1	3.420274	0.02814	4.2031	4.3224				
2/2/2	3.429145	0.02814	4.2318	4.3511				
Means for Oneway Anova								
Level Number	Mean	Std Error	Lower 95%	Upper 95%				
1/1/1	3.516998	0.59662	49.825	52.076				
1/1/2	3.499883	0.59662	50.334	53.076				
1/2/1	3.492752	0.59662	48.612	51.364				
1/2/2	3.492752	0.59662	47.899	50.651				
Summary of Fit								
Rsquare	0.663705							
Adj Rsquare	0.516576							
Root Mean Square Error	0.048738							
Mean of Response	4.260948							
Observations (or Sum Wgts)	24							
Analysis of Variance								
Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F			
Set/Block/Sub-Block	7	0.07500940	0.010716	4.5110	0.0060			
Error	16	0.03500682	0.002375					
C. Total	23	0.11301622						
Means for Oneway Anova								
Level Number	Mean	Std Error	Lower 95%	Upper 95%				
1/1/1	50.54096							
1/1/2	50.54096							
1/2/1	50.54096							
1/2/2	50.54096							
Summary of Fit								
Rsquare	0.564118							
Adj Rsquare	0.406662							
Root Mean Square Error	1.03338							
Mean of Response	50.54096							
Observations (or Sum Wgts)	12							
Analysis of Variance								
Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F			
Set/Block/Sub-Block	3	11.056314	3.68544	3.4512	0.0716			
Error	8	8.542995						
C. Total	11	19.599309						
Means for Oneway Anova								
Level Number	Mean	Std Error	Lower 95%	Upper 95%				
1/1/1	51.5							
1/1/2	51.5							
1/2/1	51.5							
1/2/2	51.5							
Summary of Fit								
Rsquare	0.564118							
Adj Rsquare	0.406662							
Root Mean Square Error	1.03338							
Mean of Response	50.54096							
Observations (or Sum Wgts)	12							

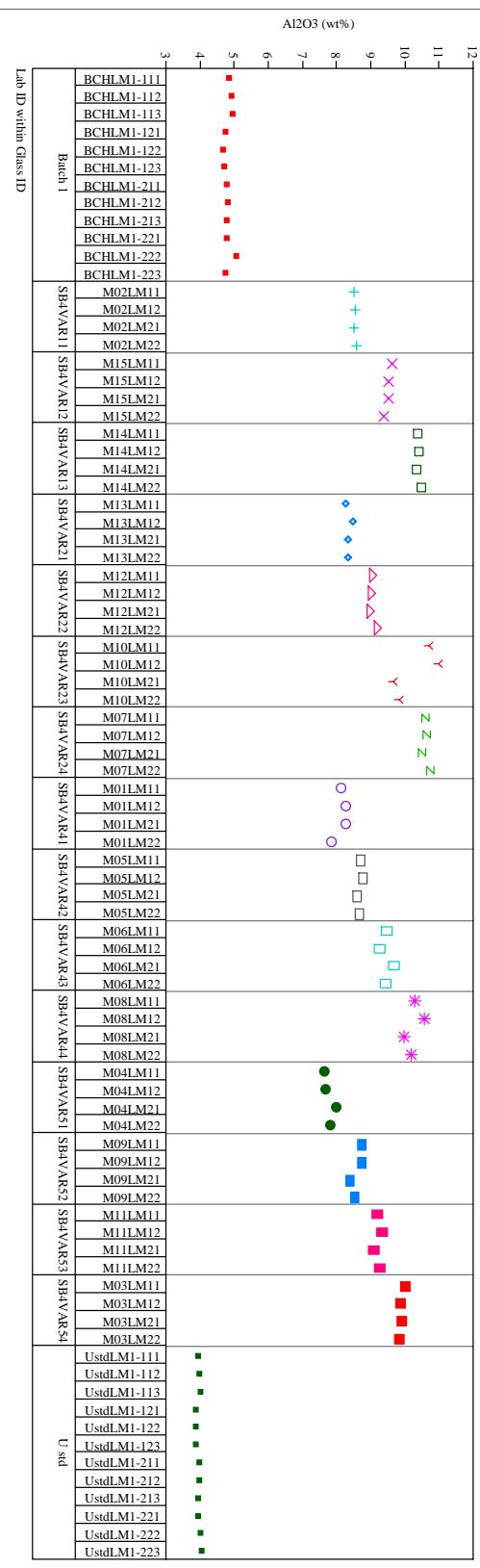
Std Error uses a pooled estimate of error variance

## Exhibit A4: PSAL Measurements by Analytical Block for Samples of the Standard Glasses Prepared Using the PF Method

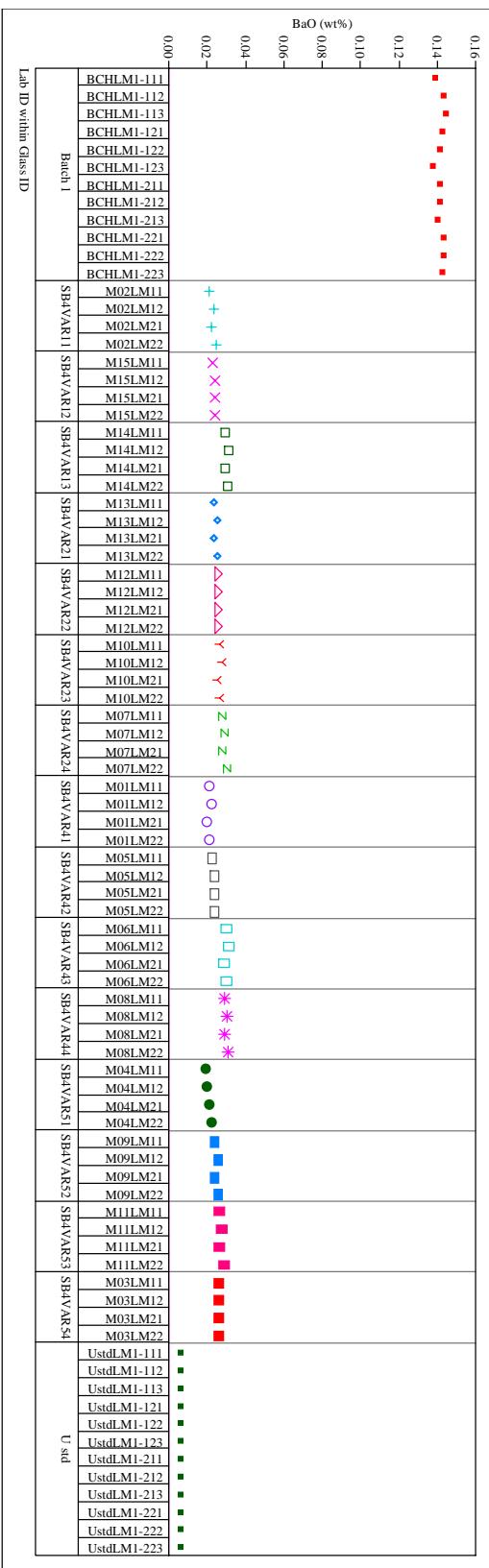


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

Set=1  
Variability Chart for Al<sub>2</sub>O<sub>3</sub> (wt%)

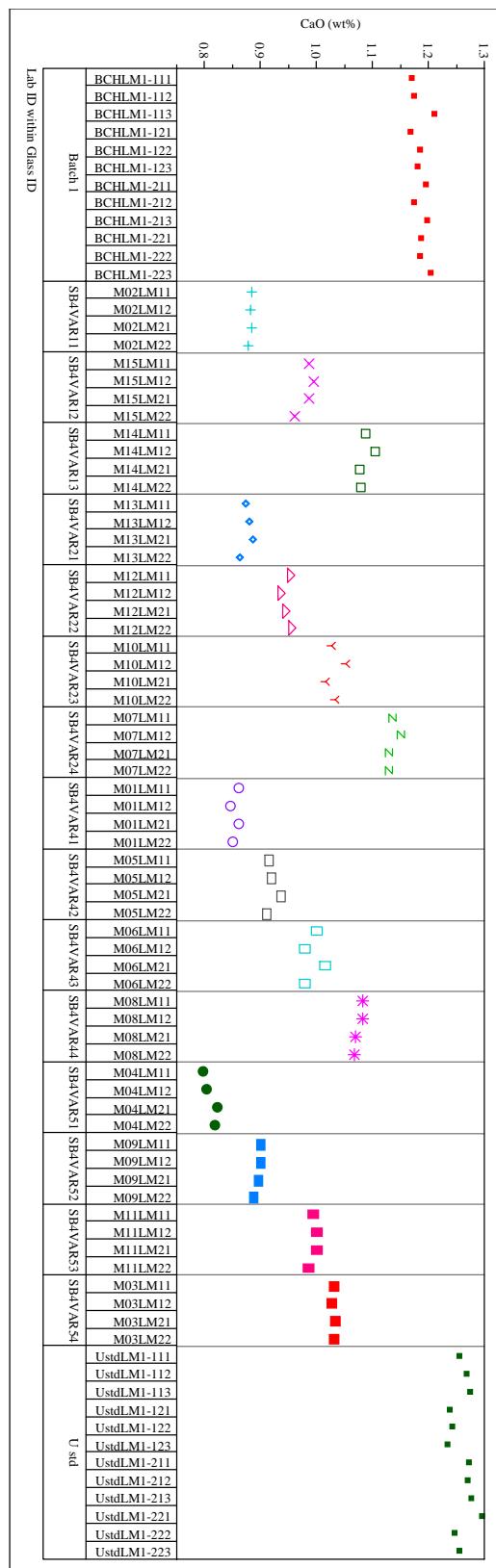


Set=1  
Variability Chart for BaO (wt%)

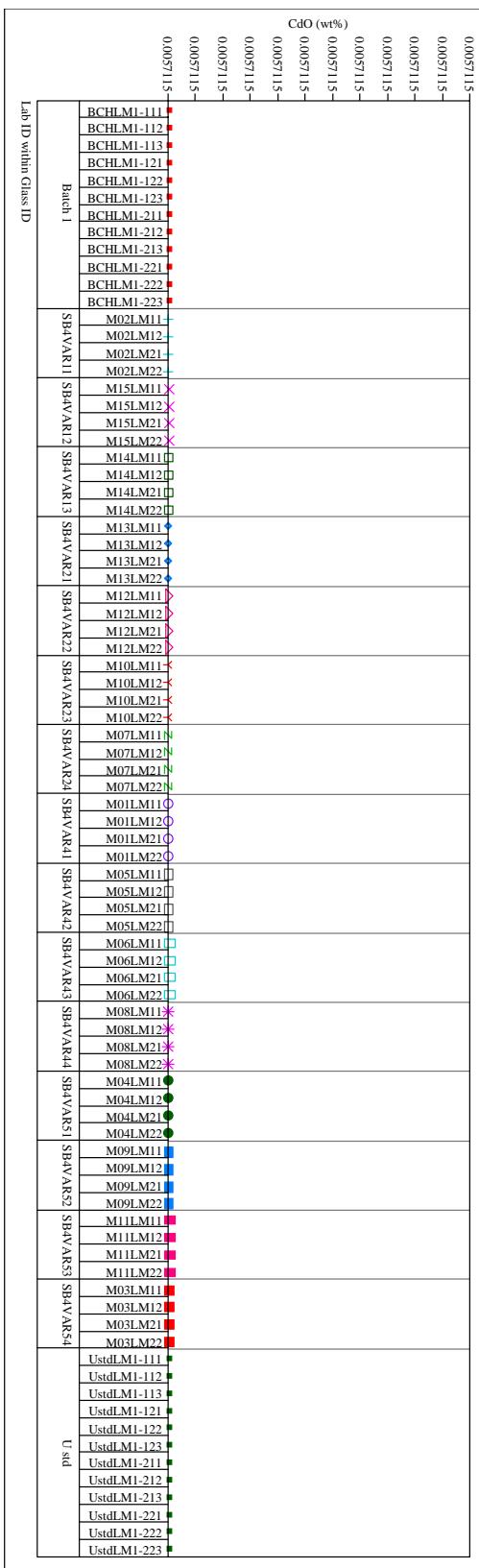


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for CaO (wt%)

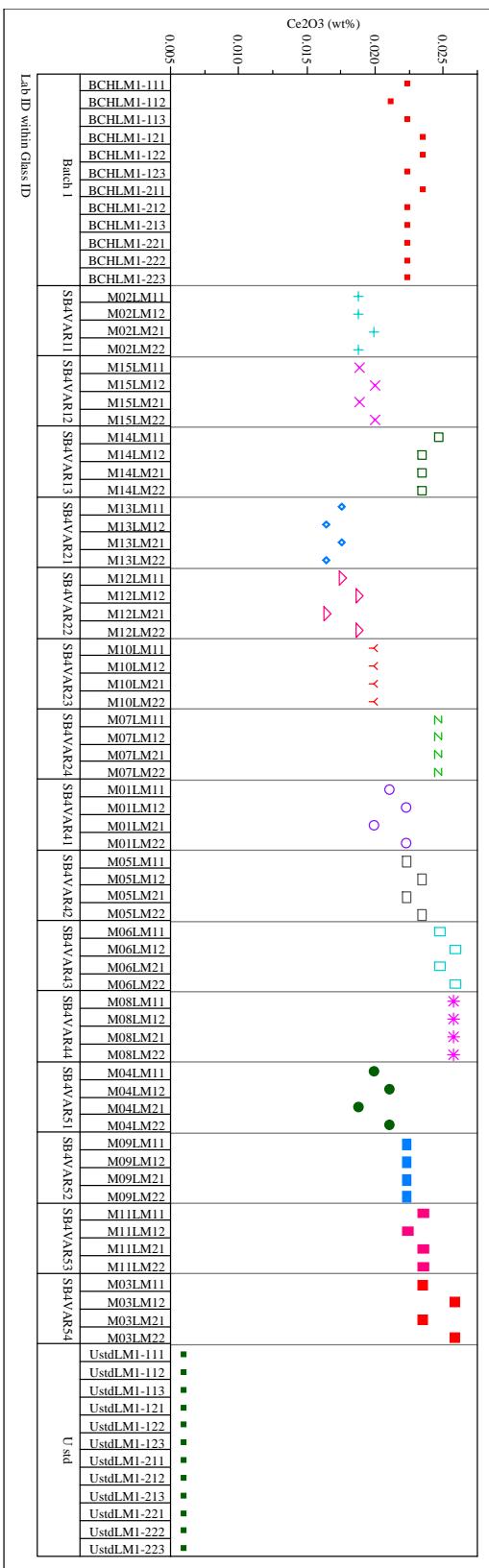


**Set=1**  
Variability Chart for CdO (wt%)

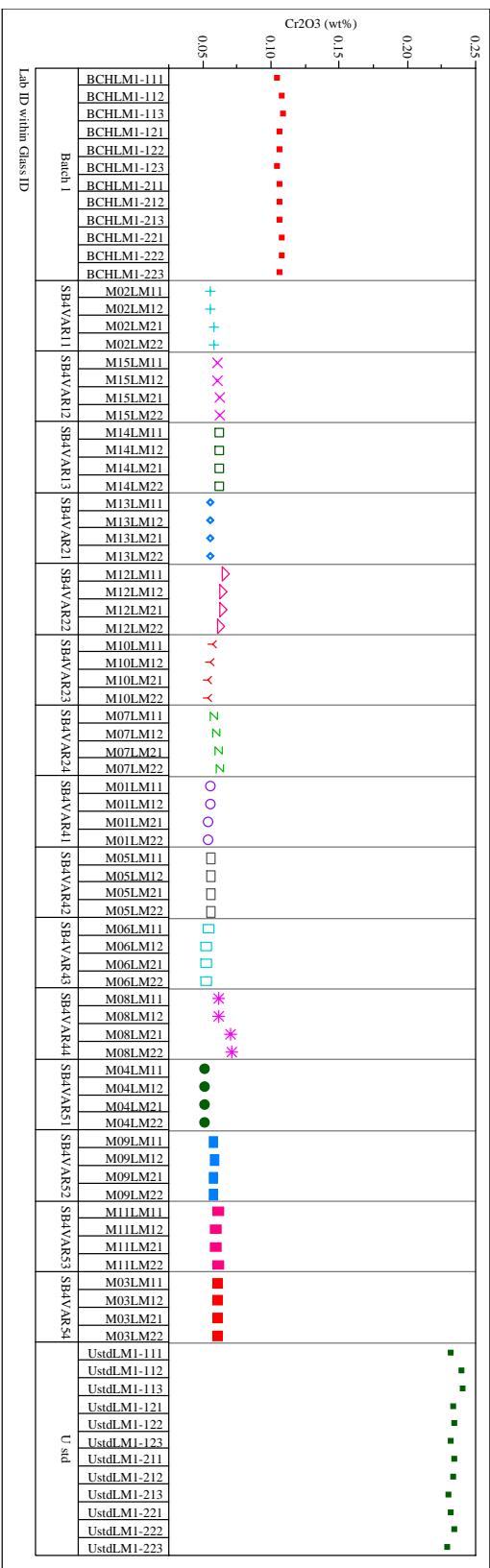


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for Ce<sub>2</sub>O<sub>3</sub> (wt%)

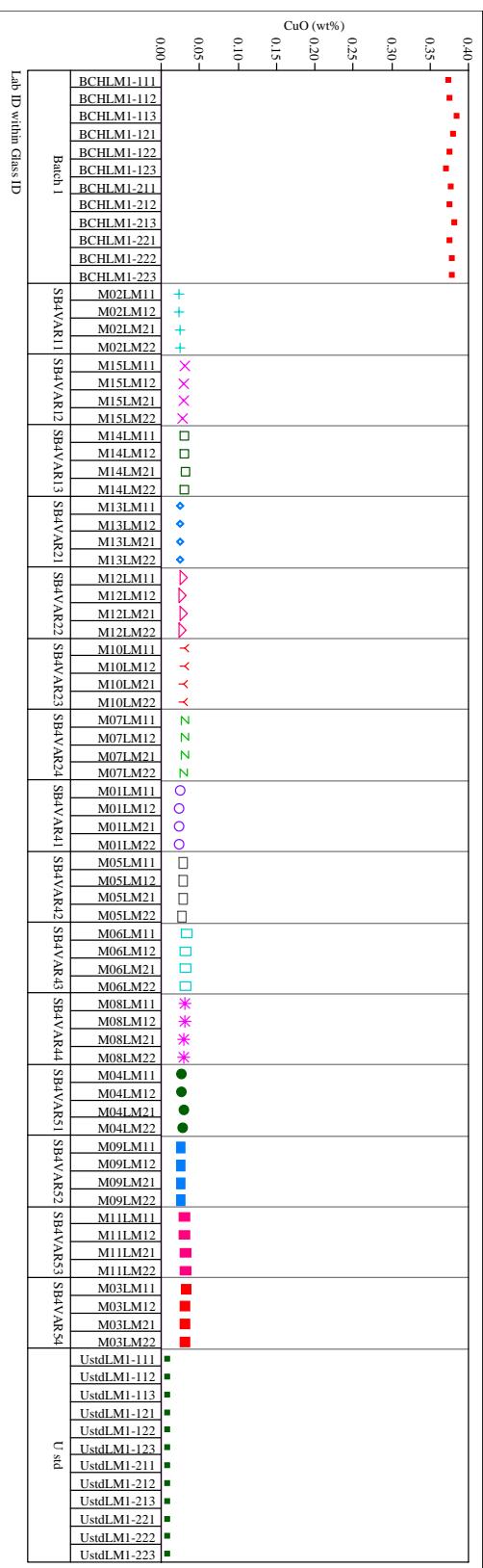


**Set=1**  
Variability Chart for Cr<sub>2</sub>O<sub>3</sub> (wt%)

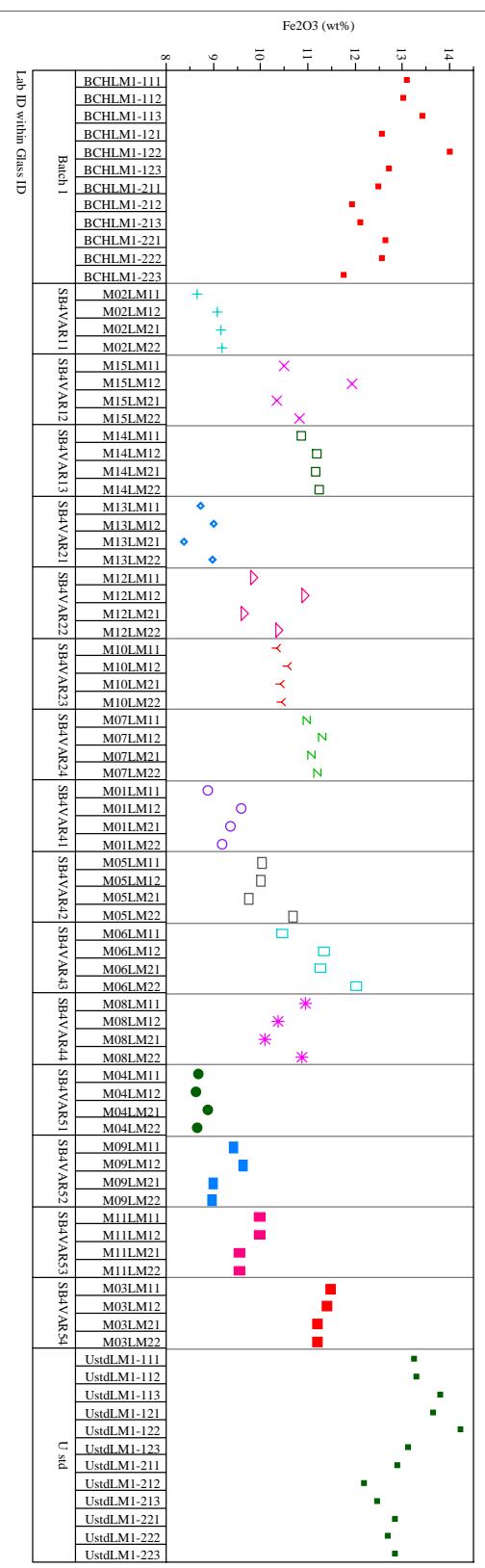


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
**Variability Chart for CuO (wt%)**



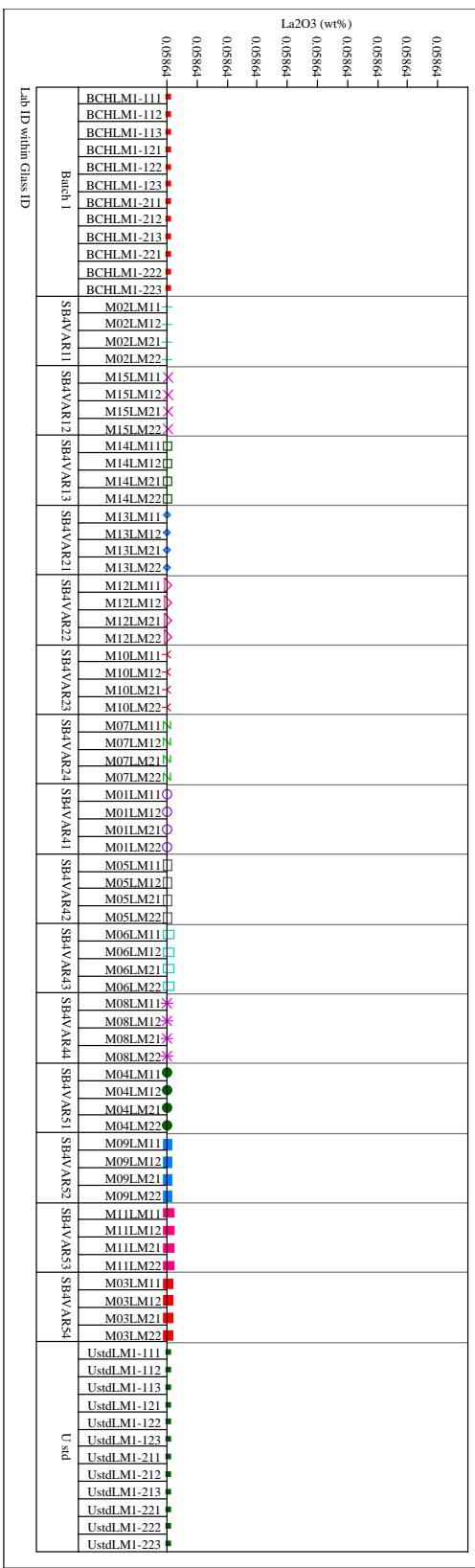
**Set=1**  
**Variability Chart for Fe2O3 (wt%)**



## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

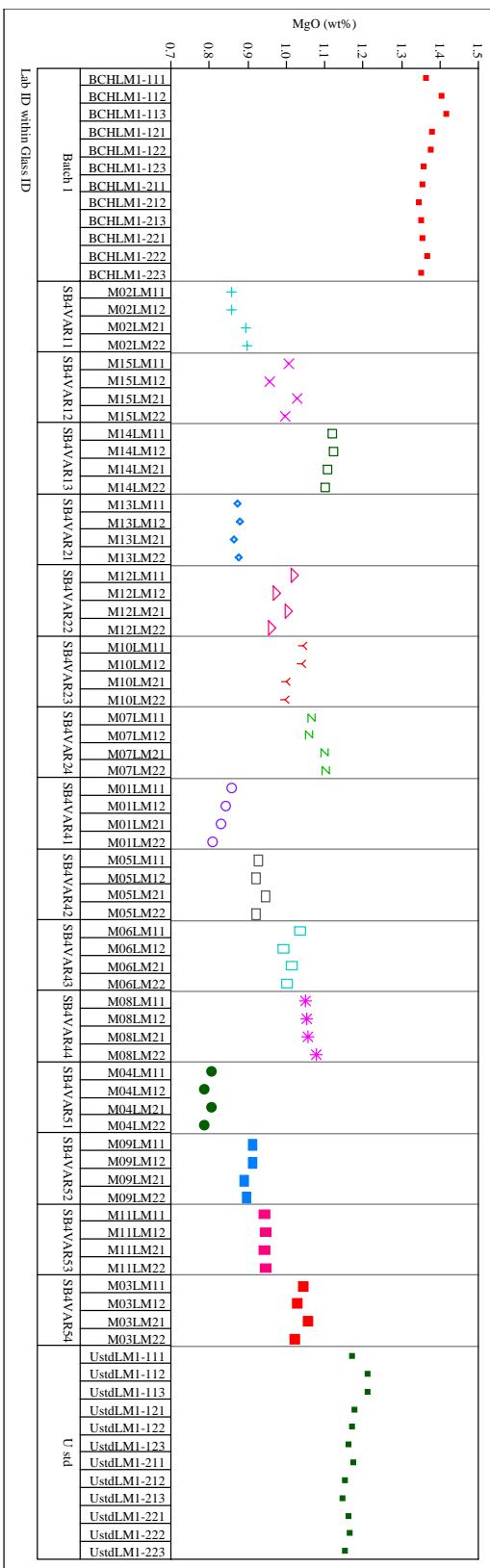


**Set=1**  
Variability Chart for La2O3 (wt%)

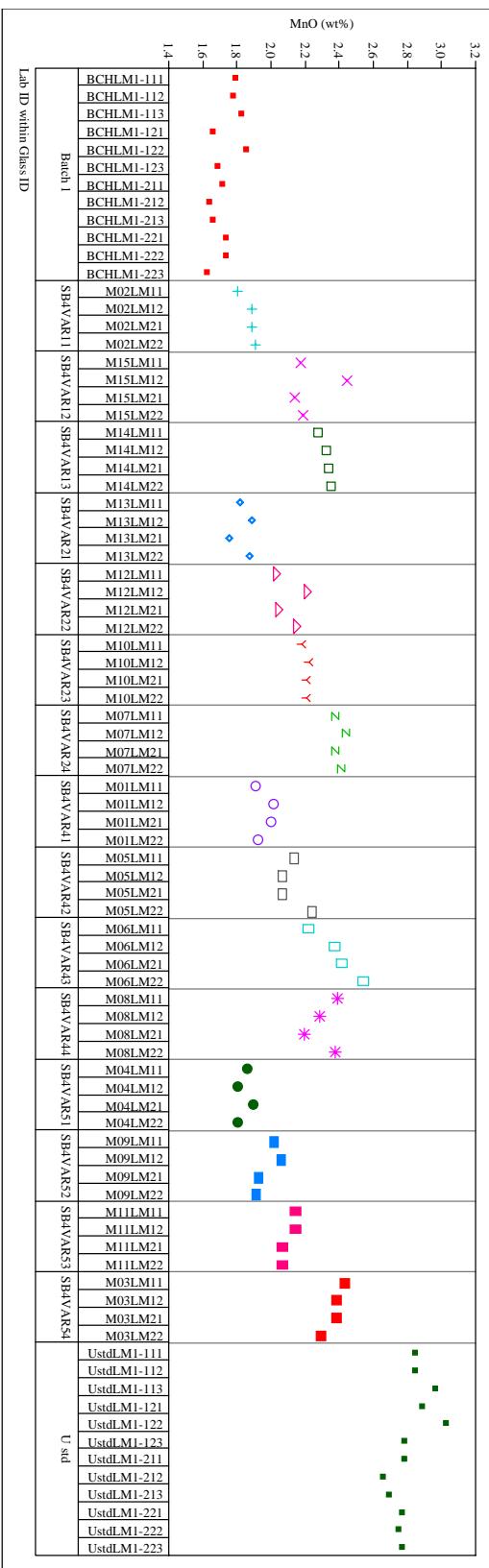


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for MgO (wt%)



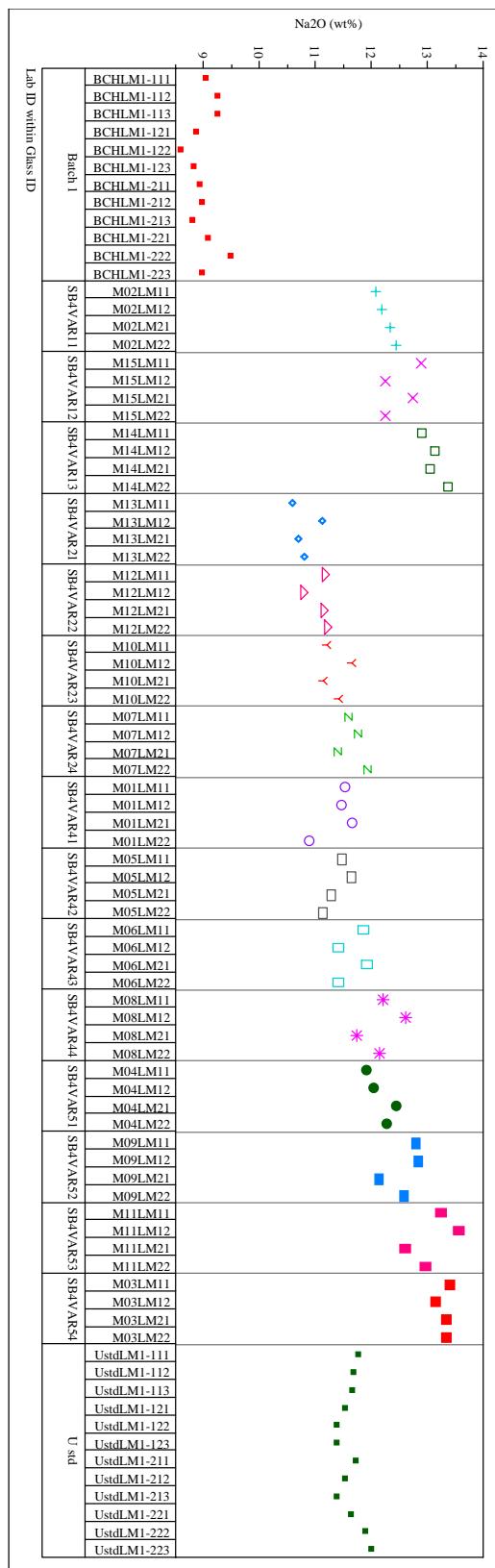
**Set=1**  
Variability Chart for MnO (wt%)



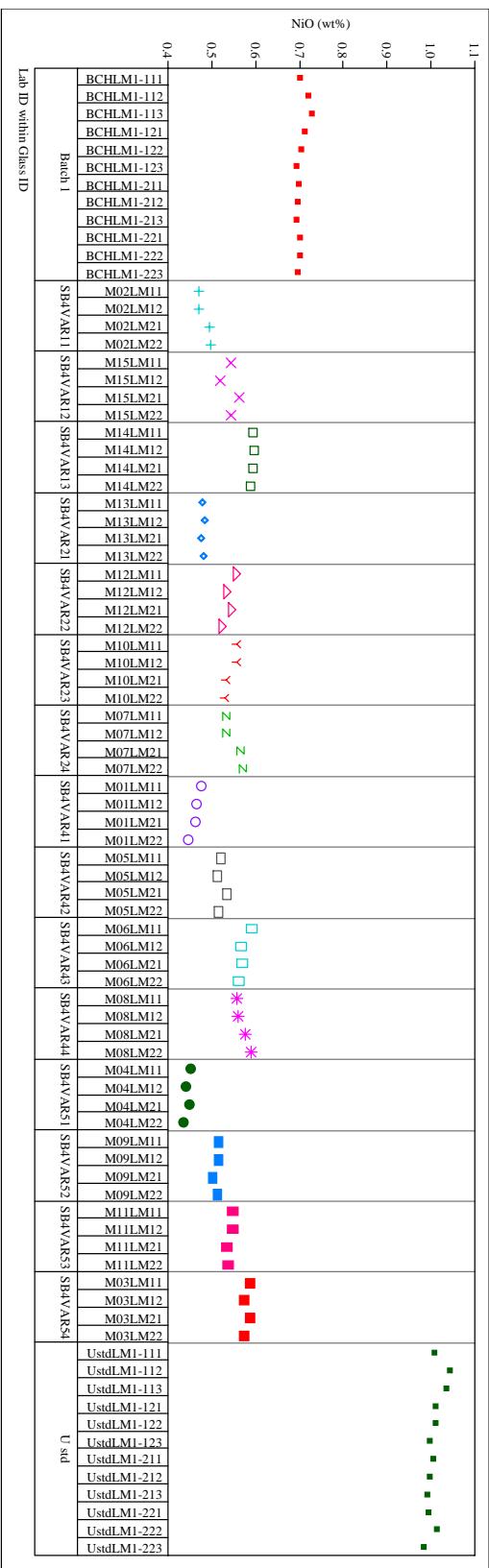
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for Na<sub>2</sub>O (wt%)



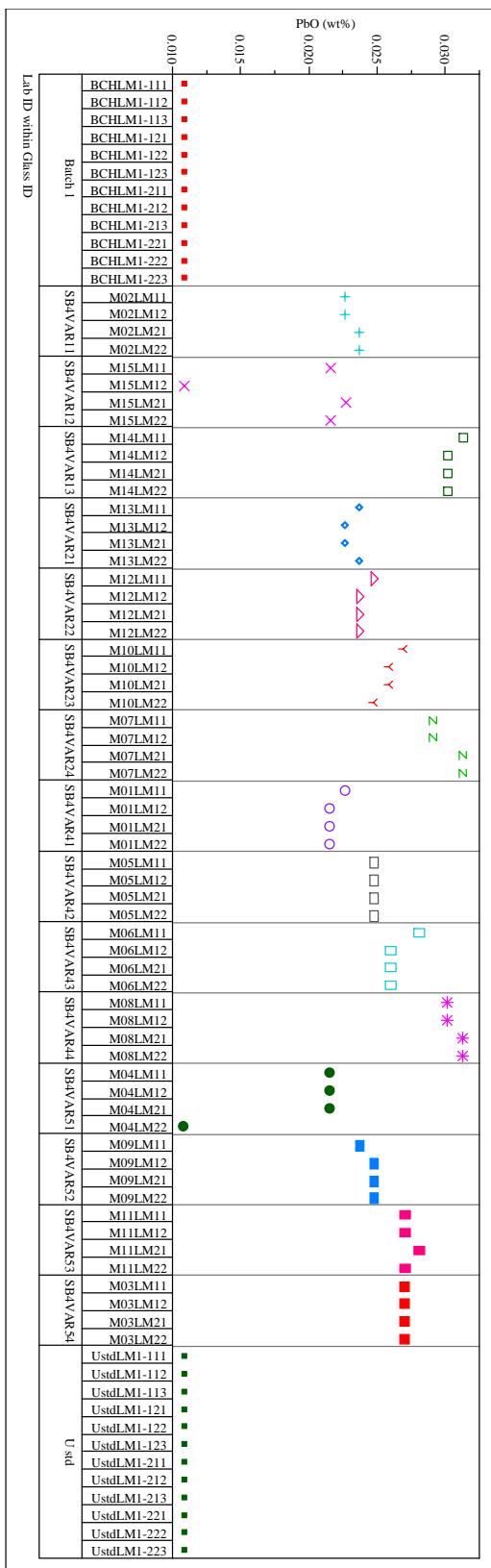
**Set=1**  
Variability Chart for NiO (wt%)



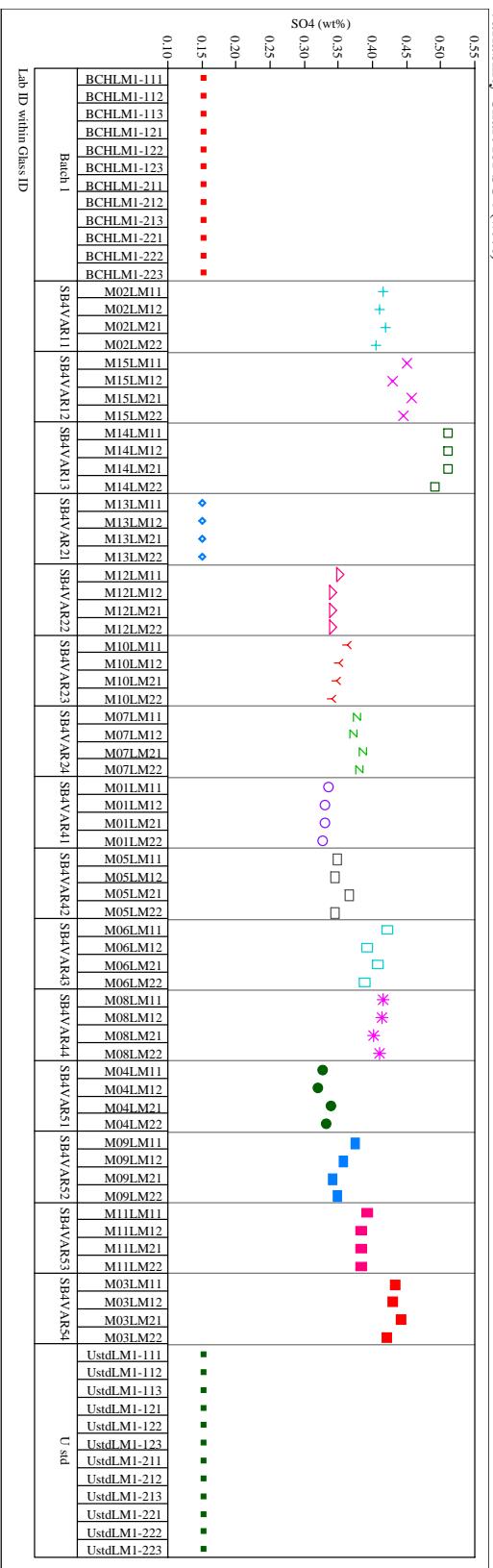
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for PbO (wt%)

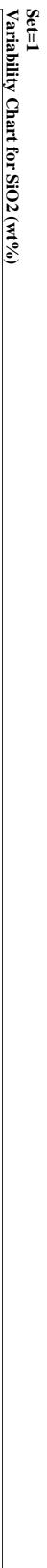


**Set=1**  
Variability Chart for SO4 (wt%)

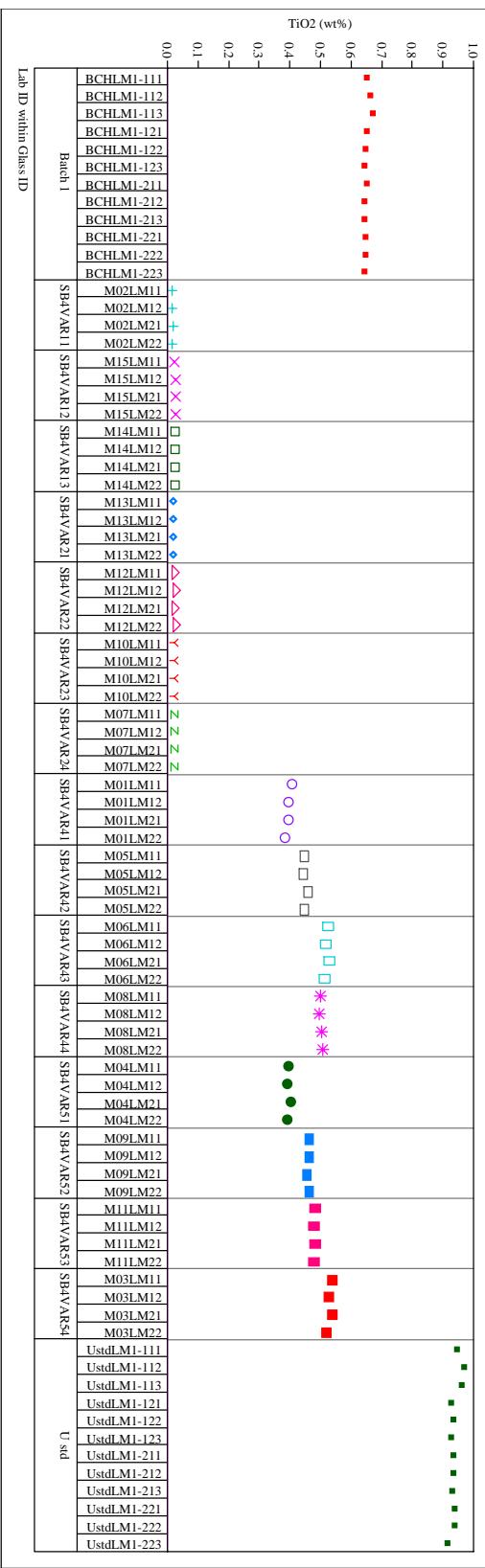


Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method



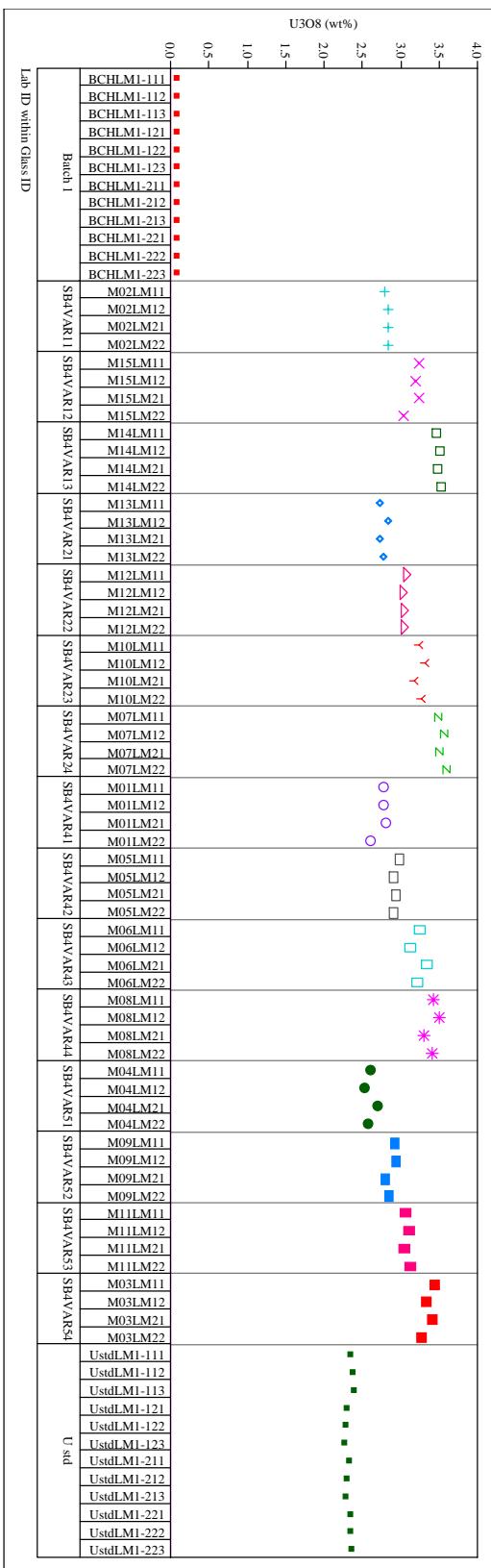
**Set=1**  
**Variability Chart for TiO<sub>2</sub> (wt%)**



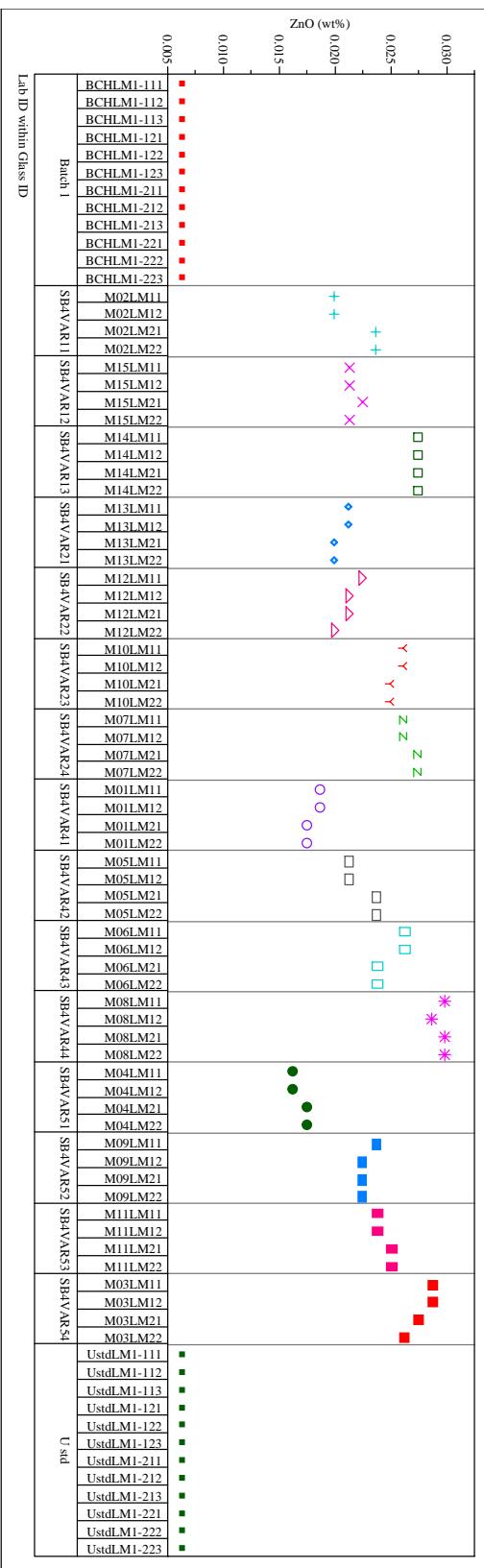
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for U3O8 (wt%)



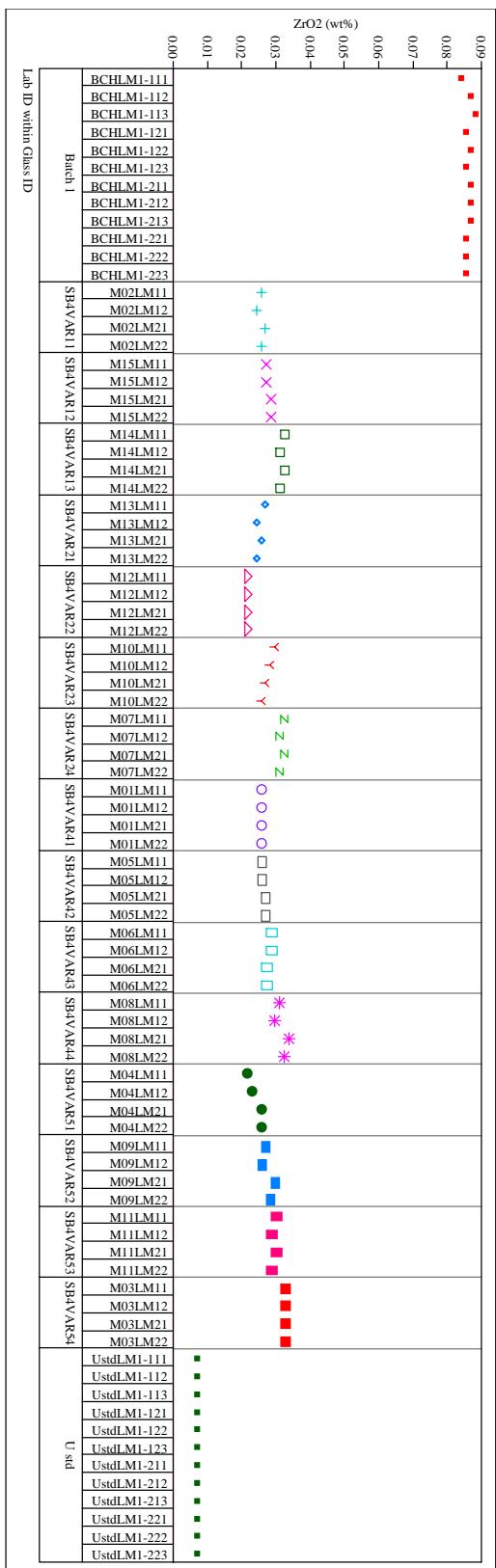
**Set=1**  
Variability Chart for ZnO (wt%)



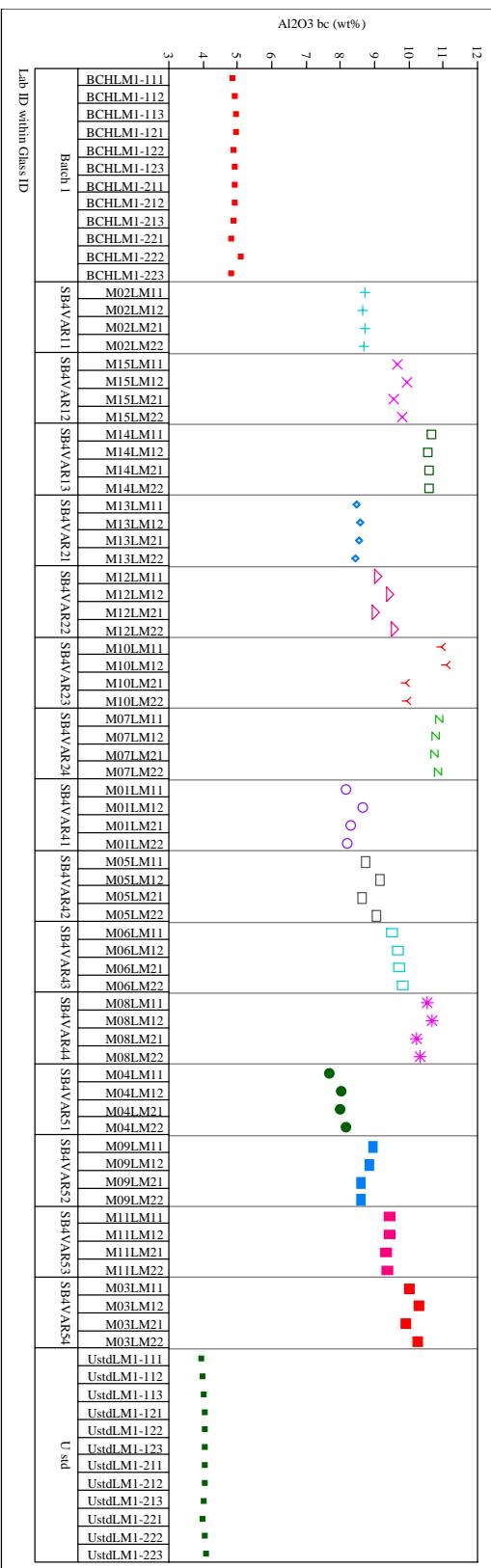
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for ZrO<sub>2</sub> (wt%)

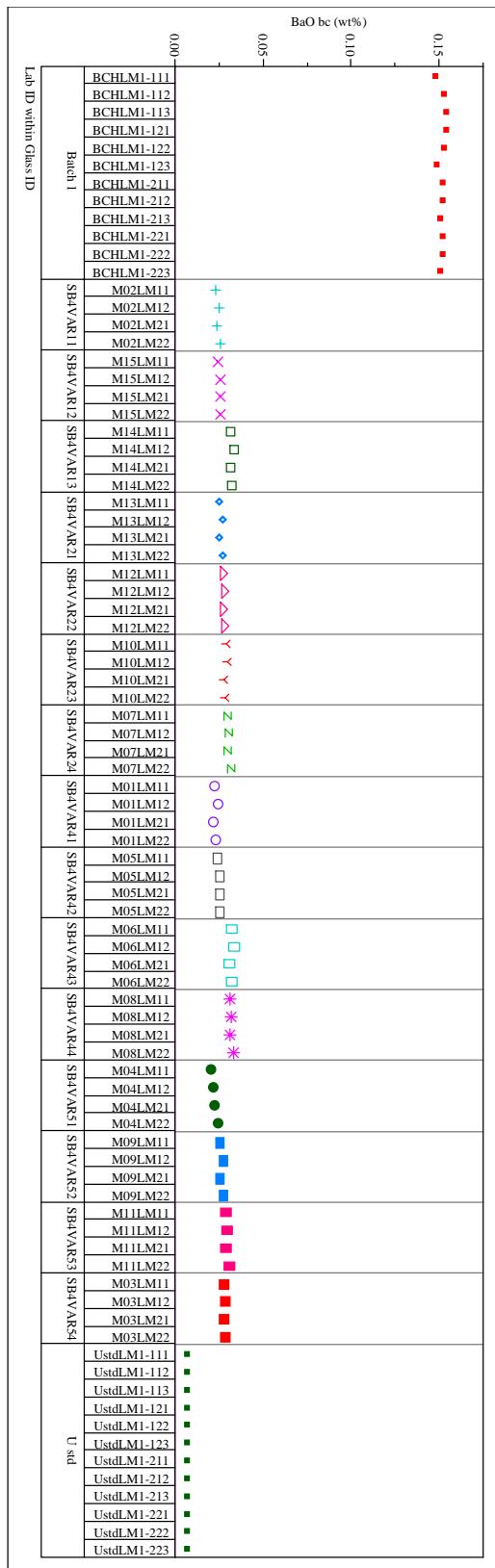


**Set=1**  
Variability Chart for Al<sub>2</sub>O<sub>3</sub> bc (wt%)

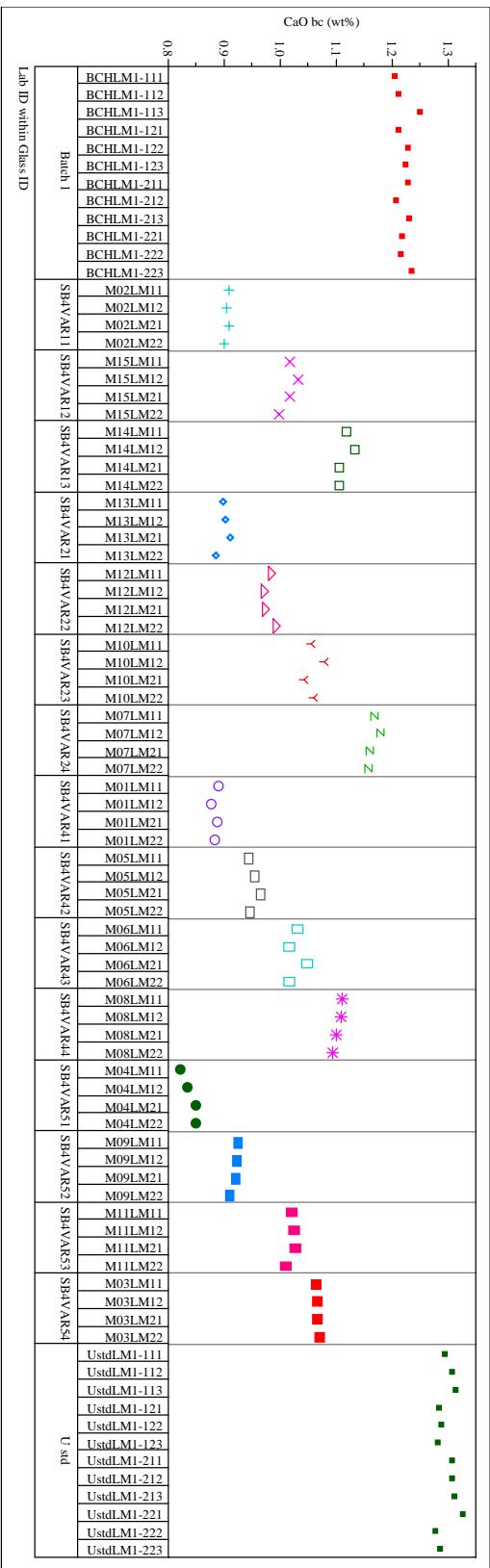


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for BaO bc (wt%)



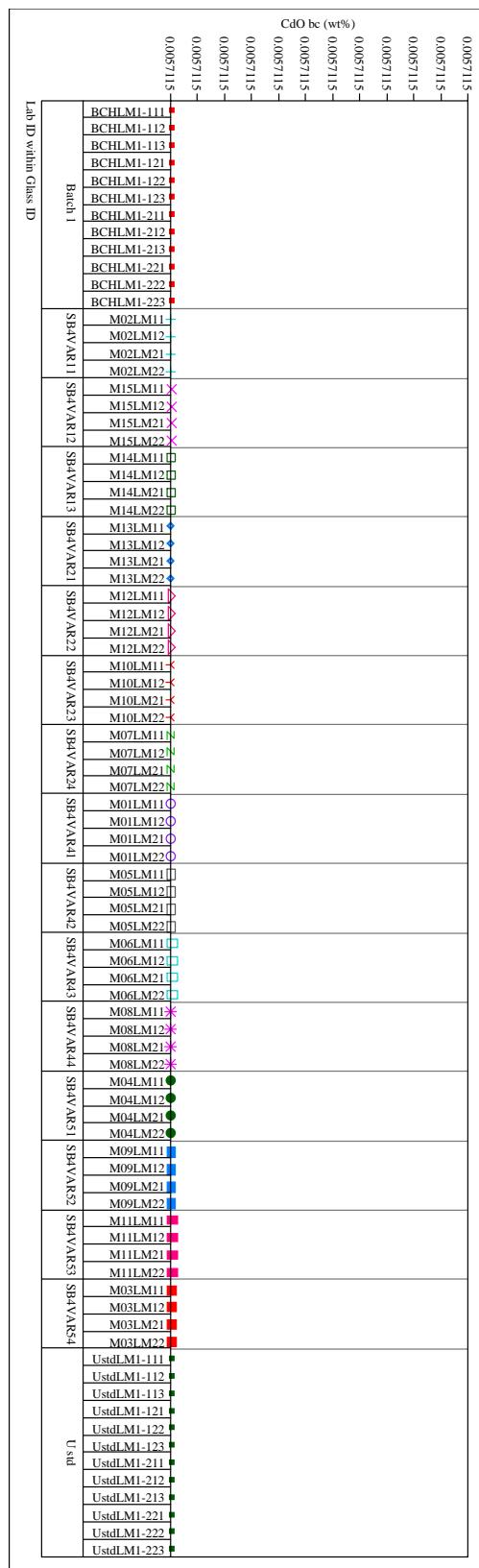
**Set=1**  
Variability Chart for CaO bc (wt%)



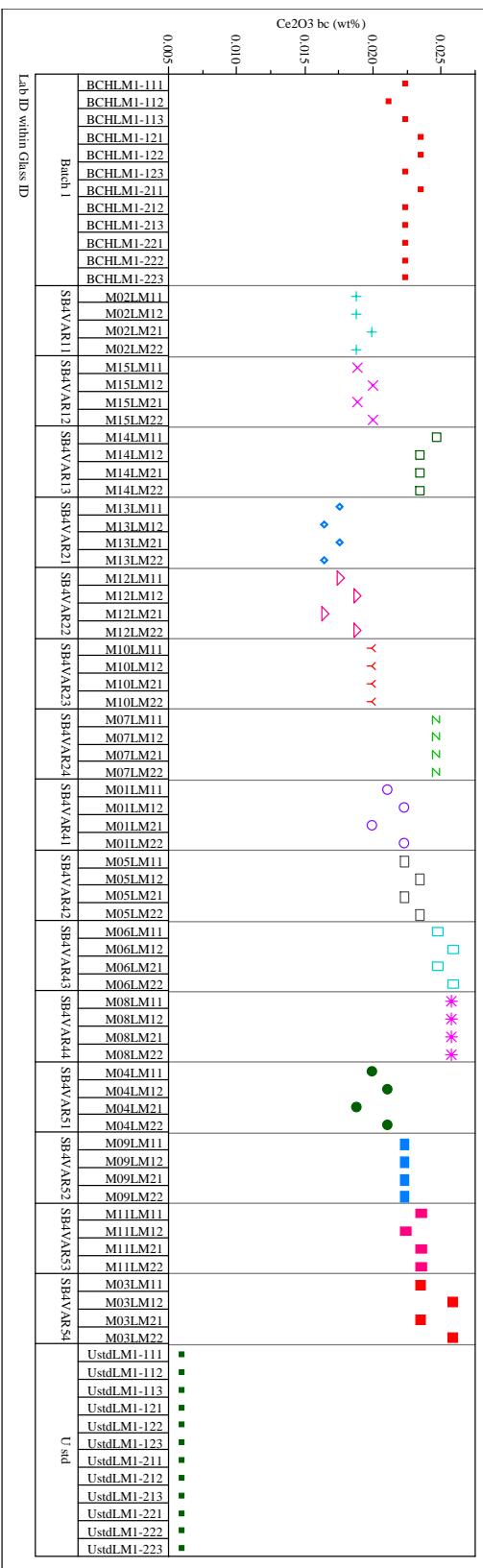
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
**Variability Chart for CdO bc (wt%)**

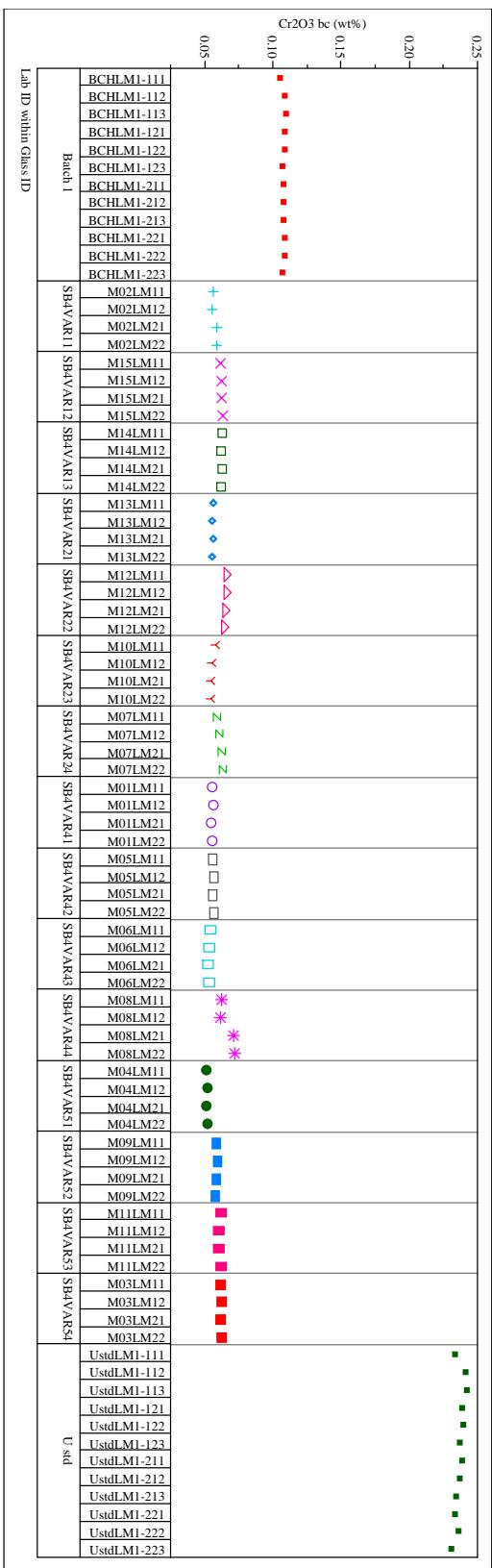


**Set=1**  
**Variability Chart for Ce2O3 bc (wt%)**

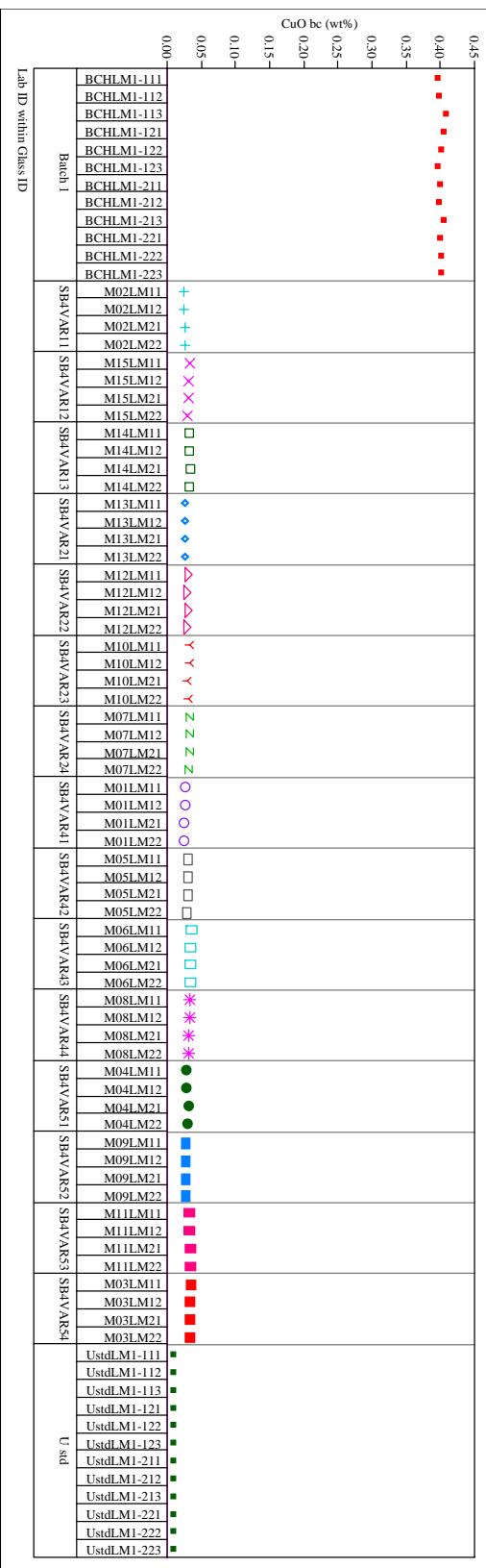


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
**Variability Chart for Cr<sub>2</sub>O<sub>3</sub> bc (wt%)**



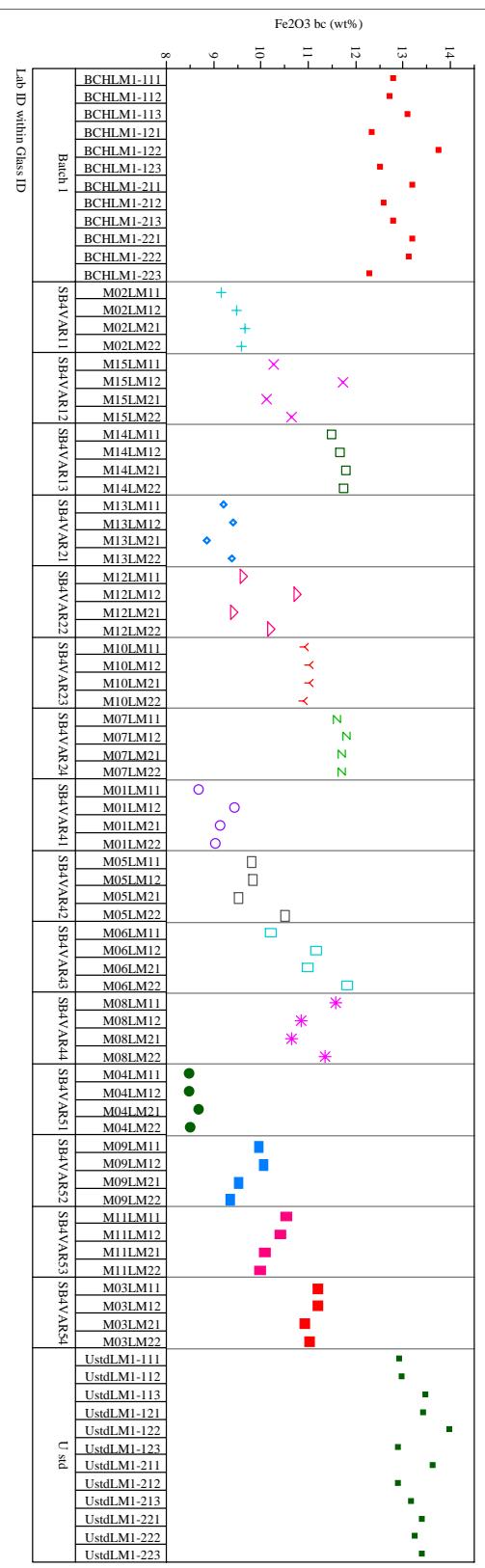
**Set=1**  
**Variability Chart for CuO bc (wt%)**



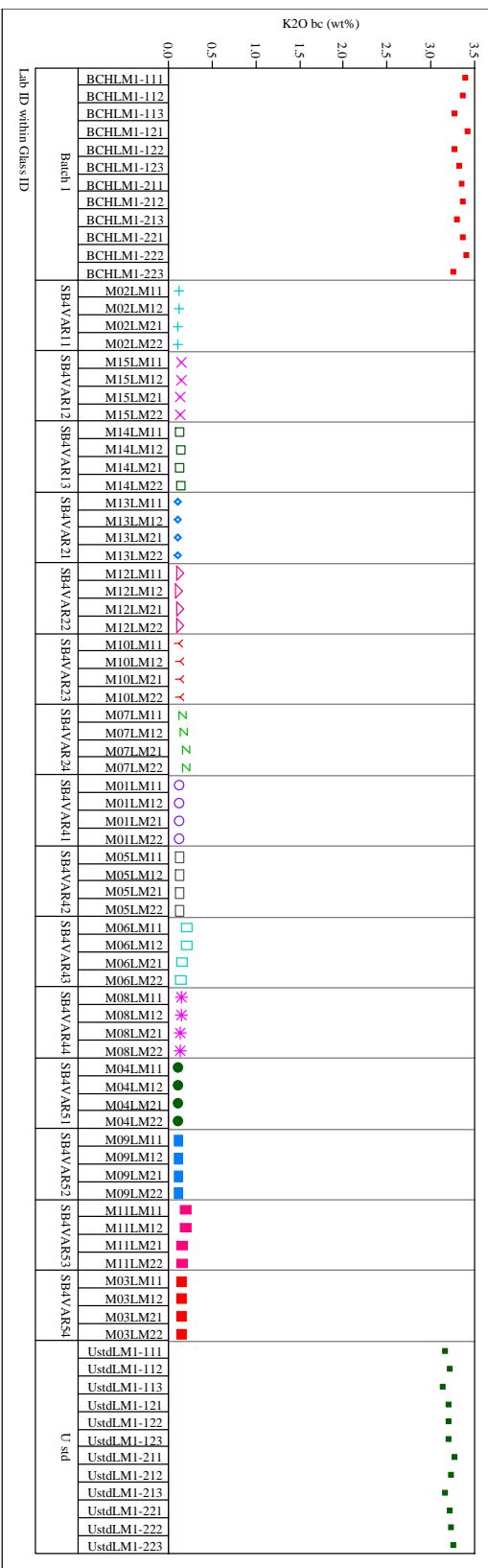
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for Fe<sub>2</sub>O<sub>3</sub> bc (wt%)



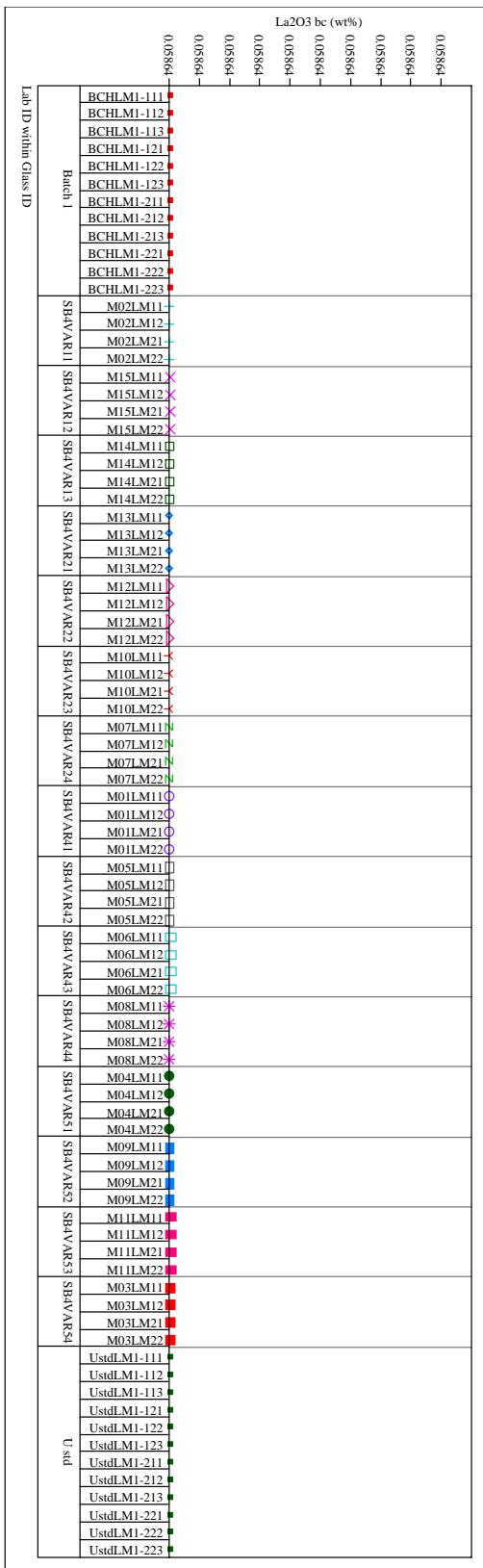
**Set=1**  
Variability Chart for K<sub>2</sub>O bc (wt%)



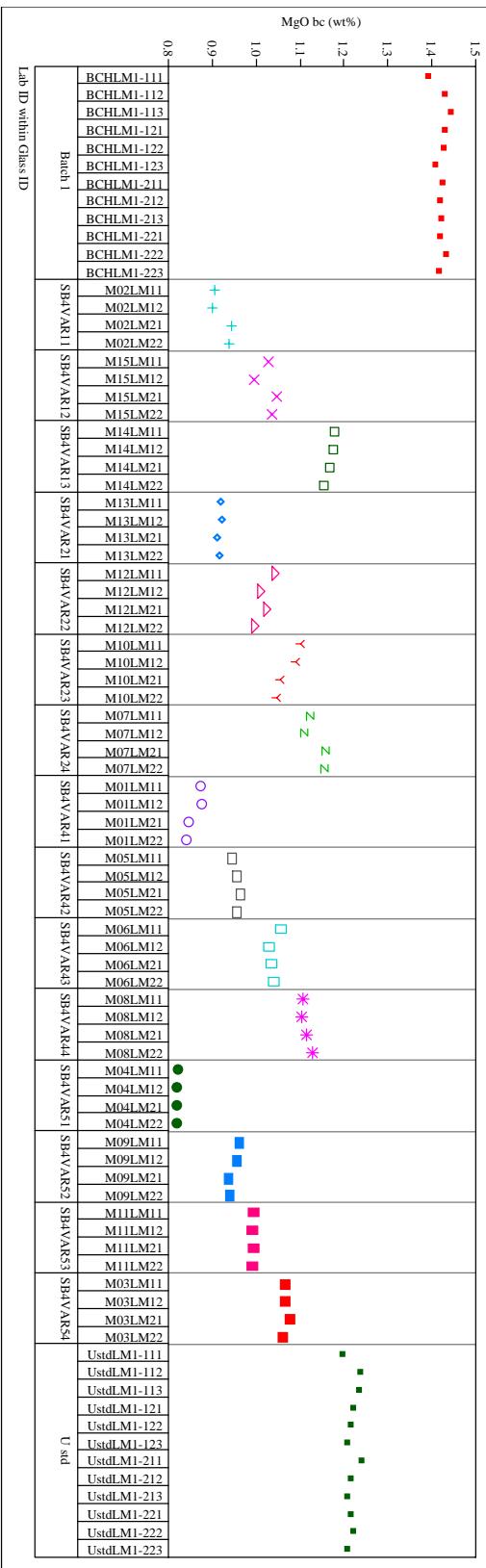
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
**Variability Chart for La<sub>2</sub>O<sub>3</sub> bc (wt%)**

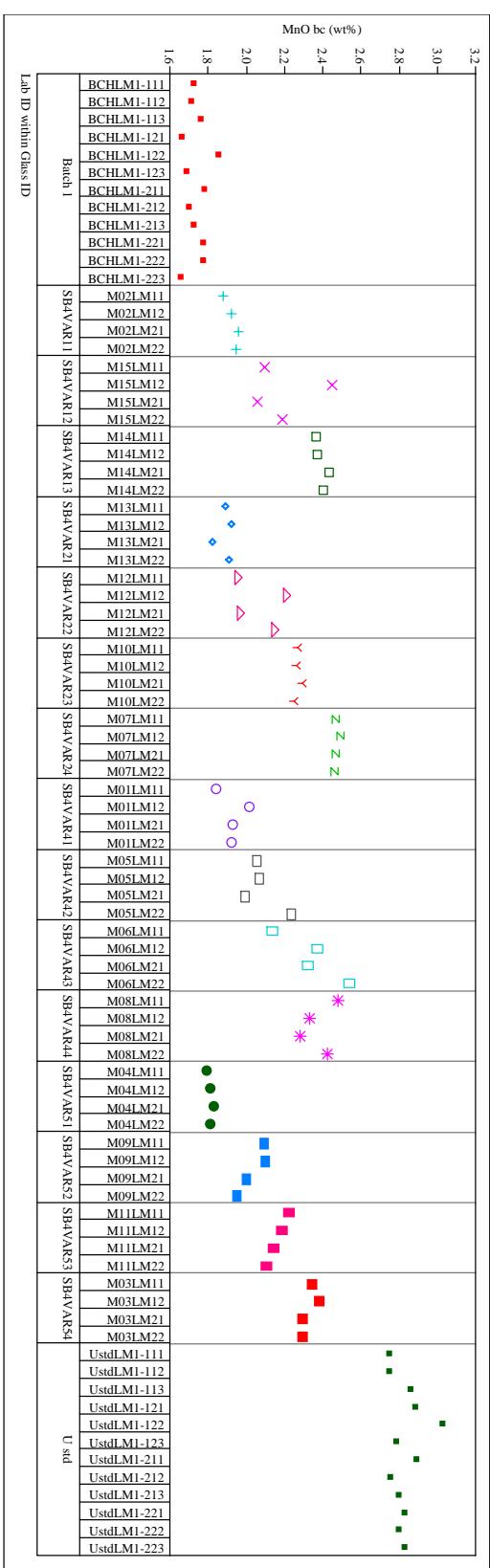


**Set=1**  
**Variability Chart for MgO bc (wt%)**

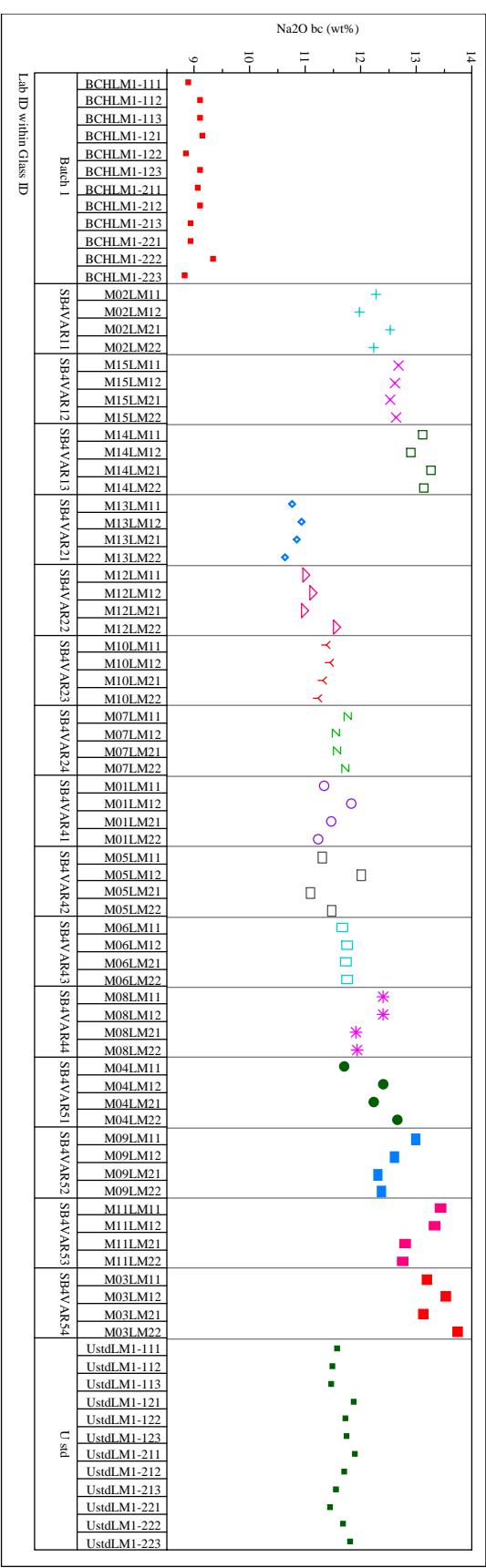


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for MnO bc (wt%)



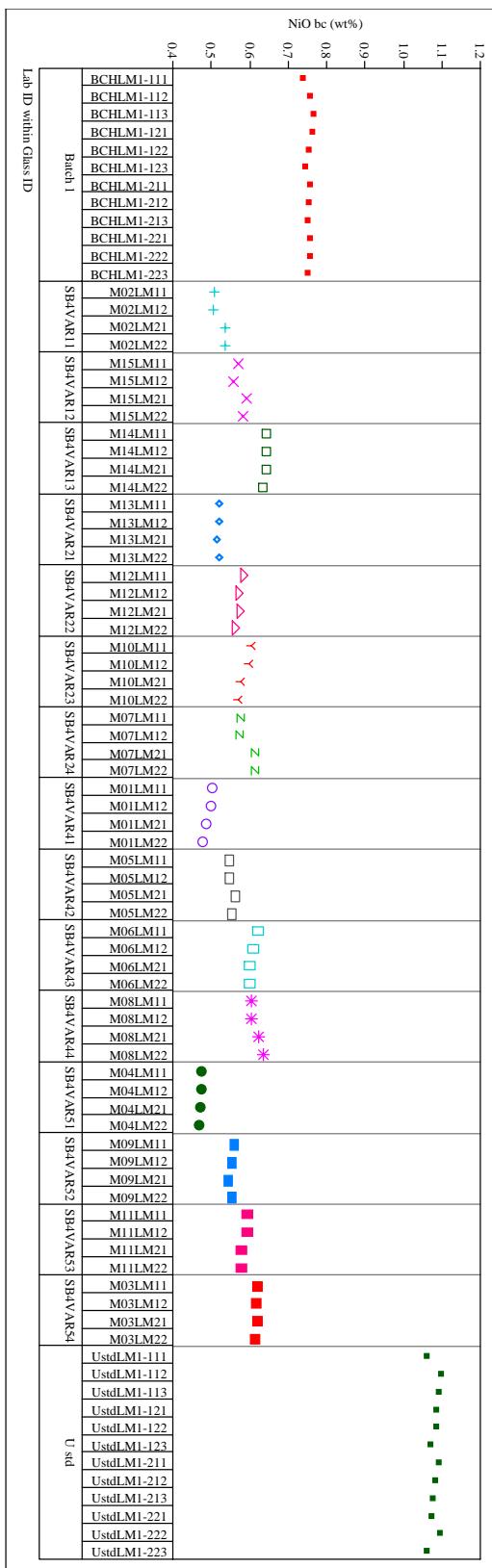
**Set=1**  
Variability Chart for Na<sub>2</sub>O bc (wt%)



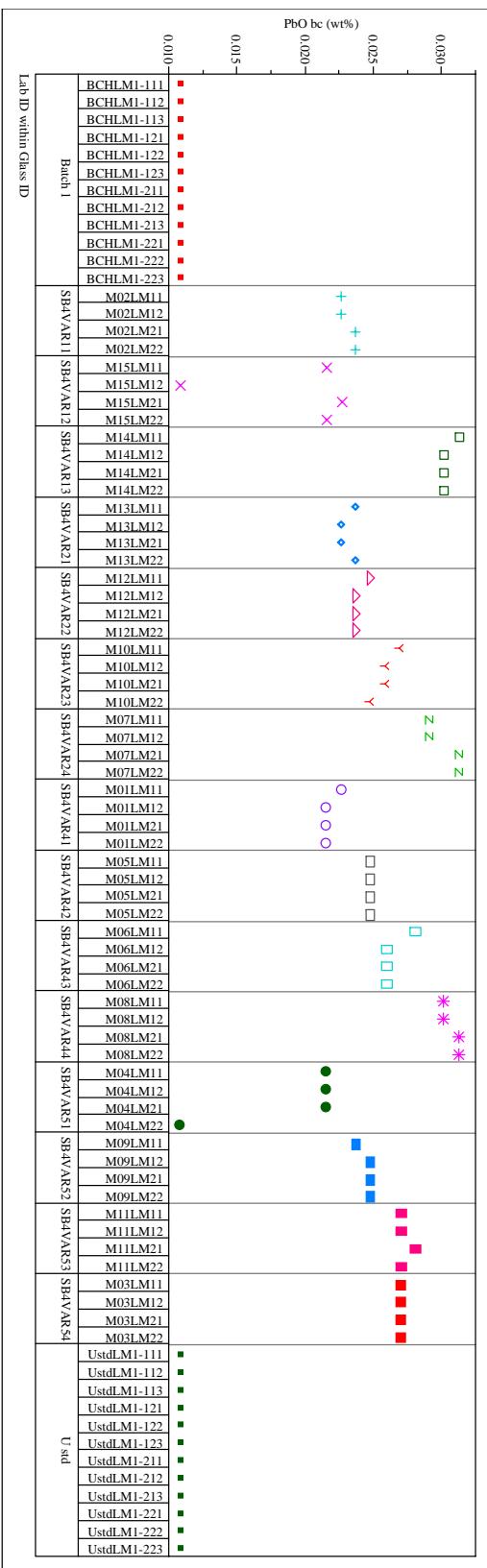
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for NiO bc (wt%)

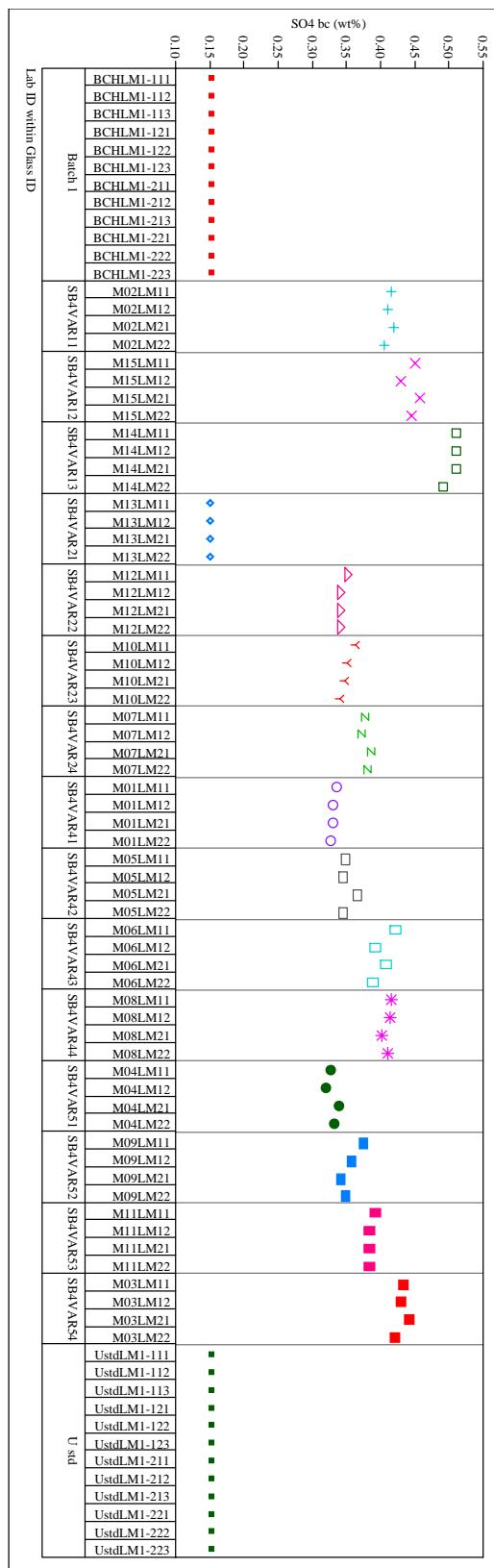


**Set=1**  
Variability Chart for PbO bc (wt%)

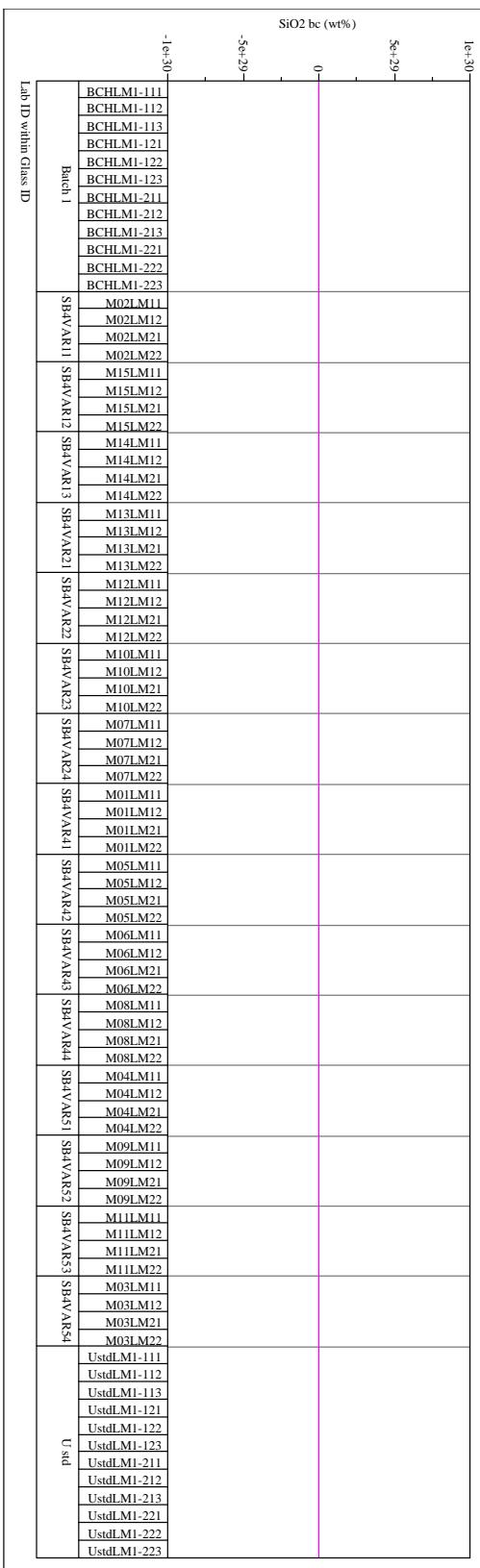


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
**Variability Chart for SO<sub>4</sub> bc (wt%)**

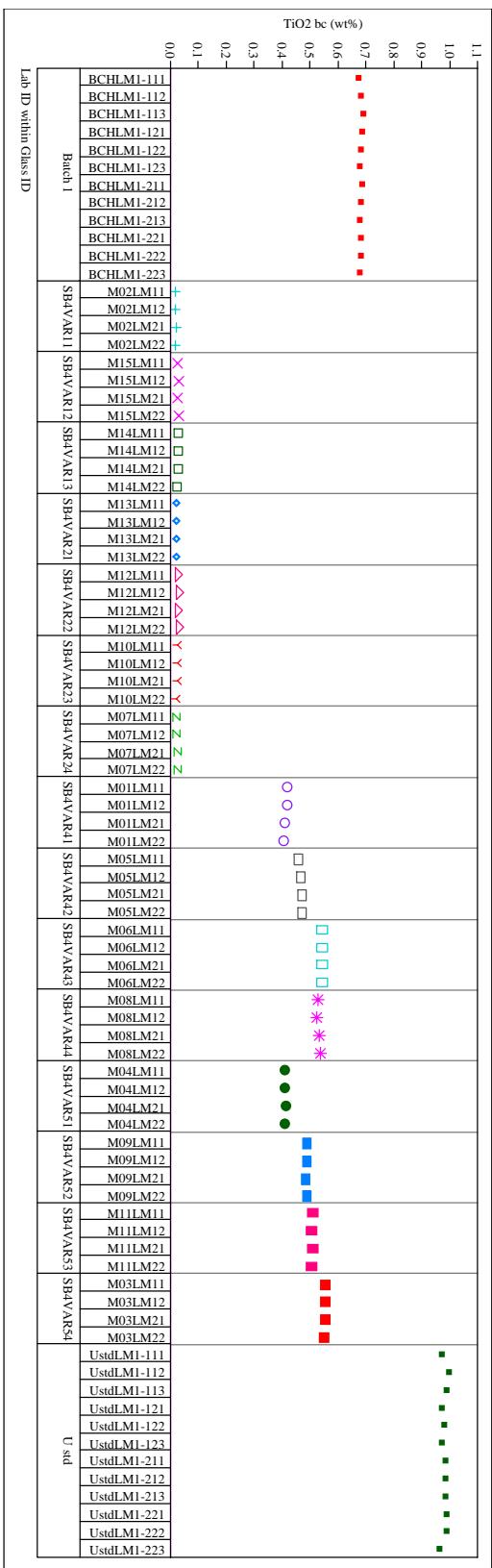


**Set=1**  
**Variability Chart for SiO<sub>2</sub> bc (wt%)**

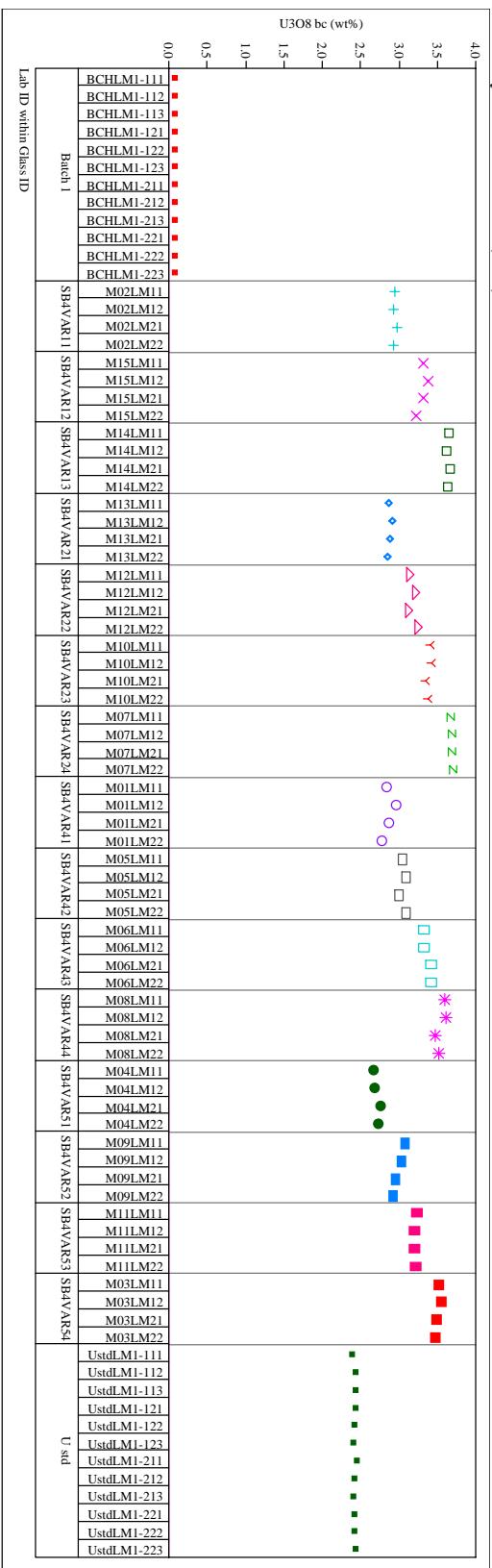


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for TiO<sub>2</sub> bc (wt%)

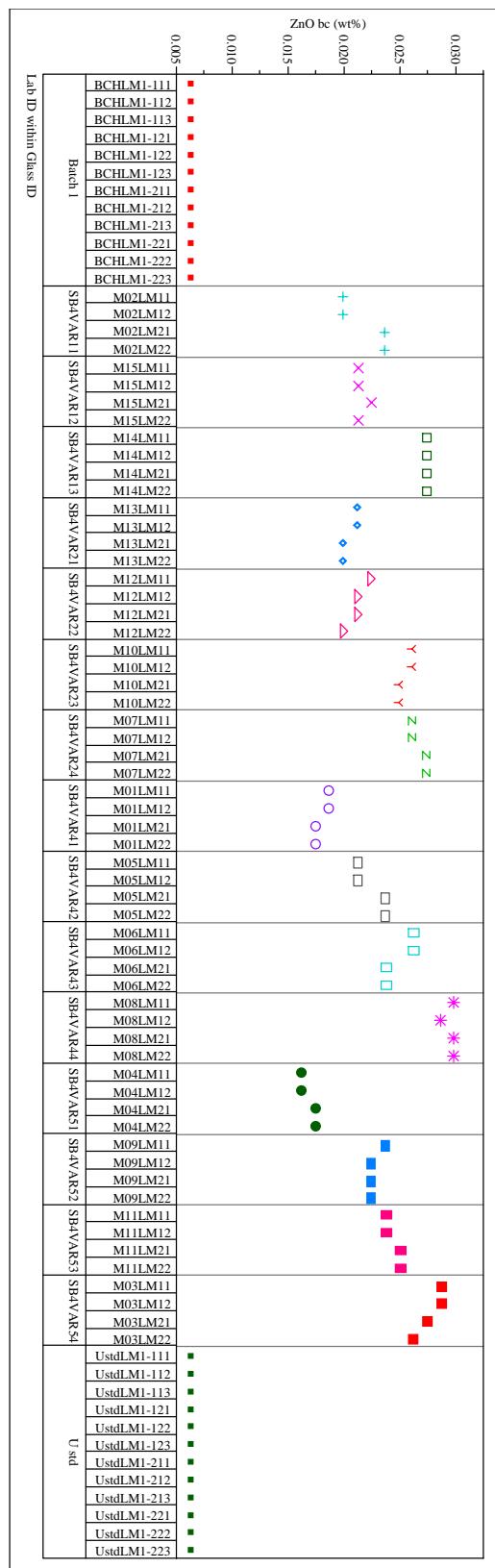


**Set=1**  
Variability Chart for U3O8 bc (wt%)

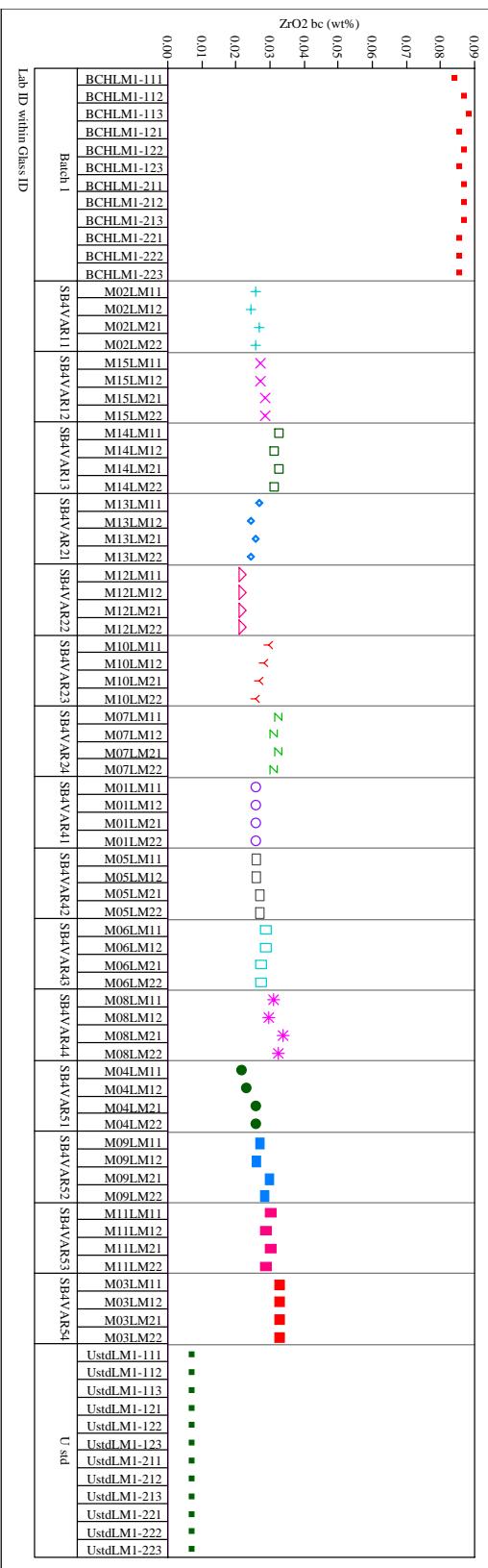


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=1**  
Variability Chart for ZnO bc (wt%)



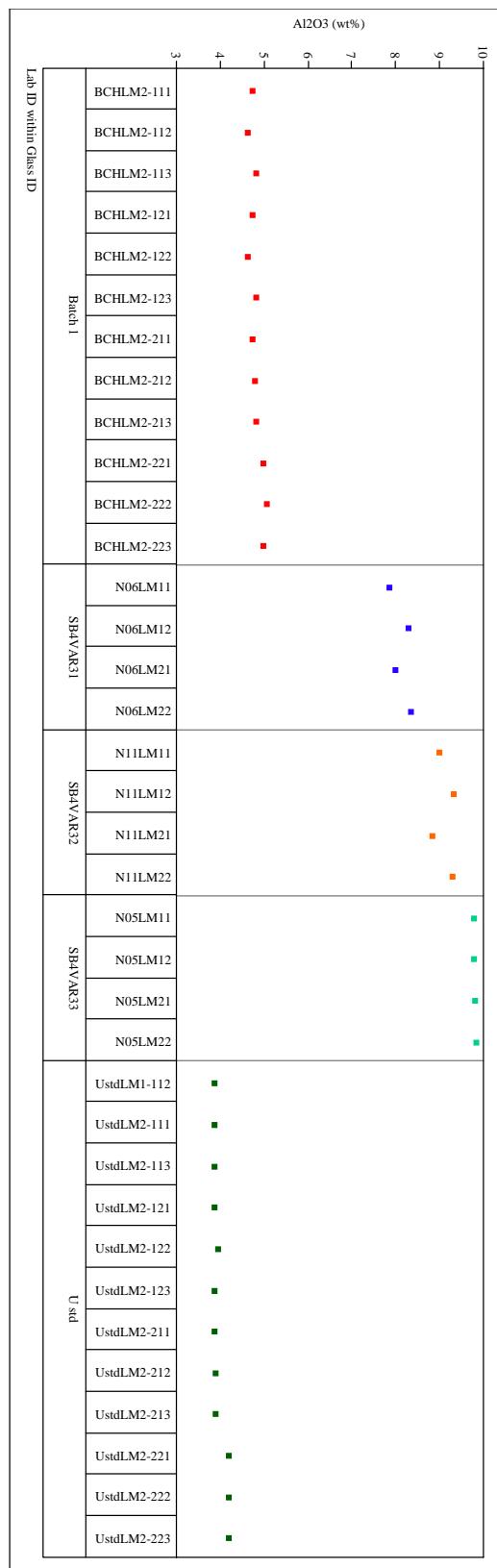
**Set=1**  
Variability Chart for ZrO2 bc (wt%)



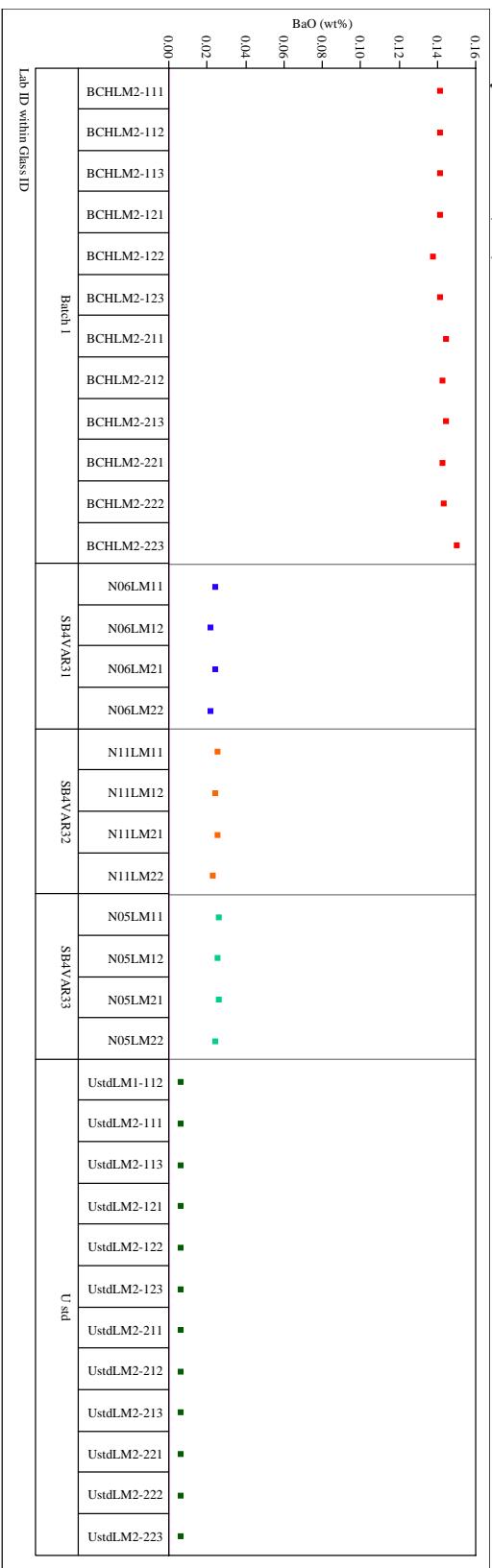
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for Al<sub>2</sub>O<sub>3</sub> (wt%)



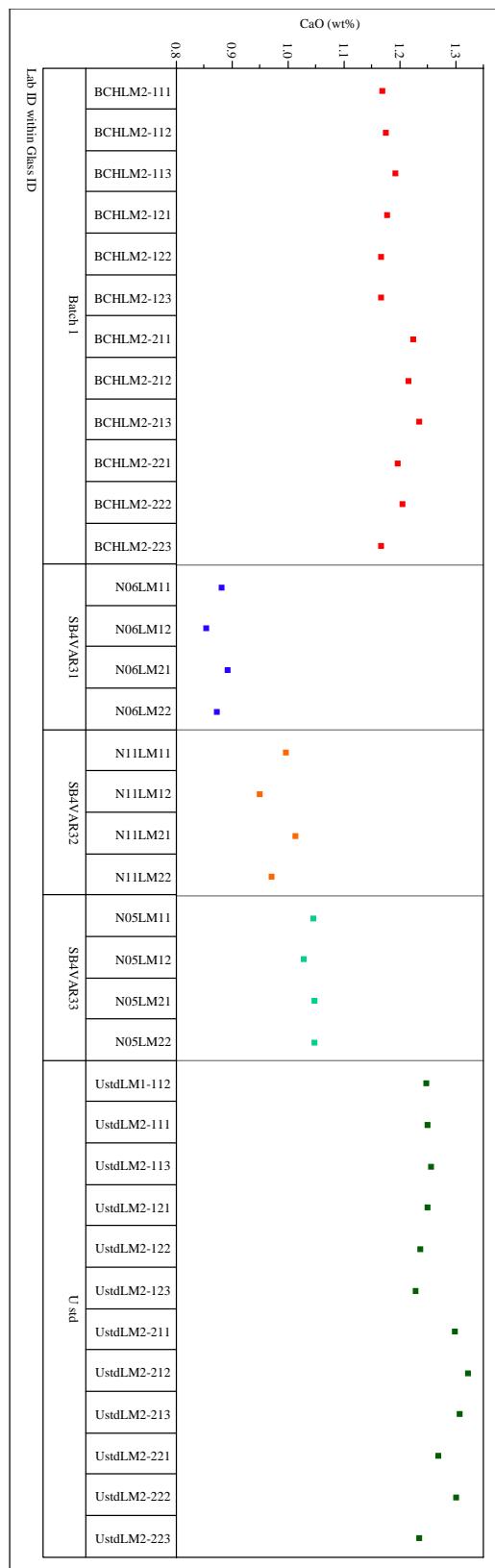
**Set=2**  
Variability Chart for BaO (wt%)



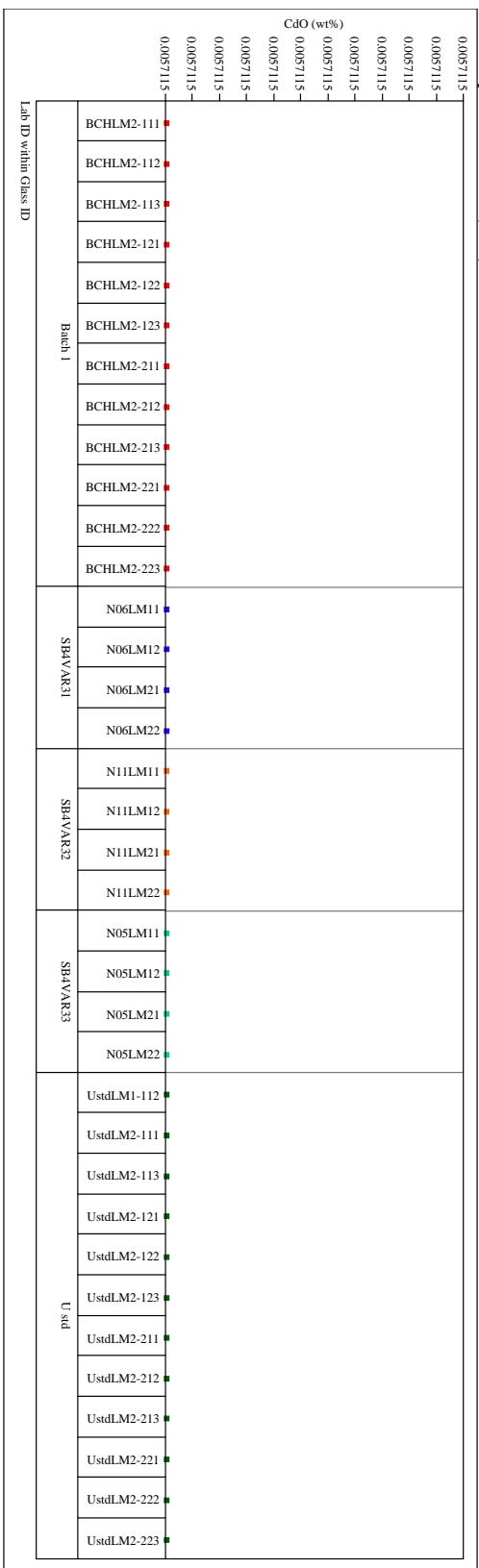
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for CaO (wt%)

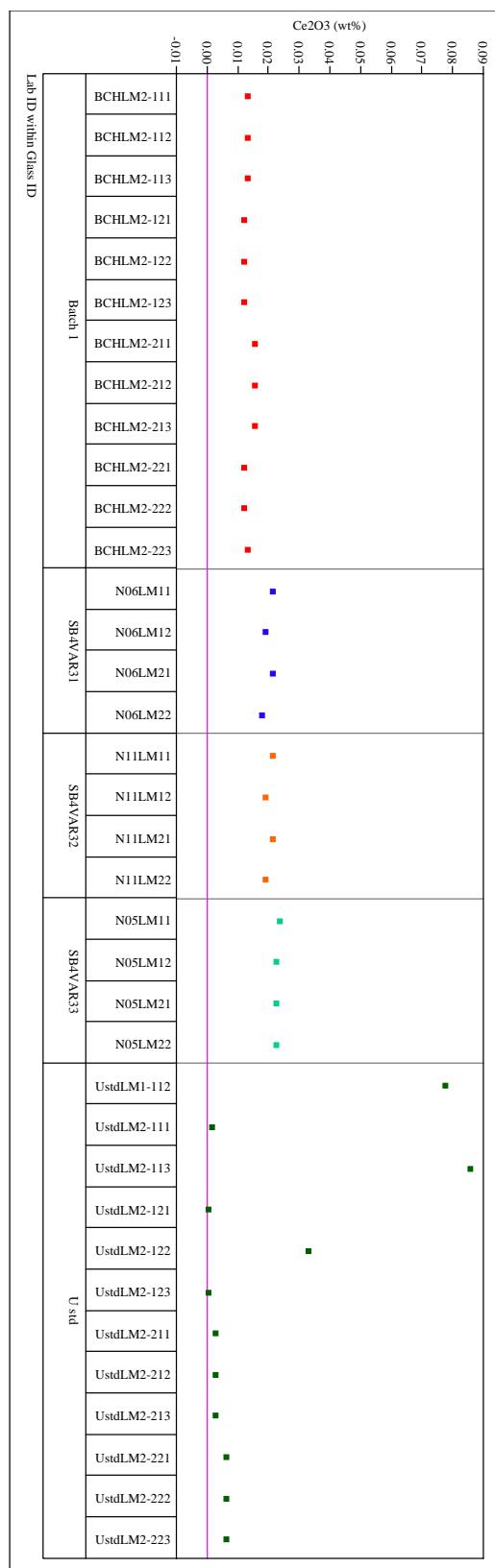


**Set=2**  
Variability Chart for CdO (wt%)

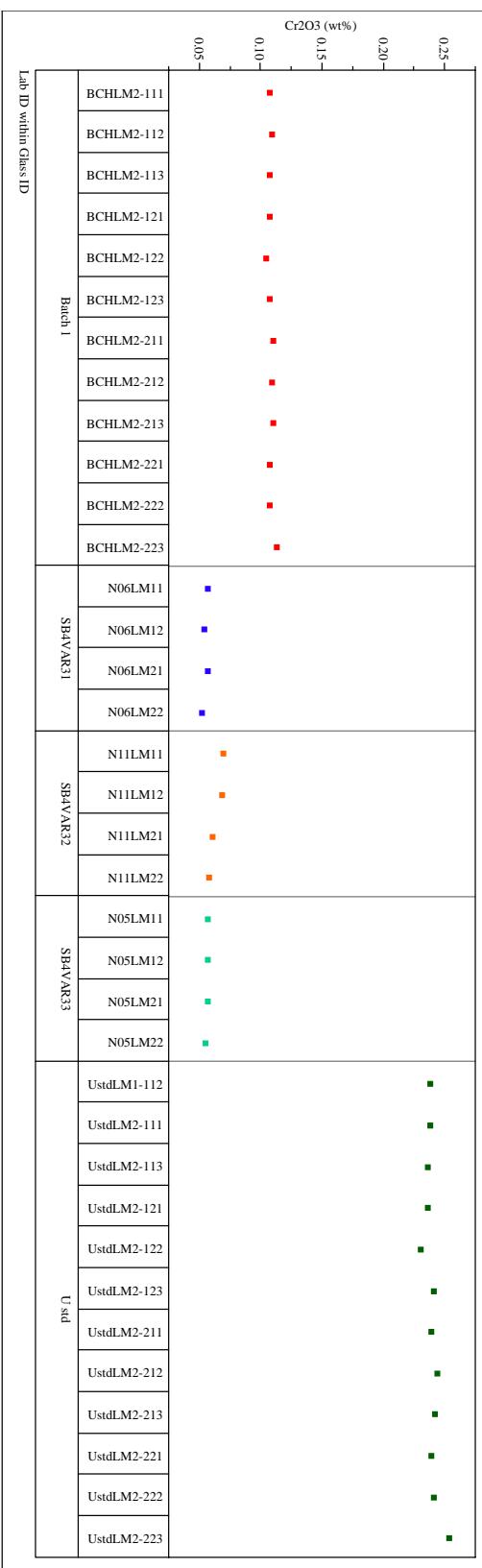


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for Ce<sub>2</sub>O<sub>3</sub> (wt%)



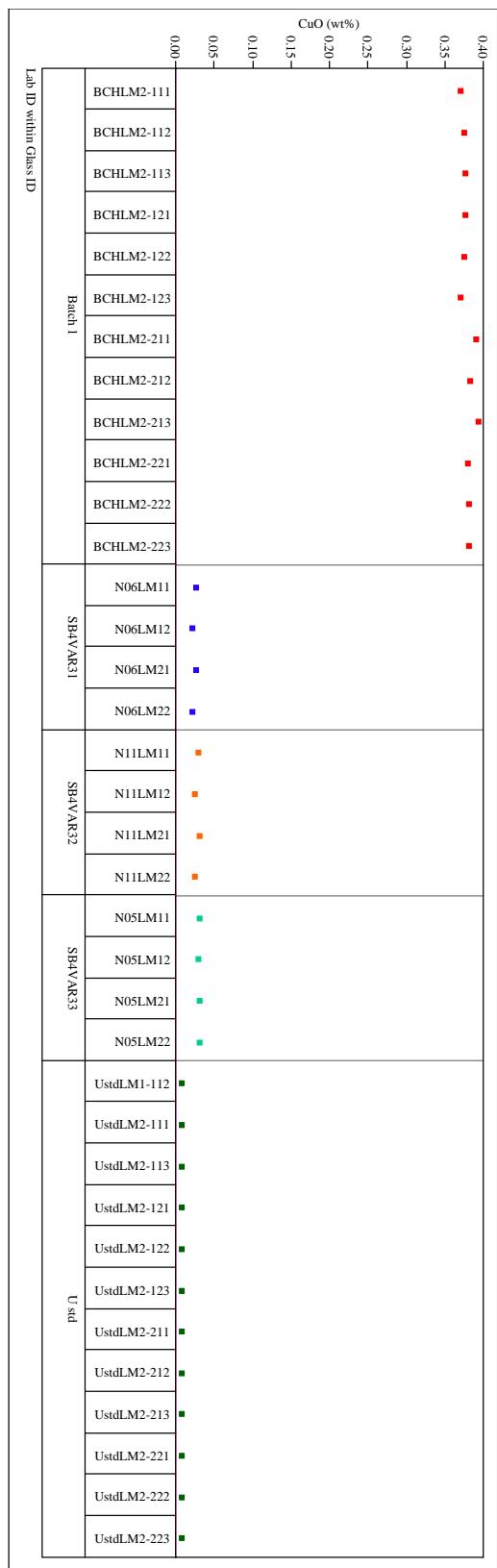
**Set=2**  
Variability Chart for Cr<sub>2</sub>O<sub>3</sub> (wt%)



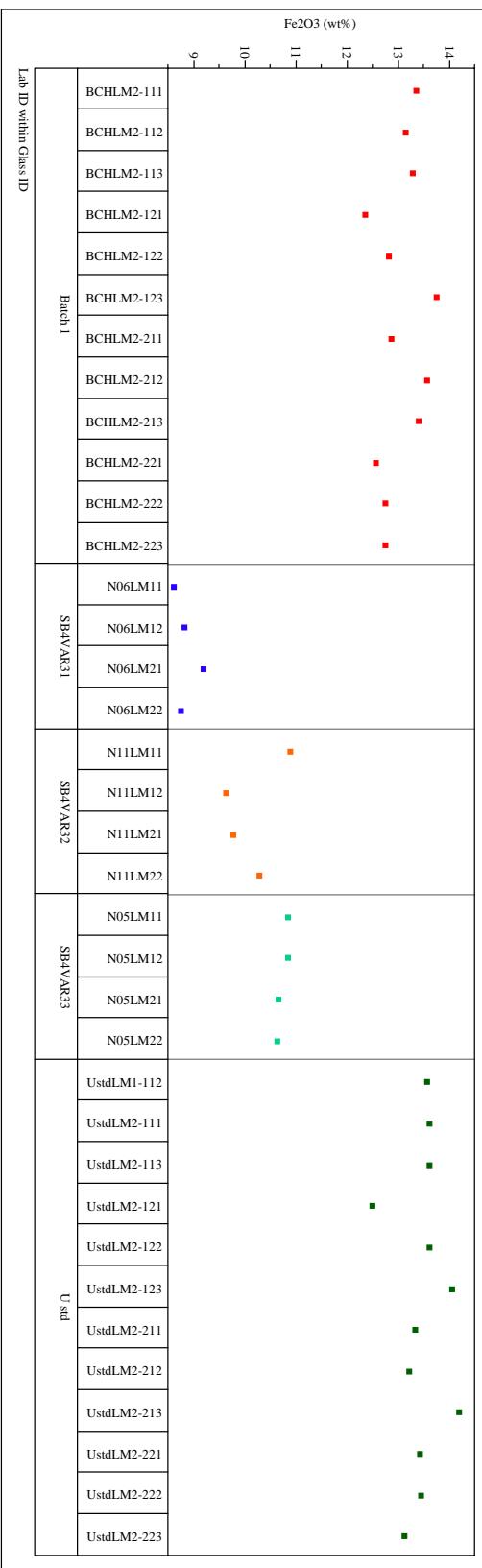
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
**Variability Chart for CuO (wt%)**



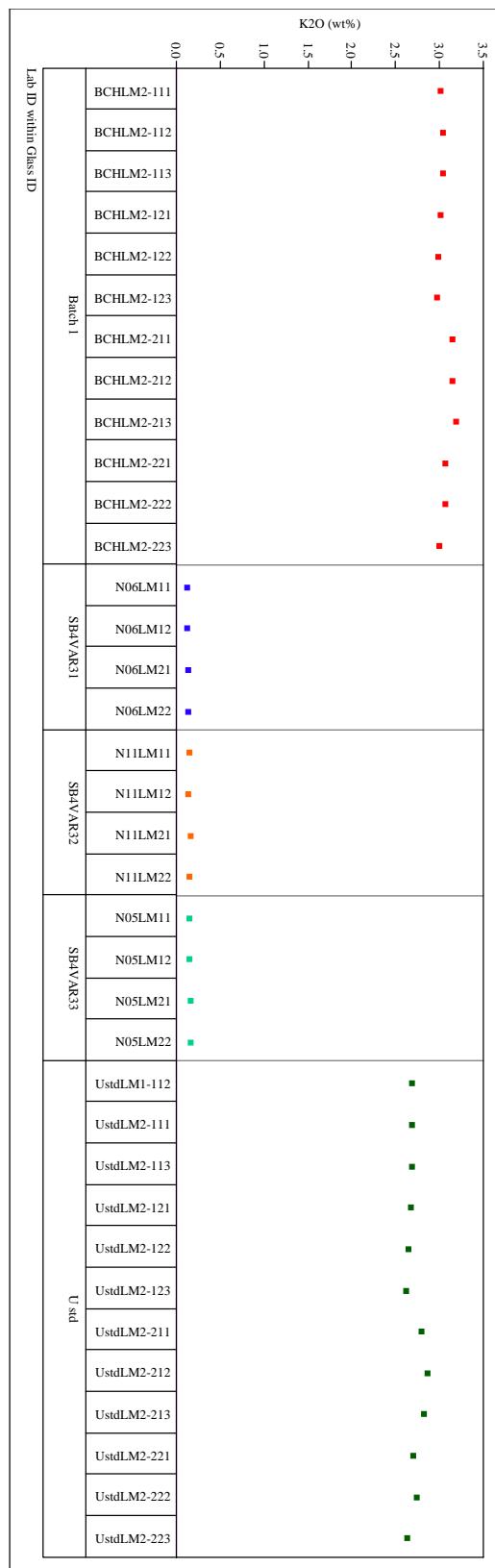
**Set=2**  
**Variability Chart for Fe2O3 (wt%)**



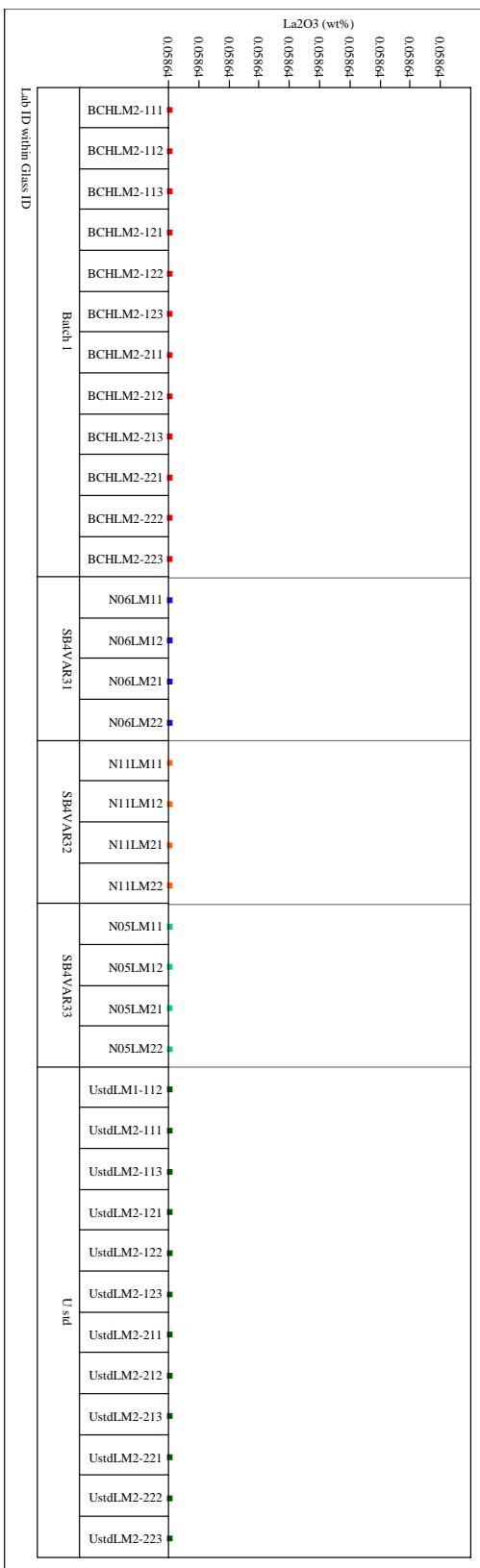
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for K<sub>2</sub>O (wt%)



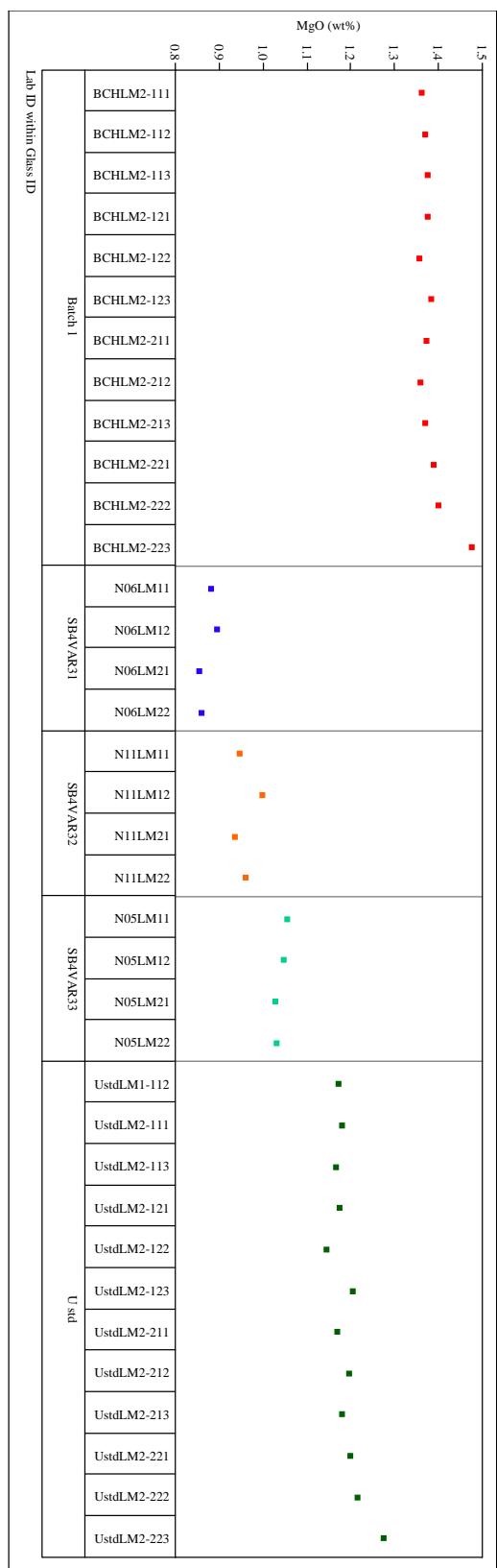
**Set=2**  
Variability Chart for La<sub>2</sub>O<sub>3</sub> (wt%)



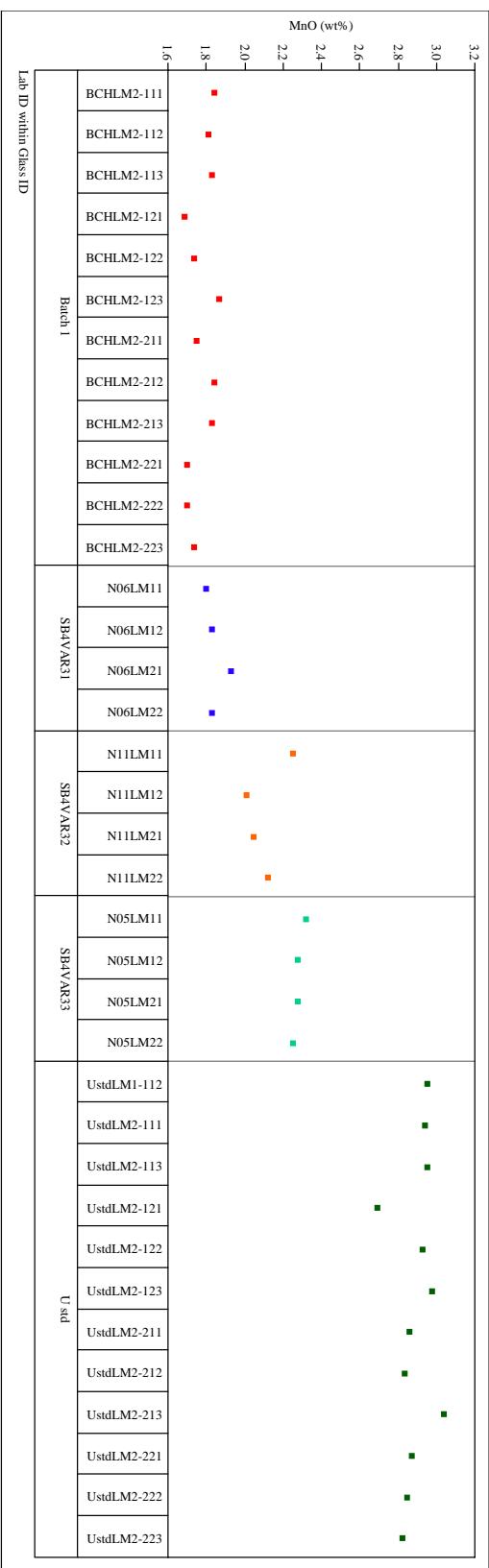
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for MgO (wt%)

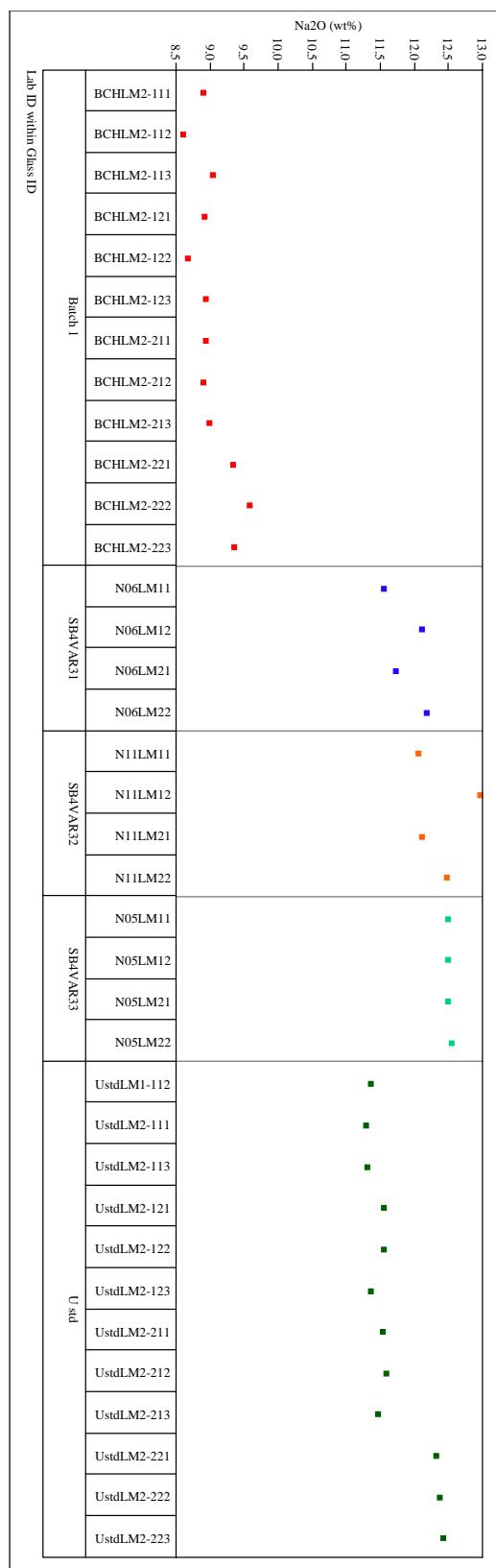


**Set=2**  
Variability Chart for MnO (wt%)

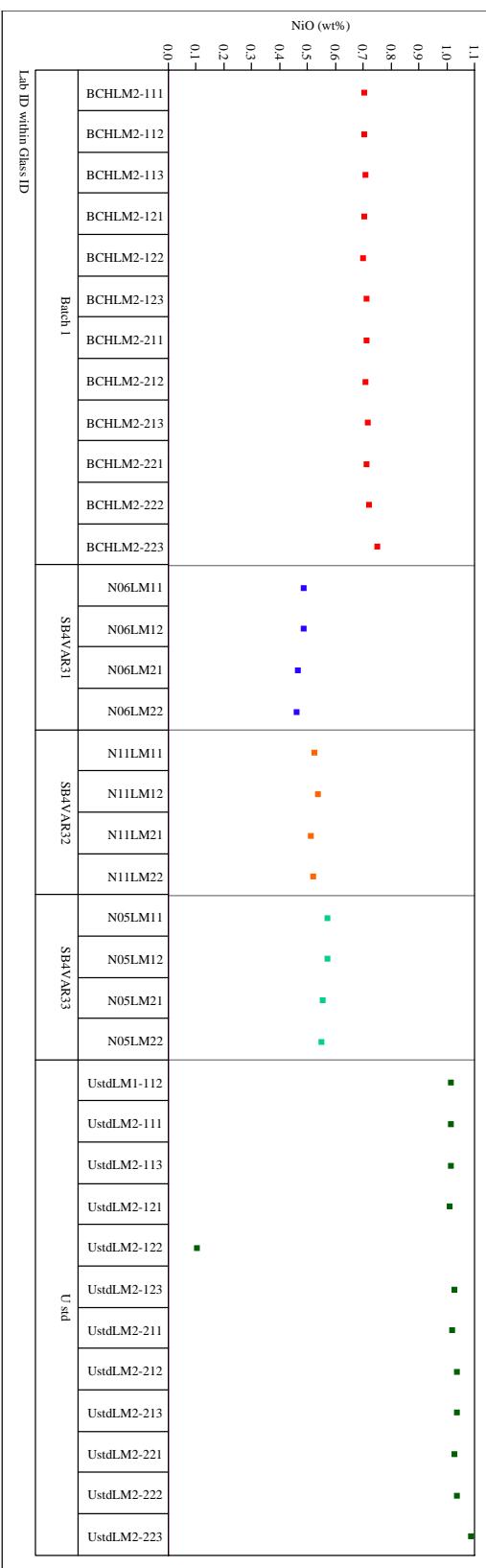


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for Na<sub>2</sub>O (wt%)



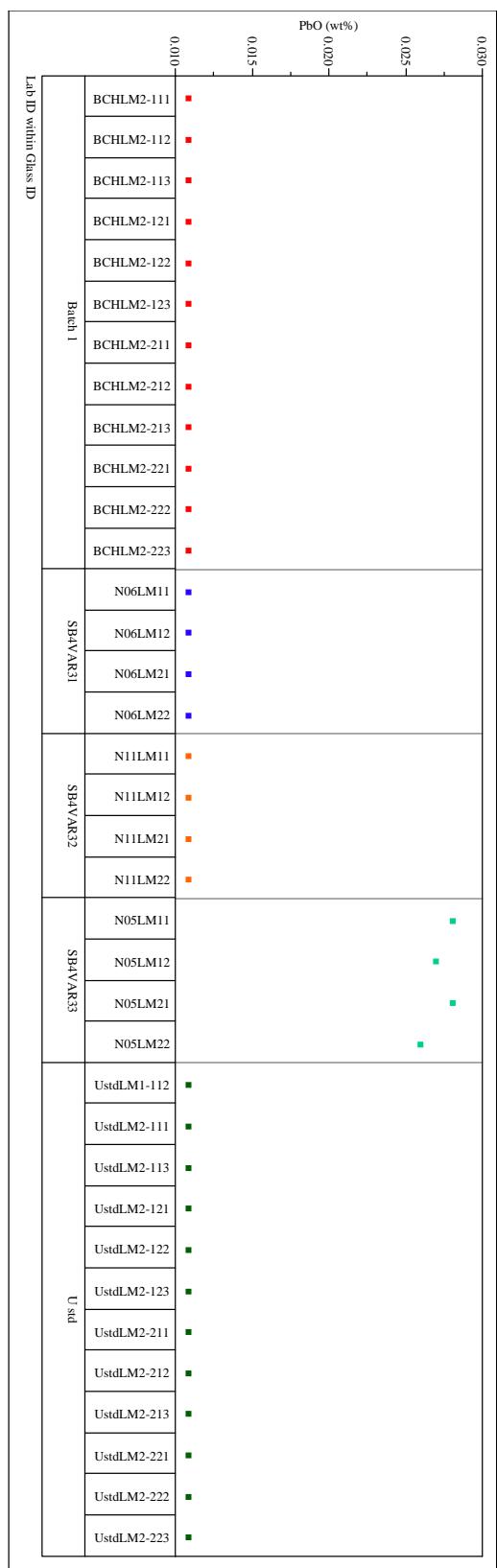
**Set=2**  
Variability Chart for NiO (wt%)



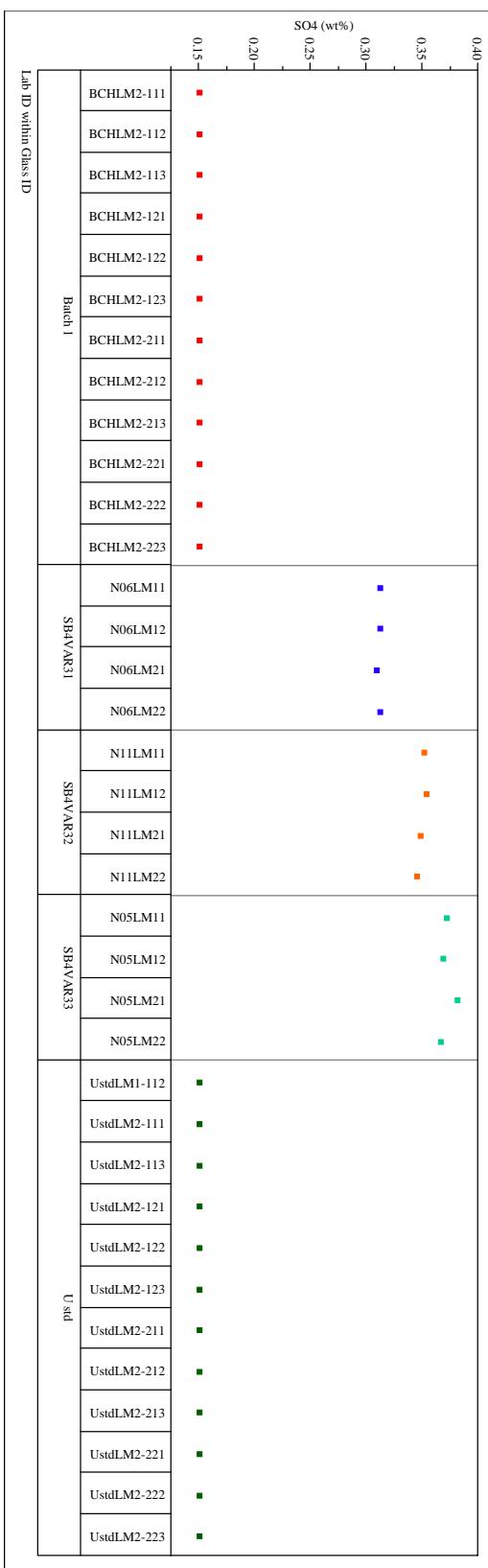
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
**Variability Chart for PbO (wt%)**



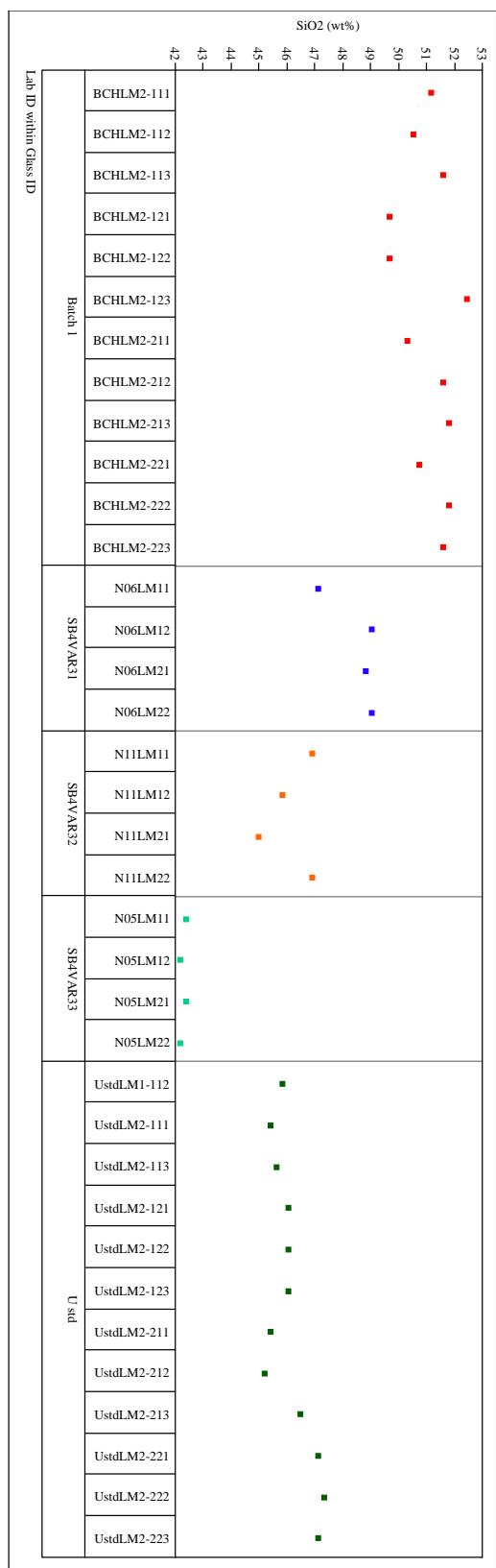
**Set=2**  
**Variability Chart for SO4 (wt%)**



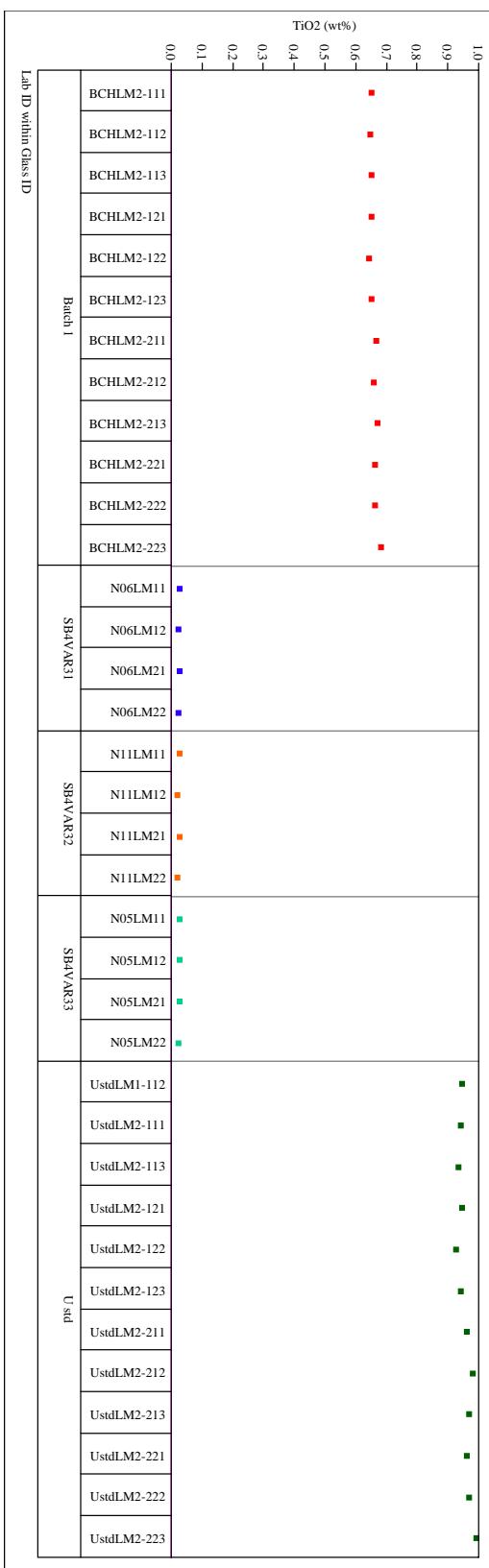
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for SiO<sub>2</sub> (wt%)



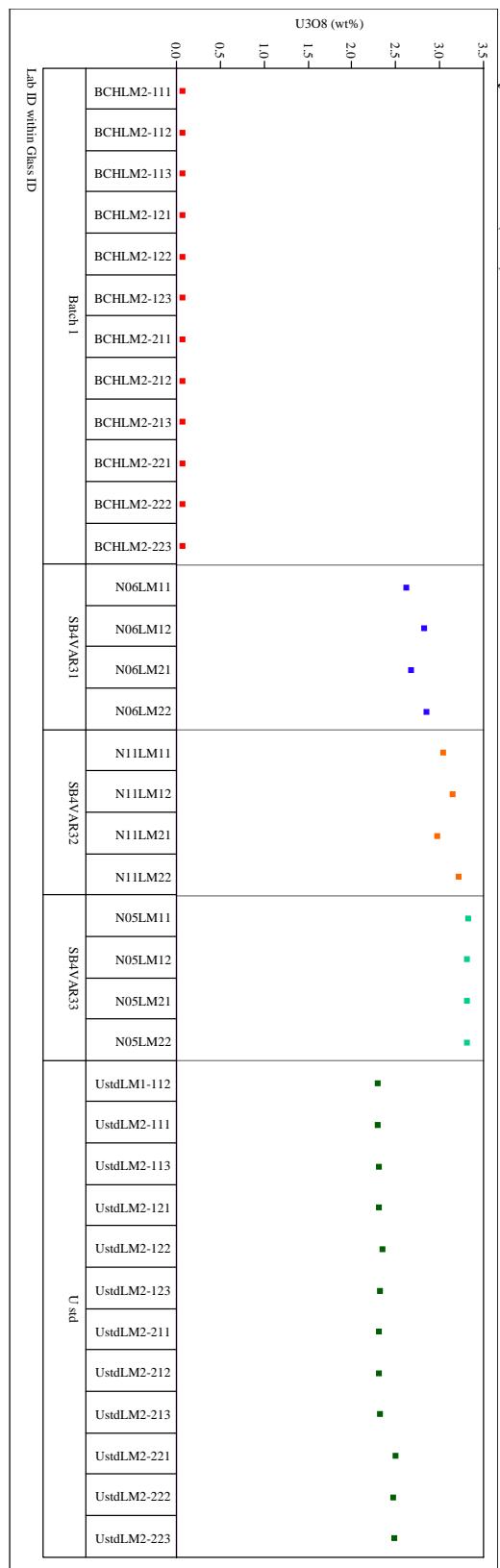
**Set=2**  
Variability Chart for TiO<sub>2</sub> (wt%)



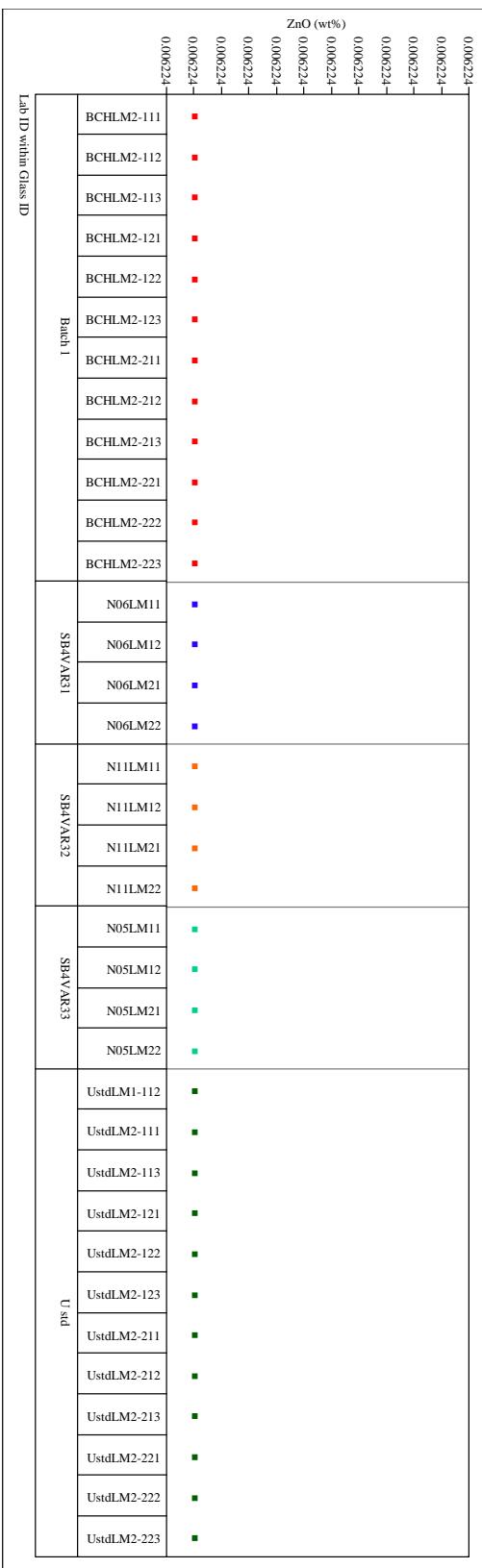
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for U3O8 (wt%)



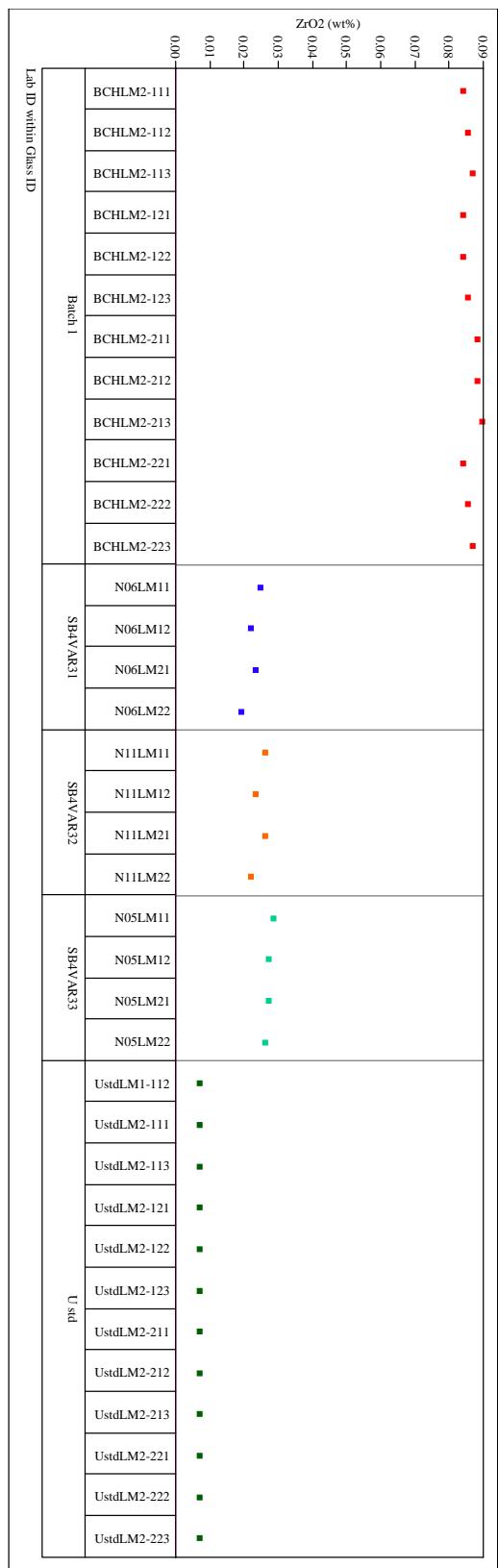
**Set=2**  
Variability Chart for ZnO (wt%)



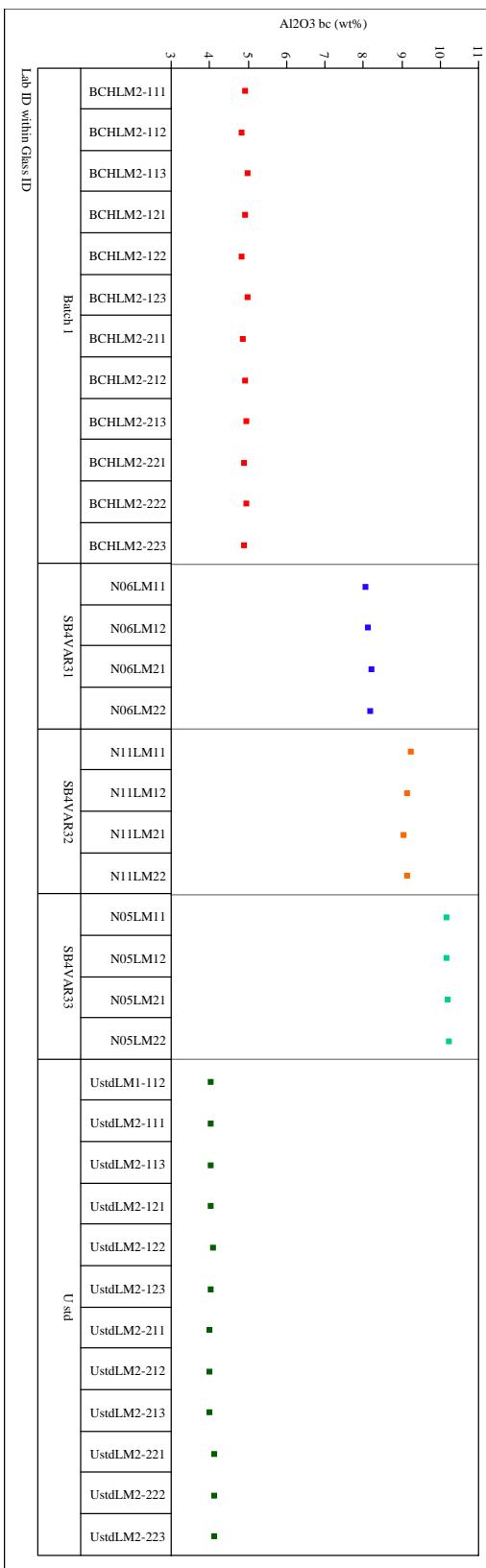
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
**Variability Chart for ZrO<sub>2</sub> (wt%)**



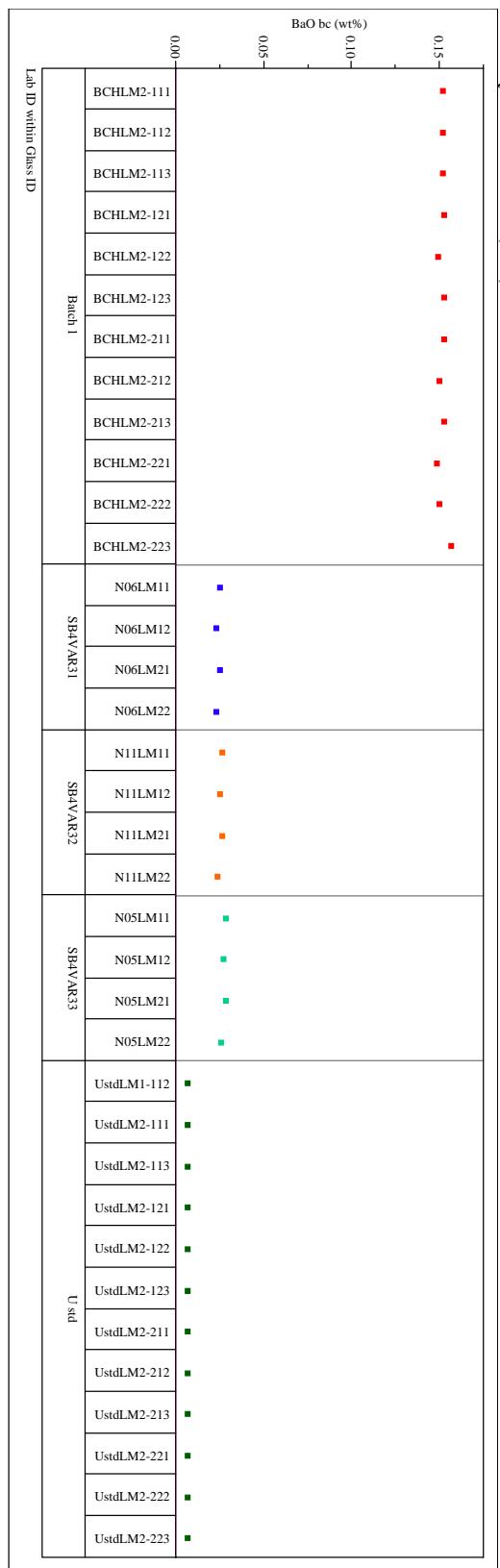
**Set=2**  
**Variability Chart for Al<sub>2</sub>O<sub>3</sub> bc (wt%)**



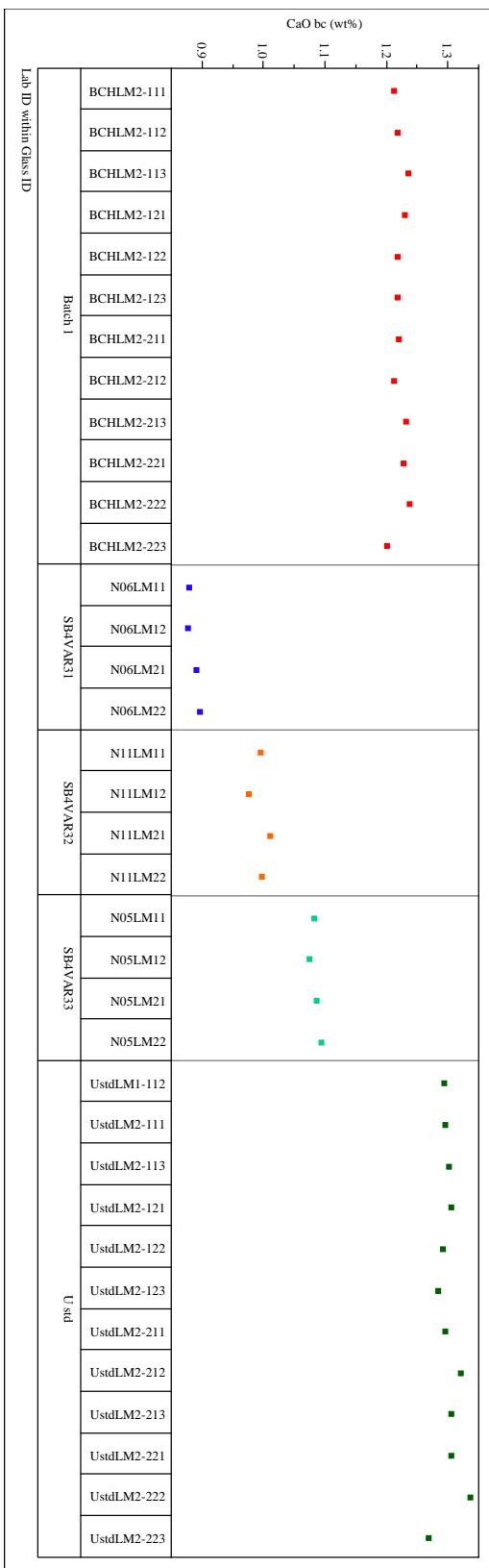
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for BaO bc (wt%)



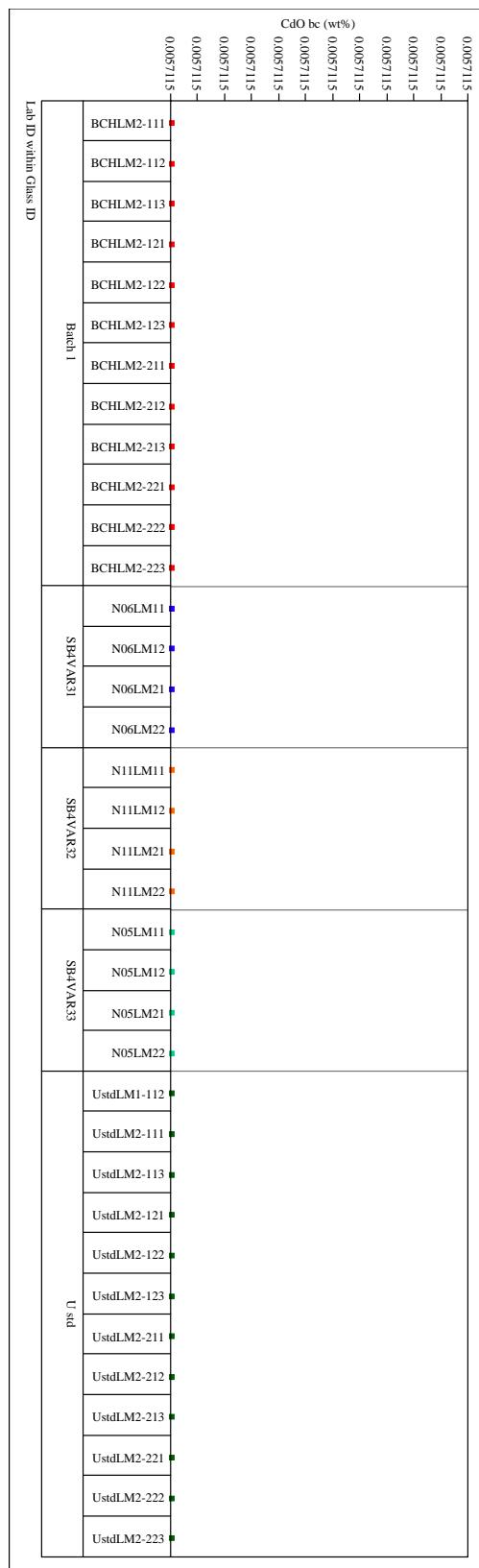
**Set=2**  
Variability Chart for CaO bc (wt%)



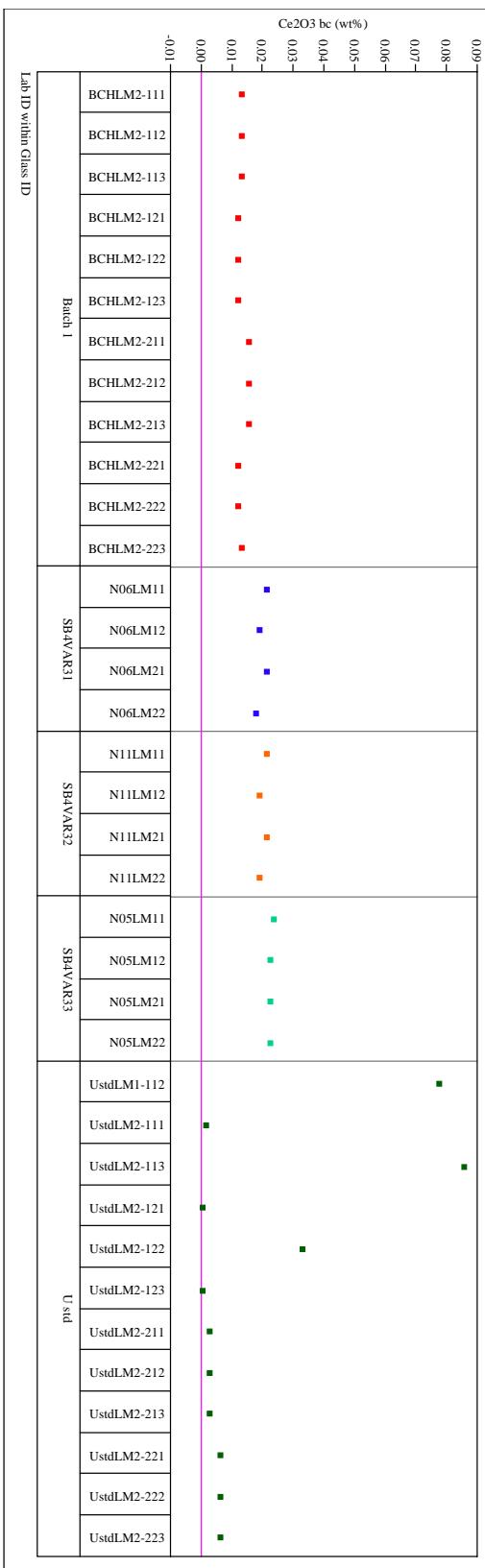
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
**Variability Chart for CdO bc (wt%)**



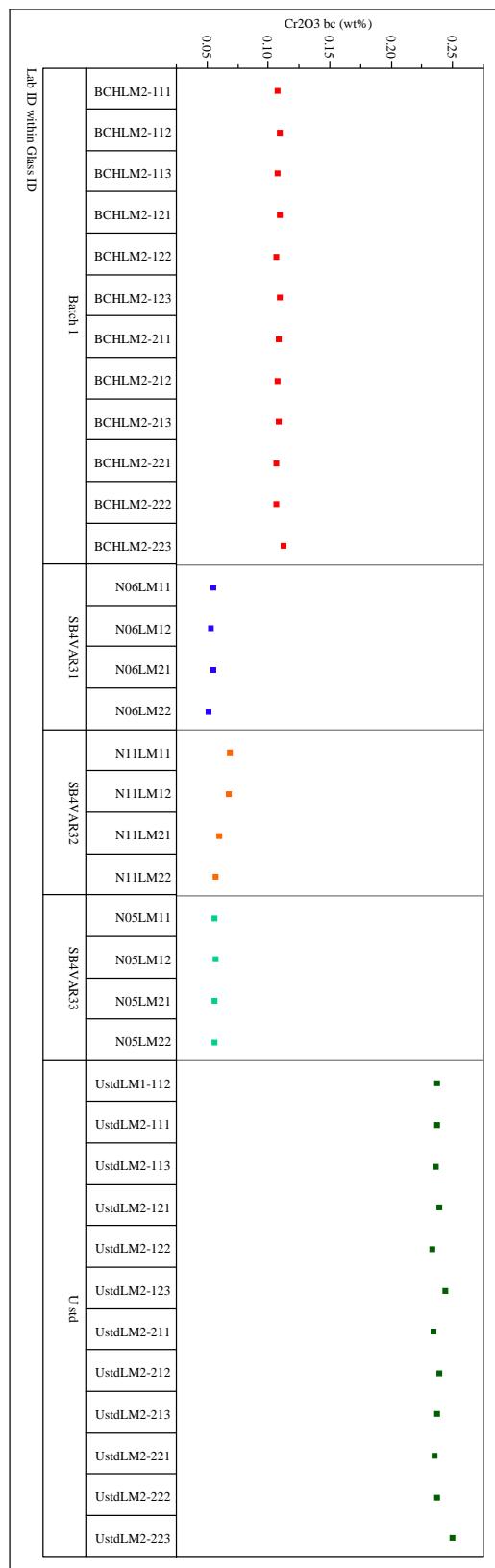
**Set=2**  
**Variability Chart for Ce<sub>2</sub>O<sub>3</sub> bc (wt%)**



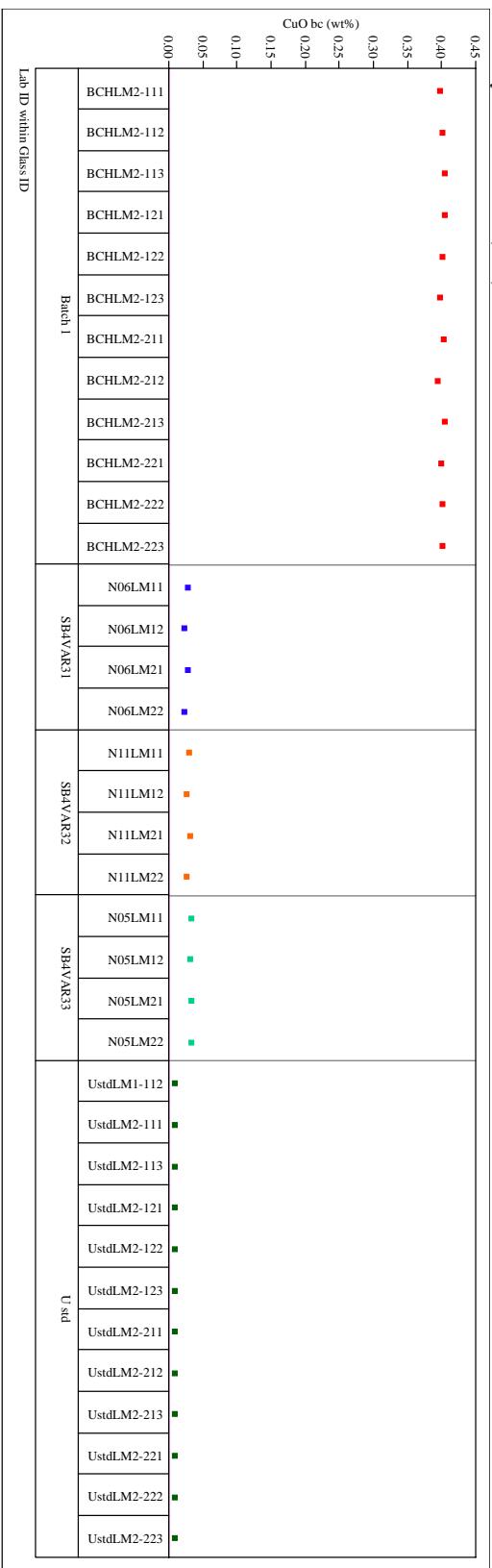
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for Cr<sub>2</sub>O<sub>3</sub> bc (wt%)



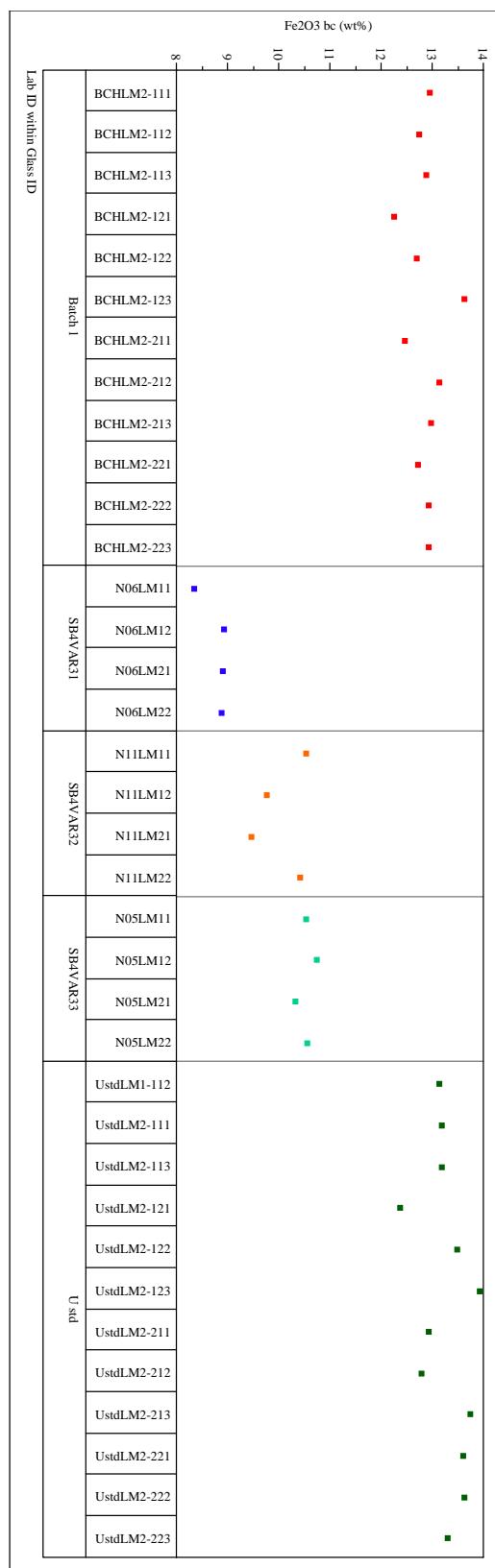
**Set=2**  
Variability Chart for CuO bc (wt%)



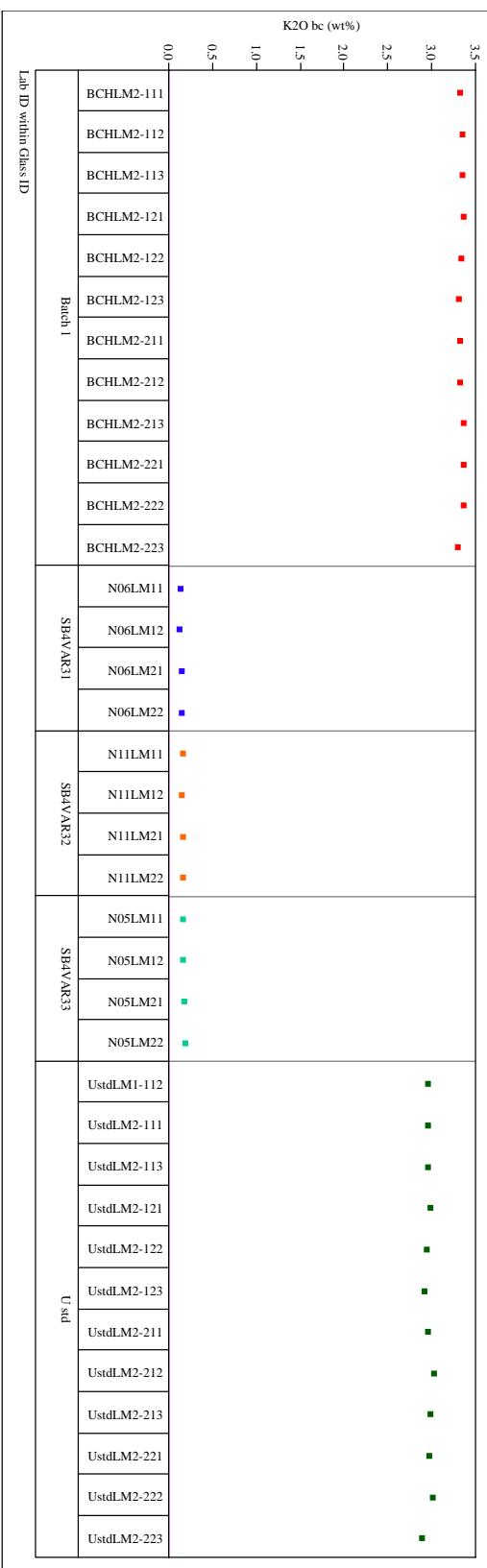
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for Fe<sub>2</sub>O<sub>3</sub> bc (wt%)



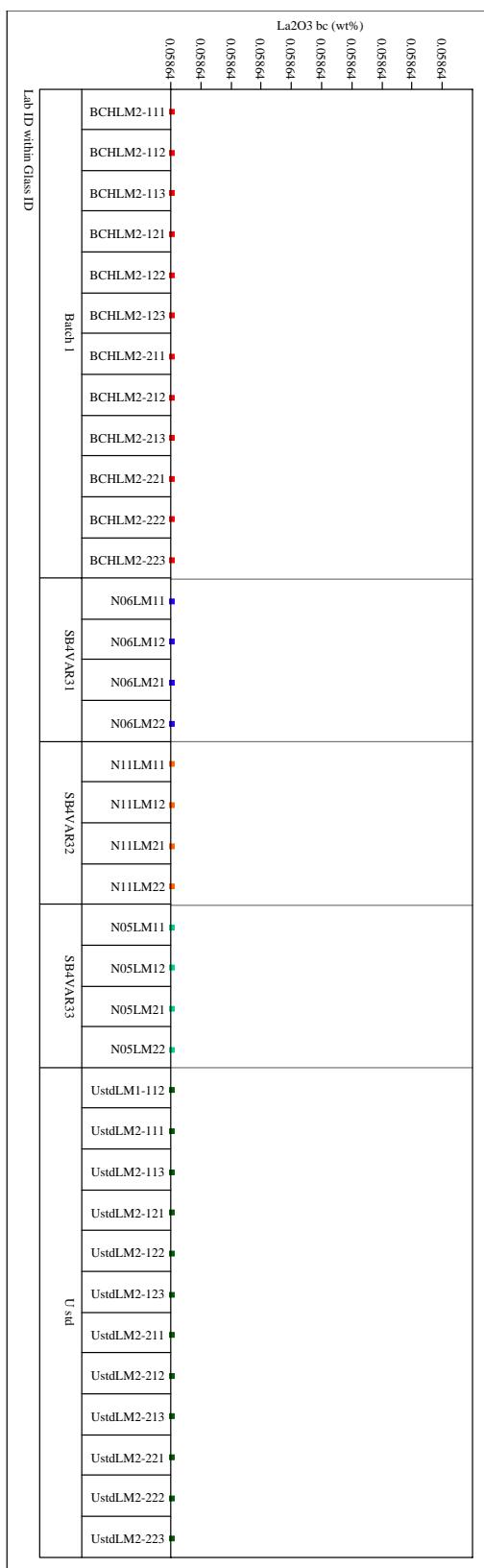
**Set=2**  
Variability Chart for K<sub>2</sub>O bc (wt%)



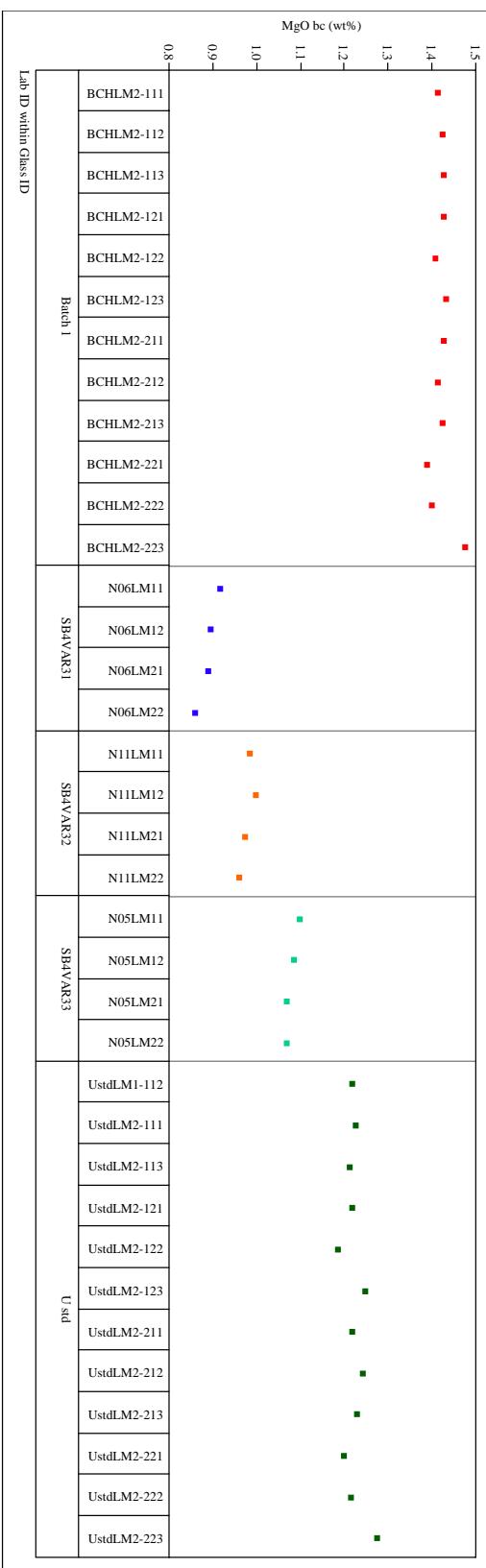
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for La<sub>2</sub>O<sub>3</sub> bc (wt%)



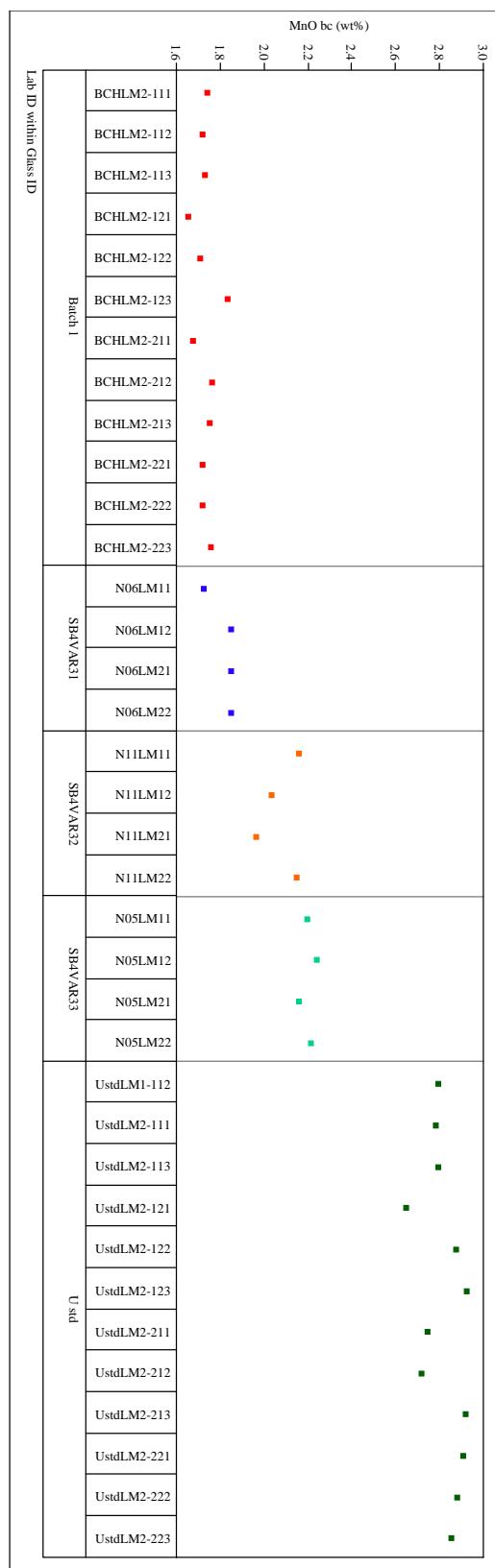
**Set=2**  
Variability Chart for MgO bc (wt%)



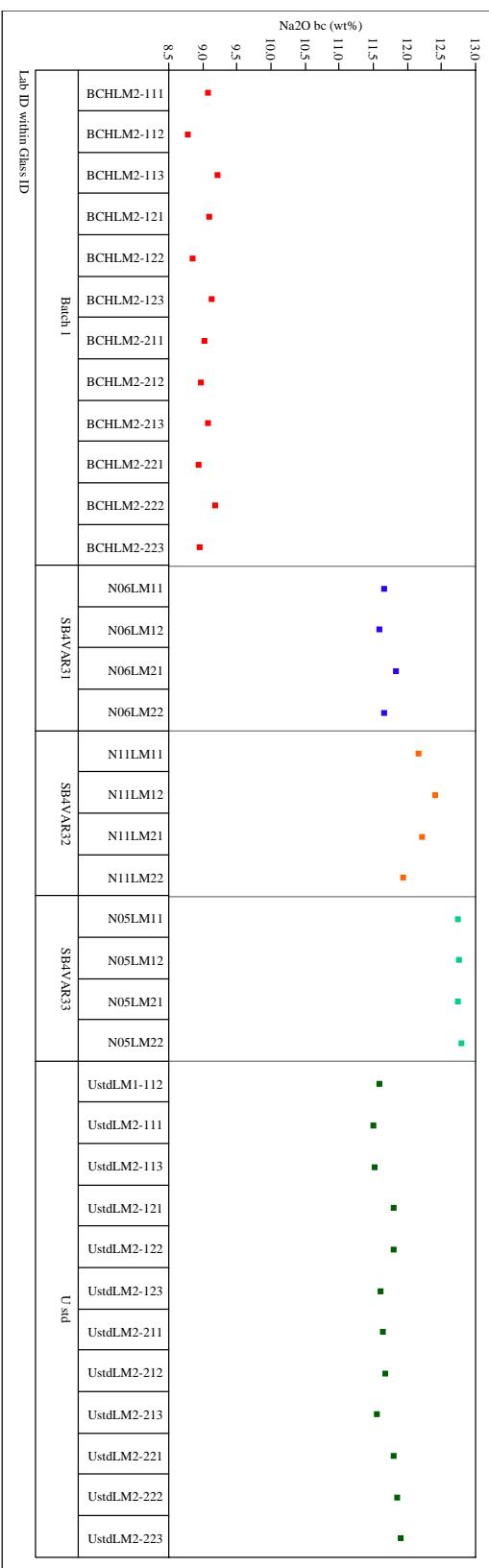
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for MnO bc (wt%)



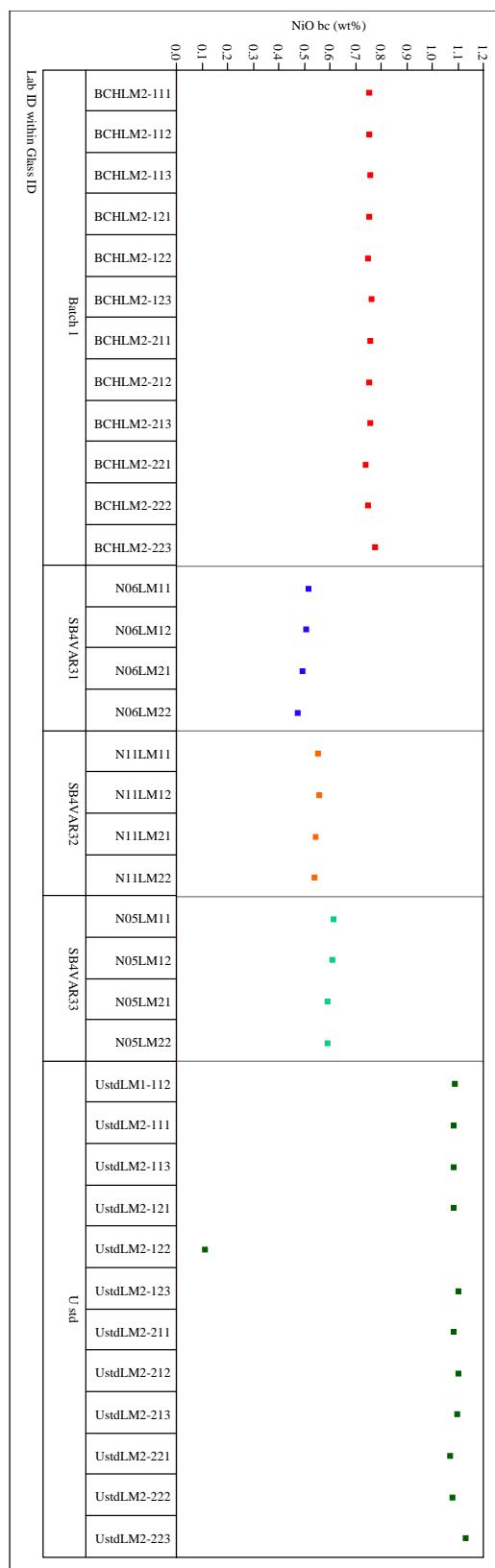
**Set=2**  
Variability Chart for Na<sub>2</sub>O bc (wt%)



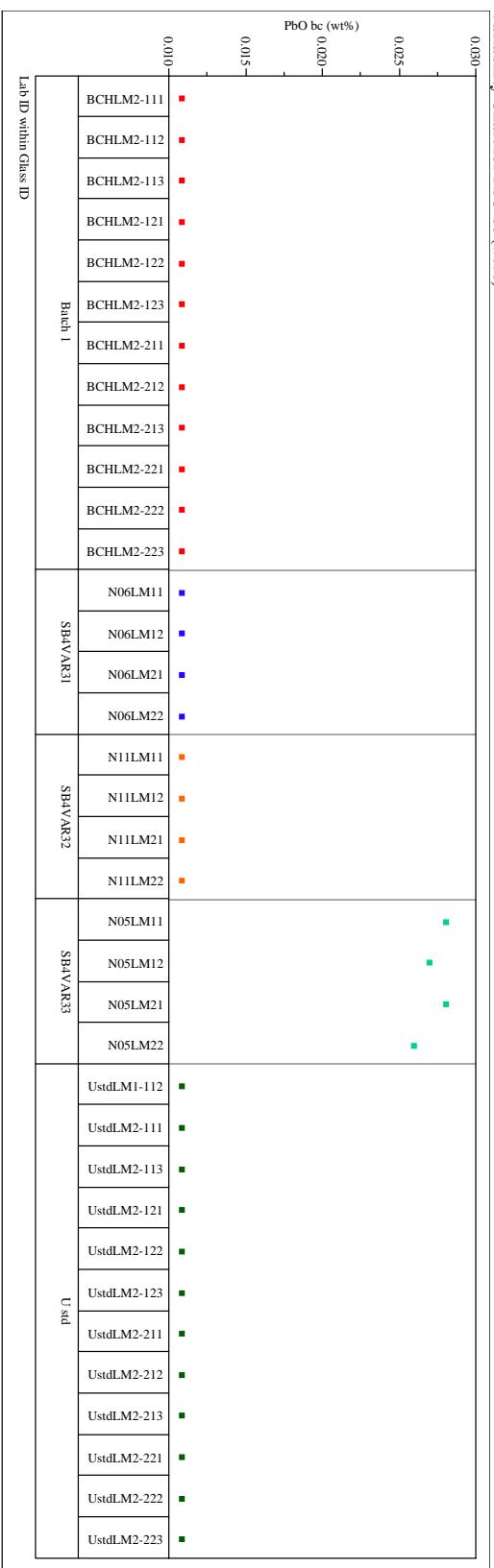
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for NiO bc (wt%)

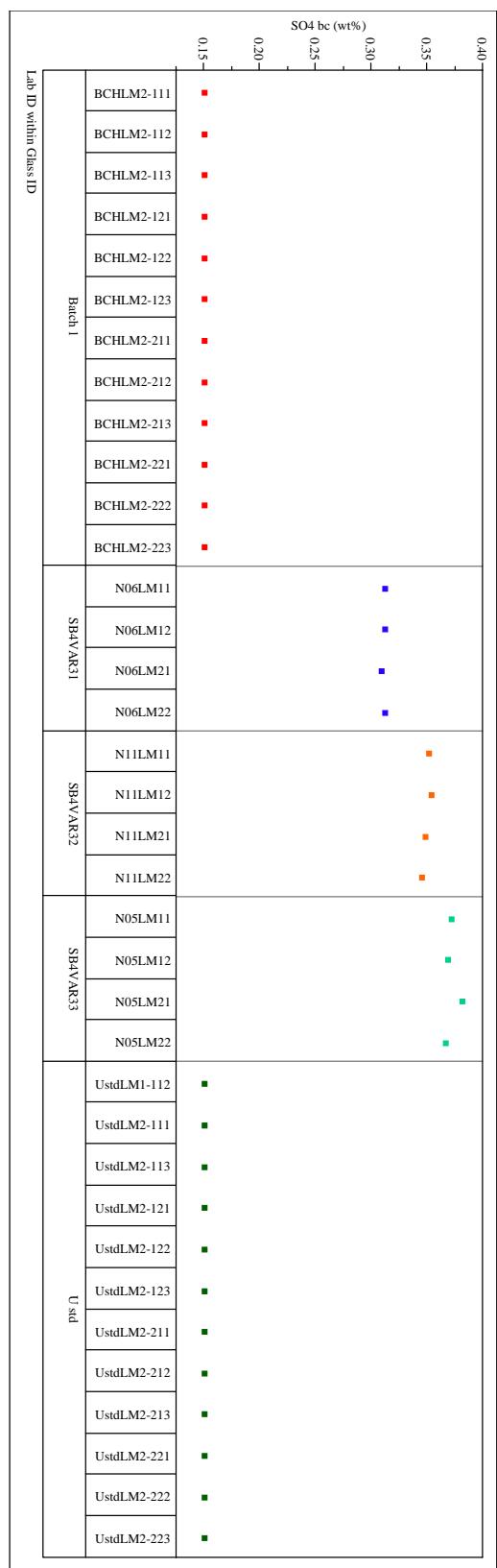


**Set=2**  
Variability Chart for PbO bc (wt%)

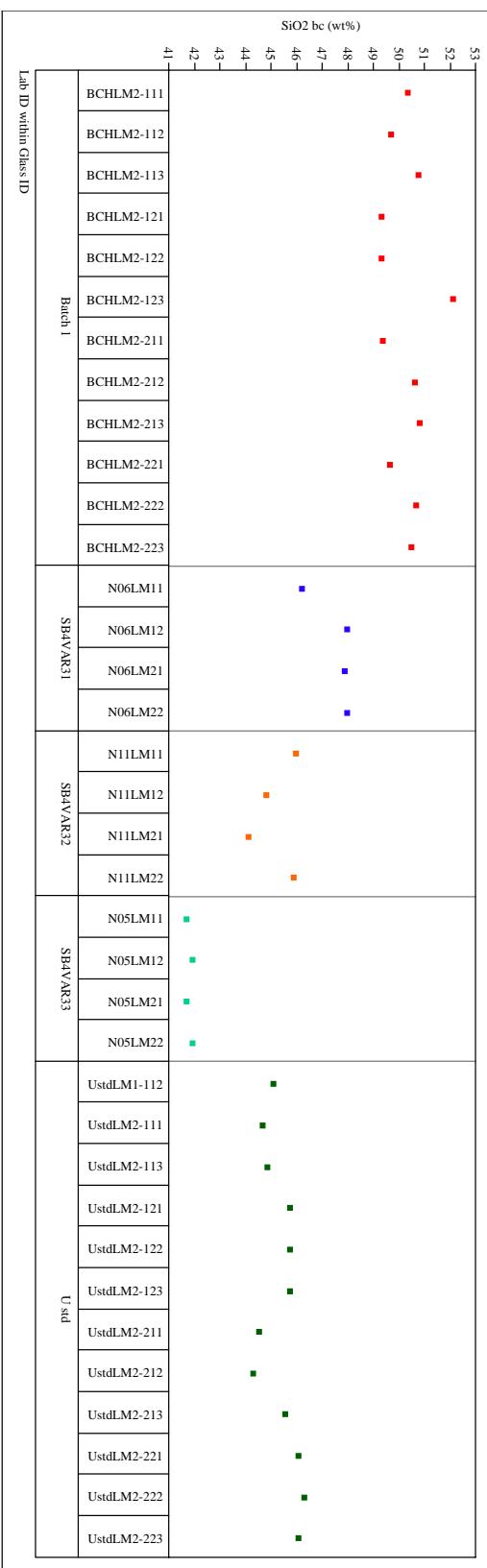


## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for SO<sub>4</sub> bc (wt%)



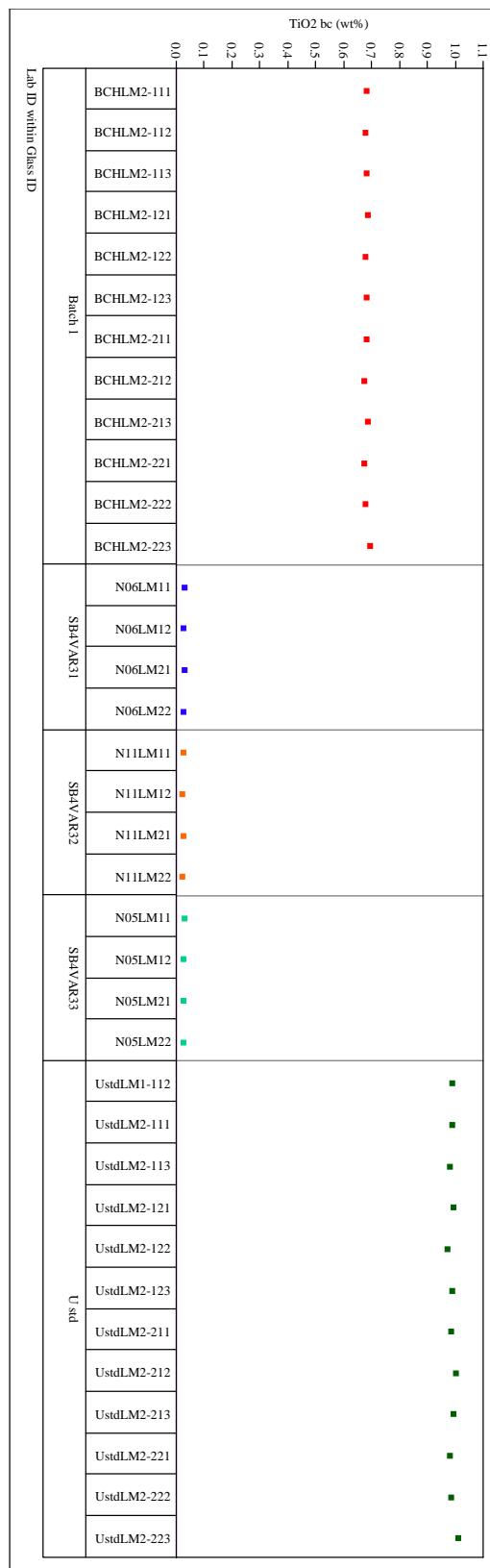
**Set=2**  
Variability Chart for SiO<sub>2</sub> bc (wt%)



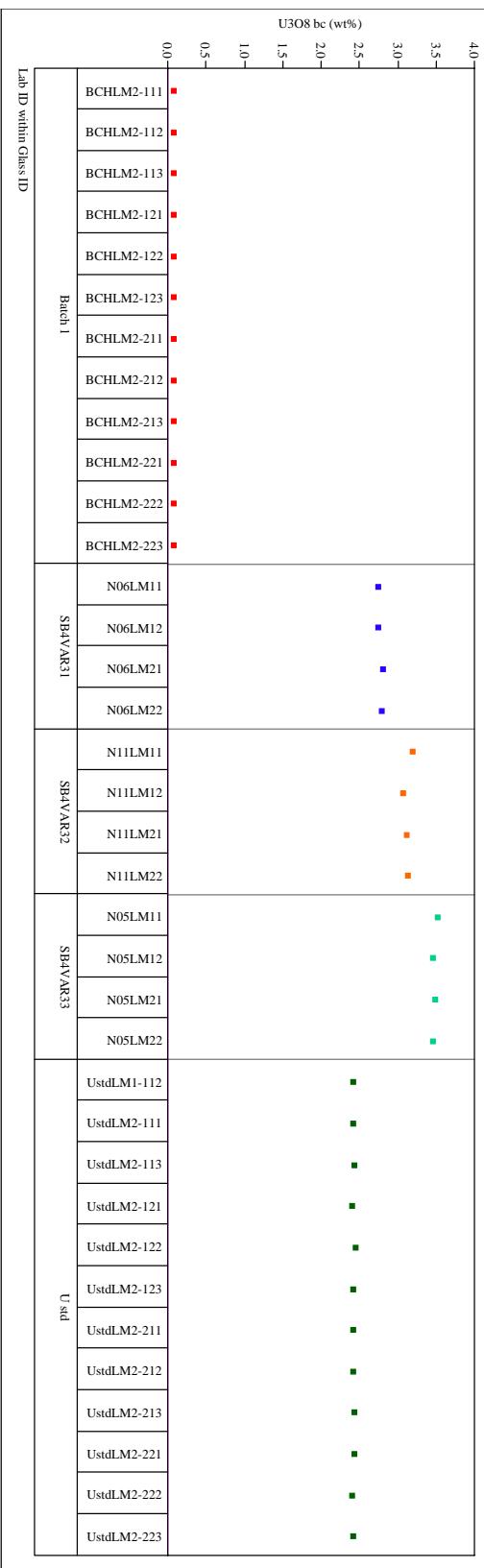
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
Variability Chart for TiO<sub>2</sub> bc (wt%)



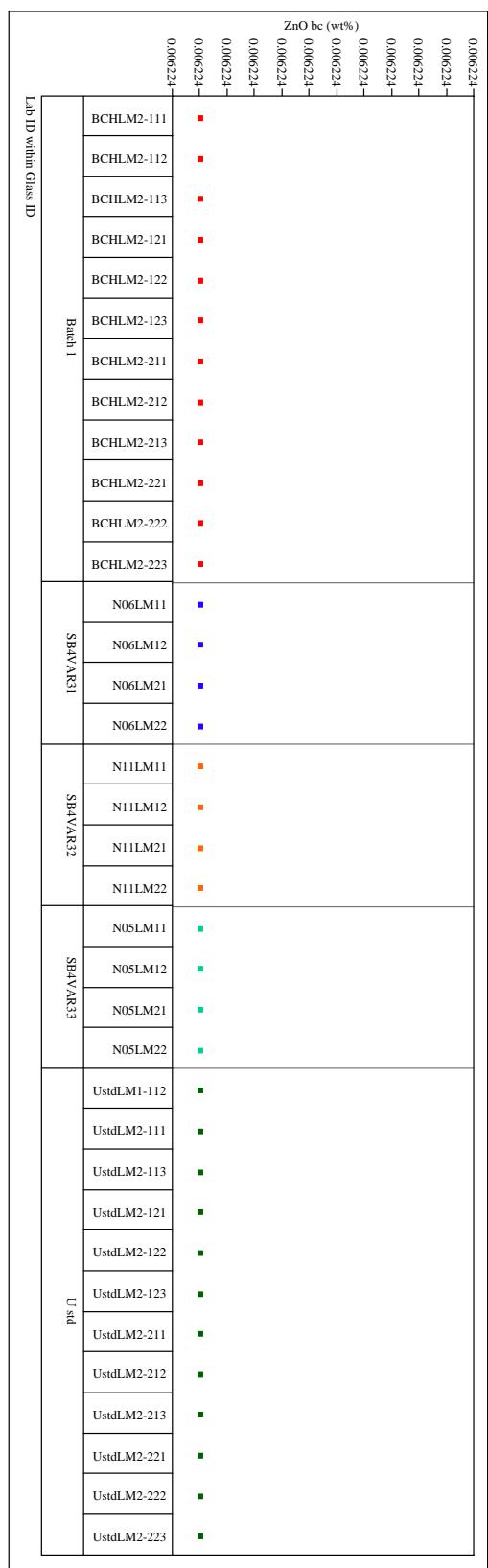
**Set=2**  
Variability Chart for U3O8 bc (wt%)



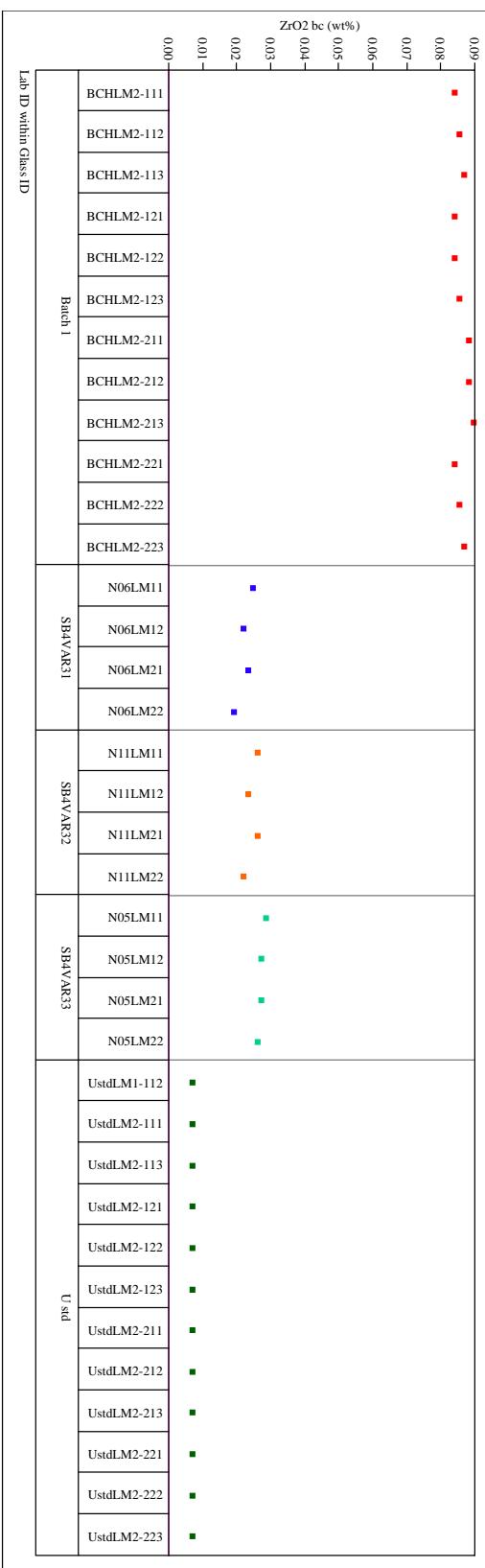
Lab ID within Glass ID

## Exhibit A5. Oxide Measurements by Solution ID for Samples Prepared Using the LM Method

**Set=2**  
**Variability Chart for ZnO bc (wt%)**

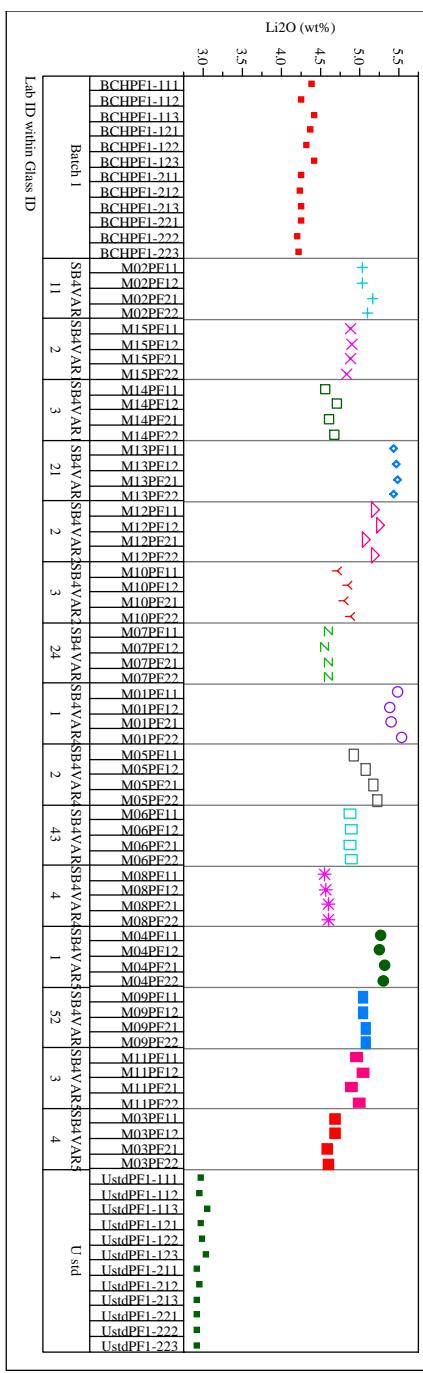


**Set=2**  
**Variability Chart for ZrO<sub>2</sub> bc (wt%)**



Lab ID within Glass ID

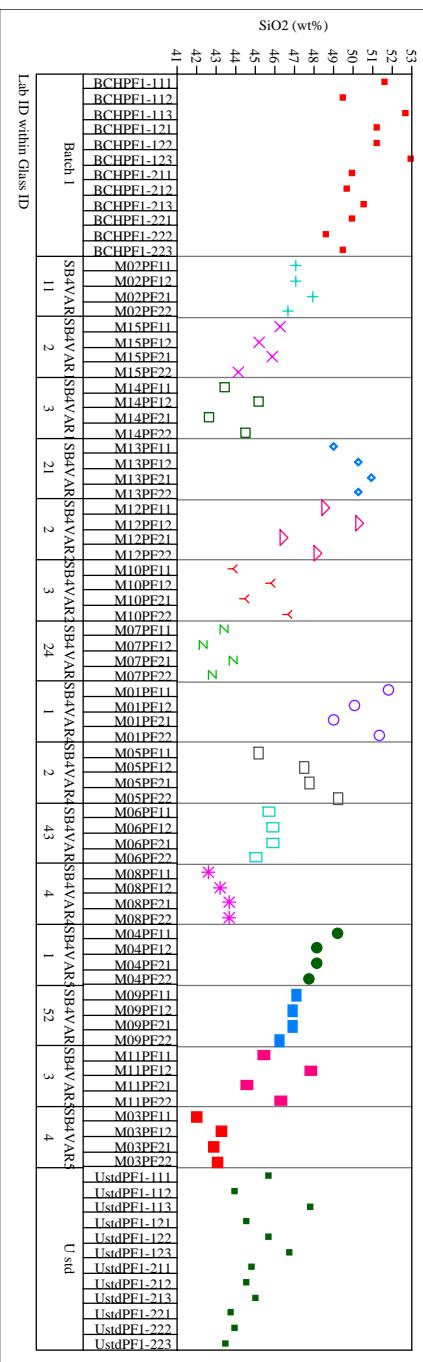
## Exhibit A6. Average Oxide Measurements by Solution ID for Samples Prepared Using the PF Method



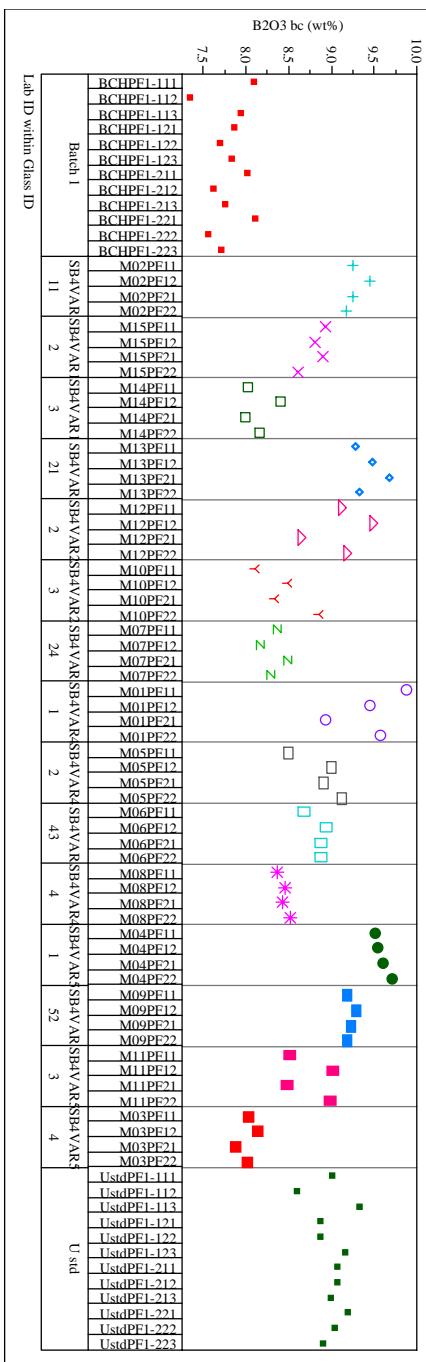
Lab ID within Glass ID

## Exhibit A6. Average Oxide Measurements by Solution ID for Samples Prepared Using the PF Method

**Set=1**  
**Variability Chart for SiO<sub>2</sub> (wt%)**

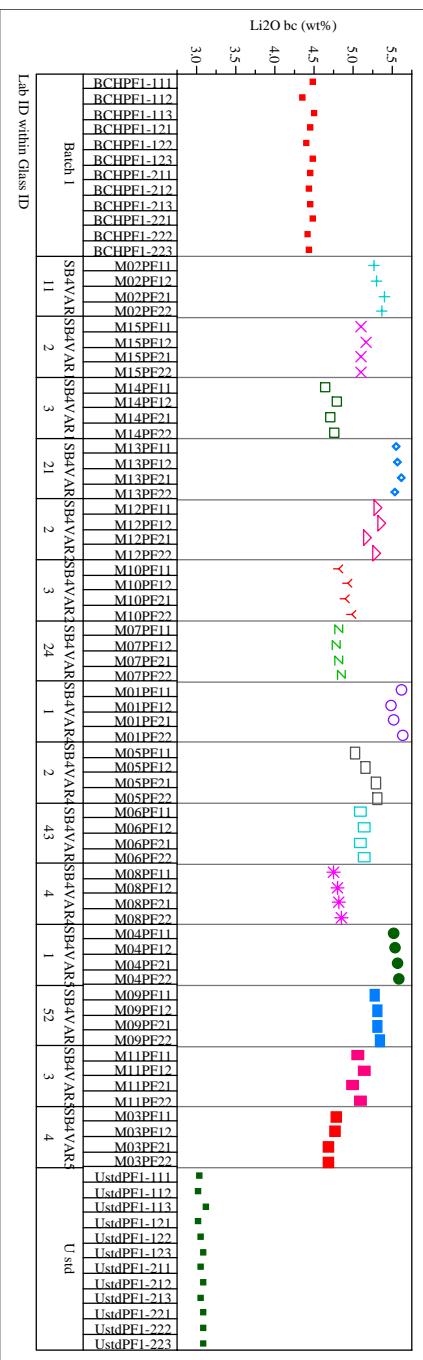


**Set=1**  
**Variability Chart for B2O<sub>3</sub> bc (wt%)**

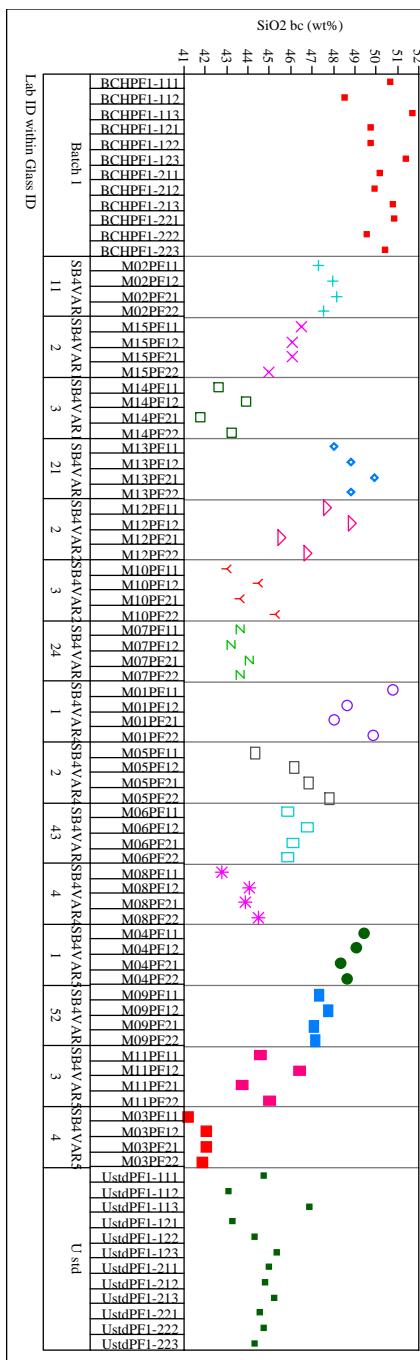


## Exhibit A6. Average Oxide Measurements by Solution ID for Samples Prepared Using the PF Method

Set=1  
Variability Chart for Li<sub>2</sub>O bc (wt%)

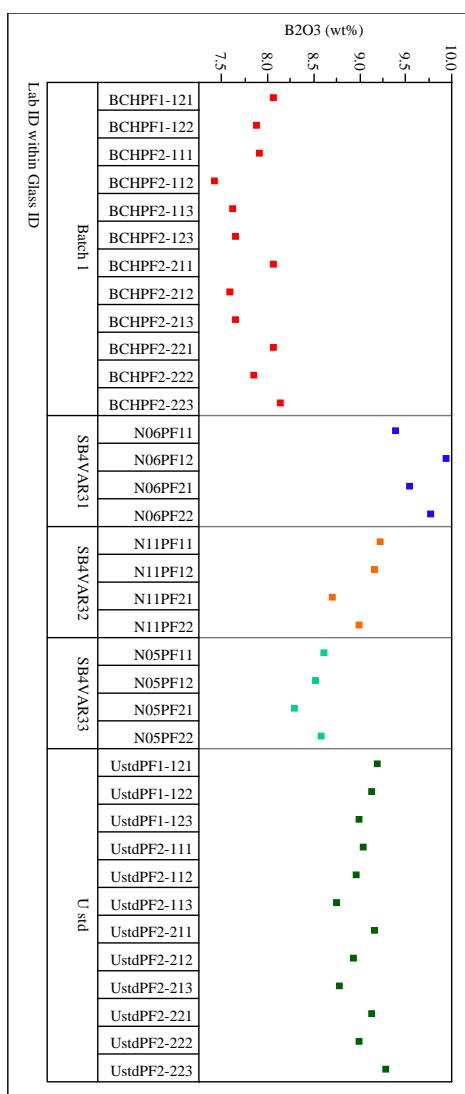


## Variability Chart for SiO<sub>2</sub> bc (wt%)

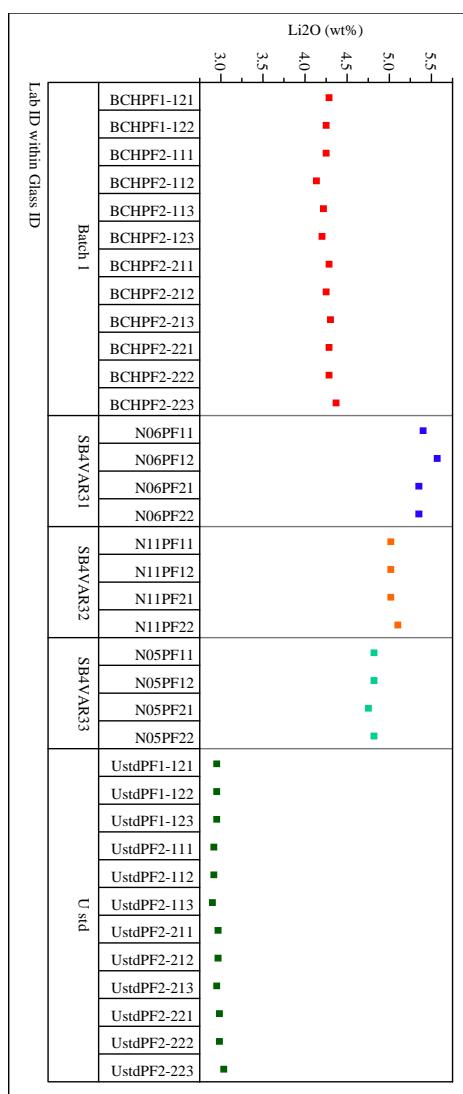


## Exhibit A6. Average Oxide Measurements by Solution ID for Samples Prepared Using the PF Method

**Set=2**  
**Variability Chart for B2O3 (wt%)**

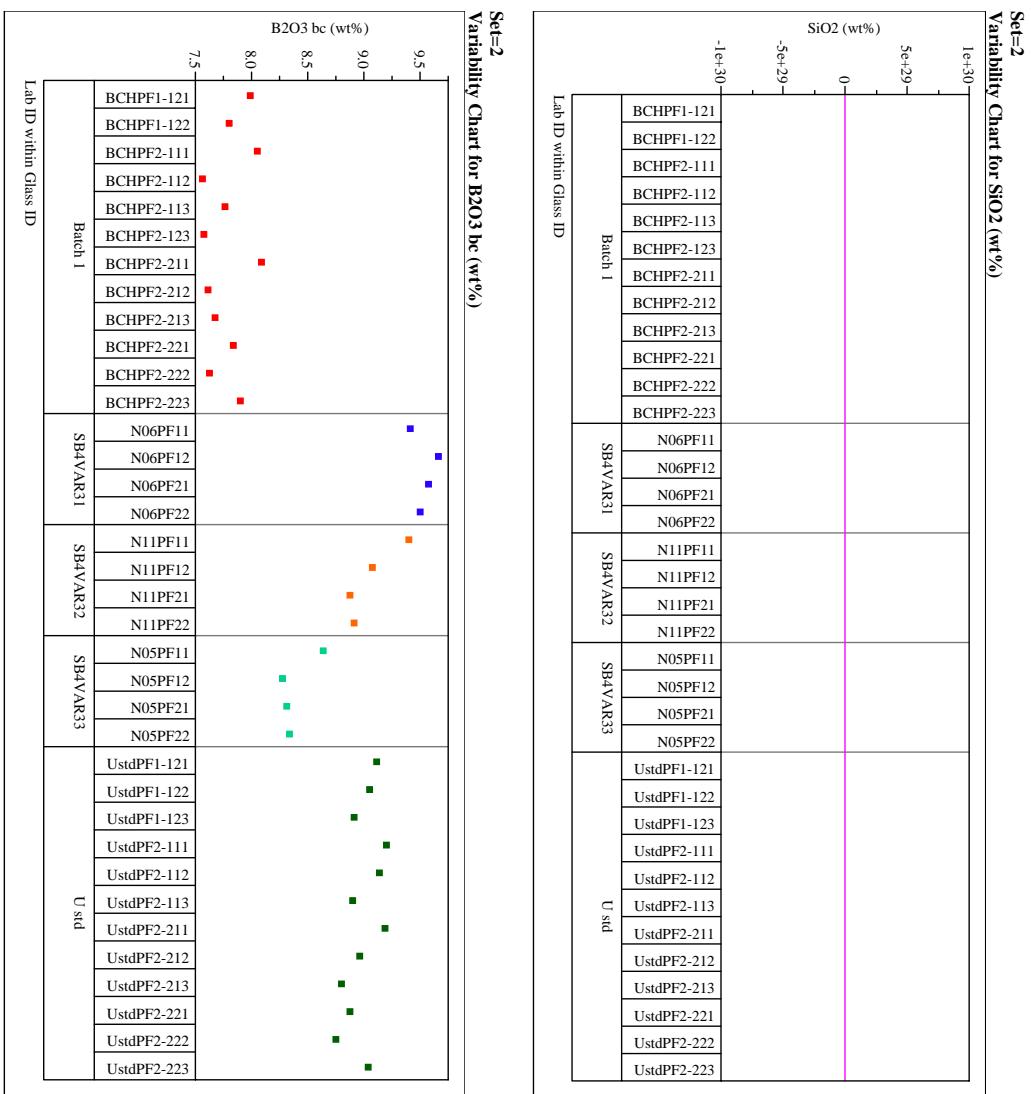


**Set=2**  
**Variability Chart for Li2O (wt%)**

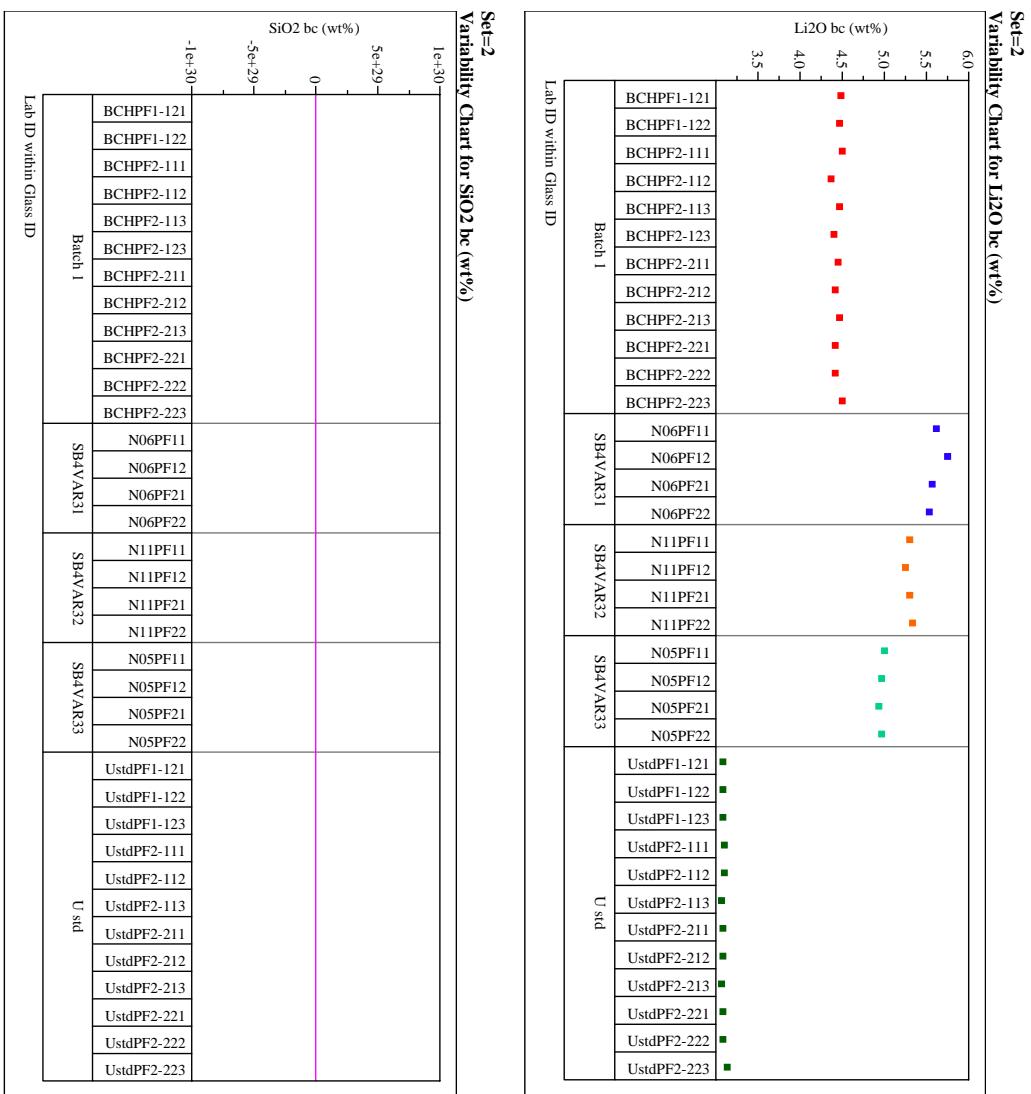


Lab ID within Glass ID

## Exhibit A6. Average Oxide Measurements by Solution ID for Samples Prepared Using the PF Method

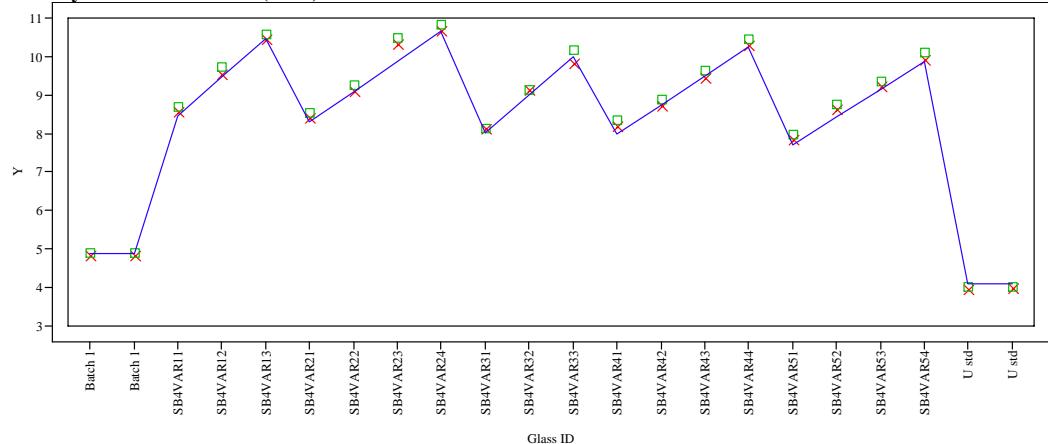


## Exhibit A6. Average Oxide Measurements by Solution ID for Samples Prepared Using the PF Method

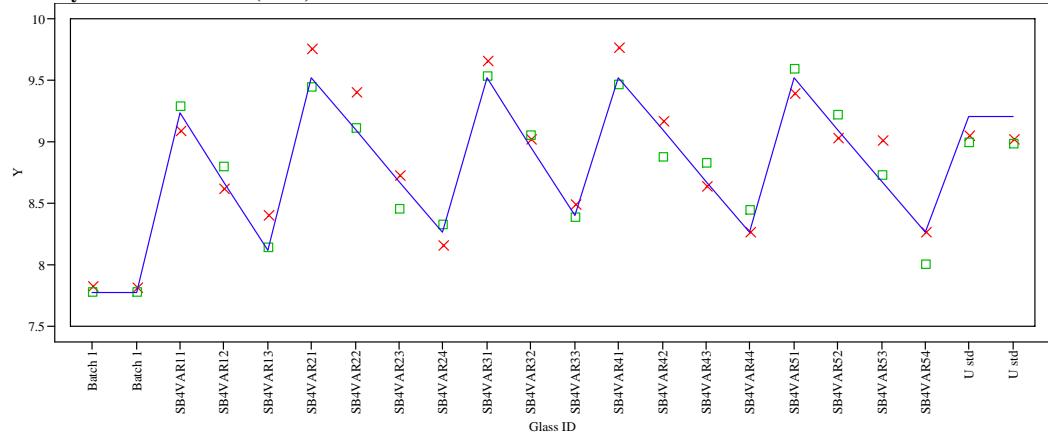


**Exhibit A7. Average Measured and Bias-Corrected (bc) Versus Targeted Compositions by Glass # by Oxide**

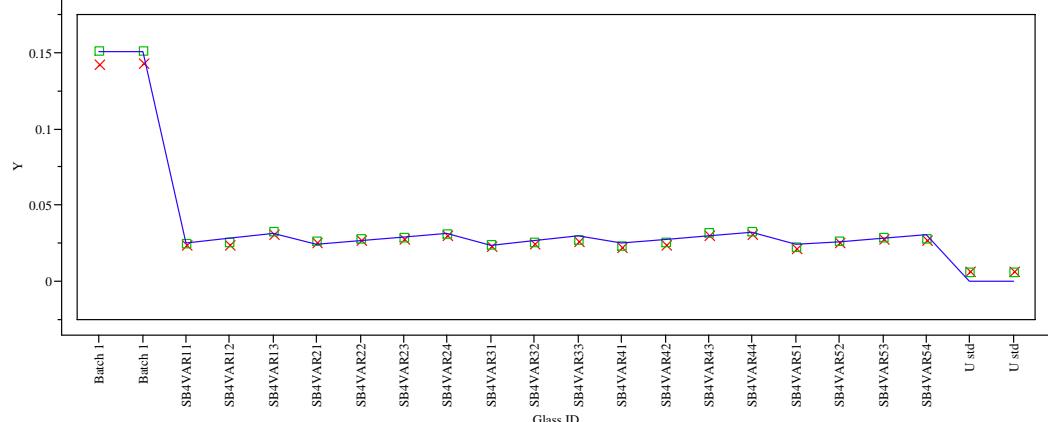
Overlay Plot Oxide=Al<sub>2</sub>O<sub>3</sub> (wt%)



Overlay Plot Oxide=B<sub>2</sub>O<sub>3</sub> (wt%)



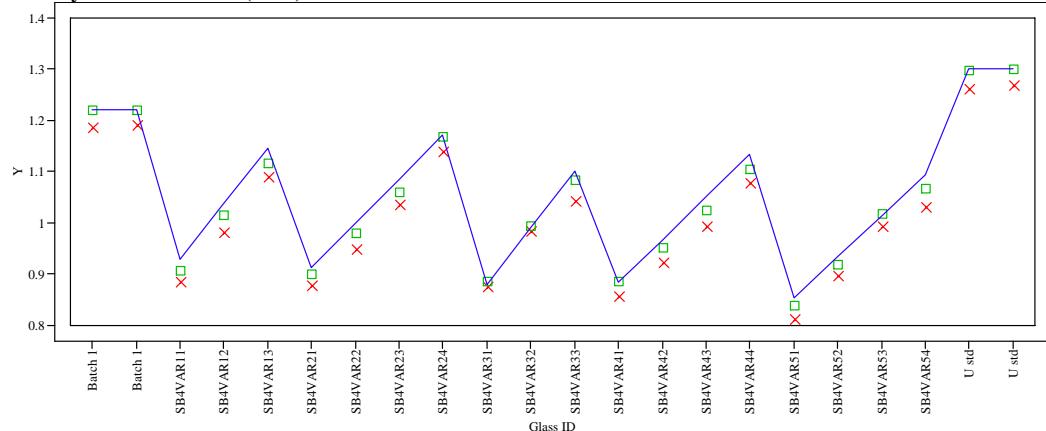
Overlay Plot Oxide=BaO (wt%)



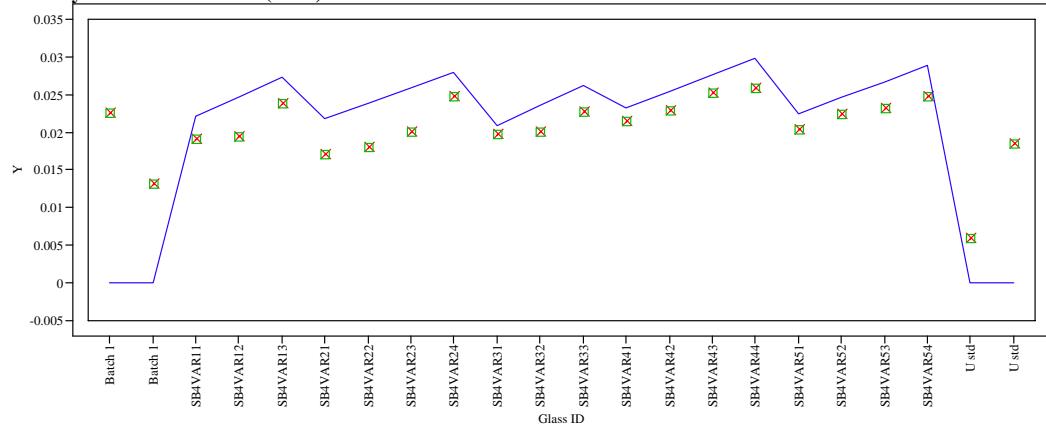
Y    x    Measured      ◻    Measured bc      —    Targeted

**Exhibit A7. Average Measured and Bias-Corrected (bc) Versus Targeted Compositions by Glass # by Oxide**

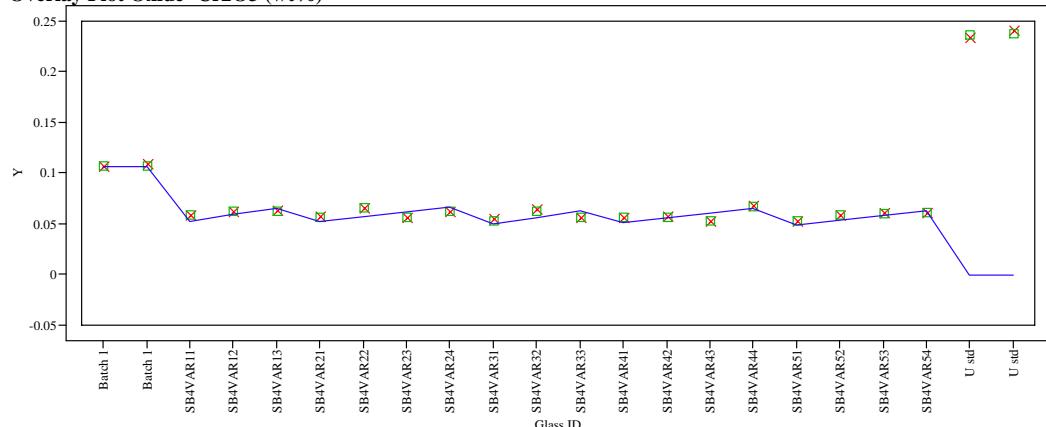
Overlay Plot Oxide=CaO (wt%)



Overlay Plot Oxide=Ce<sub>2</sub>O<sub>3</sub> (wt%)



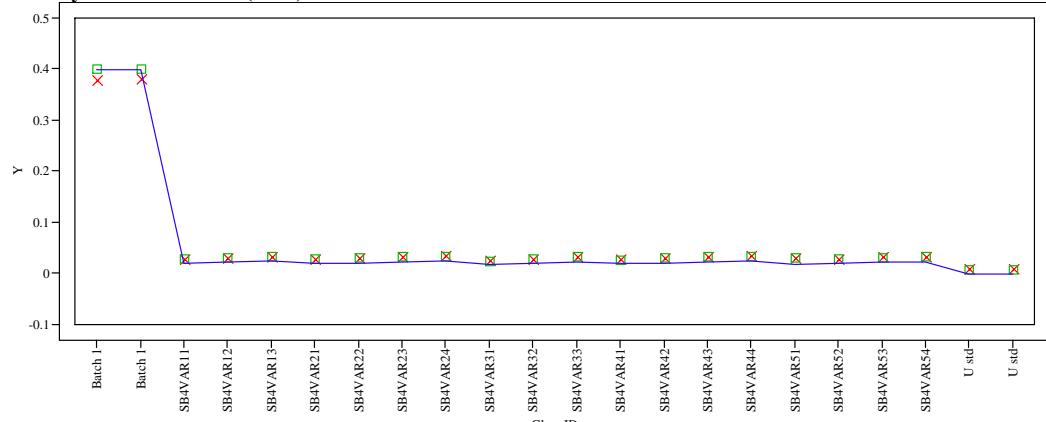
Overlay Plot Oxide=Cr<sub>2</sub>O<sub>3</sub> (wt%)



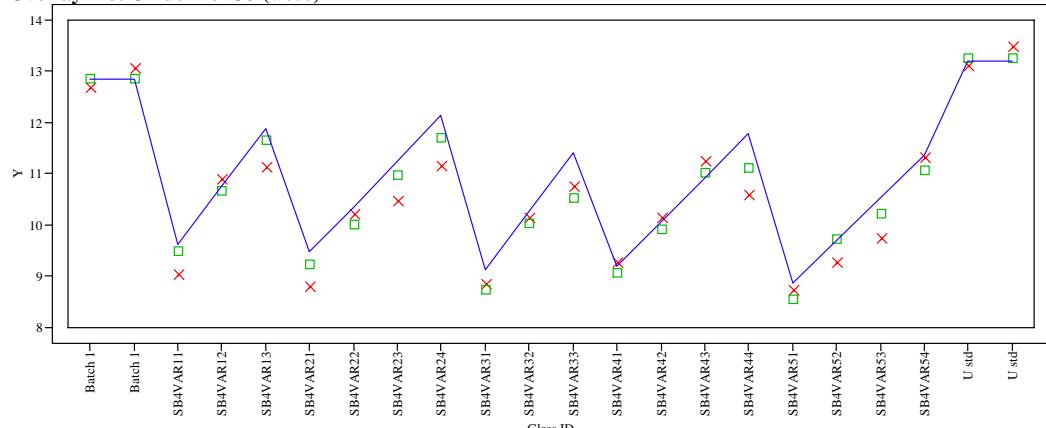
Y    x    Measured      ◻    Measured bc      —    Targeted

**Exhibit A7. Average Measured and Bias-Corrected (bc) Versus Targeted Compositions by Glass # by Oxide**

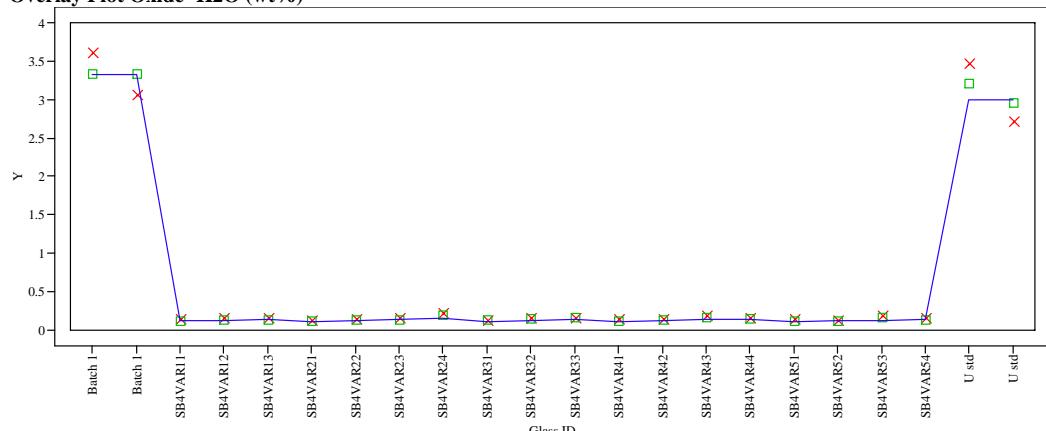
Overlay Plot Oxide=CuO (wt%)



Overlay Plot Oxide=Fe<sub>2</sub>O<sub>3</sub> (wt%)



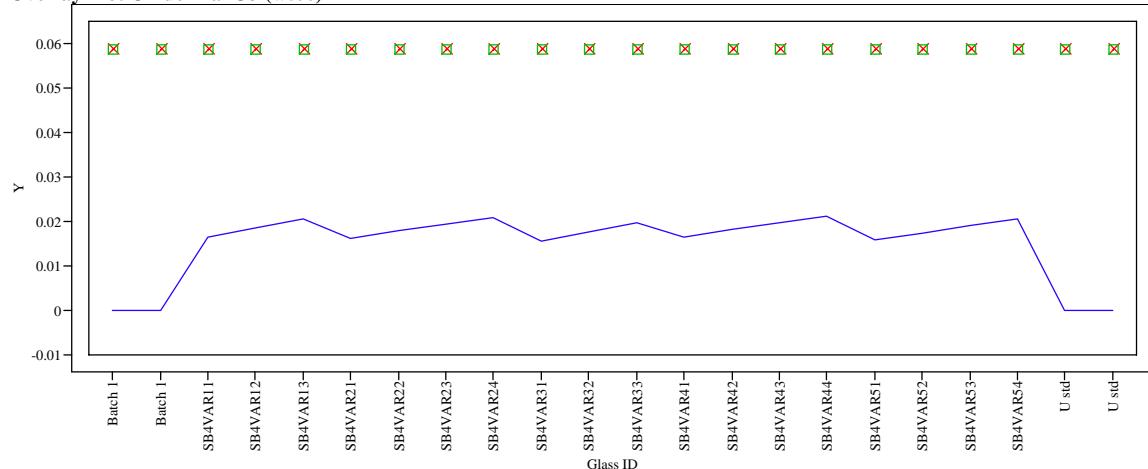
Overlay Plot Oxide=K<sub>2</sub>O (wt%)



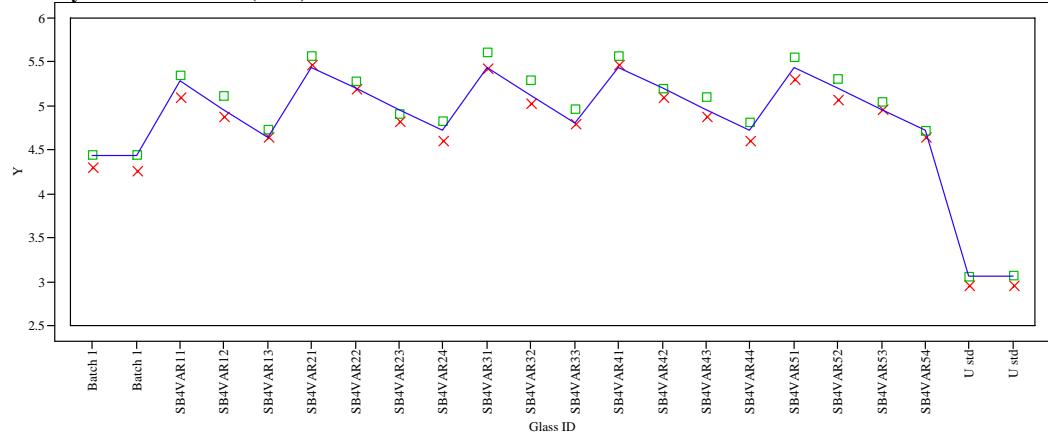
Y    x    Measured      ◻    Measured bc      — Targeted

**Exhibit A7. Average Measured and Bias-Corrected (bc) Versus Targeted Compositions by Glass # by Oxide**

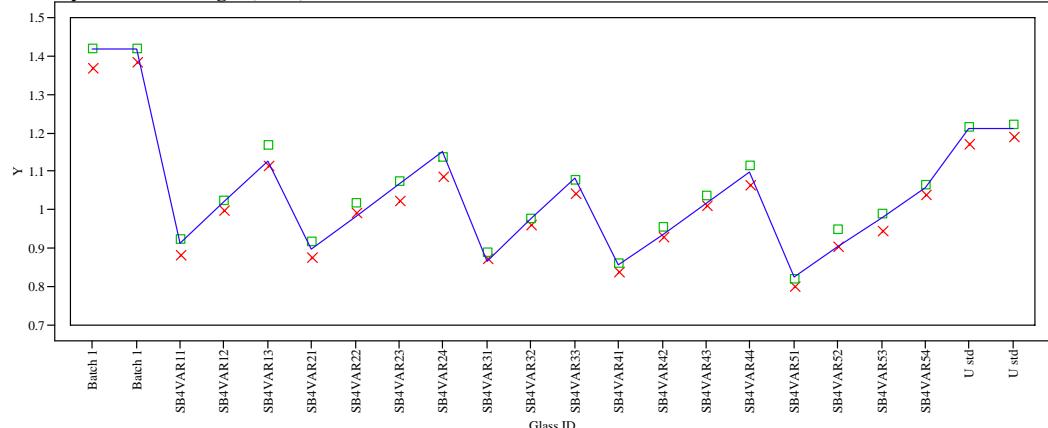
Overlay Plot Oxide=La<sub>2</sub>O<sub>3</sub> (wt%)



Overlay Plot Oxide=Li<sub>2</sub>O (wt%)



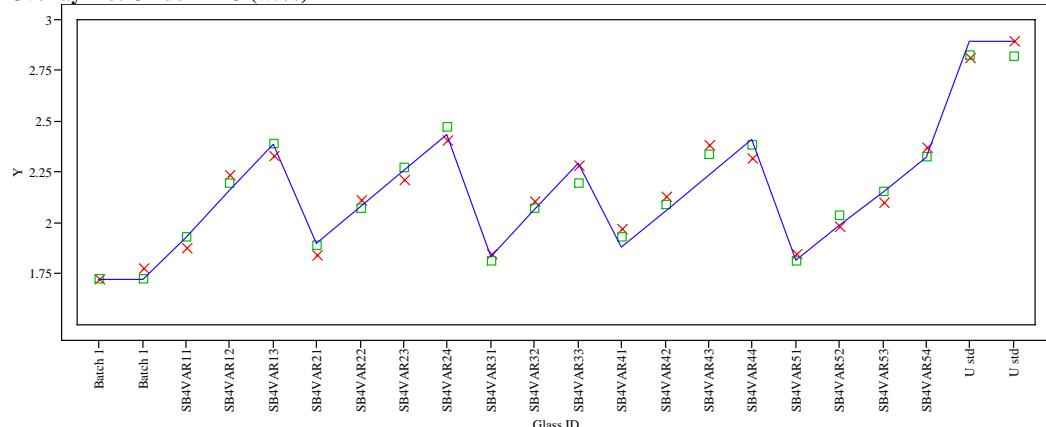
Overlay Plot Oxide=MgO (wt%)



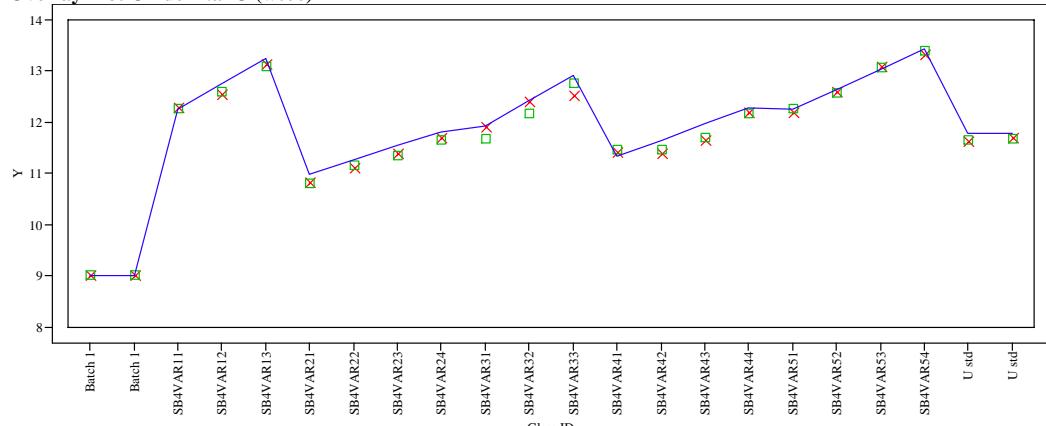
Y    x    Measured      ◻    Measured bc      — Targeted

**Exhibit A7. Average Measured and Bias-Corrected (bc) Versus Targeted Compositions by Glass # by Oxide**

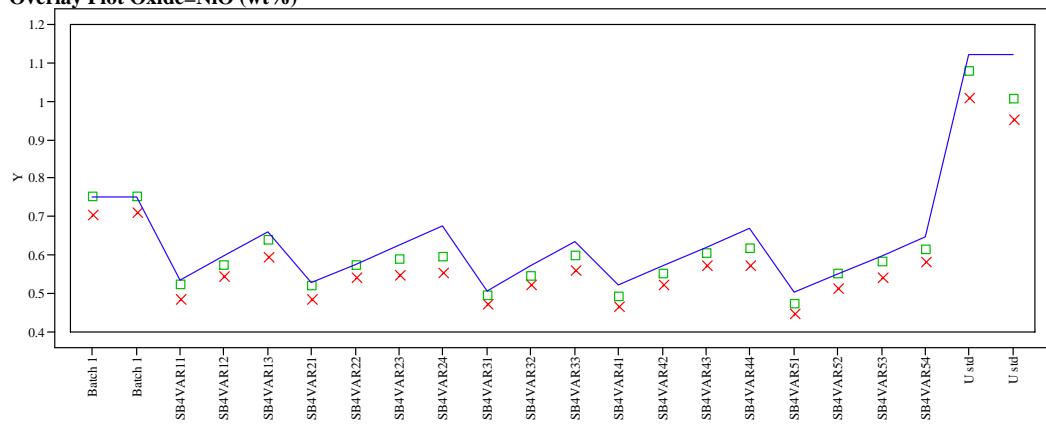
**Overlay Plot Oxide=MnO (wt%)**



**Overlay Plot Oxide=Na<sub>2</sub>O (wt%)**

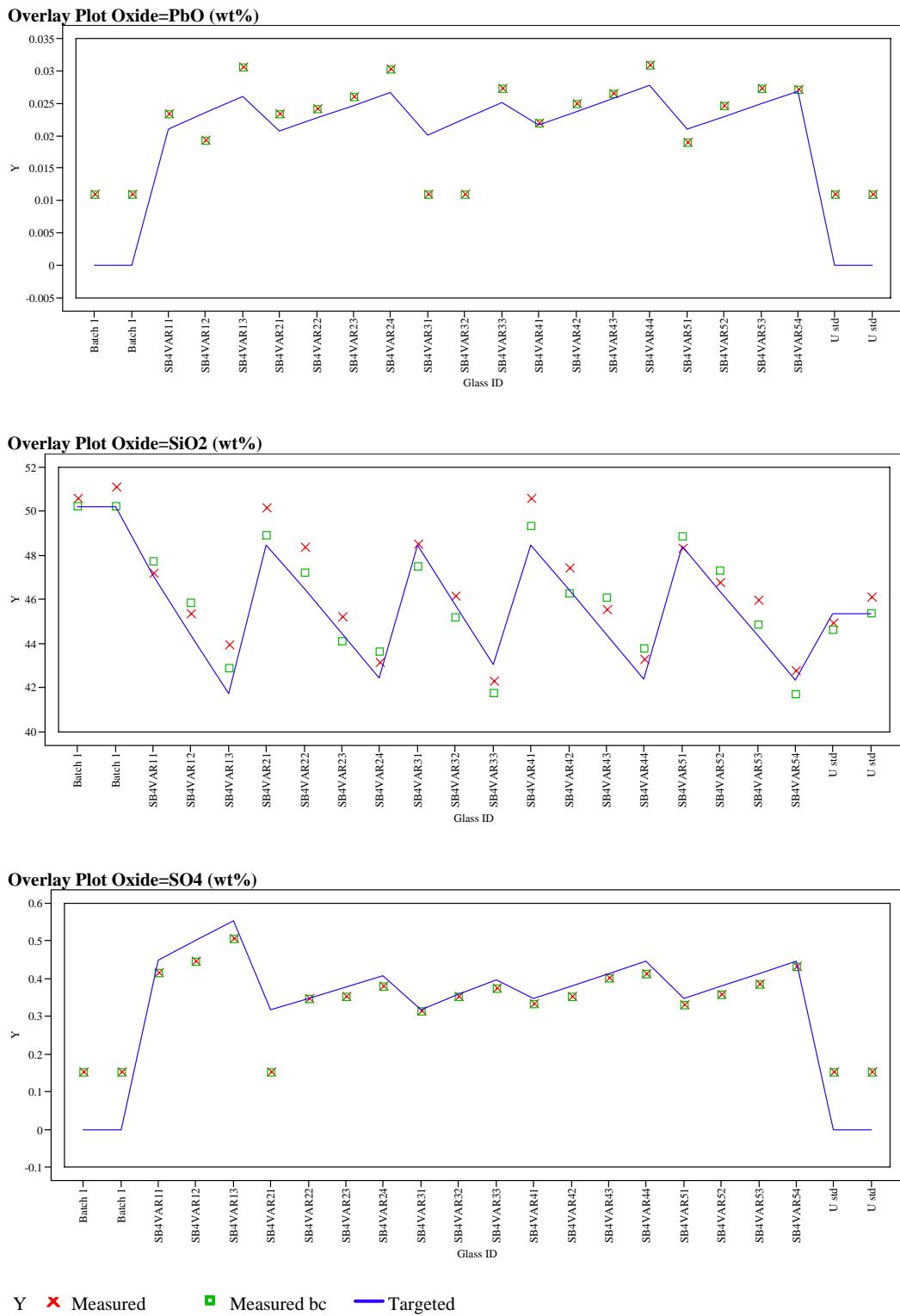


**Overlay Plot Oxide=NiO (wt%)**

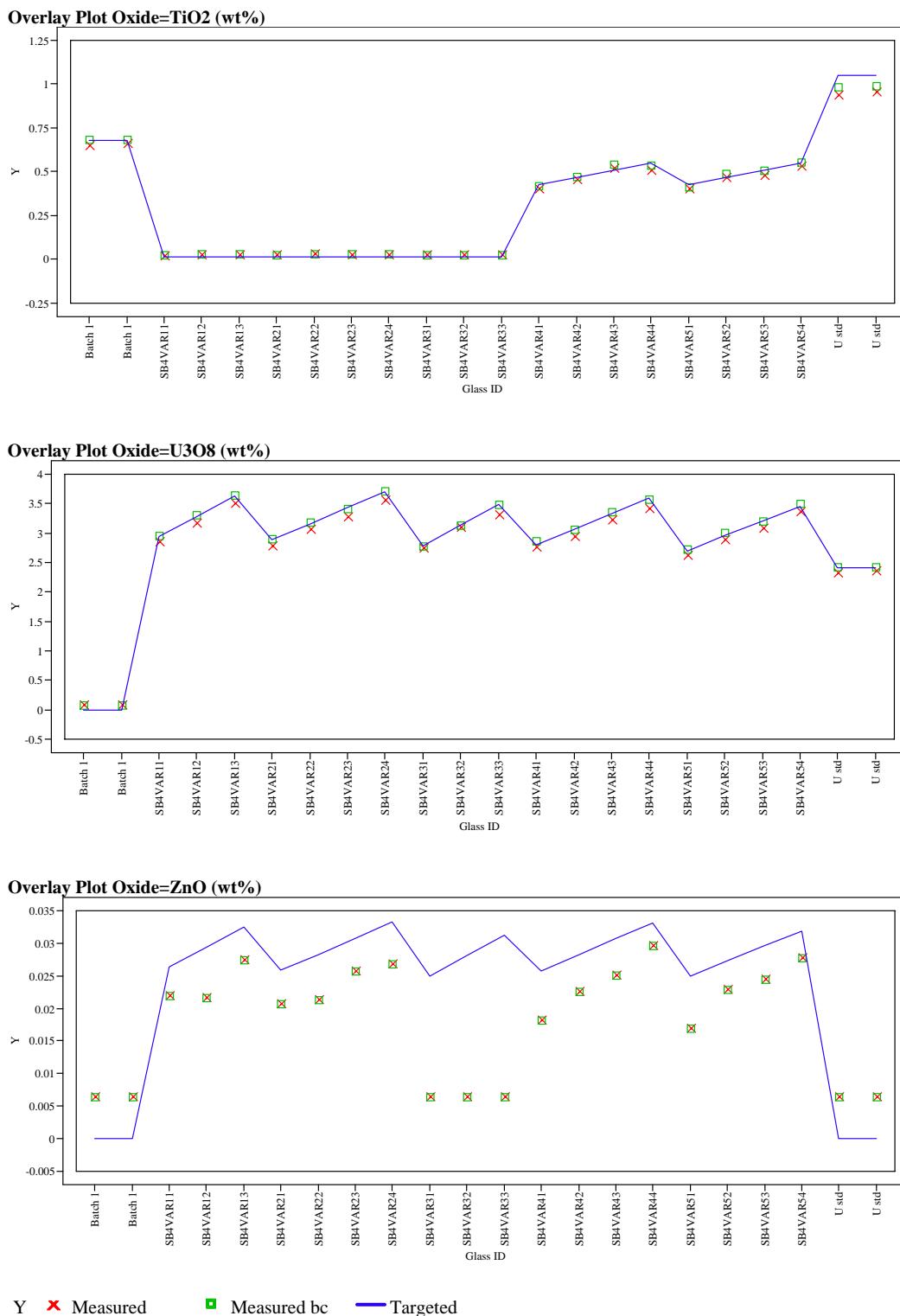


Y    X    Measured      □    Measured bc      — Targeted

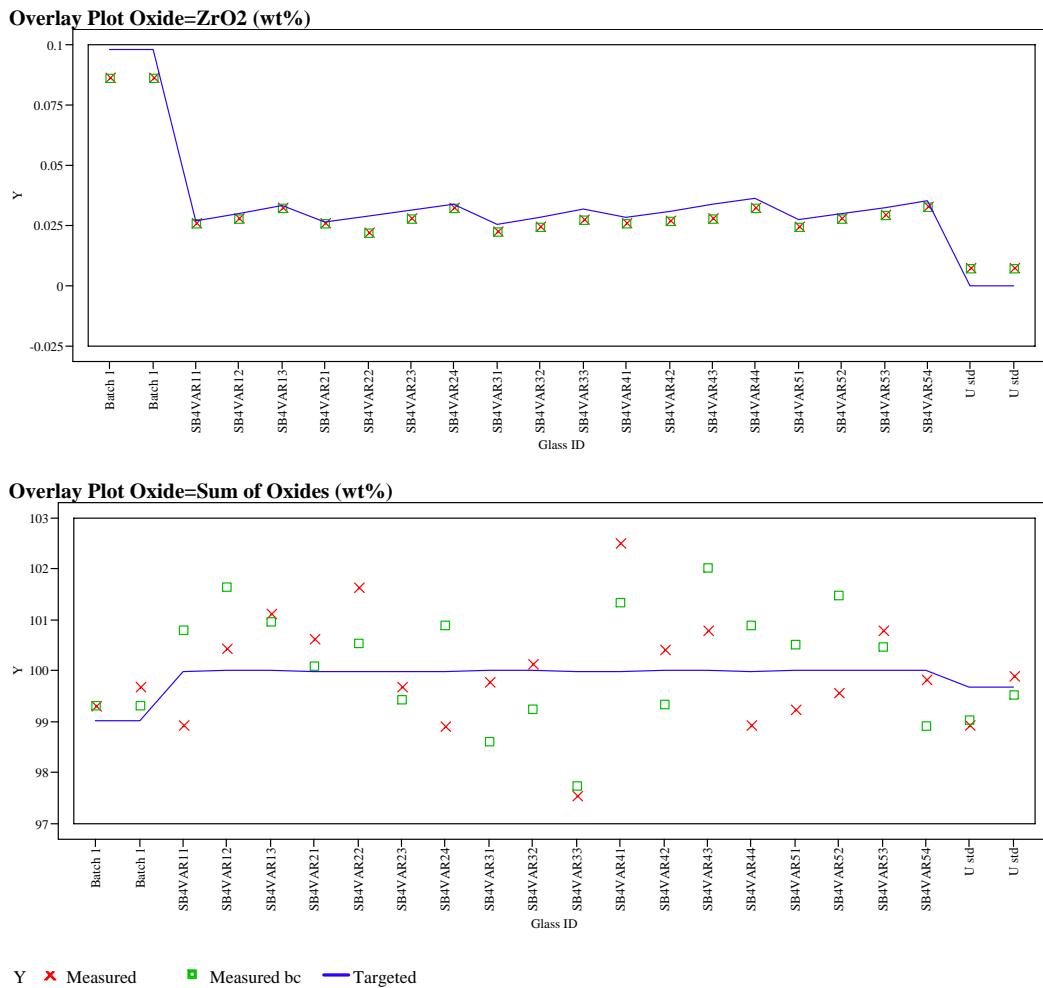
**Exhibit A7. Average Measured and Bias-Corrected (bc) Versus Targeted Compositions by Glass # by Oxide**



**Exhibit A7. Average Measured and Bias-Corrected (bc) Versus Targeted Compositions by Glass # by Oxide**



**Exhibit A7. Average Measured and Bias-Corrected (bc) Versus Targeted Compositions by Glass # by Oxide**



## **APPENDIX B**

### **TABLES AND EXHIBITS SUPPORTING THE ANALYSIS OF THE PCT RESULTS FOR THE SB4-DECANT VARIABILITY STUDY GLASSES**

*This page intentionally left blank.*

**Table B1. PSAL Measurements of the PCT Solutions for the Study Glasses As-Received (ar) and After Appropriate Adjustments (in ppm)**

Set	Glass ID (w HT)	Block	Seq	Lab ID	B ar	Li ar	Na ar	Si ar	B (ppm)	Li (ppm)	Na (ppm)	Si (ppm)
q	Soln Std	1	1	STD-11-1	20.6	9.81	79.9	49.1	20.600	9.810	79.900	49.100
q	SB4VAR21ccc	1	2	Q49	12.1	11	29.1	61.3	20.167	18.334	48.501	102.169
q	SB4VAR54ccc	1	3	Q47	16.1	13.1	54.2	61.6	26.834	21.834	90.335	102.669
q	EA	1	4	Q67	34.3	10.6	91.8	50.4	571.668	176.667	1530.003	840.002
q	SB4VAR22	1	5	Q30	12.3	10.8	31.8	58.2	20.500	18.000	53.001	97.002
q	SB4VAR44	1	6	Q25	12.1	10.2	40.2	55.2	20.167	17.000	67.001	92.002
q	SB4VAR21	1	7	Q69	11.9	10.9	30.2	59.4	19.834	18.167	50.334	99.002
q	SB4VAR42ccc	1	8	Q45	11.9	10.8	34.3	58.6	19.834	18.000	57.168	97.669
q	SB4VAR23	1	9	Q14	11.8	10.5	35.2	54.7	19.667	17.500	58.668	91.168
q	SB4VAR41	1	10	Q59	12.3	11.2	33.9	61	20.500	18.667	56.501	101.669
q	SB4VAR51	1	11	Q53	11.9	10.6	36.7	58.8	19.834	17.667	61.168	98.002
q	ARM-1	1	12	Q24	12.3	9.44	25.3	39.3	20.500	15.734	42.168	65.501
q	SB4VAR22ccc	1	13	Q79	11.6	10.6	32.9	57.8	19.334	17.667	54.834	96.335
q	blank	1	14	Q23	<1.00	<1.00	<1.00	<1.00	0.833	0.833	0.833	0.083
q	Soln Std	1	15	STD-11-2	19.7	9.94	81.5	48.8	19.700	9.940	81.500	48.800
q	SB4VAR42	1	16	Q42	12.2	10.8	35.7	59	20.334	18.000	59.501	98.335
q	SB4VAR24	1	17	Q52	12.5	10.7	39.3	55.3	20.834	17.834	65.501	92.169
q	SB4VAR52	1	18	Q19	12.6	10.9	41.2	60.3	21.000	18.167	68.668	100.502
q	SB4VAR44ccc	1	19	Q01	13.7	11.8	43.1	56.7	22.834	19.667	71.835	94.502
q	SB4VAR24ccc	1	20	Q71	28.2	22.3	60.6	72.4	47.001	37.167	101.002	120.669
q	SB4VAR41ccc	1	21	Q48	13.1	12	34.3	65.4	21.834	20.000	57.168	109.002
q	SB4VAR53ccc	1	22	Q61	12.3	10.8	43.9	58.1	20.500	18.000	73.168	96.835
q	SB4VAR53	1	23	Q51	12.6	10.8	46.8	59.1	21.000	18.000	78.002	98.502
q	SB4VAR52ccc	1	24	Q13	12.4	11	41	60.9	20.667	18.334	68.335	101.502
q	SB4VAR43	1	25	Q80	11.8	10.6	38.3	57.1	19.667	17.667	63.835	95.169
q	SB4VAR43ccc	1	26	Q77	11.5	10.4	36.8	55.4	19.167	17.334	61.335	92.335
q	SB4VAR51ccc	1	27	Q60	12.6	11.5	37.4	63.5	21.000	19.167	62.335	105.835
q	SB4VAR54	1	28	Q76	12.3	10.3	49.2	55.8	20.500	17.167	82.002	93.002
q	SB4VAR23ccc	1	29	Q18	12.3	10.9	36.6	57	20.500	18.167	61.001	95.002
q	Soln Std	1	30	STD-11-3	20.3	10.1	82.2	50.2	20.300	10.100	82.200	50.200
q	Soln Std	2	1	STD-12-1	20.7	9.74	78.2	50.3	20.700	9.740	78.200	50.300
q	ARM-1	2	2	Q28	11.9	8.7	23.1	38.2	19.834	14.500	38.501	63.668
q	SB4VAR23ccc	2	3	Q12	12.3	10.5	34	57.7	20.500	17.500	56.668	96.169
q	SB4VAR52	2	4	Q03	12.5	10.7	40.8	61	20.834	17.834	68.001	101.669
q	SB4VAR21ccc	2	5	Q75	11.7	10.7	30.7	61.1	19.500	17.834	51.168	101.835
q	SB4VAR54	2	6	Q08	12.6	10.4	49	58.5	21.000	17.334	81.668	97.502
q	SB4VAR24	2	7	Q09	12.1	10.4	38	56.1	20.167	17.334	63.335	93.502
q	SB4VAR23	2	8	Q74	11.8	10.6	35.4	57.3	19.667	17.667	59.001	95.502
q	SB4VAR44ccc	2	9	Q63	13.4	11.9	43	58.1	22.334	19.834	71.668	96.835
q	SB4VAR53	2	10	Q07	12.1	10.5	45.8	59.9	20.167	17.500	76.335	99.835
q	SB4VAR44	2	11	Q29	11	9.64	38.4	53.8	18.334	16.067	64.001	89.668
q	SB4VAR24ccc	2	12	Q55	27.6	21.8	59.1	73.2	46.001	36.334	98.502	122.002
q	SB4VAR43ccc	2	13	Q41	11.2	10	35.5	56.8	18.667	16.667	59.168	94.669
q	SB4VAR21	2	14	Q32	12	11.3	31.2	62.6	20.000	18.834	52.001	104.335
q	Soln Std	2	15	STD-12-2	20	9.9	81.5	50.8	20.000	9.900	81.500	50.800
q	SB4VAR52ccc	2	16	Q02	12.7	11	39.6	63.7	21.167	18.334	66.001	106.169
q	SB4VAR42ccc	2	17	Q26	12.4	11.2	35.5	63.1	20.667	18.667	59.168	105.169
q	SB4VAR54ccc	2	18	Q64	16.1	13.2	53.9	63.6	26.834	22.000	89.835	106.002
q	SB4VAR22	2	19	Q10	12.1	11	32.3	61.2	20.167	18.334	53.834	102.002
q	SB4VAR41	2	20	Q44	12.4	11.4	32.5	64.1	20.667	19.000	54.168	106.835
q	SB4VAR42	2	21	Q34	11.9	10.8	33.8	61.1	19.834	18.000	56.334	101.835
q	EA	2	22	Q31	39	11.4	99.3	56.6	650.001	190.000	1655.003	943.335
q	SB4VAR51	2	23	Q06	12.9	11.2	36.1	65.3	21.500	18.667	60.168	108.836
q	SB4VAR43	2	24	Q70	12.5	10.8	37.1	61.4	20.834	18.000	61.835	102.335
q	SB4VAR41ccc	2	25	Q65	13	11.8	32.5	67.9	21.667	19.667	54.168	113.169
q	SB4VAR53ccc	2	26	Q38	12.2	10.7	42.7	60.6	20.334	17.834	71.168	101.002
q	SB4VAR22ccc	2	27	Q15	11.5	10.6	32.7	59.7	19.167	17.667	54.501	99.502
q	SB4VAR51ccc	2	28	Q16	12.3	11.4	36.9	64.6	20.500	19.000	61.501	107.669
q	Soln Std	2	29	STD-12-3	20.1	9.9	80.7	50.8	20.100	9.900	80.700	50.800
q	Soln Std	3	1	STD-13-1	20	9.75	79.3	50.5	20.000	9.750	79.300	50.500

**Table B1. PSAL Measurements of the PCT Solutions for the Study Glasses As-Received (ar) and After Appropriate Adjustments (in ppm)**

Set	Glass ID (w HT)	Block	Seq	Lab ID	B ar	Li ar	Na ar	Si ar	B (ppm)	Li (ppm)	Na (ppm)	Si (ppm)
q	SB4VAR53	3	2	Q04	11.2	10.1	44.8	56.6	18.667	16.834	74.668	94.335
q	SB4VAR52ccc	3	3	Q68	11.2	10.4	38.9	59.1	18.667	17.334	64.835	98.502
q	SB4VAR22ccc	3	4	Q78	11.1	10.4	31.3	58.2	18.500	17.334	52.168	97.002
q	EA	3	5	Q62	37.5	11.5	102	55.4	625.001	191.667	1700.003	923.335
q	SB4VAR42	3	6	Q58	11.2	10.5	34.2	59	18.667	17.500	57.001	98.335
q	SB4VAR53ccc	3	7	Q57	11	10	41.4	57.6	18.334	16.667	69.001	96.002
q	SB4VAR22	3	8	Q43	11.1	10.6	30.9	58.1	18.500	17.667	51.501	96.835
q	SB4VAR23ccc	3	9	Q73	10.8	10.3	33.7	56.3	18.000	17.167	56.168	93.835
q	SB4VAR42ccc	3	10	Q17	11	10.7	33.6	59.6	18.334	17.834	56.001	99.335
q	SB4VAR54	3	11	Q39	11.3	9.85	47.2	56.5	18.834	16.417	78.668	94.169
q	SB4VAR51ccc	3	12	Q33	11.2	11	35.1	62.3	18.667	18.334	58.501	103.835
q	SB4VAR43	3	13	Q27	10.4	9.92	37.3	56.6	17.334	16.534	62.168	94.335
q	SB4VAR51	3	14	Q72	11.4	10.9	37.3	61.8	19.000	18.167	62.168	103.002
q	Soln Std	3	15	STD-13-2	19.1	9.8	78.9	50.4	19.100	9.800	78.900	50.400
q	SB4VAR43ccc	3	16	Q36	10.7	10.1	33.8	56.6	17.834	16.834	56.334	94.335
q	SB4VAR44ccc	3	17	Q37	12.9	11.5	40.6	57.6	21.500	19.167	67.668	96.002
q	SB4VAR24ccc	3	18	Q66	26.5	21.1	56.9	71.3	44.168	35.167	94.835	118.836
q	SB4VAR54ccc	3	19	Q56	14.9	12.6	50.4	61.1	24.834	21.000	84.002	101.835
q	blank	3	20	Q20	<1.00	<1.00	<1.00	0.142	0.833	0.833	0.833	0.237
q	SB4VAR24	3	21	Q40	10.9	10.1	35.6	53.9	18.167	16.834	59.335	89.835
q	SB4VAR21ccc	3	22	Q35	10.6	10.4	27.7	59.4	17.667	17.334	46.168	99.002
q	SB4VAR52	3	23	Q22	11.1	10.5	38.5	59.9	18.500	17.500	64.168	99.835
q	SB4VAR44	3	24	Q50	10.4	9.85	38.3	53.1	17.334	16.417	63.835	88.502
q	SB4VAR41	3	25	Q54	10.5	10.5	30.2	58.9	17.500	17.500	50.334	98.169
q	ARM-1	3	26	Q46	9.5	8.24	21.2	36.1	15.834	13.734	35.334	60.168
q	SB4VAR21	3	27	Q05	10.7	10.7	28.1	59.7	17.834	17.834	46.834	99.502
q	SB4VAR23	3	28	Q11	10.5	10	32.4	54	17.500	16.667	54.001	90.002
q	SB4VAR41ccc	3	29	Q21	10.9	10.9	30.1	62	18.167	18.167	50.168	103.335
q	Soln Std	3	30	STD-13-3	19.1	10.1	83.1	50.3	19.100	10.100	83.100	50.300
r	Soln Std	1	1	STD-21-1	20.5	9.89	79.3	50.7	20.500	9.890	79.300	50.700
r	EA	1	2	R62	36.5	11	98.2	53.3	608.335	183.334	1636.670	888.335
r	SB5-17	1	3	R55	11.9	11.3	34.1	59.4	19.834	18.834	56.834	99.002
r	SB4VAR13ccc	1	4	R09	23.8	17.9	65.9	71.6	39.667	29.834	109.836	119.336
r	SB5-18ccc	1	5	R38	11.7	8.53	45.8	58	19.500	14.217	76.335	96.669
r	SB4VAR33	1	6	R77	12.5	10.3	44.9	57.5	20.834	17.167	74.835	95.835
r	SB4VAR11ccc	1	7	R06	12.2	10.6	35.2	61.1	20.334	17.667	58.668	101.835
r	SB5-14ccc	1	8	R49	11.1	10.5	60.5	68.5	18.500	17.500	100.835	114.169
r	SB5-17ccc	1	9	R45	11.3	10.5	32	58.4	18.834	17.500	53.334	97.335
r	SB4VAR33ccc	1	10	R84	13.1	10.7	43.6	59.1	21.834	17.834	72.668	98.502
r	SB5-20ccc	1	11	R26	11.7	4.55	39	49.9	19.500	7.583	65.001	83.168
r	SB4VAR32	1	12	R52	12.3	10.4	37.7	59.9	20.500	17.334	62.835	99.835
r	SB5-16	1	13	R68	15	6.42	55.3	56.2	25.001	10.700	92.169	93.669
r	ARM-1	1	14	R17	10.2	8.03	21.1	36	17.000	13.384	35.167	60.001
r	SB5-15	1	15	R69	13.3	8.12	58.9	59.2	22.167	13.534	98.169	98.669
r	Soln Std	1	16	STD-21-2	19.8	9.69	79.1	49.4	19.800	9.690	79.100	49.400
r	SB5-16ccc	1	17	R61	13.8	5.94	48.2	54.4	23.000	9.900	80.335	90.668
r	SB4VAR12	1	18	R85	12.9	10.5	41.5	59.1	21.500	17.500	69.168	98.502
r	SB5-15ccc	1	19	R78	12.8	7.93	51.6	57.3	21.334	13.217	86.002	95.502
r	SB4VAR13	1	20	R57	13.3	10.5	48.7	56.6	22.167	17.500	81.168	94.335
r	SB5-20	1	21	R31	11.8	4.44	41.1	48.3	19.667	7.400	68.501	80.502
r	SB4VAR31	1	22	R30	12.4	10.9	34.3	61.2	20.667	18.167	57.168	102.002
r	blank	1	23	R08	<1.00	<1.00	<1.00	0.116	0.833	0.833	0.833	0.193
r	SB4VAR12ccc	1	24	R46	12.2	10.3	46.2	57.7	20.334	17.167	77.002	96.169
r	SB5-18	1	25	R48	11.7	8.35	46.7	57.4	19.500	13.917	77.835	95.669
r	SB4VAR11	1	26	R01	12.7	10.7	36.9	62	21.167	17.834	61.501	103.335
r	SB4VAR31ccc	1	27	R59	12.4	11.1	34.3	62.2	20.667	18.500	57.168	103.669
r	SB5-19	1	28	R65	12.3	5.63	51.5	52.8	20.500	9.384	85.835	88.002
r	SB4VAR32ccc	1	29	R02	12	10.4	38.4	58.4	20.000	17.334	64.001	97.335
r	SB5-19ccc	1	30	R37	11.9	5.66	49.7	51.8	19.834	9.434	82.835	86.335
r	SB5-14	1	31	R53	11.1	10.2	64.4	67.8	18.500	17.000	107.335	113.002

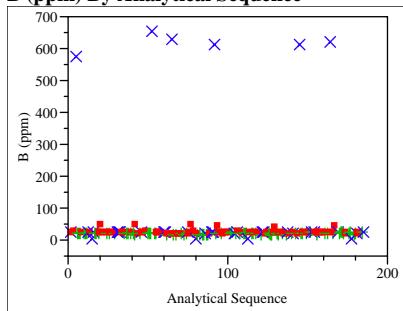
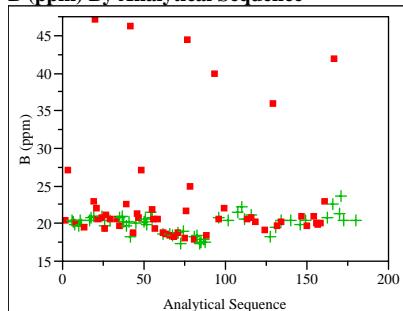
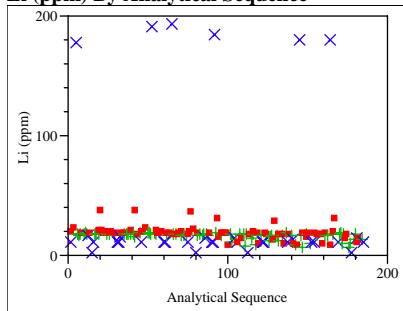
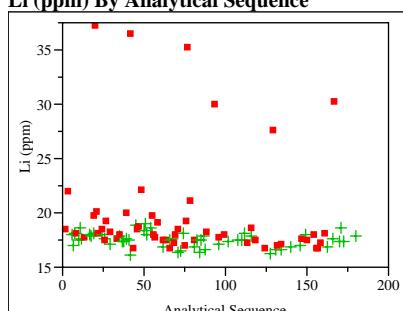
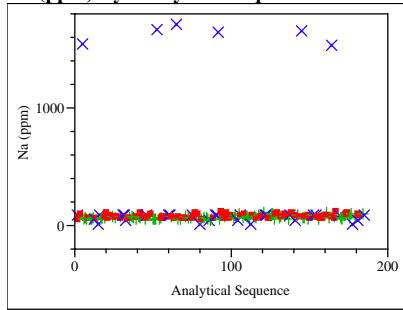
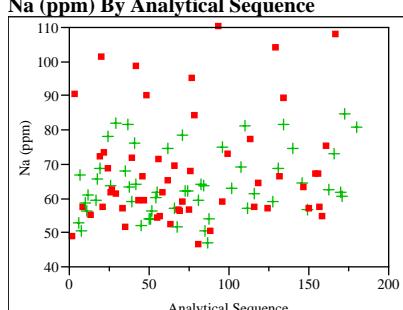
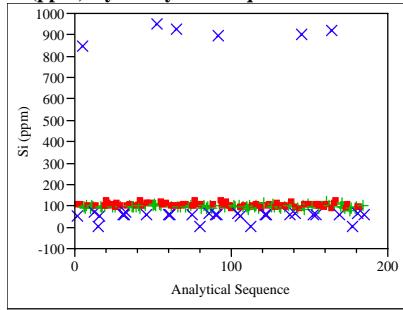
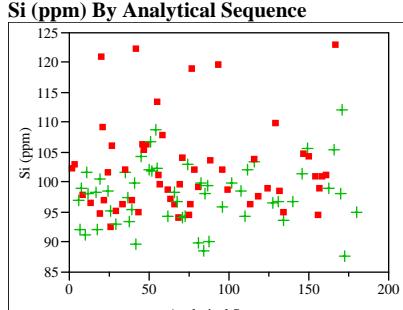
**Table B1. PSAL Measurements of the PCT Solutions for the Study Glasses As-  
Received (ar) and After Appropriate Adjustments (in ppm)**

Set	Glass ID (w HT)	Block	Seq	Lab ID	B ar	Li ar	Na ar	Si ar	B (ppm)	Li (ppm)	Na (ppm)	Si (ppm)
r	Soln Std	1	32	STD-21-3	20.1	9.82	79.4	49.9	20.100	9.820	79.400	49.900
r	Soln Std	2	1	STD-22-1	20.1	9.63	78.7	50.8	20.100	9.630	78.700	50.800
r	SB5-17ccc	2	2	R83	10.8	10.4	31.5	58.1	18.000	17.334	52.501	96.835
r	SB4VAR11ccc	2	3	R03	11.4	10	34.1	59.3	19.000	16.667	56.834	98.835
r	SB5-15	2	4	R20	12.3	7.6	56.8	56.8	20.500	12.667	94.669	94.669
r	SB5-14	2	5	R54	10.1	9.53	61.3	65	16.834	15.884	102.169	108.336
r	SB4VAR11	2	6	R13	11	9.73	35.4	57.9	18.334	16.217	59.001	96.502
r	SB5-15ccc	2	7	R80	11.4	7.42	52.8	55.1	19.000	12.367	88.002	91.835
r	SB4VAR13ccc	2	8	R47	21.5	16.5	62.3	65.8	35.834	27.501	103.835	109.669
r	SB4VAR12	2	9	R82	11.7	10	41.3	58.1	19.500	16.667	68.835	96.835
r	SB5-18	2	10	R66	10.4	7.51	44.6	54.6	17.334	12.517	74.335	91.002
r	SB4VAR12ccc	2	11	R32	11.7	10.1	39.7	59	19.500	16.834	66.168	98.335
r	SB4VAR13	2	12	R40	12.2	10	48.9	56.2	20.334	16.667	81.502	93.669
r	SB4VAR33ccc	2	13	R74	12	10.2	53.4	56.9	20.000	17.000	89.002	94.835
r	SB5-19ccc	2	14	R50	11.2	5.38	48.9	52.3	18.667	8.967	81.502	87.168
r	SB5-17	2	15	R27	11.1	11	34.3	60.2	18.500	18.334	57.168	100.335
r	Soln Std	2	16	STD-22-2	19.6	9.64	80.1	50.9	19.600	9.640	80.100	50.900
r	SB5-14ccc	2	17	R81	10.4	10.1	60.5	68.1	17.334	16.834	100.835	113.502
r	SB4VAR33	2	18	R42	12.2	10.1	44.7	58.1	20.334	16.834	74.501	96.835
r	ARM-1	2	19	R25	9.64	7.65	20.5	35.6	16.067	12.750	34.167	59.335
r	SB5-16ccc	2	20	R35	12.4	5.52	47.9	52.6	20.667	9.200	79.835	87.668
r	SB5-19	2	21	R41	12.2	5.6	52.9	53.6	20.334	9.334	88.168	89.335
r	SB5-20ccc	2	22	R19	11.1	4.34	40.6	49.6	18.500	7.233	67.668	82.668
r	EA	2	23	R51	36.6	10.7	98.6	53.8	610.001	178.334	1643.337	896.668
r	SB4VAR32	2	24	R36	11.9	10.2	38.8	60.9	19.834	17.000	64.668	101.502
r	SB5-20	2	25	R11	11.7	4.3	41.1	51.1	19.500	7.167	68.501	85.168
r	SB4VAR32ccc	2	26	R34	12.5	10.5	37.8	62.7	20.834	17.500	63.001	104.502
r	SB4VAR31	2	27	R24	12.3	10.8	34.1	63.4	20.500	18.000	56.834	105.669
r	SB5-18ccc	2	28	R12	11.5	8.4	46.1	59.9	19.167	14.000	76.835	99.835
r	SB4VAR31ccc	2	29	R72	11.7	10.4	34.1	62.4	19.500	17.334	56.834	104.002
r	SB5-16	2	30	R70	14.8	6.11	55.1	57.2	24.667	10.184	91.835	95.335
r	Soln Std	2	31	STD-22-3	21.5	10.1	81.5	54.3	21.500	10.100	81.500	54.300
r	Soln Std	3	1	STD-23-1	20.8	9.7	79.1	49.9	20.800	9.700	79.100	49.900
r	SB4VAR32ccc	3	2	R73	12.5	10.7	40.2	60.4	20.834	17.834	67.001	100.669
r	SB5-17	3	3	R60	11.1	10.1	31.8	54.8	18.500	16.834	53.001	91.335
r	SB4VAR12ccc	3	4	R23	11.9	10	40.1	56.6	19.834	16.667	66.835	94.335
r	SB4VAR11ccc	3	5	R15	11.8	10	34.2	59.2	19.667	16.667	57.001	98.669
r	SB4VAR31ccc	3	6	R58	11.9	10.3	32.7	60.5	19.834	17.167	54.501	100.835
r	SB5-19ccc	3	7	R76	12.5	5.46	48.4	54.5	20.834	9.100	80.668	90.835
r	SB5-14	3	8	R79	11.5	10	63.7	70.2	19.167	16.667	106.169	117.002
r	SB4VAR33ccc	3	9	R63	13.7	10.8	45.1	60.6	22.834	18.000	75.168	101.002
r	SB4VAR32	3	10	R67	12.5	10.1	37.5	59.4	20.834	16.834	62.501	99.002
r	EA	3	11	R64	36.9	10.7	91.3	55	615.001	178.334	1521.670	916.669
r	SB5-20ccc	3	12	R22	12.6	4.39	40.2	51.4	21.000	7.317	67.001	85.668
r	SB4VAR12	3	13	R44	13.6	10.6	43.9	63.3	22.667	17.667	73.168	105.502
r	SB5-17ccc	3	14	R07	12.6	11.2	33	64.2	21.000	18.667	55.001	107.002
r	SB4VAR13ccc	3	15	R28	25	18.1	64.6	73.7	41.668	30.167	107.669	122.836
r	Soln Std	3	16	STD-23-2	22	10.1	80	54.6	22.000	10.100	80.000	54.600
r	SB4VAR11	3	17	R33	12.8	10.4	37.1	58.9	21.334	17.334	61.835	98.169
r	SB4VAR31	3	18	R04	14.2	11.2	36.4	67.2	23.667	18.667	60.668	112.002
r	SB5-19	3	19	R86	14	6	56	57.2	23.334	10.000	93.335	95.335
r	SB4VAR13	3	20	R10	12.3	10.4	50.9	52.6	20.500	17.334	84.835	87.668
r	SB5-15ccc	3	21	R16	11.4	7.68	55.1	51.2	19.000	12.800	91.835	85.335
r	SB5-14ccc	3	22	R71	9.94	10.2	62.5	60.3	16.567	17.000	104.169	100.502
r	SB5-20	3	23	R56	11.3	4.29	42.3	46.7	18.834	7.150	70.501	77.835
r	SB5-16	3	24	R75	13.8	6.17	58	53.3	23.000	10.284	96.669	88.835
r	blank	3	25	R39	<1.00	<1.00	<1.00	0.456	0.833	0.833	0.833	0.760
r	SB5-18	3	26	R21	10.9	8.22	49.7	53.5	18.167	13.700	82.835	89.168
r	SB4VAR33	3	27	R18	12.3	10.7	48.4	57	20.500	17.834	80.668	95.002
r	ARM-1	3	28	R29	10.1	8.25	23.2	35	16.834	13.750	38.667	58.335

**Table B1. PSAL Measurements of the PCT Solutions for the Study Glasses As-  
Received (ar) and After Appropriate Adjustments (in ppm)**

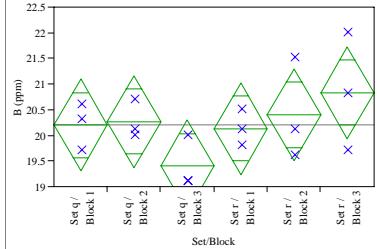
Set	Glass ID (w HT)	Block	Seq	Lab ID	B ar	Li ar	Na ar	Si ar	B (ppm)	Li (ppm)	Na (ppm)	Si (ppm)
r	SB5-16ccc	3	29	R14	13.7	6.3	55.1	53.2	22.834	10.500	91.835	88.668
r	SB5-18ccc	3	30	R43	10.8	8.28	48.5	54.2	18.000	13.800	80.835	90.335
r	SB5-15	3	31	R05	14.4	8.23	58.7	61.6	24.000	13.717	97.835	102.669
r	Soln Std	3	32	STD-23-3	19.7	10.2	83.1	50	19.700	10.200	83.100	50.000

**Exhibit B1. Laboratory PCT Measurements in Analytical Sequence for Study Glasses with and without Other Results from the Analytical Plans**

**B (ppm) By Analytical Sequence****B (ppm) By Analytical Sequence****Li (ppm) By Analytical Sequence****Li (ppm) By Analytical Sequence****Na (ppm) By Analytical Sequence****Na (ppm) By Analytical Sequence****Si (ppm) By Analytical Sequence****Si (ppm) By Analytical Sequence**

## Exhibit B2. Measurements of the Multi-Element Solution Standard by ICP Block

Oneway Analysis of B (ppm) By Set/Block



Oneway Anova  
Summary of Fit

Rsquare	0.349694
Adj Rsquare	0.078733
Root Mean Square Error	0.711805
Mean of Response	20.20556
Observations (or Sum Wgts)	18

### Analysis of Variance

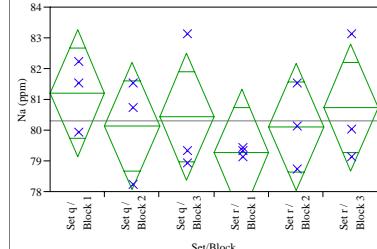
Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block	5	3.2694444	0.653889	1.2906	0.3305
Error	12	6.0800000	0.506667		
C. Total	17	9.3494444			

### Means for Oneway Anova

Level	Number	Mean	Std Error	Lower 95%	Upper 95%
Set q/Block 1	3	20.2000	0.41096	19.305	21.095
Set q/Block 2	3	20.2667	0.41096	19.371	21.162
Set q/Block 3	3	19.4000	0.41096	18.505	20.295
Set r/Block 1	3	20.1333	0.41096	19.238	21.029
Set r/Block 2	3	20.4000	0.41096	19.505	21.295
Set r/Block 3	3	20.8333	0.41096	19.938	21.729

Std Error uses a pooled estimate of error variance

Oneway Analysis of Na (ppm) By Set/Block



Oneway Anova  
Summary of Fit

Rsquare	0.166791
Adj Rsquare	-0.18038
Root Mean Square Error	1.638766
Mean of Response	80.31111
Observations (or Sum Wgts)	18

### Analysis of Variance

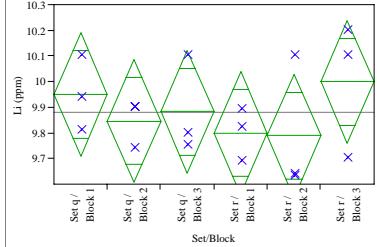
Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block	5	6.451111	1.29022	0.4804	0.7844
Error	12	32.226667	2.68556		
C. Total	17	38.677778			

### Means for Oneway Anova

Level	Number	Mean	Std Error	Lower 95%	Upper 95%
Set q/Block 1	3	81.2000	0.94614	79.139	83.261
Set q/Block 2	3	80.1333	0.94614	78.072	82.195
Set q/Block 3	3	80.4333	0.94614	78.372	82.495
Set r/Block 1	3	79.2667	0.94614	77.205	81.328
Set r/Block 2	3	80.1000	0.94614	78.039	82.161
Set r/Block 3	3	80.7333	0.94614	78.672	82.795

Std Error uses a pooled estimate of error variance

Oneway Analysis of Li (ppm) By Set/Block



Oneway Anova  
Summary of Fit

Rsquare	0.193758
Adj Rsquare	-0.14218
Root Mean Square Error	0.190555
Mean of Response	9.878333
Observations (or Sum Wgts)	18

### Analysis of Variance

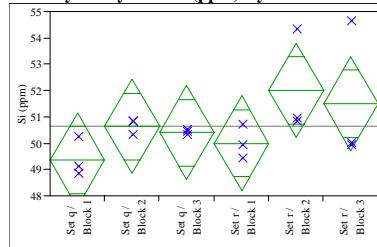
Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block	5	0.10471667	0.020943	0.5768	0.7173
Error	12	0.43573333	0.036311		
C. Total	17	0.54045000			

### Means for Oneway Anova

Level	Number	Mean	Std Error	Lower 95%	Upper 95%
Set q/Block 1	3	9.9500	0.11002	9.7103	10.190
Set q/Block 2	3	9.8467	0.11002	9.6070	10.086
Set q/Block 3	3	9.8833	0.11002	9.6436	10.123
Set r/Block 1	3	9.8000	0.11002	9.5603	10.040
Set r/Block 2	3	9.7900	0.11002	9.5503	10.030
Set r/Block 3	3	10.0000	0.11002	9.7603	10.240

Std Error uses a pooled estimate of error variance

Oneway Analysis of Si (ppm) By Set/Block



Oneway Anova  
Summary of Fit

Rsquare	0.364222
Adj Rsquare	0.099315
Root Mean Square Error	1.428675
Mean of Response	50.65
Observations (or Sum Wgts)	18

### Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Set/Block	5	14.031667	2.80633	1.3749	0.3005
Error	12	24.493333	2.04111		
C. Total	17	38.525000			

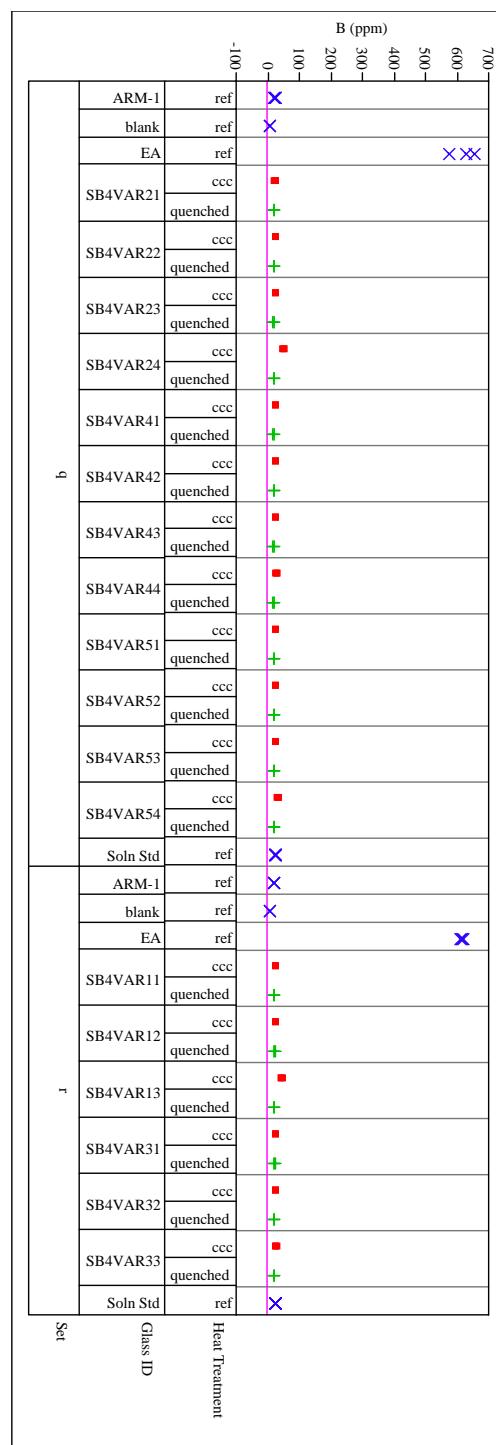
### Means for Oneway Anova

Level	Number	Mean	Std Error	Lower 95%	Upper 95%
Set q/Block 1	3	49.3667	0.82485	47.569	51.164
Set q/Block 2	3	50.6333	0.82485	48.836	52.431
Set q/Block 3	3	50.4000	0.82485	48.603	52.197
Set r/Block 1	3	50.0000	0.82485	48.203	51.797
Set r/Block 2	3	52.0000	0.82485	50.203	53.797
Set r/Block 3	3	51.5000	0.82485	49.703	53.297

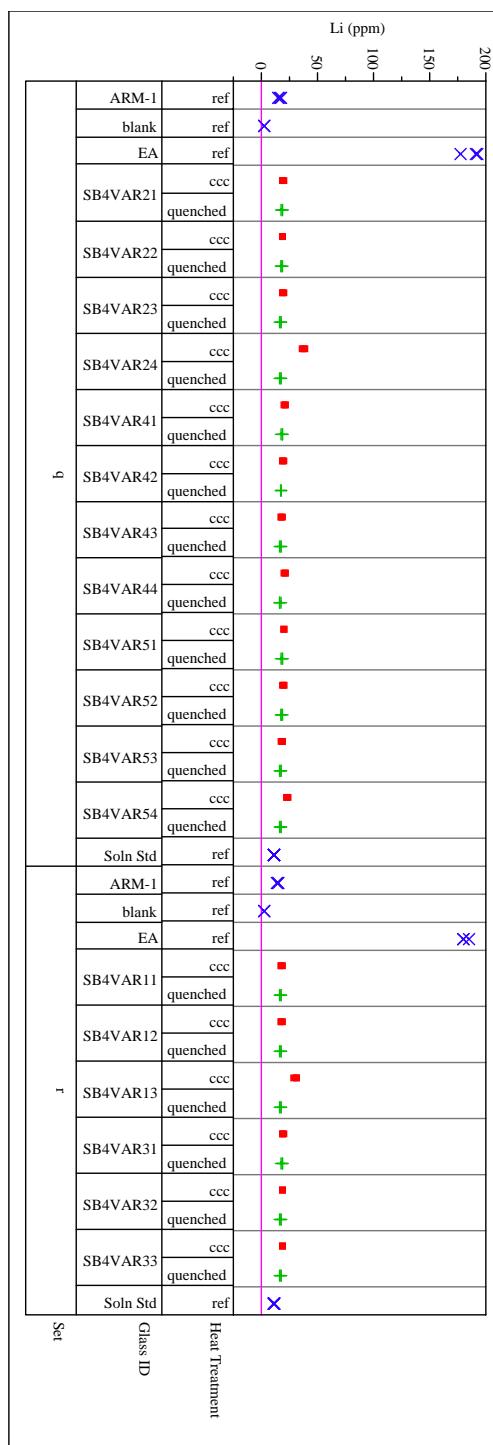
Std Error uses a pooled estimate of error variance

## Exhibit B3. Laboratory PCT Measurements by Glass Identifier for Study Glasses and Standards

Variability Chart for B (ppm)

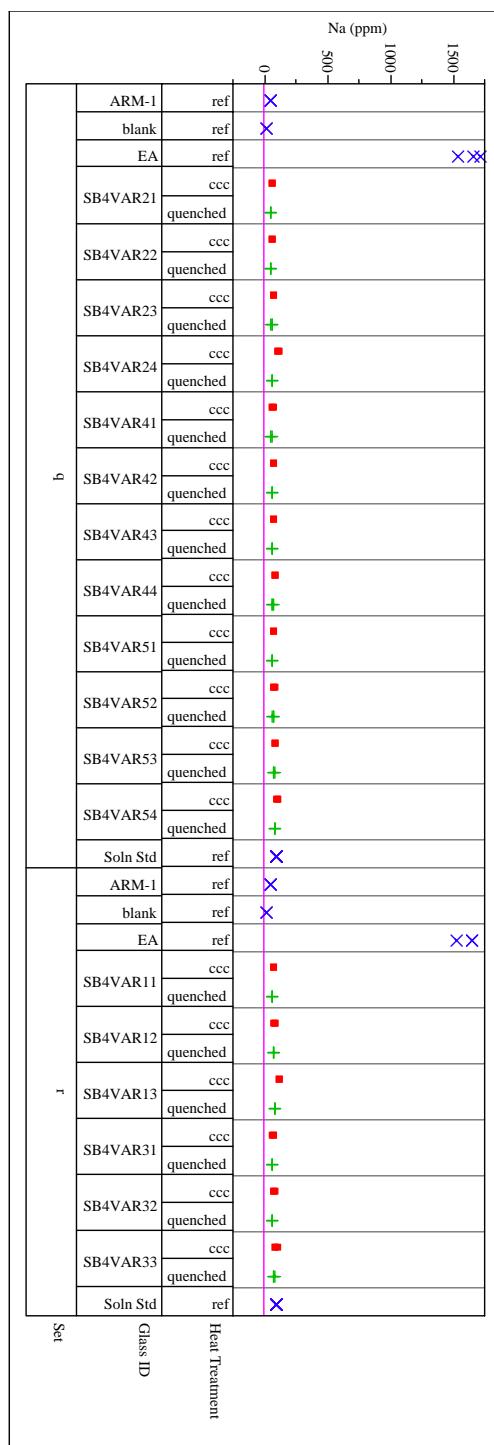


Variability Chart for Li (ppm)

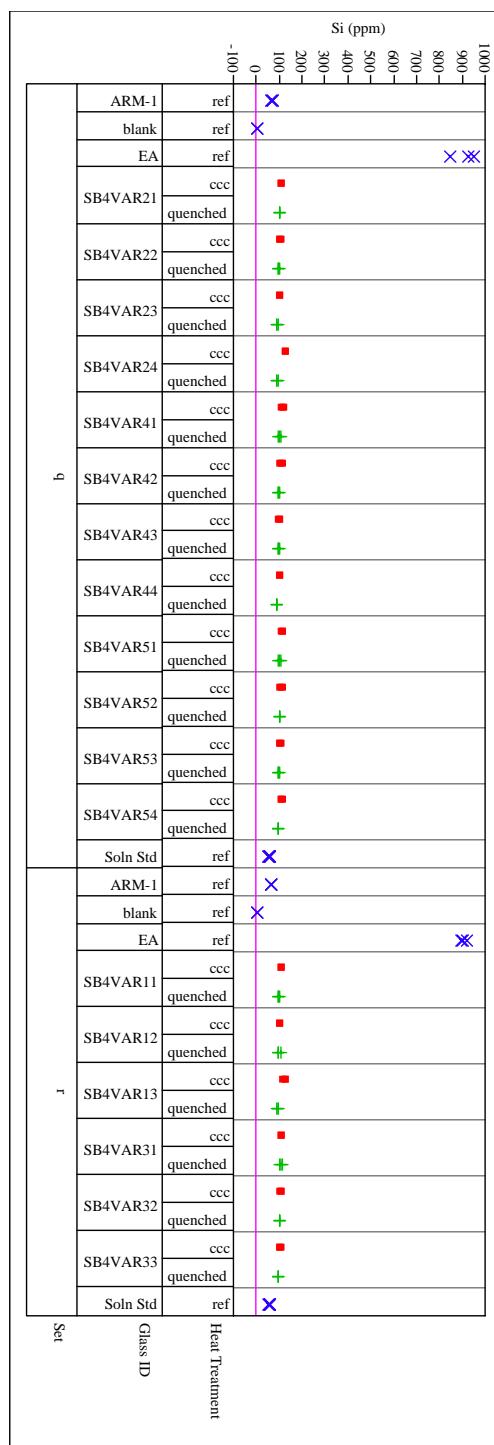


## Exhibit B3. Laboratory PCT Measurements by Glass Identifier for Study Glasses and Standards

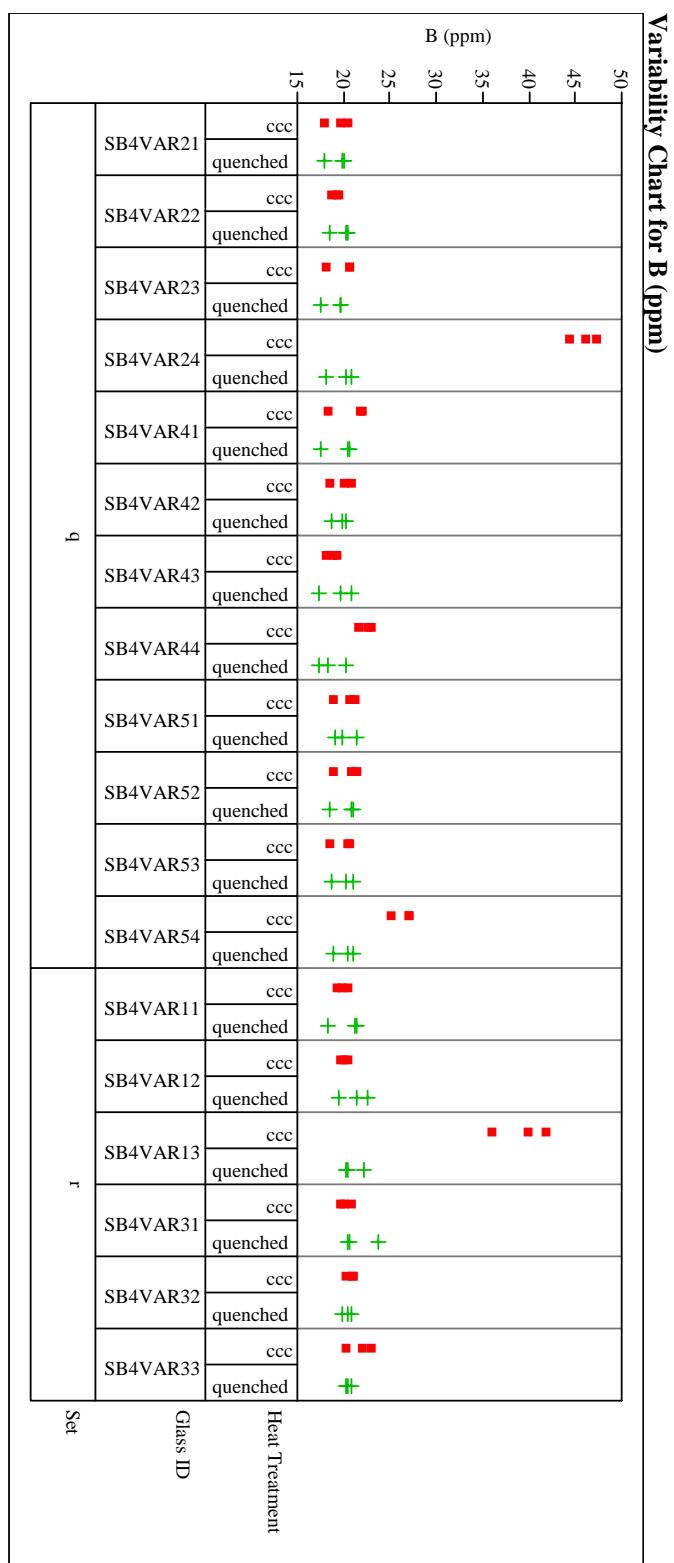
Variability Chart for Na (ppm)



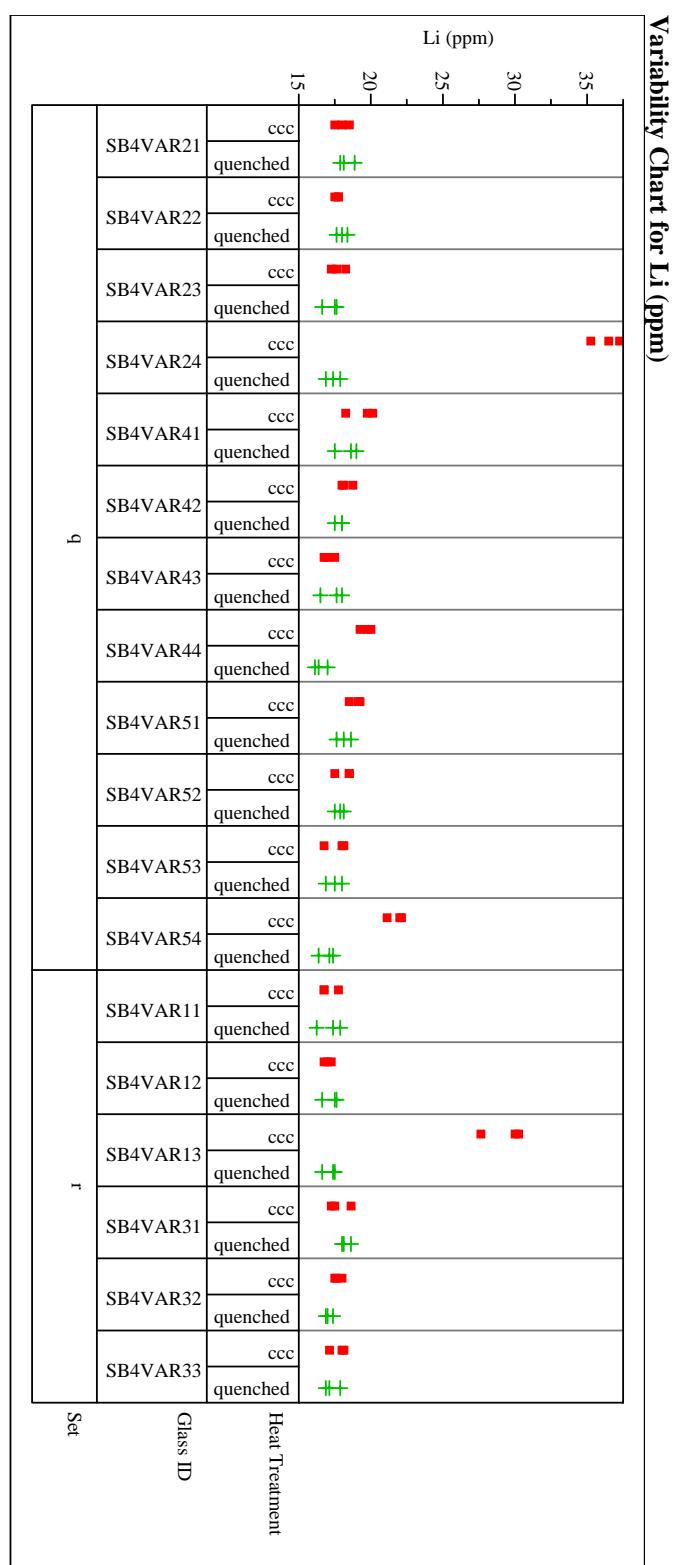
Variability Chart for Si (ppm)



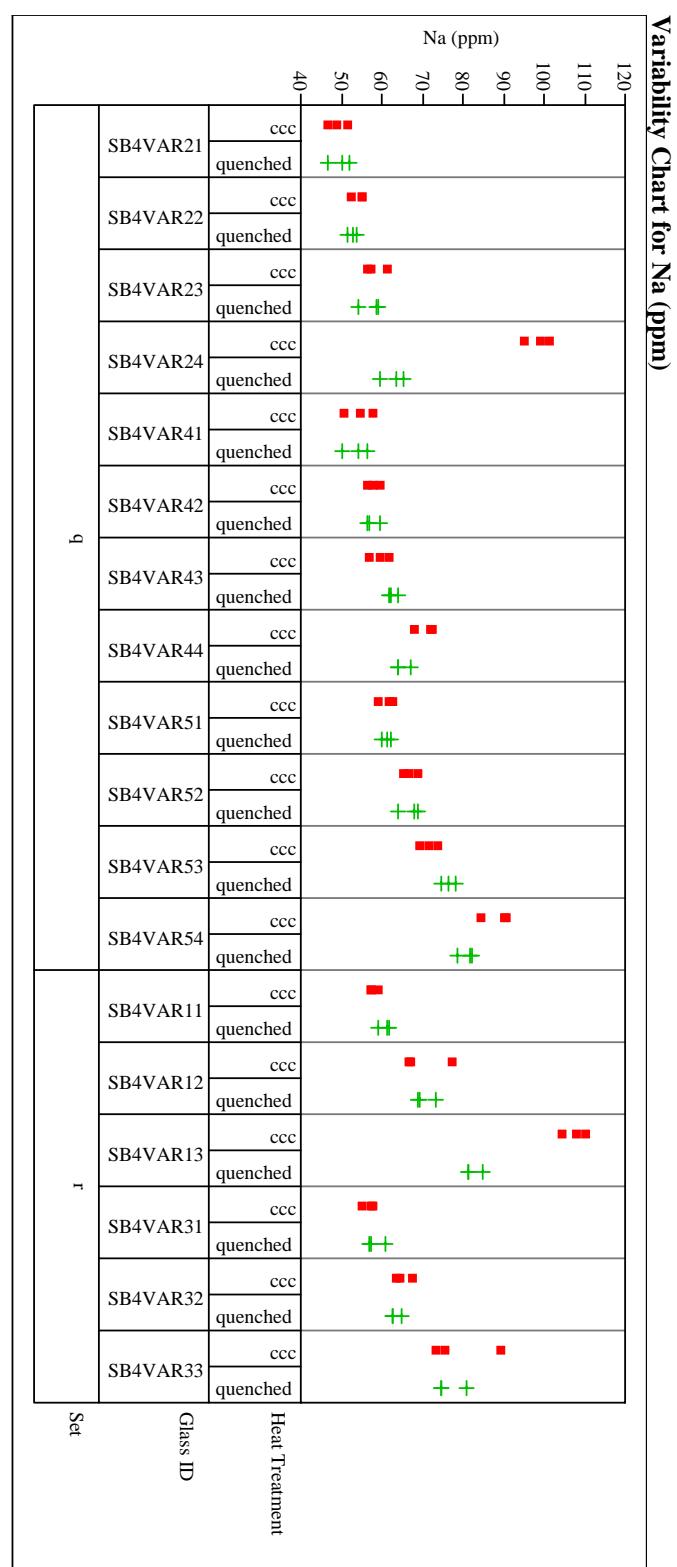
## Exhibit B4. Laboratory PCT Measurements by Glass Identifier for Study Glasses



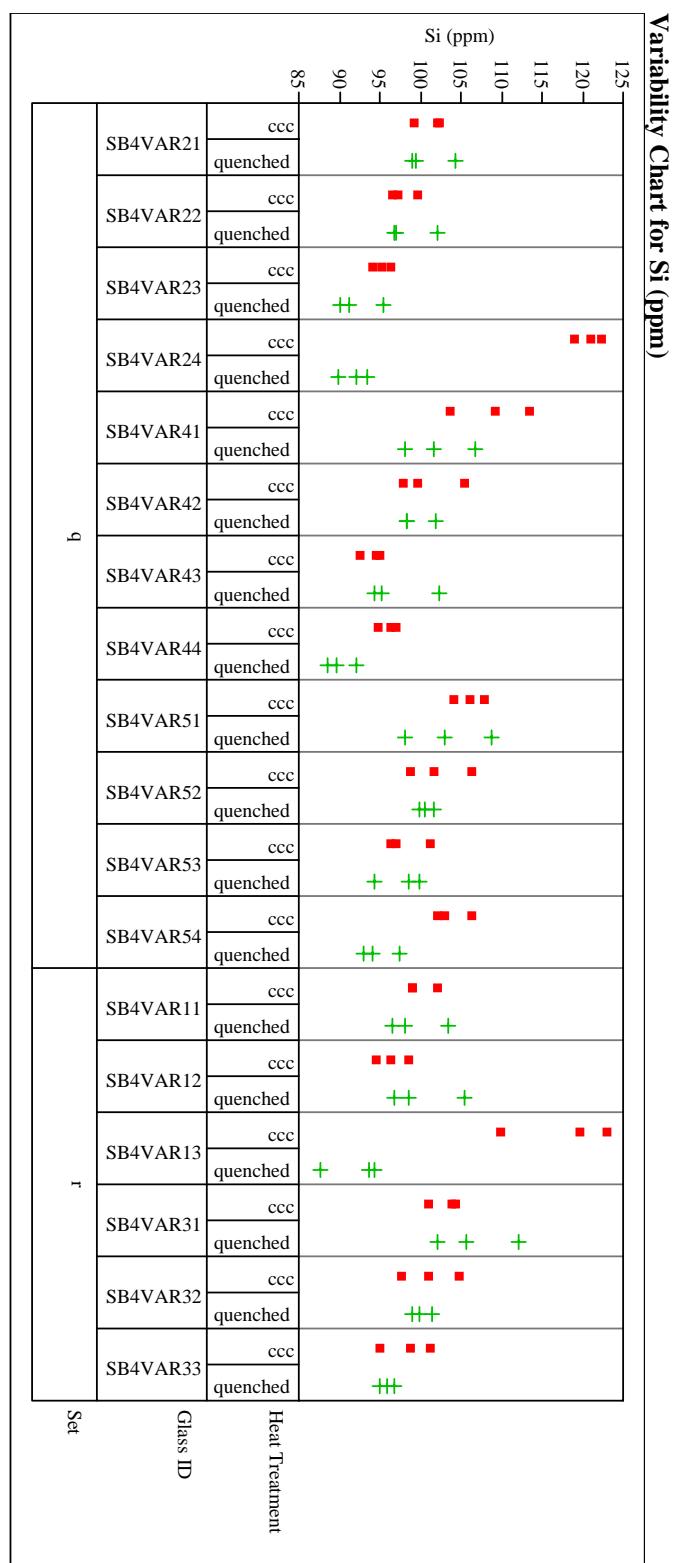
### Exhibit B4. Laboratory PCT Measurements by Glass Identifier for Study Glasses



## Exhibit B4. Laboratory PCT Measurements by Glass Identifier for Study Glasses



### Exhibit B4. Laboratory PCT Measurements by Glass Identifier for Study Glasses

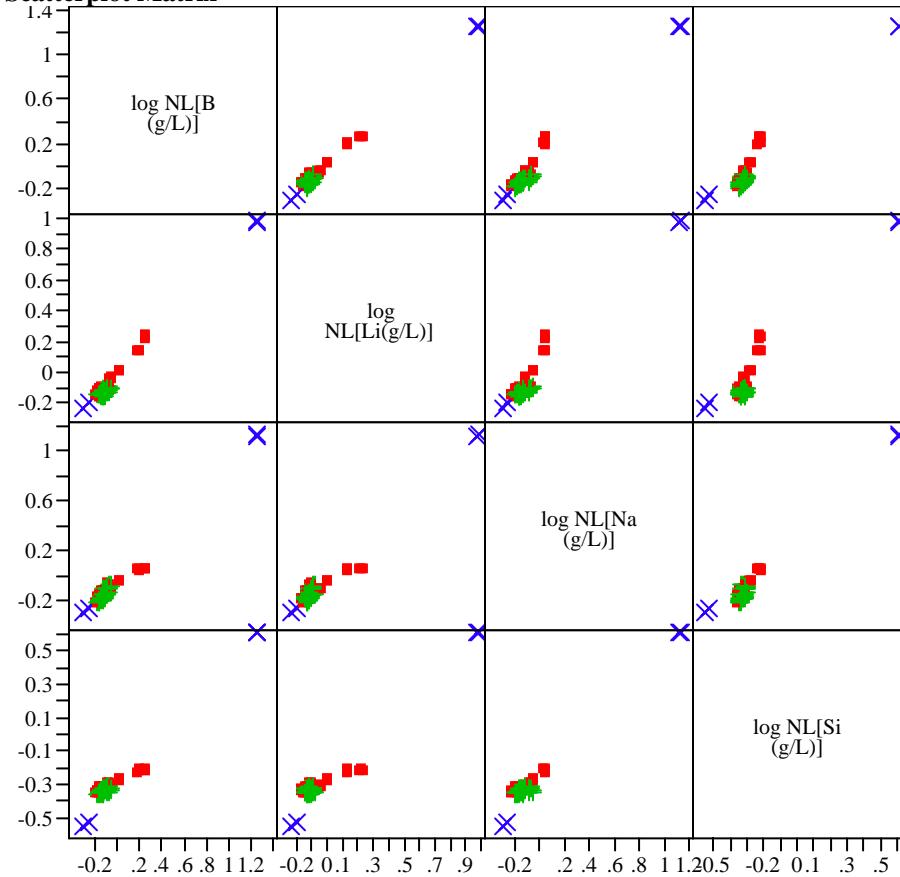


**Exhibit B5. Correlations and Scatter Plots of Normalized PCTs  
Over All Compositional Views and Heat Treatments**

**Correlations**

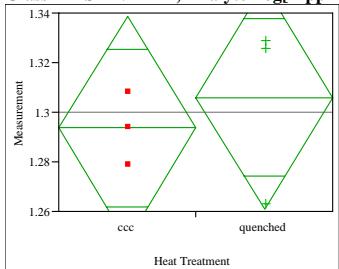
	log NL[B (g/L)]	log NL[Li(g/L)]	log NL[Na (g/L)]	log NL[Si (g/L)]
log NL[B (g/L)]	1.0000	0.9942	0.9820	0.9641
log NL[Li(g/L)]	0.9942	1.0000	0.9702	0.9529
log NL[Na (g/L)]	0.9820	0.9702	1.0000	0.9776
log NL[Si (g/L)]	0.9641	0.9529	0.9776	1.0000

**Scatterplot Matrix**



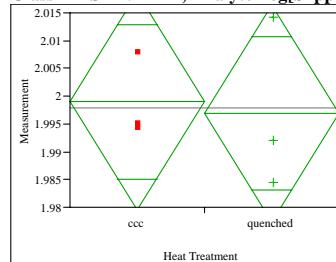
## Exhibit B6. Effects of Heat Treatment on PCT log(ppm)-Response of Study Glasses

Glass ID=SB4VAR11, Analyte=log[B ppm]



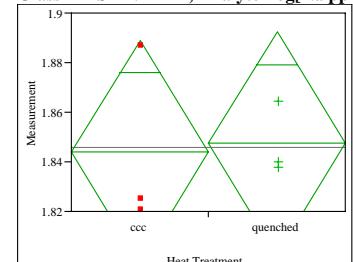
Difference	0.01242	t Ratio	0.539481
Std Err Dif	0.02302	DF	4
Upper CL Dif	0.07634	Prob >  t	0.6182
Lower CL Dif	-0.05150	Prob > t	0.3091
Confidence	0.95	Prob < t	0.6909

Glass ID=SB4VAR11, Analyte=log[Si ppm]



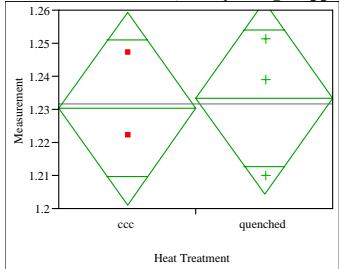
Difference	-0.00208	t Ratio	-0.20821
Std Err Dif	0.00998	DF	4
Upper CL Dif	0.02562	Prob >  t	0.8452
Lower CL Dif	-0.02978	Prob > t	0.5774
Confidence	0.95	Prob < t	0.4226

Glass ID=SB4VAR12, Analyte=log[Na ppm]



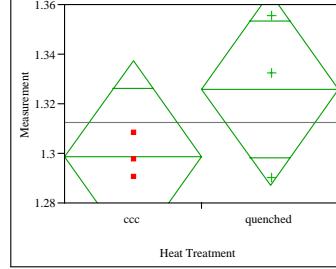
Difference	0.00330	t Ratio	0.143887
Std Err Dif	0.02290	DF	4
Upper CL Dif	0.06688	Prob >  t	0.8925
Lower CL Dif	-0.06029	Prob > t	0.4463
Confidence	0.95	Prob < t	0.5537

Glass ID=SB4VAR11, Analyte=log[Li ppm]



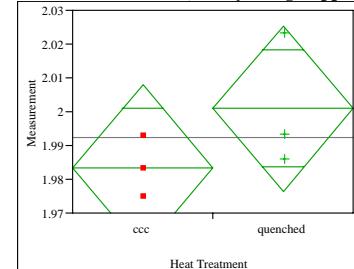
Difference	0.00307	t Ratio	0.206957
Std Err Dif	0.01486	DF	4
Upper CL Dif	0.04432	Prob >  t	0.8462
Lower CL Dif	-0.03817	Prob > t	0.4231
Confidence	0.95	Prob < t	0.5769

Glass ID=SB4VAR12, Analyte=log[B ppm]



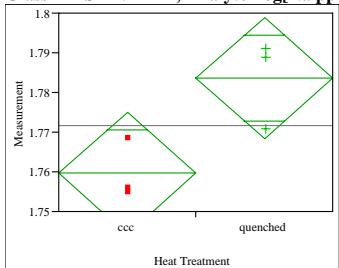
Difference	0.02741	t Ratio	1.380256
Std Err Dif	0.01986	DF	4
Upper CL Dif	0.08254	Prob >  t	0.2396
Lower CL Dif	-0.02772	Prob > t	0.1198
Confidence	0.95	Prob < t	0.8802

Glass ID=SB4VAR12, Analyte=log[Si ppm]



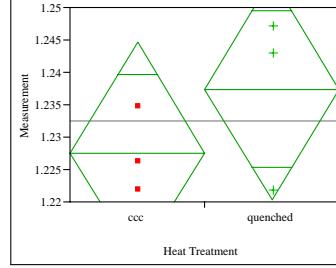
Difference	0.01744	t Ratio	1.393767
Std Err Dif	0.01251	DF	4
Upper CL Dif	0.05218	Prob >  t	0.2358
Lower CL Dif	-0.01730	Prob > t	0.1179
Confidence	0.95	Prob < t	0.8821

Glass ID=SB4VAR11, Analyte=log[Na ppm]



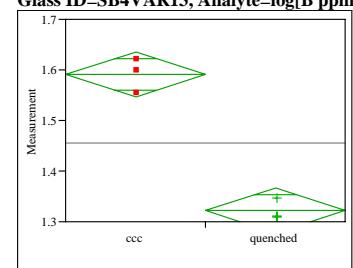
Difference	0.024027	t Ratio	3.082351
Std Err Dif	0.007795	DF	4
Upper CL Dif	0.045669	Prob >  t	0.0368
Lower CL Dif	0.002385	Prob > t	0.0184
Confidence	0.95	Prob < t	0.9816

Glass ID=SB4VAR12, Analyte=log[Li ppm]



Difference	0.00978	t Ratio	1.124053
Std Err Dif	0.00870	DF	4
Upper CL Dif	0.03393	Prob >  t	0.3239
Lower CL Dif	-0.01438	Prob > t	0.1619
Confidence	0.95	Prob < t	0.8381

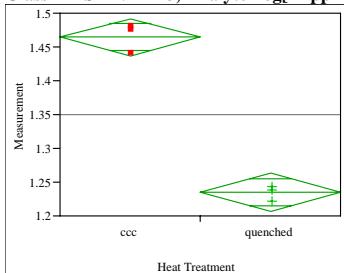
Glass ID=SB4VAR13, Analyte=log[B ppm]



Difference	-0.26895	t Ratio	-11.854
Std Err Dif	0.02269	DF	4
Upper CL Dif	-0.20595	Prob >  t	0.0003
Lower CL Dif	-0.33194	Prob > t	0.9999
Confidence	0.95	Prob < t	0.0001

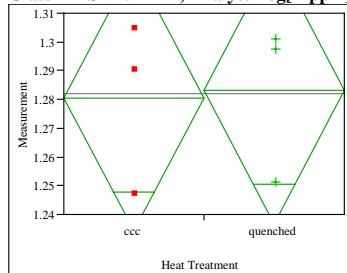
## Exhibit B6. Effects of Heat Treatment on PCT log(ppm)-Response of Study Glasses

Glass ID=SB4VAR13, Analyte=log[Li ppm]



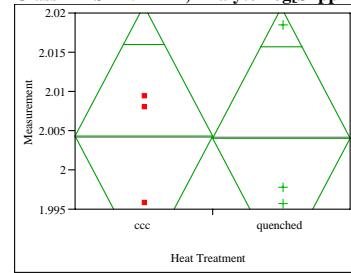
Difference -0.22993 t Ratio -16.1551  
Std Err Dif 0.01423 DF 4  
Upper CL Dif -0.19041 Prob > |t| <.0001  
Lower CL Dif -0.26945 Prob > t 1.0000  
Confidence 0.95 Prob < t <.0001

Glass ID=SB4VAR21, Analyte=log[B ppm]



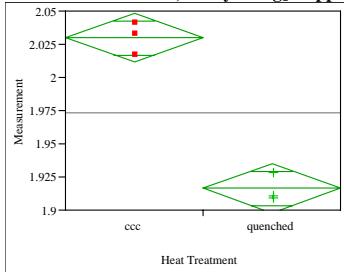
Difference 0.00261 t Ratio 0.110914  
Std Err Dif 0.02355 DF 4  
Upper CL Dif 0.06799 Prob > |t| 0.9170  
Lower CL Dif -0.06276 Prob > t 0.4585  
Confidence 0.95 Prob < t 0.5415

Glass ID=SB4VAR21, Analyte=log[Si ppm]



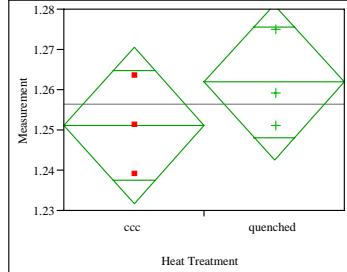
Difference -0.00032 t Ratio -0.03756  
Std Err Dif 0.00846 DF 4  
Upper CL Dif 0.02316 Prob > |t| 0.9718  
Lower CL Dif -0.02380 Prob > t 0.5141  
Confidence 0.95 Prob < t 0.4859

Glass ID=SB4VAR13, Analyte=log[Na ppm]



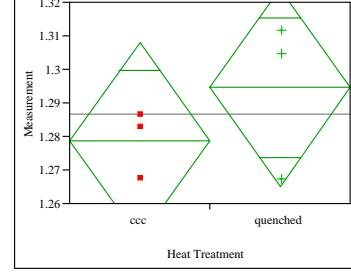
Difference -0.11335 t Ratio -12.0511  
Std Err Dif 0.00941 DF 4  
Upper CL Dif -0.08724 Prob > |t| 0.0003  
Lower CL Dif -0.13946 Prob > t 0.9999  
Confidence 0.95 Prob < t 0.0001

Glass ID=SB4VAR21, Analyte=log[Li ppm]



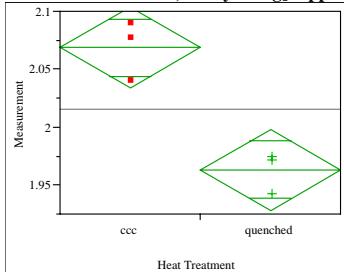
Difference 0.01069 t Ratio 1.081002  
Std Err Dif 0.00989 DF 4  
Upper CL Dif 0.03816 Prob > |t| 0.3405  
Lower CL Dif -0.01677 Prob > t 0.1703  
Confidence 0.95 Prob < t 0.8297

Glass ID=SB4VAR22, Analyte=log[B ppm]



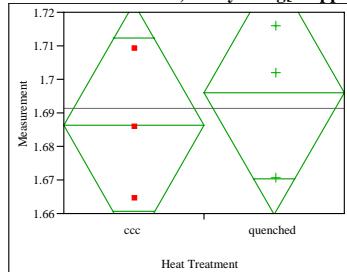
Difference 0.01584 t Ratio 1.055237  
Std Err Dif 0.01502 DF 4  
Upper CL Dif 0.05753 Prob > |t| 0.3508  
Lower CL Dif -0.02584 Prob > t 0.1754  
Confidence 0.95 Prob < t 0.8246

Glass ID=SB4VAR13, Analyte=log[Si ppm]



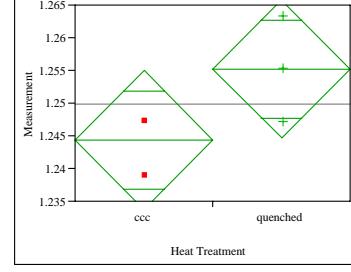
Difference -0.10569 t Ratio -5.89922  
Std Err Dif 0.01792 DF 4  
Upper CL Dif -0.05595 Prob > |t| 0.0041  
Lower CL Dif -0.15543 Prob > t 0.9979  
Confidence 0.95 Prob < t 0.0021

Glass ID=SB4VAR21, Analyte=log[Na ppm]



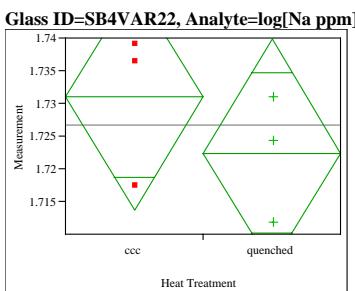
Difference 0.00979 t Ratio 0.525625  
Std Err Dif 0.01862 DF 4  
Upper CL Dif 0.06147 Prob > |t| 0.6269  
Lower CL Dif -0.04190 Prob > t 0.3135  
Confidence 0.95 Prob < t 0.6865

Glass ID=SB4VAR22, Analyte=log[Li ppm]

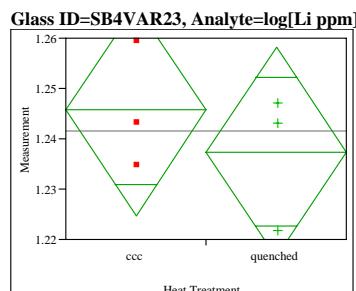


Difference 0.01083 t Ratio 2.004426  
Std Err Dif 0.00540 DF 4  
Upper CL Dif 0.02582 Prob > |t| 0.1155  
Lower CL Dif -0.00417 Prob > t 0.0578  
Confidence 0.95 Prob < t 0.9422

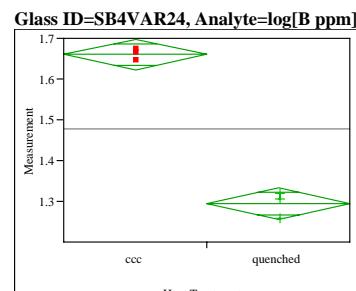
## Exhibit B6. Effects of Heat Treatment on PCT log(ppm)-Response of Study Glasses



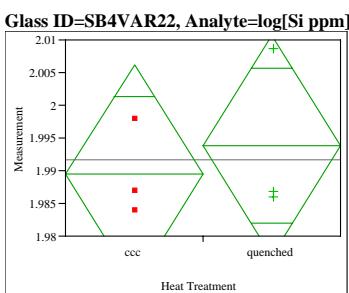
Difference -0.00857 t Ratio -0.96838  
Std Err Dif 0.00885 DF 4  
Upper CL Dif 0.01599 Prob > |t| 0.3877  
Lower CL Dif -0.03131 Prob > t 0.8062  
Confidence 0.95 Prob < t 0.1938



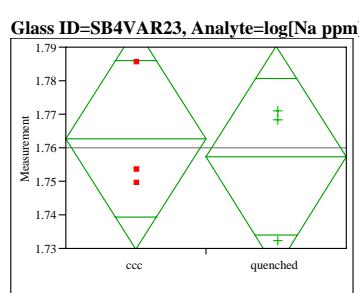
Difference -0.00832 t Ratio -0.78063  
Std Err Dif 0.01066 DF 4  
Upper CL Dif 0.02127 Prob > |t| 0.4786  
Lower CL Dif -0.03791 Prob > t 0.7607  
Confidence 0.95 Prob < t 0.2393



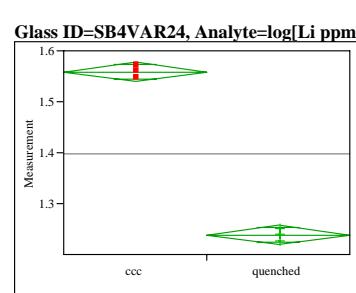
Difference -0.36576 t Ratio -18.6495  
Std Err Dif 0.01961 DF 4  
Upper CL Dif -0.31131 Prob > |t| <.0001  
Lower CL Dif -0.42021 Prob > t 1.0000  
Confidence 0.95 Prob < t <.0001



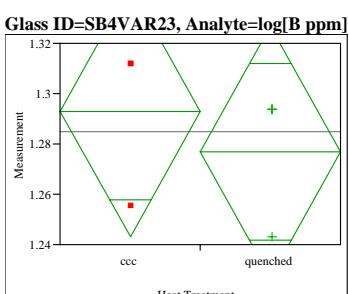
Difference 0.00434 t Ratio 0.507958  
Std Err Dif 0.00855 DF 4  
Upper CL Dif 0.02807 Prob > |t| 0.6382  
Lower CL Dif -0.01939 Prob > t 0.3191  
Confidence 0.95 Prob < t 0.6809



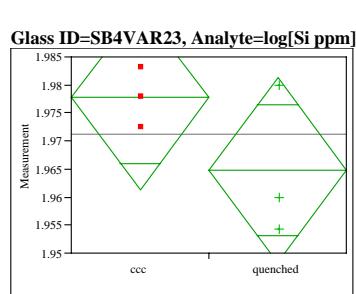
Difference -0.00550 t Ratio -0.32656  
Std Err Dif 0.01684 DF 4  
Upper CL Dif 0.04126 Prob > |t| 0.7604  
Lower CL Dif -0.05226 Prob > t 0.6198  
Confidence 0.95 Prob < t 0.3802



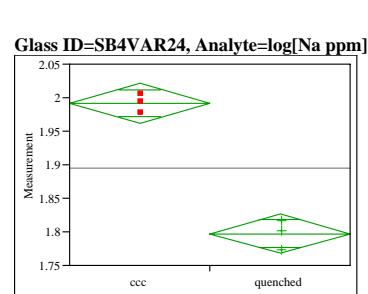
Difference -0.32010 t Ratio -31.8581  
Std Err Dif 0.01005 DF 4  
Upper CL Dif -0.29220 Prob > |t| <.0001  
Lower CL Dif -0.34800 Prob > t 1.0000  
Confidence 0.95 Prob < t <.0001



Difference -0.01609 t Ratio -0.63616  
Std Err Dif 0.02530 DF 4  
Upper CL Dif 0.05414 Prob > |t| 0.5593  
Lower CL Dif -0.08633 Prob > t 0.7204  
Confidence 0.95 Prob < t 0.2796

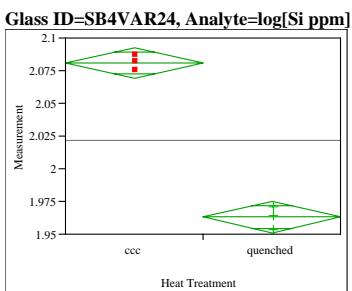


Difference -0.01301 t Ratio -1.54718  
Std Err Dif 0.00841 DF 4  
Upper CL Dif 0.01033 Prob > |t| 0.1967  
Lower CL Dif -0.03635 Prob > t 0.9016  
Confidence 0.95 Prob < t 0.0984

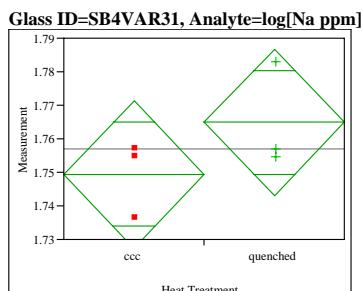


Difference -0.19452 t Ratio -13.0505  
Std Err Dif 0.01490 DF 4  
Upper CL Dif -0.15313 Prob > |t| 0.0002  
Lower CL Dif -0.23590 Prob > t 0.9999  
Confidence 0.95 Prob < t <.0001

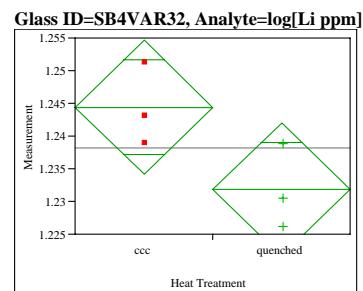
## Exhibit B6. Effects of Heat Treatment on PCT log(ppm)-Response of Study Glasses



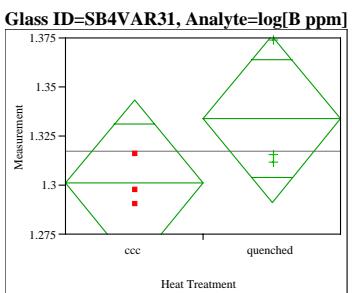
Difference -0.11802 t Ratio -19.4577  
Std Err Dif 0.00607 DF 4  
Upper CL Dif -0.10118 Prob > |t| <.0001  
Lower CL Dif -0.13486 Prob > t 1.0000  
Confidence 0.95 Prob < t <.0001



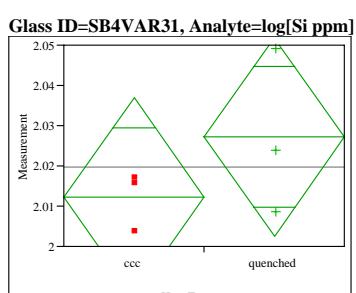
Difference 0.01552 t Ratio 1.389704  
Std Err Dif 0.01117 DF 4  
Upper CL Dif 0.04652 Prob > |t| 0.2370  
Lower CL Dif -0.01548 Prob > t 0.1185  
Confidence 0.95 Prob < t 0.8815



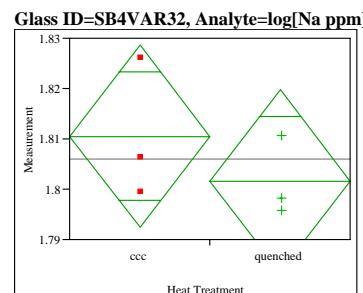
Difference -0.01255 t Ratio -2.41045  
Std Err Dif 0.00521 DF 4  
Upper CL Dif 0.00191 Prob > |t| 0.0735  
Lower CL Dif -0.02701 Prob > t 0.9632  
Confidence 0.95 Prob < t 0.0368



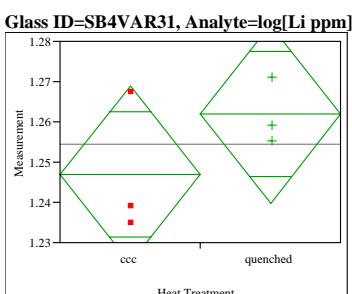
Difference 0.03282 t Ratio 1.521106  
Std Err Dif 0.02158 DF 4  
Upper CL Dif 0.09273 Prob > |t| 0.2029  
Lower CL Dif -0.02709 Prob > t 0.1014  
Confidence 0.95 Prob < t 0.8986



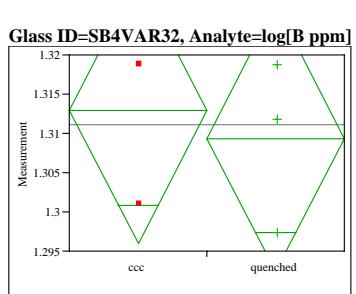
Difference 0.01516 t Ratio 1.204516  
Std Err Dif 0.01259 DF 4  
Upper CL Dif 0.05010 Prob > |t| 0.2948  
Lower CL Dif -0.01978 Prob > t 0.1474  
Confidence 0.95 Prob < t 0.8526



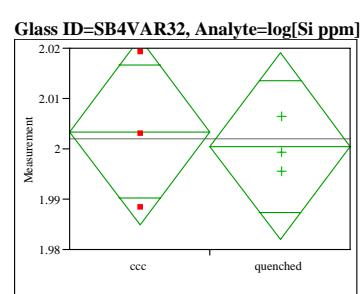
Difference -0.00895 t Ratio -0.96814  
Std Err Dif 0.00924 DF 4  
Upper CL Dif 0.01671 Prob > |t| 0.3878  
Lower CL Dif -0.03461 Prob > t 0.8061  
Confidence 0.95 Prob < t 0.1939



Difference 0.01496 t Ratio 1.329729  
Std Err Dif 0.01125 DF 4  
Upper CL Dif 0.04619 Prob > |t| 0.2544  
Lower CL Dif -0.01627 Prob > t 0.1272  
Confidence 0.95 Prob < t 0.8728



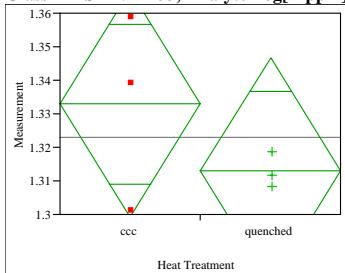
Difference -0.00355 t Ratio -0.41099  
Std Err Dif 0.00863 DF 4  
Upper CL Dif 0.02041 Prob > |t| 0.7021  
Lower CL Dif -0.02750 Prob > t 0.6489  
Confidence 0.95 Prob < t 0.3511



Difference -0.00296 t Ratio -0.31306  
Std Err Dif 0.00946 DF 4  
Upper CL Dif 0.02331 Prob > |t| 0.7699  
Lower CL Dif -0.02923 Prob > t 0.6151  
Confidence 0.95 Prob < t 0.3849

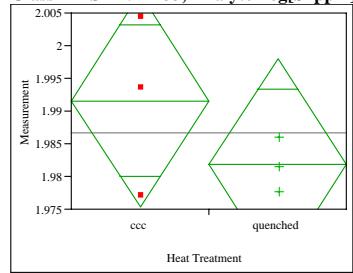
## Exhibit B6. Effects of Heat Treatment on PCT log(ppm)-Response of Study Glasses

Glass ID=SB4VAR33, Analyte=log[B ppm]



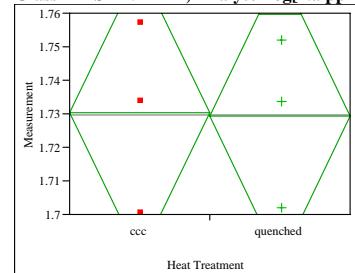
Difference	-0.02000	t Ratio	-1.1641
Std Err Dif	0.01718	DF	4
Upper CL Dif	0.02770	Prob >  t	0.3091
Lower CL Dif	-0.06770	Prob > t	0.8455
Confidence	0.95	Prob < t	0.1545

Glass ID=SB4VAR33, Analyte=log[Si ppm]



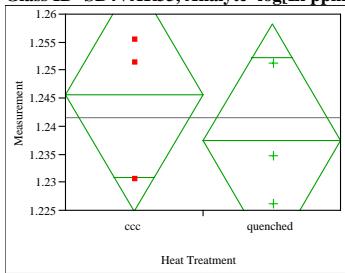
Difference	-0.00982	t Ratio	-1.18187
Std Err Dif	0.00831	DF	4
Upper CL Dif	0.01325	Prob >  t	0.3027
Lower CL Dif	-0.03288	Prob > t	0.8486
Confidence	0.95	Prob < t	0.1514

Glass ID=SB4VAR41, Analyte=log[Na ppm]



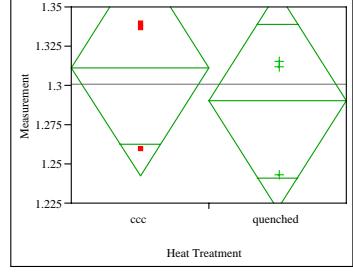
Difference	-0.00122	t Ratio	-0.05525
Std Err Dif	0.02204	DF	4
Upper CL Dif	0.05999	Prob >  t	0.9586
Lower CL Dif	-0.06242	Prob > t	0.5207
Confidence	0.95	Prob < t	0.4793

Glass ID=SB4VAR33, Analyte=log[Li ppm]



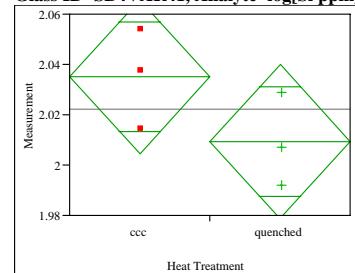
Difference	-0.00829	t Ratio	-0.77877
Std Err Dif	0.01064	DF	4
Upper CL Dif	0.02126	Prob >  t	0.4796
Lower CL Dif	-0.03784	Prob > t	0.7602
Confidence	0.95	Prob < t	0.2398

Glass ID=SB4VAR41, Analyte=log[B ppm]



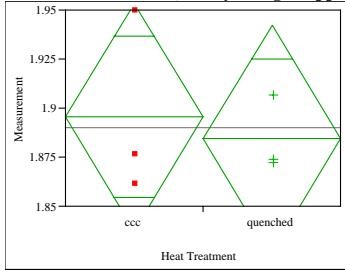
Difference	-0.02138	t Ratio	-0.60875
Std Err Dif	0.03511	DF	4
Upper CL Dif	0.07611	Prob >  t	0.5756
Lower CL Dif	-0.11886	Prob > t	0.7122
Confidence	0.95	Prob < t	0.2878

Glass ID=SB4VAR41, Analyte=log[Si ppm]



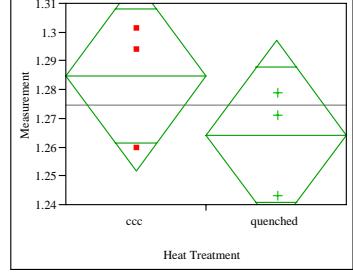
Difference	-0.02585	t Ratio	-1.65185
Std Err Dif	0.01565	DF	4
Upper CL Dif	0.01760	Prob >  t	0.1739
Lower CL Dif	-0.06929	Prob > t	0.9130
Confidence	0.95	Prob < t	0.0870

Glass ID=SB4VAR33, Analyte=log[Na ppm]



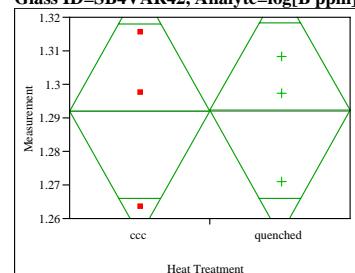
Difference	-0.01127	t Ratio	-0.38263
Std Err Dif	0.02945	DF	4
Upper CL Dif	0.07050	Prob >  t	0.7215
Lower CL Dif	-0.09303	Prob > t	0.6393
Confidence	0.95	Prob < t	0.3607

Glass ID=SB4VAR41, Analyte=log[Li ppm]



Difference	-0.02039	t Ratio	-1.211
Std Err Dif	0.01684	DF	4
Upper CL Dif	0.02636	Prob >  t	0.2926
Lower CL Dif	-0.06715	Prob > t	0.8537
Confidence	0.95	Prob < t	0.1463

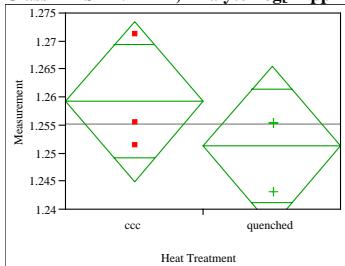
Glass ID=SB4VAR42, Analyte=log[B ppm]



Difference	0.00025	t Ratio	0.013515
Std Err Dif	0.01883	DF	4
Upper CL Dif	0.05254	Prob >  t	0.9899
Lower CL Dif	-0.05203	Prob > t	0.4949
Confidence	0.95	Prob < t	0.5051

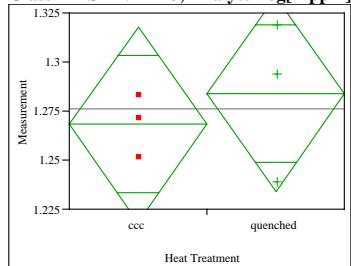
## Exhibit B6. Effects of Heat Treatment on PCT log(ppm)-Response of Study Glasses

Glass ID=SB4VAR42, Analyte=log(Li ppm)



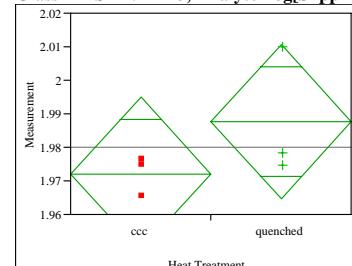
Difference	-0.00800	t Ratio	-1.09576
Std Err Dif	0.00730	DF	4
Upper CL Dif	0.01226	Prob >  t	0.3347
Lower CL Dif	-0.02826	Prob > t	0.8326
Confidence	0.95	Prob < t	0.1674

Glass ID=SB4VAR43, Analyte=log(B ppm)



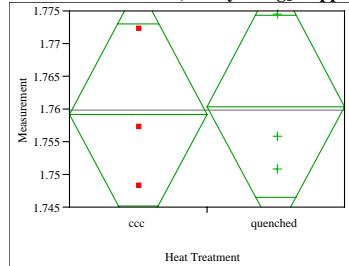
Difference	0.01551	t Ratio	0.613009
Std Err Dif	0.02530	DF	4
Upper CL Dif	0.08575	Prob >  t	0.5730
Lower CL Dif	-0.05473	Prob > t	0.2865
Confidence	0.95	Prob < t	0.7135

Glass ID=SB4VAR43, Analyte=log(Si ppm)



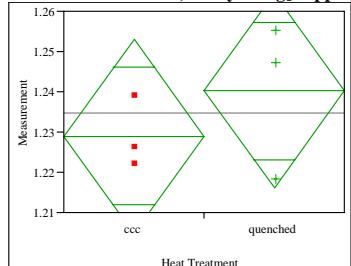
Difference	0.01565	t Ratio	1.337219
Std Err Dif	0.01170	DF	4
Upper CL Dif	0.04814	Prob >  t	0.2521
Lower CL Dif	-0.01684	Prob > t	0.1261
Confidence	0.95	Prob < t	0.8739

Glass ID=SB4VAR42, Analyte=log(Na ppm)



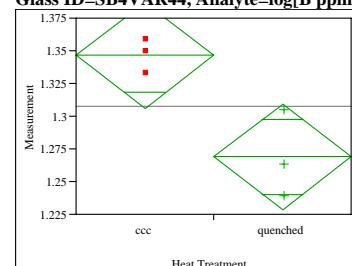
Difference	0.00125	t Ratio	0.124572
Std Err Dif	0.01003	DF	4
Upper CL Dif	0.02910	Prob >  t	0.9069
Lower CL Dif	-0.02660	Prob > t	0.4534
Confidence	0.95	Prob < t	0.5466

Glass ID=SB4VAR43, Analyte=log(Li ppm)



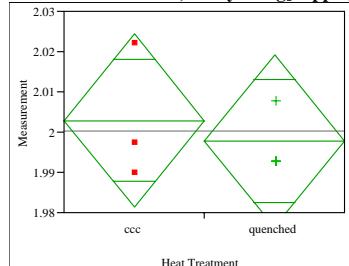
Difference	0.01130	t Ratio	0.917546
Std Err Dif	0.01231	DF	4
Upper CL Dif	0.04548	Prob >  t	0.4108
Lower CL Dif	-0.02288	Prob > t	0.2054
Confidence	0.95	Prob < t	0.7946

Glass ID=SB4VAR44, Analyte=log(B ppm)



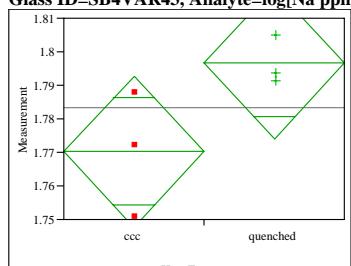
Difference	-0.07773	t Ratio	-3.76378
Std Err Dif	0.02065	DF	4
Upper CL Dif	-0.02039	Prob >  t	0.0197
Lower CL Dif	-0.13508	Prob > t	0.9901
Confidence	0.95	Prob < t	0.0099

Glass ID=SB4VAR42, Analyte=log(Si ppm)



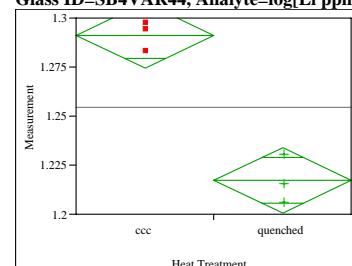
Difference	-0.00514	t Ratio	-0.46923
Std Err Dif	0.01096	DF	4
Upper CL Dif	0.02529	Prob >  t	0.6633
Lower CL Dif	-0.03557	Prob > t	0.6683
Confidence	0.95	Prob < t	0.3317

Glass ID=SB4VAR43, Analyte=log(Na ppm)



Difference	0.02643	t Ratio	2.293333
Std Err Dif	0.01152	DF	4
Upper CL Dif	0.05843	Prob >  t	0.0835
Lower CL Dif	-0.00557	Prob > t	0.0418
Confidence	0.95	Prob < t	0.9582

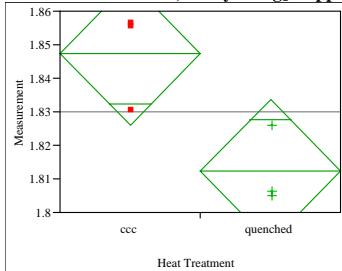
Glass ID=SB4VAR44, Analyte=log(Li ppm)



Difference	-0.07400	t Ratio	-8.78293
Std Err Dif	0.00843	DF	4
Upper CL Dif	-0.05061	Prob >  t	0.0009
Lower CL Dif	-0.09740	Prob > t	0.9995
Confidence	0.95	Prob < t	0.0005

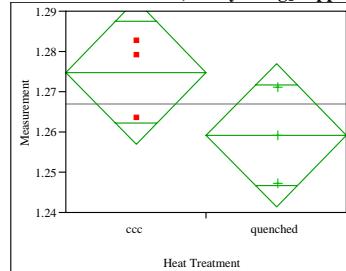
## Exhibit B6. Effects of Heat Treatment on PCT log(ppm)-Response of Study Glasses

Glass ID=SB4VAR44, Analyte=log[Na ppm]



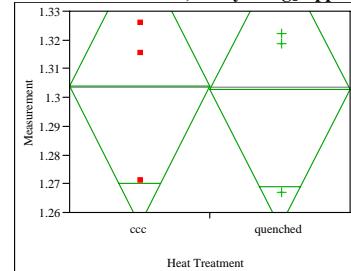
Difference -0.03491 t Ratio -3.20437  
 Std Err Dif 0.01089 DF 4  
 Upper CL Dif -0.00466 Prob > |t| 0.0328  
 Lower CL Dif -0.06515 Prob > t 0.9836  
 Confidence 0.95 Prob < t 0.0164

Glass ID=SB4VAR51, Analyte=log[Li ppm]



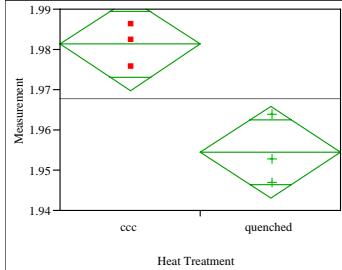
Difference -0.01568 t Ratio -1.72624  
 Std Err Dif 0.00908 DF 4  
 Upper CL Dif 0.00954 Prob > |t| 0.1594  
 Lower CL Dif -0.04090 Prob > t 0.9203  
 Confidence 0.95 Prob < t 0.0797

Glass ID=SB4VAR52, Analyte=log[B ppm]



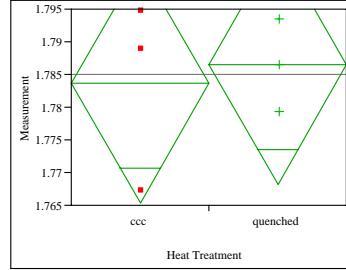
Difference -0.00128 t Ratio -0.05239  
 Std Err Dif 0.02443 DF 4  
 Upper CL Dif 0.06655 Prob > |t| 0.9607  
 Lower CL Dif -0.06911 Prob > t 0.5196  
 Confidence 0.95 Prob < t 0.4804

Glass ID=SB4VAR44, Analyte=log[Si ppm]



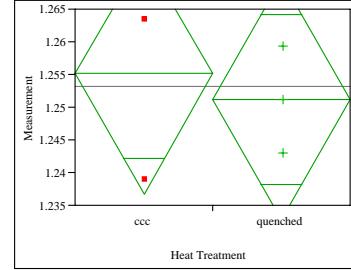
Difference -0.02679 t Ratio -4.58805  
 Std Err Dif 0.00584 DF 4  
 Upper CL Dif -0.01058 Prob > |t| 0.0101  
 Lower CL Dif -0.04300 Prob > t 0.9949  
 Confidence 0.95 Prob < t 0.0051

Glass ID=SB4VAR51, Analyte=log[Na ppm]



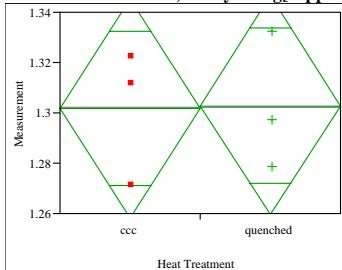
Difference 0.00289 t Ratio 0.309871  
 Std Err Dif 0.00933 DF 4  
 Upper CL Dif 0.02881 Prob > |t| 0.7721  
 Lower CL Dif -0.02302 Prob > t 0.3861  
 Confidence 0.95 Prob < t 0.6139

Glass ID=SB4VAR52, Analyte=log[Li ppm]



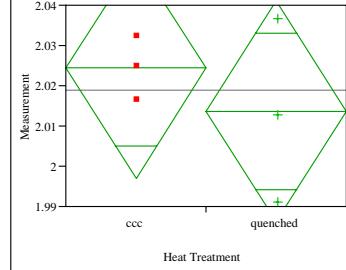
Difference -0.00394 t Ratio -0.42021  
 Std Err Dif 0.00938 DF 4  
 Upper CL Dif 0.02209 Prob > |t| 0.6959  
 Lower CL Dif -0.02997 Prob > t 0.6520  
 Confidence 0.95 Prob < t 0.3480

Glass ID=SB4VAR51, Analyte=log[B ppm]



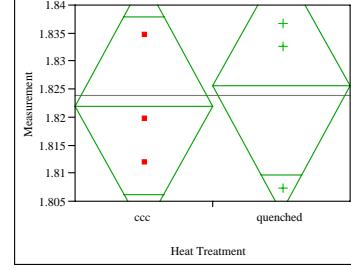
Difference 0.00118 t Ratio 0.053367  
 Std Err Dif 0.02216 DF 4  
 Upper CL Dif 0.06271 Prob > |t| 0.9600  
 Lower CL Dif -0.06034 Prob > t 0.4800  
 Confidence 0.95 Prob < t 0.5200

Glass ID=SB4VAR51, Analyte=log[Si ppm]



Difference -0.01074 t Ratio -0.77174  
 Std Err Dif 0.01391 DF 4  
 Upper CL Dif 0.02789 Prob > |t| 0.4833  
 Lower CL Dif -0.04937 Prob > t 0.7583  
 Confidence 0.95 Prob < t 0.2417

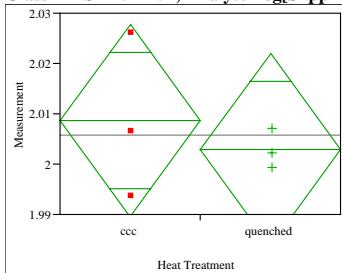
Glass ID=SB4VAR52, Analyte=log[Na ppm]



Difference 0.00353 t Ratio 0.310347  
 Std Err Dif 0.01137 DF 4  
 Upper CL Dif 0.03511 Prob > |t| 0.7718  
 Lower CL Dif -0.02805 Prob > t 0.3859  
 Confidence 0.95 Prob < t 0.6141

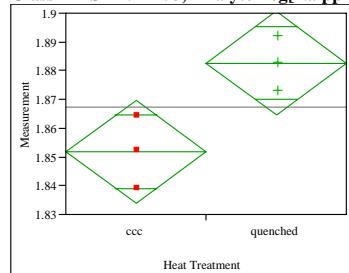
## Exhibit B6. Effects of Heat Treatment on PCT log(ppm)-Response of Study Glasses

Glass ID=SB4VAR52, Analyte=log[Si ppm]



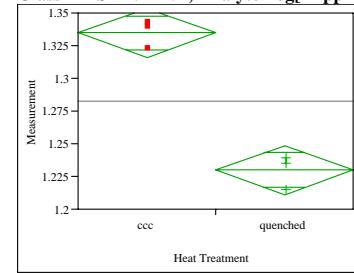
Difference -0.00576 t Ratio -0.59124  
Std Err Dif 0.00974 DF 4  
Upper CL Dif 0.02128 Prob > |t| 0.5862  
Lower CL Dif -0.03279 Prob > t 0.7069  
Confidence 0.95 Prob < t 0.2931

Glass ID=SB4VAR53, Analyte=log[Na ppm]



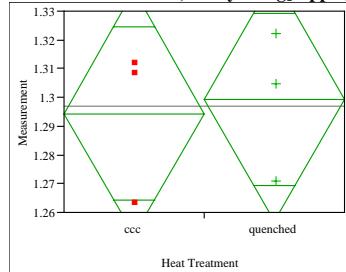
Difference 0.030832 t Ratio 3.362631  
Std Err Dif 0.009169 DF 4  
Upper CL Dif 0.056290 Prob > |t| 0.0282  
Lower CL Dif 0.005375 Prob > t 0.0141  
Confidence 0.95 Prob < t 0.9859

Glass ID=SB4VAR54, Analyte=log[Li ppm]



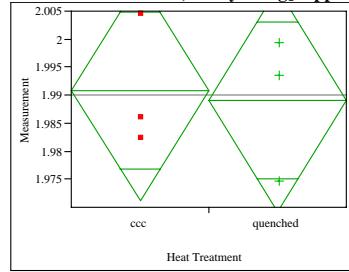
Difference -0.10497 t Ratio -10.9453  
Std Err Dif 0.00959 DF 4  
Upper CL Dif -0.07834 Prob > |t| 0.0004  
Lower CL Dif -0.13160 Prob > t 0.9998  
Confidence 0.95 Prob < t 0.0002

Glass ID=SB4VAR53, Analyte=log[B ppm]



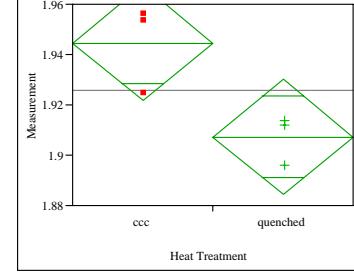
Difference 0.00491 t Ratio 0.22653  
Std Err Dif 0.02165 DF 4  
Upper CL Dif 0.06503 Prob > |t| 0.8319  
Lower CL Dif -0.05522 Prob > t 0.4159  
Confidence 0.95 Prob < t 0.5841

Glass ID=SB4VAR53, Analyte=log[Si ppm]



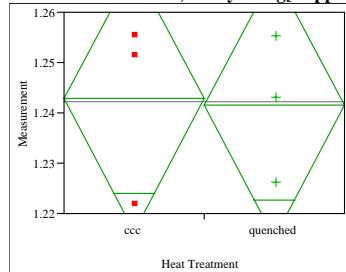
Difference -0.00175 t Ratio -0.17338  
Std Err Dif 0.01008 DF 4  
Upper CL Dif 0.02623 Prob > |t| 0.8708  
Lower CL Dif -0.02972 Prob > t 0.5646  
Confidence 0.95 Prob < t 0.4354

Glass ID=SB4VAR54, Analyte=log[Na ppm]



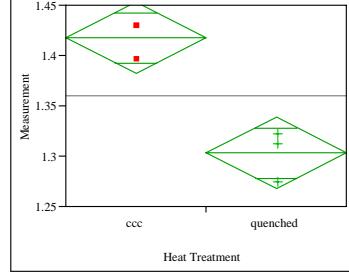
Difference -0.03731 t Ratio -3.20101  
Std Err Dif 0.01165 DF 4  
Upper CL Dif -0.00495 Prob > |t| 0.0329  
Lower CL Dif -0.06966 Prob > t 0.9836  
Confidence 0.95 Prob < t 0.0164

Glass ID=SB4VAR53, Analyte=log[Li ppm]



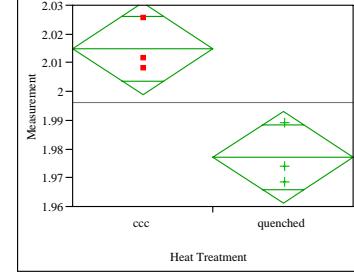
Difference -0.00129 t Ratio -0.09567  
Std Err Dif 0.01349 DF 4  
Upper CL Dif 0.03618 Prob > |t| 0.9284  
Lower CL Dif -0.03876 Prob > t 0.5358  
Confidence 0.95 Prob < t 0.4642

Glass ID=SB4VAR54, Analyte=log[B ppm]



Difference -0.11449 t Ratio -6.28923  
Std Err Dif 0.01820 DF 4  
Upper CL Dif -0.06395 Prob > |t| 0.0033  
Lower CL Dif -0.16504 Prob > t 0.9984  
Confidence 0.95 Prob < t 0.0016

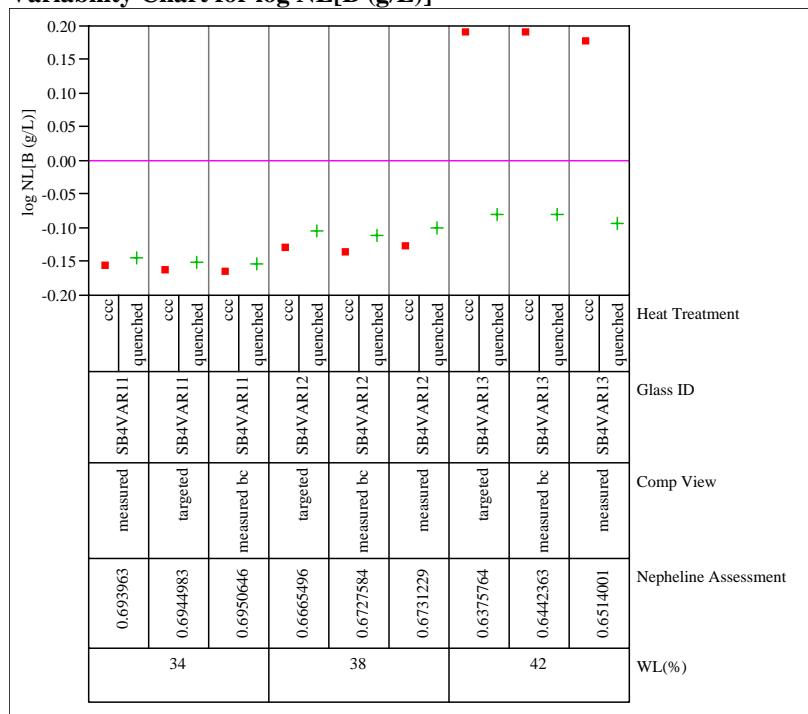
Glass ID=SB4VAR54, Analyte=log[Si ppm]



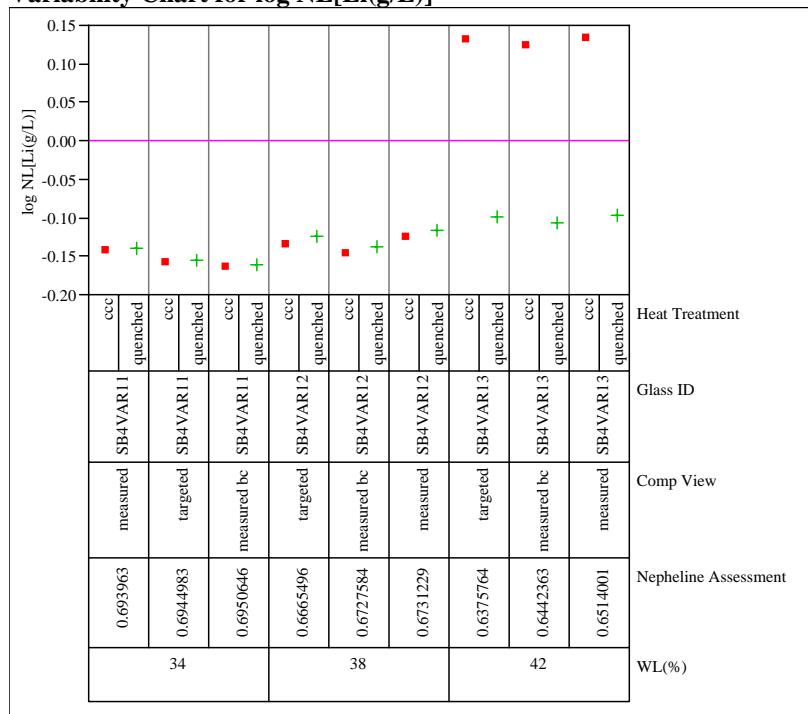
Difference -0.03775 t Ratio -4.64811  
Std Err Dif 0.00812 DF 4  
Upper CL Dif -0.01520 Prob > |t| 0.0097  
Lower CL Dif -0.06029 Prob > t 0.9952  
Confidence 0.95 Prob < t 0.0048

## Exhibit B7. Effects of Heat Treatment for Study Glasses by Compositional View

**Sludge Case=Case 1**  
**Variability Chart for log NL[B (g/L)]**



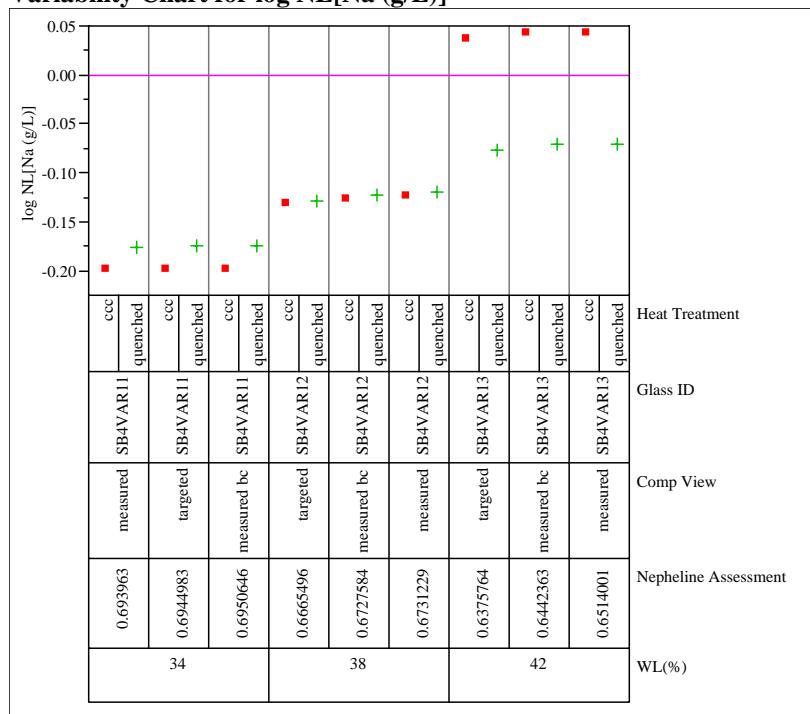
**Sludge Case=Case 1**  
**Variability Chart for log NL[Li(g/L)]**



## Exhibit B7. Effects of Heat Treatment for Study Glasses by Compositional View

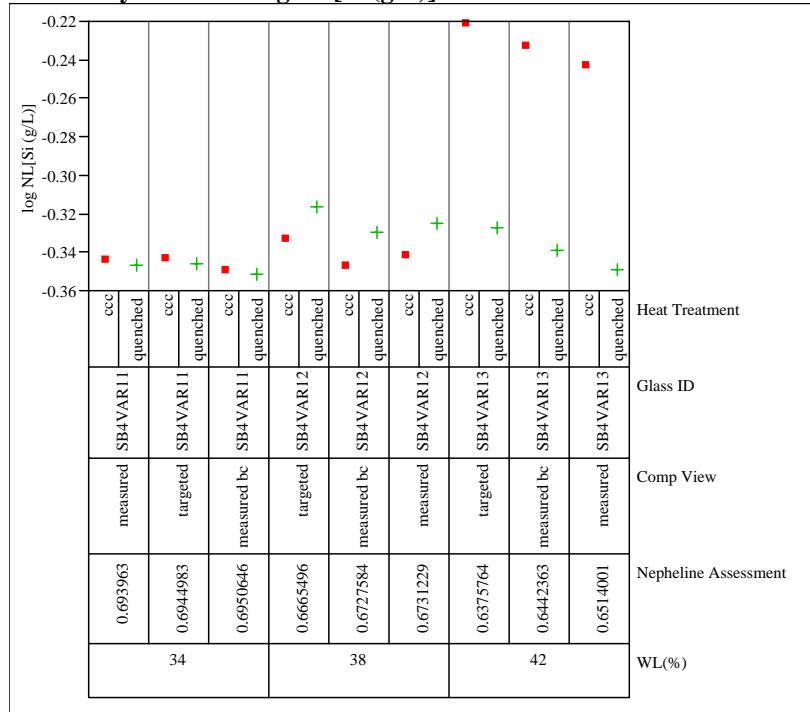
### Sludge Case=Case 1

#### Variability Chart for log NL[Na (g/L)]



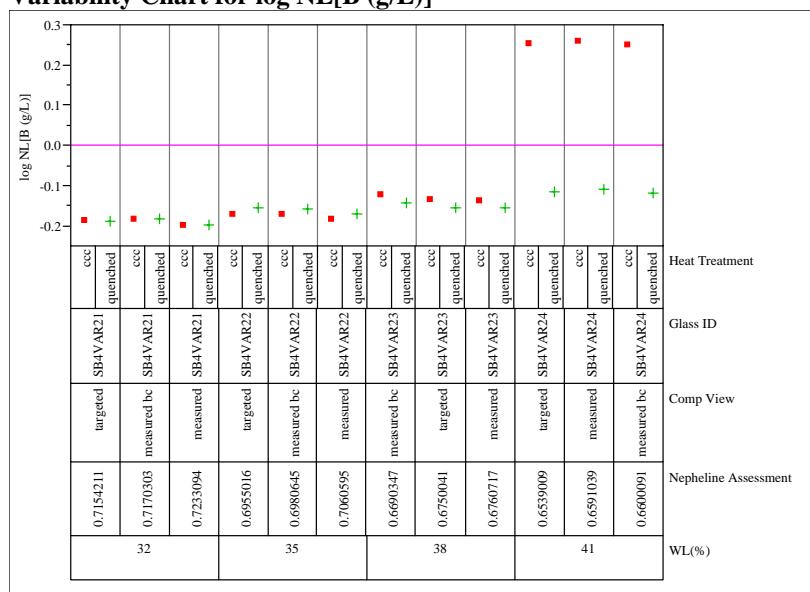
### Sludge Case=Case 1

#### Variability Chart for log NL[Si (g/L)]

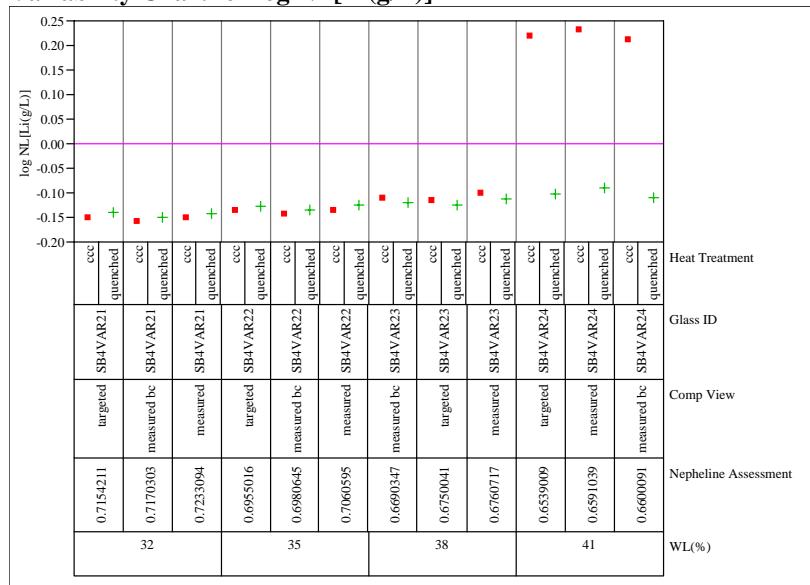


## Exhibit B7. Effects of Heat Treatment for Study Glasses by Compositional View

**Sludge Case=Case 2**  
**Variability Chart for log NL[B (g/L)]**



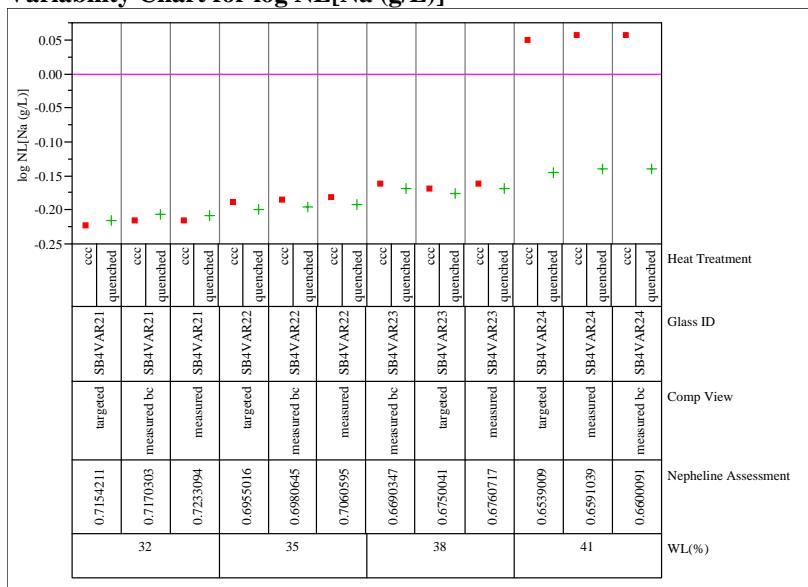
**Sludge Case=Case 2**  
**Variability Chart for log NL[Li(g/L)]**



## Exhibit B7. Effects of Heat Treatment for Study Glasses by Compositional View

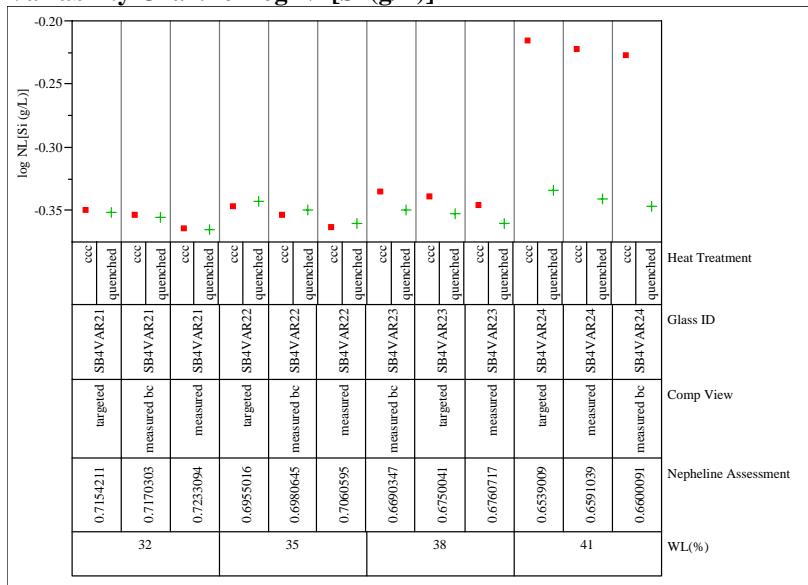
### Sludge Case=Case 2

#### Variability Chart for log NL[Na (g/L)]



### Sludge Case=Case 2

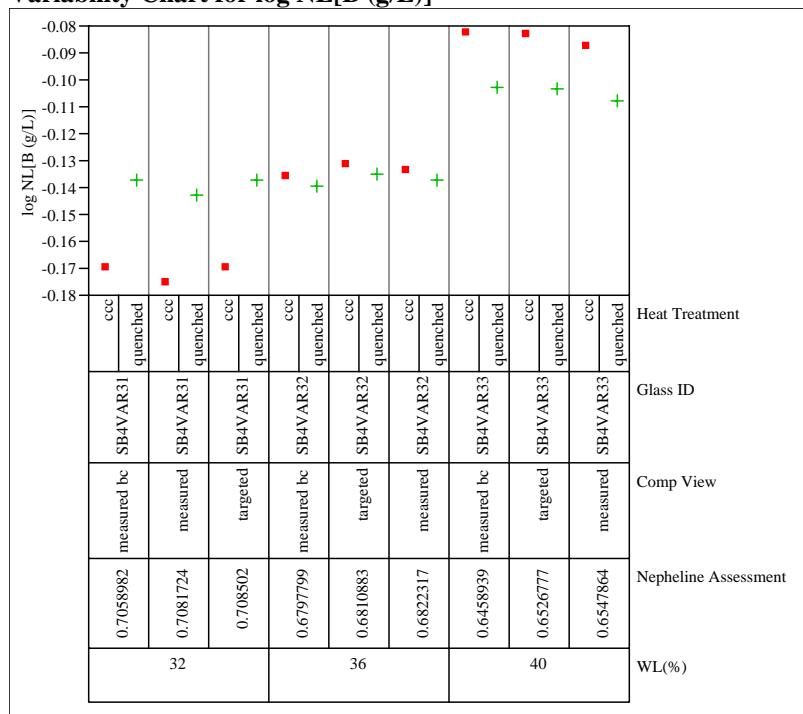
#### Variability Chart for log NL[Si (g/L)]



## Exhibit B7. Effects of Heat Treatment for Study Glasses by Compositional View

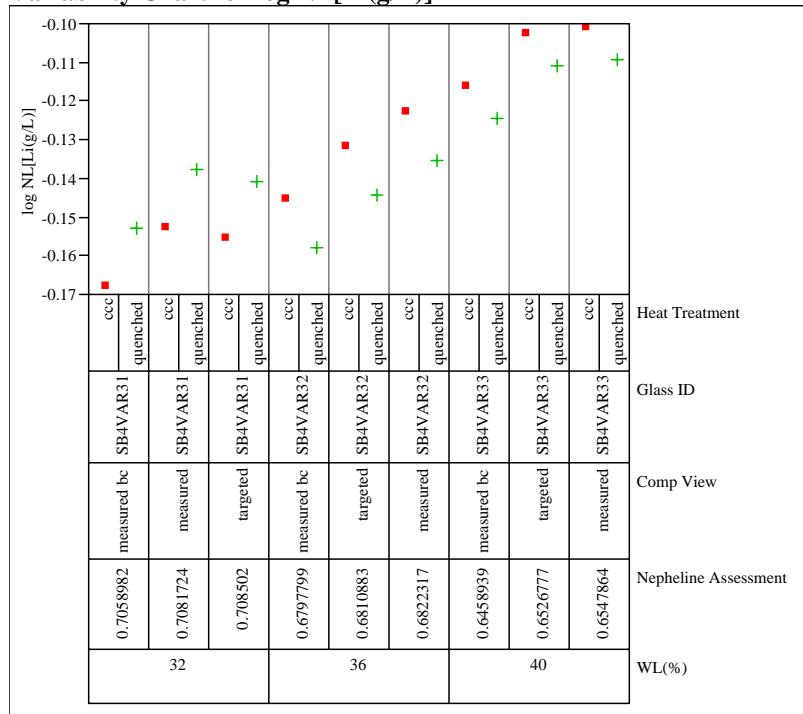
### Sludge Case=Case 3

#### Variability Chart for log NL[B (g/L)]



### Sludge Case=Case 3

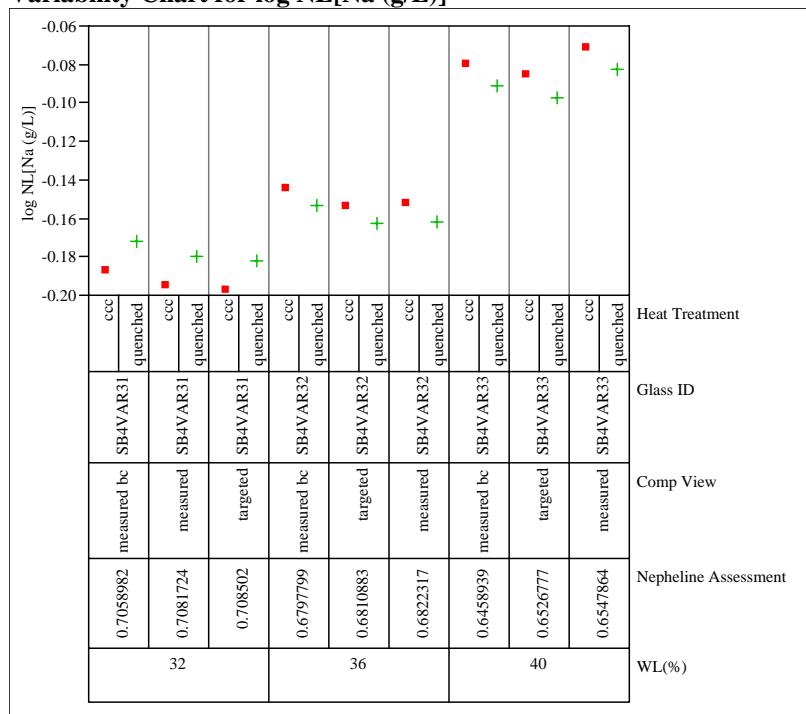
#### Variability Chart for log NL[Li(g/L)]



## Exhibit B7. Effects of Heat Treatment for Study Glasses by Compositional View

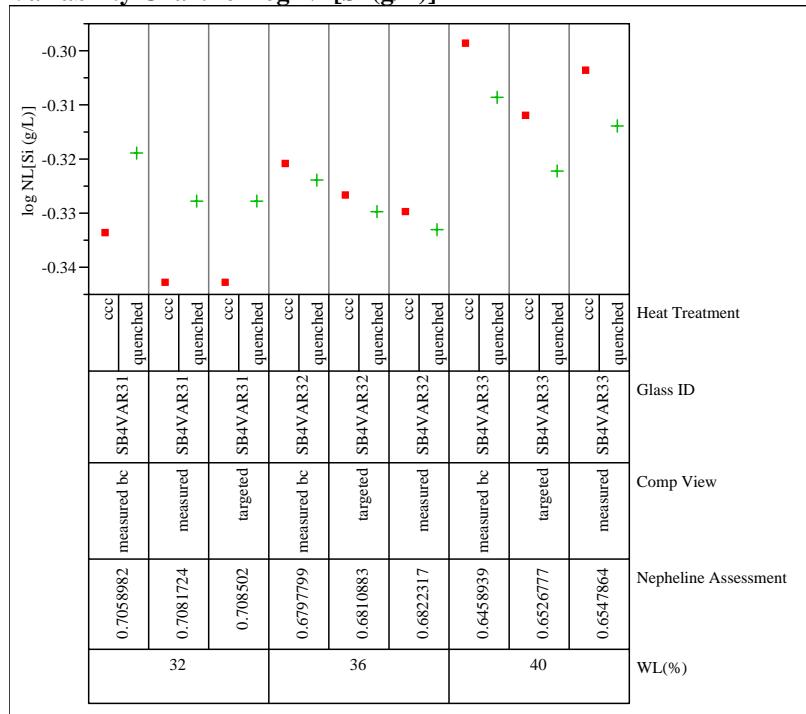
### Sludge Case=Case 3

#### Variability Chart for log NL[Na (g/L)]



### Sludge Case=Case 3

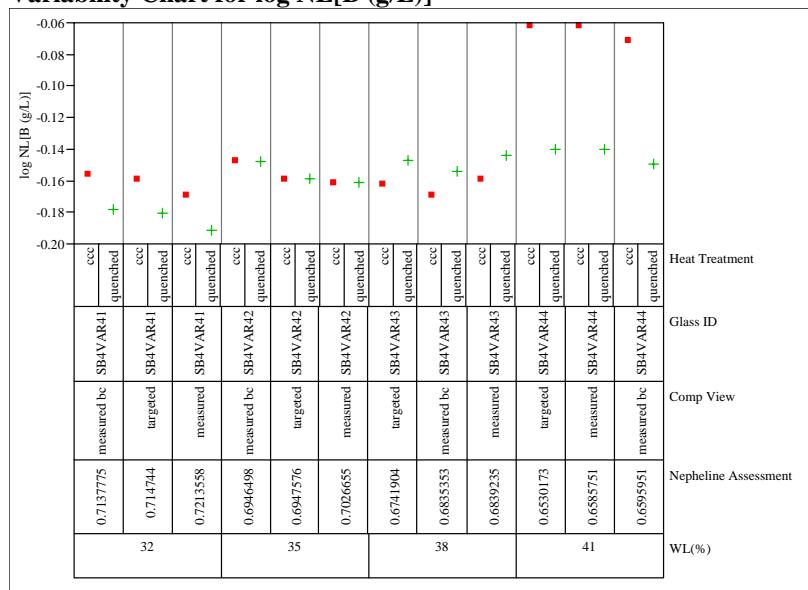
#### Variability Chart for log NL[Si (g/L)]



## Exhibit B7. Effects of Heat Treatment for Study Glasses by Compositional View

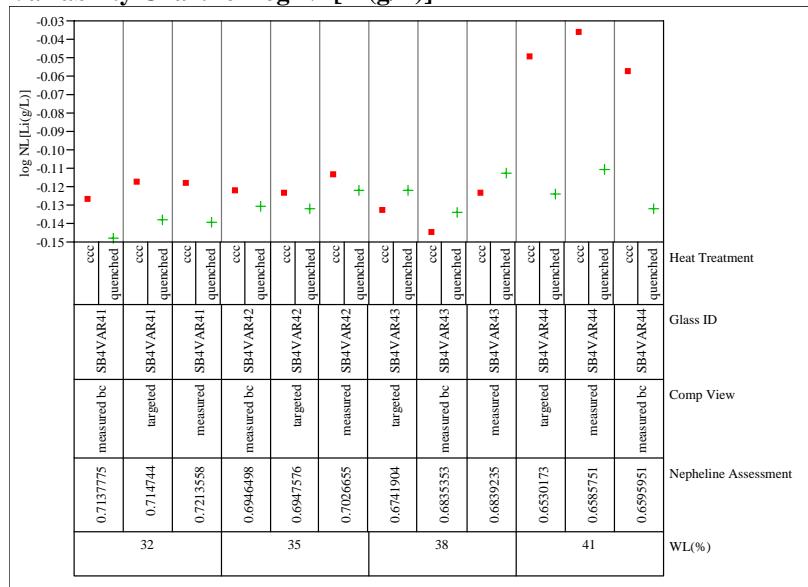
Sludge Case=Case 4

Variability Chart for log NL[B (g/L)]



Sludge Case=Case 4

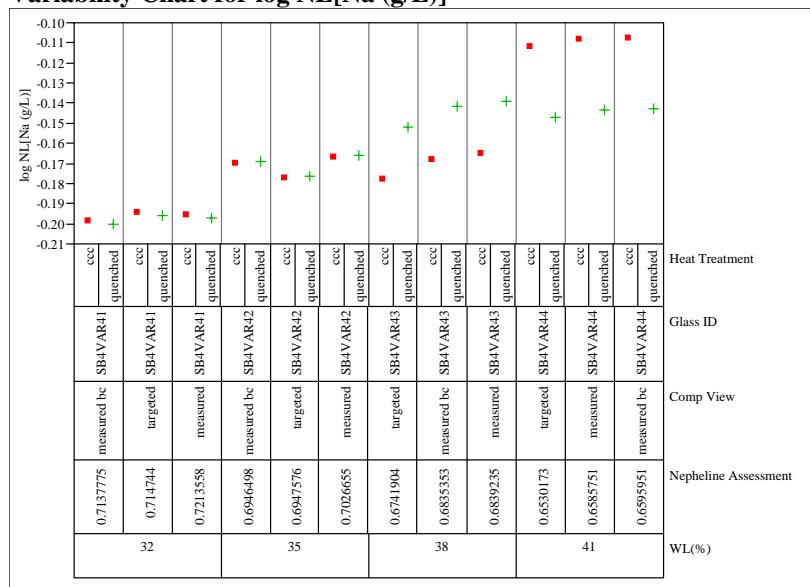
Variability Chart for log NL[Li(g/L)]



## Exhibit B7. Effects of Heat Treatment for Study Glasses by Compositional View

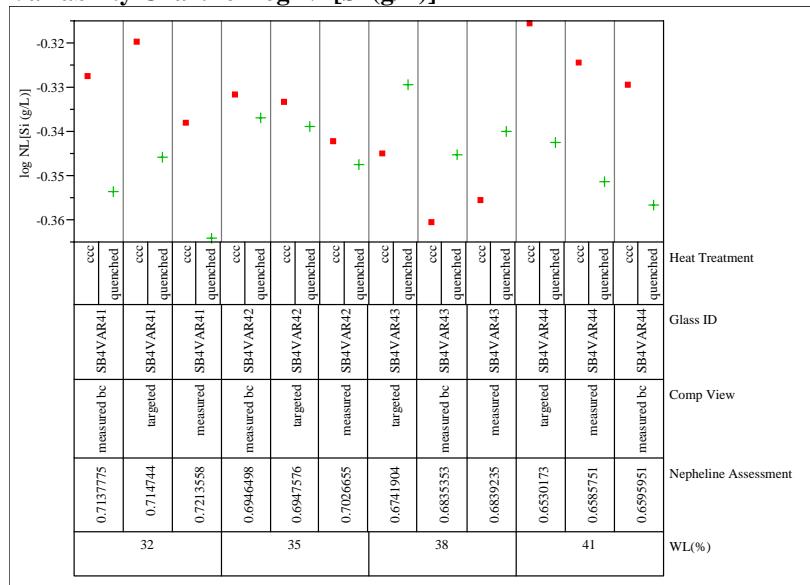
### Sludge Case=Case 4

#### Variability Chart for log NL[Na (g/L)]



### Sludge Case=Case 4

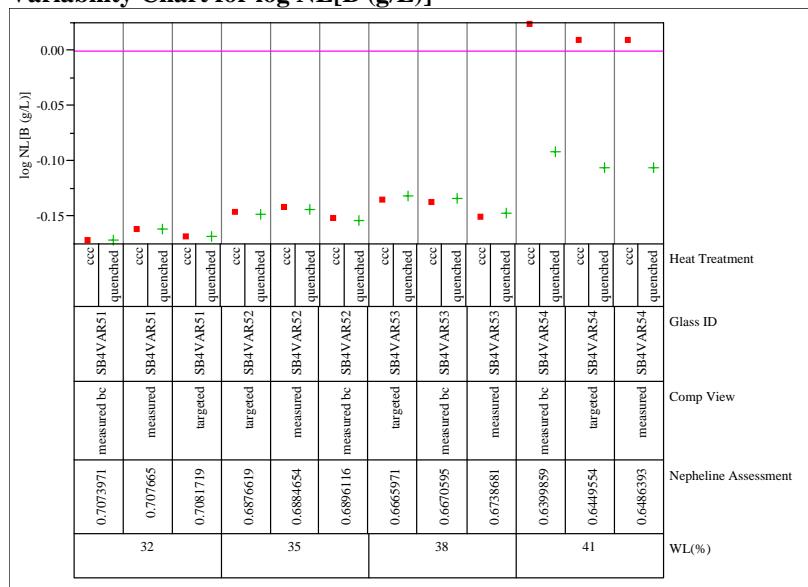
#### Variability Chart for log NL[Si (g/L)]



## Exhibit B7. Effects of Heat Treatment for Study Glasses by Compositional View

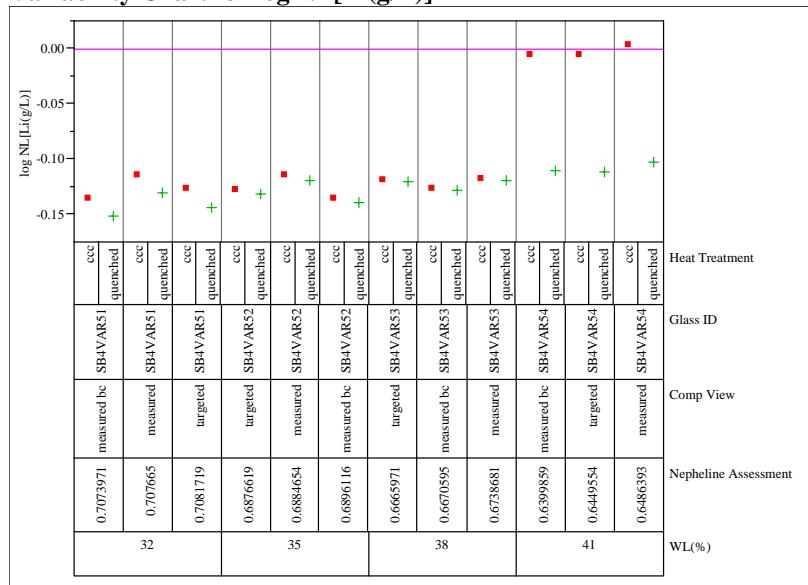
### Sludge Case=Case 5

#### Variability Chart for log NL[B (g/L)]



### Sludge Case=Case 5

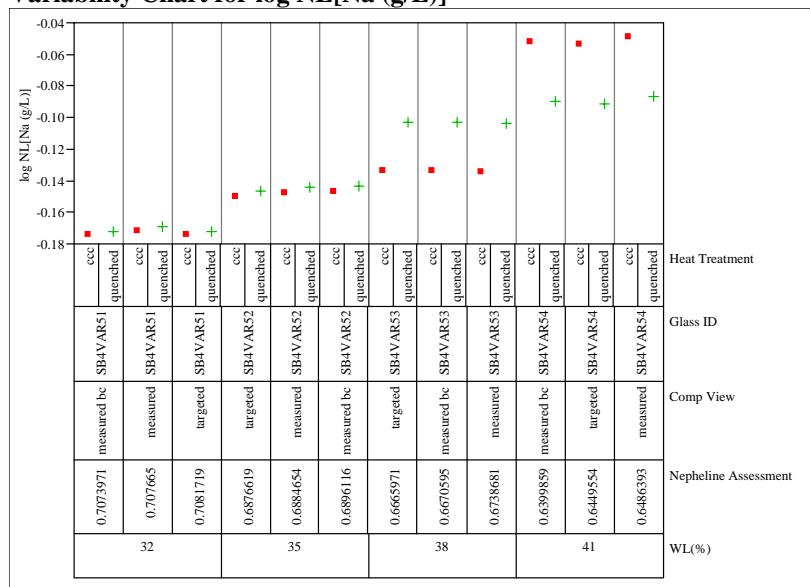
#### Variability Chart for log NL[Li(g/L)]



## Exhibit B7. Effects of Heat Treatment for Study Glasses by Compositional View

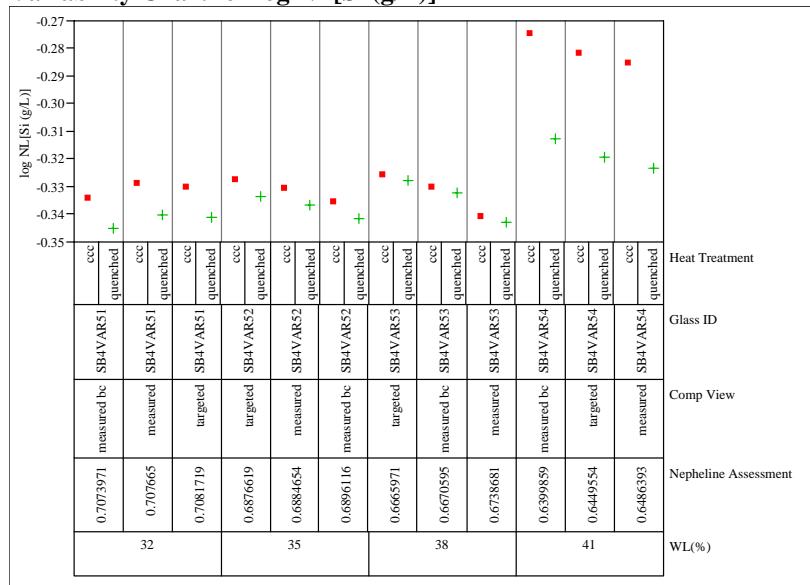
### Sludge Case=Case 5

#### Variability Chart for log NL[Na (g/L)]



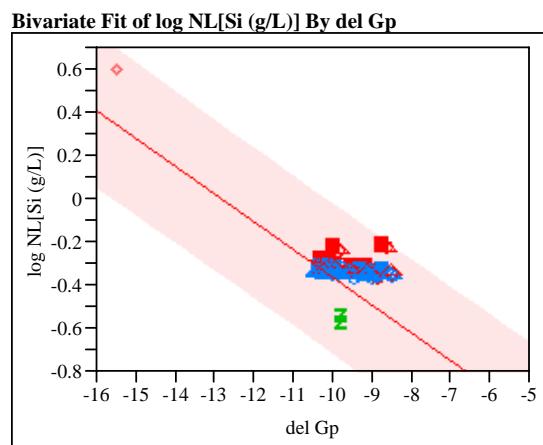
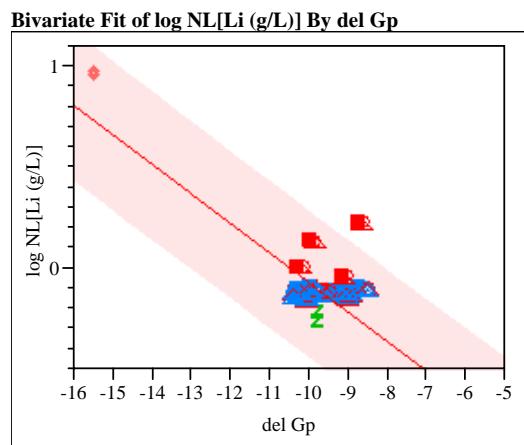
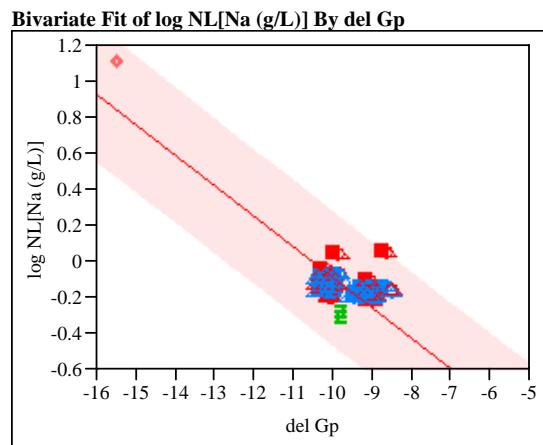
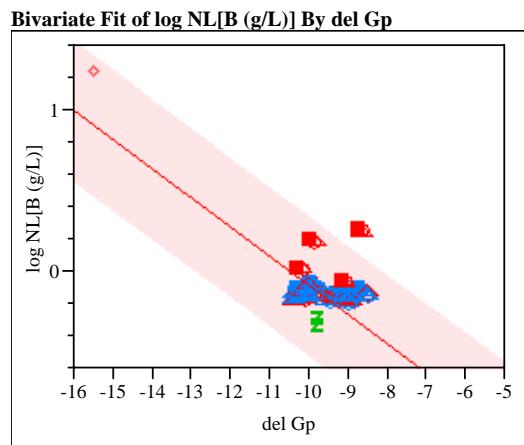
### Sludge Case=Case 5

#### Variability Chart for log NL[Si (g/L)]



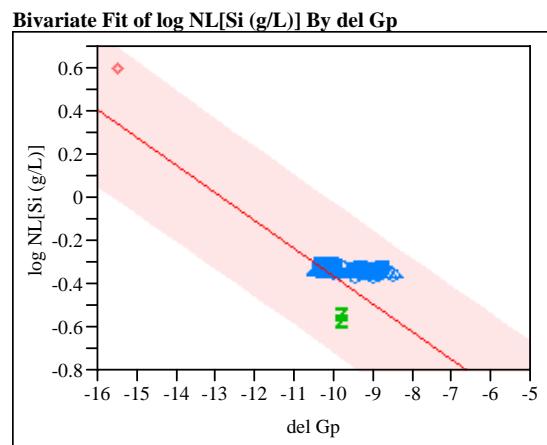
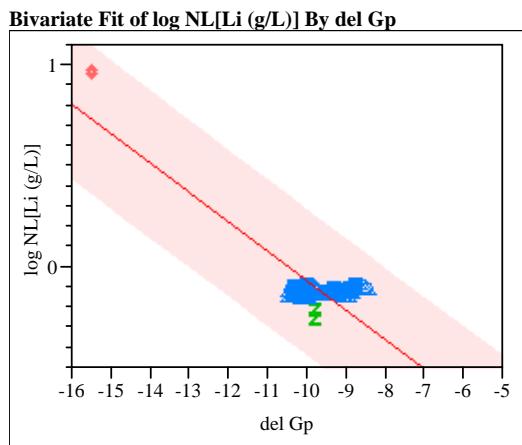
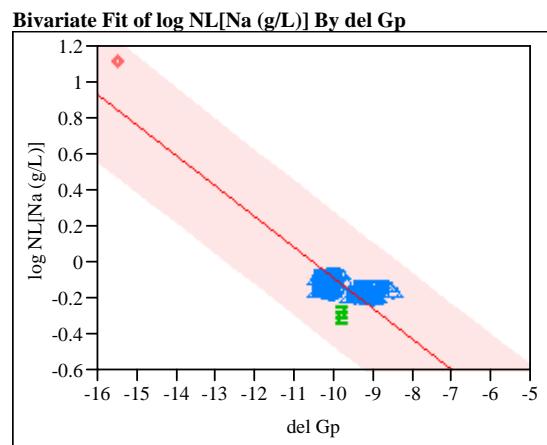
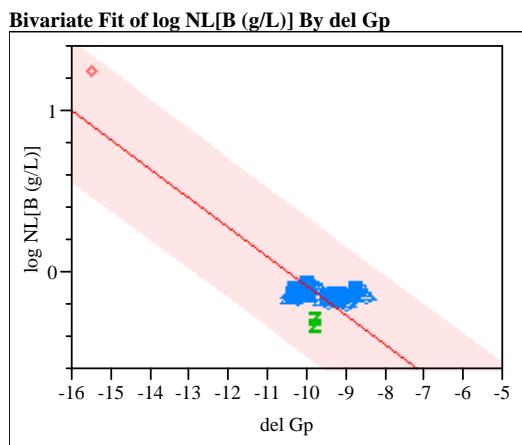
**Exhibit B8. del G<sub>p</sub> ( $\Delta G_p$ ) Predictions versus Common Logarithm Normalized Leachate (log NL[.]) for B, Li, Na, and Si Over All Compositional Views and Heat Treatments**

Legend		Heat Treatment	Composition
<b>z</b>	<b>1</b>	ARM	ARM
<b>o</b>	<b>2</b>	ccc	measured
<b>△</b>	<b>3</b>	ccc	measured bc
<b>■</b>	<b>4</b>	ccc	targeted
<b>◊</b>	<b>5</b>	EA	EA
<b>○</b>	<b>6</b>	quenched	measured
<b>△</b>	<b>7</b>	quenched	measured bc
<b>■</b>	<b>8</b>	quenched	targeted



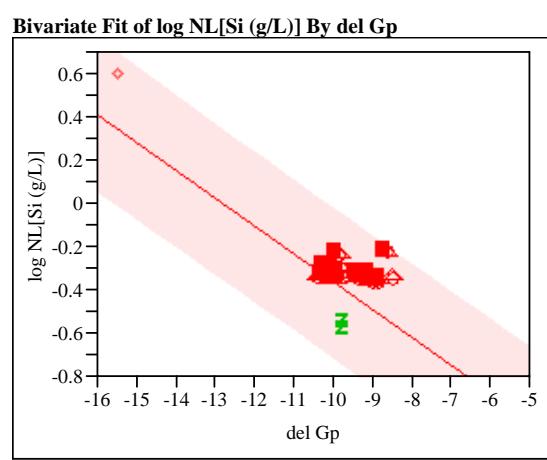
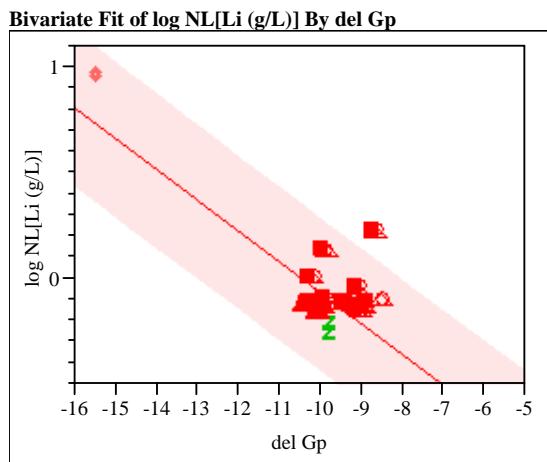
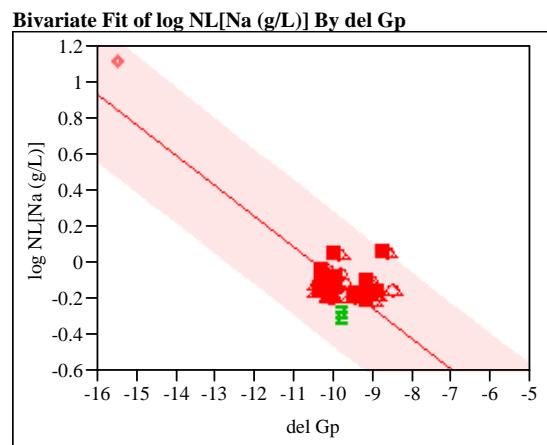
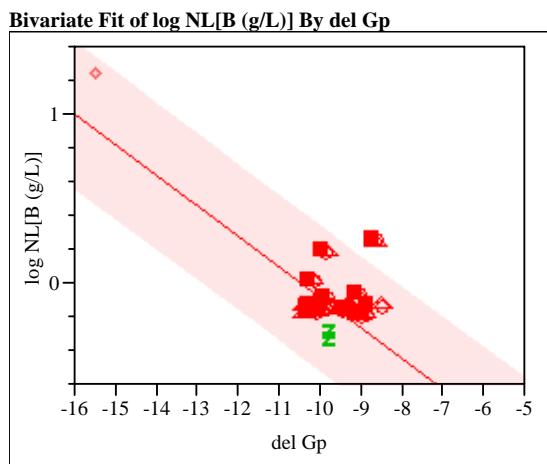
**Exhibit B9. del G<sub>p</sub> ( $\Delta G_p$ ) Predictions versus Common Logarithm Normalized Leachate (log NL[.]) for B, Li, Na, and Si Over All Compositional Views for Quenched Glasses**

Legend		Heat Treatment	Composition
z	1	ARM	ARM
o	2	ccc	measured
△	3	ccc	measured bc
■	4	ccc	targeted
◊	5	EA	EA
○	6	quenched	measured
△	7	quenched	measured bc
■	8	quenched	targeted



**Exhibit B10. del Gp ( $\Delta G_p$ ) Predictions versus Common Logarithm Normalized Leachate (log NL[.]) for B, Li, Na, and Si Over All Compositional Views for ccc Glasses**

Legend		Heat Treatment	Composition
	1	ARM	ARM
	2	ccc	measured
	3	ccc	measured bc
	4	ccc	targeted
	5	EA	EA
	6	quenched	measured
	7	quenched	measured bc
	8	quenched	targeted



## **APPENDIX C**

### **COMPARISON OF SME BATCH COMPOSITIONS TO VARIABILITY STUDY GLASS COMPOSITIONS**

SME Batch	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	Na <sub>2</sub> O	U <sub>3</sub> O <sub>8</sub>
	wt%			
402	6.61	12.50	12.72	3.31
403	7.11	9.74	11.22	2.43
404	7.90	9.33	11.56	2.42
405	8.06	8.64	10.54	2.42
406	8.35	9.26	11.44	2.35
407	7.79	8.79	11.18	2.19
408	7.86	8.63	11.60	2.81
409	8.33	9.24	11.26	2.43
410	7.80	8.93	11.80	2.35
411	8.76	9.75	10.69	2.46
412	8.22	9.40	11.39	2.41
413	7.80	8.83	11.09	2.28
414	7.97	9.09	10.86	2.34
415	8.12	9.38	9.47	2.30
416	8.45	9.33	10.47	2.26
417	8.32	9.46	10.35	2.15
418	8.47	9.64	10.43	2.08
419	8.14	8.98	11.04	2.51
420	7.88	9.02	11.76	2.16
421	8.21	9.27	10.36	2.63
422	7.52	8.73	10.97	2.15
423	7.72	8.76	10.81	2.21
424	7.87	8.80	11.39	2.15
425	8.18	9.44	12.39	2.36
426	7.74	8.56	11.34	2.04
427	8.43	8.57	11.56	1.95
428	8.46	8.98	12.29	2.20
429	8.33	8.83	11.23	2.15
430	8.29	9.07	11.00	3.02
431	8.54	9.46	11.68	3.14
432	7.88	8.63	11.66	2.96
433	8.13	9.12	11.47	2.94
434	7.65	8.12	12.19	2.75
435	7.29	7.94	11.86	2.66
436	8.03	8.73	11.63	2.46
<b>MINIMUM</b>	6.61	7.94	9.47	1.95
<b>MAXIMUM</b>	8.76	12.50	12.72	3.31

Glass ID	WL (%)	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	Na <sub>2</sub> O	U <sub>3</sub> O <sub>8</sub>
		wt%			
<b>SB4VAR11</b>	34	8.46	9.62	12.26	2.94
<b>SB4VAR12</b>	38	9.46	10.75	12.76	3.28
<b>SB4VAR13</b>	42	10.46	11.88	13.26	3.63
<b>SB4VAR21</b>	32	8.31	9.47	10.98	2.89
<b>SB4VAR22</b>	35	9.09	10.36	11.26	3.16
<b>SB4VAR23</b>	38	9.86	11.25	11.54	3.43
<b>SB4VAR24</b>	41	10.64	12.14	11.82	3.70
<b>SB4VAR31</b>	32	8.00	9.13	11.93	2.79
<b>SB4VAR32</b>	36	9.01	10.27	12.42	3.13
<b>SB4VAR33</b>	40	10.01	11.41	12.92	3.48
<b>SB4VAR41</b>	32	8.00	9.20	11.34	2.80
<b>SB4VAR42</b>	35	8.75	10.06	11.66	3.06
<b>SB4VAR43</b>	38	9.50	10.92	11.97	3.32
<b>SB4VAR44</b>	41	10.25	11.79	12.28	3.59
<b>SB4VAR51</b>	32	7.71	8.87	12.25	2.70
<b>SB4VAR52</b>	35	8.43	9.70	12.65	2.95
<b>SB4VAR53</b>	38	9.15	10.53	13.04	3.21
<b>SB4VAR54</b>	41	9.88	11.37	13.44	3.46
<b>MINIMUM</b>		7.71	8.87	10.98	2.70
<b>MAXIMUM</b>		<b>10.64</b>	12.14	<b>13.44</b>	<b>3.70</b>
<b>SB4PS1</b>		7.61	8.07	12.12	2.73
<b>SB4PS2</b>		7.37	8.03	11.98	2.68
<b>SB4PS3</b>		7.92	9.00	11.99	2.75
<b>SB4PS4</b>		8.29	9.42	12.18	2.88
<b>SB4PS5</b>		8.49	9.65	12.28	2.94
<b>MINIMUM</b>		7.37	8.03	11.98	2.68
<b>MAXIMUM</b>		8.49	9.65	12.28	2.94

**Table C1. Comparison of SME batch compositions and variability study glass compositions.** Note – the variability study glass compositions (SB4VAR11 – SB4VAR54 and SB4PS1 – SB4PS5) are target compositions. The maximum contents of the variability study glasses in bold indicate that these are outside the range of the SME batch compositions.

**Distribution:**

C.J. Bannochie, 773-42A  
A.B. Barnes, 999-W  
D.R. Best, 786-1A  
D.B. Burns, 786-5A  
D.A. Crowley, 999-W  
B.A. Davis, 704-27S  
T.B. Edwards, 999-W  
H.H. Elder, 766-H  
T.L. Fellinger, 704-26S  
K.M. Fox, 999-W  
J.M. Gillam, 766-H  
J.C. Griffin, 773-A  
B.A. Hamm, 766-H  
C.C. Herman, 999-W  
J.F. Iaukea, 704-30S  
J.E. Marra, 773-A  
R.T. McNew, 704-27S  
T.A. Nance, 773-42A  
J.D. Newell, 999-W  
J.E. Occhipinti, 704-S  
D.K. Peeler, 999-W  
F.C. Raszewski, 999-W  
J.W. Ray, 704-S  
I.A. Reamer, 999-1W  
H.B. Shah, 766-H  
M.E. Smith, 999-W  
M.E. Stone, 999-W  
J. Stuberfield, 766-H  
M.F. Williams, 999-1W  
R.J. Workman, 999-1W  
A.L. Youchak, 999-W