

QUANTIFICATION OF FUGITIVE REACTIVE ALKENE EMISSIONS FROM
PETROCHEMICAL PLANTS WITH PERFLUOROCARBON TRACERS

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Introduction

Recent studies demonstrate the impact of fugitive emissions of reactive alkenes on the atmospheric chemistry of the Houston Texas metropolitan area (1). Petrochemical plants located in and around the Houston area emit atmospheric alkenes, such as ethene, propene and 1,3-butadiene. The magnitude of emissions is a major uncertainty in assessing their effects. Even though the petrochemical industry reports that fugitive emissions of alkenes have been reduced to less than 0.1% of daily production, recent measurement data, obtained during the TexAQS 2000 experiment indicates that emissions are perhaps a factor of ten larger than estimated values. Industry figures for fugitive emissions are based on adding up estimated emission factors for every component in the plant to give a total estimated emission from the entire facility. The dramatic difference between estimated and measured rates indicates either that calculating emission fluxes by summing estimates for individual components is seriously flawed, possibly due to individual components leaking well beyond their estimated tolerances, that not all sources of emissions for a facility are being considered in emissions estimates, or that there are known sources of emissions that are not being reported. This experiment was designed to confirm estimates of reactive alkene emissions derived from analysis of the TexAQS 2000 data by releasing perfluorocarbon tracers (PFTs) at a known flux from a petrochemical plant and sampling both the perfluorocarbon tracer and reactive alkenes downwind using the Piper-Aztec research aircraft operated by Baylor University.

PFTs have been extensively used to determine leaks in pipelines, air infiltration in buildings, and to characterize the transport and dispersion of air parcels in the atmosphere. Over 20 years of development by the Tracer Technology Center (TTC) has produced a range of analysis instruments, field samplers and PFT release equipment that have been successfully deployed in a large variety of experiments. PFTs are inert, nontoxic, noncombustible and non-reactive. Up to seven unique PFTs can be simultaneously released, sampled and analyzed and the technology is well suited for determining emission fluxes from large petrochemical facilities.

The PFT experiment described here was designed to quantitate alkene emissions from a single petrochemical facility, but such experiments could be applied to other industrial sources or groups of sources in the Houston area.

Experimental Procedure

Measurement of the reactive alkene fugitive emission factor of an individual plant

The analysis of the TexAQS 2000 data provided a preliminary alkene (propene and ethene) emission flux from the Conoco/Phillips Sweeny petrochemical plant in Old Ocean, Texas. This flux was calculated from measurements of the concentrations of ethene, propene and NO_x in the plume downwind from the plant. An alkene emission flux of about ten times larger than estimated was found (1).

In this project, the reactive alkene flux from the Sweeny facility is estimated by releasing PFTs at known rate from the plant. The reactive alkenes and the PFT concentrations were estimated from canister samples collected by aircraft flying in the plume downwind of the plant. Alkene emission fluxes, $[\text{alkene}]_{\text{flux}}$, were calculated from

$$[\text{alkene}]_{\text{flux}} = ([\text{alkene}]_{\text{conc}} / [\text{PFT}]_{\text{conc}}) [\text{PFT}]_{\text{flux}}$$

where $([\text{alkene}]_{\text{conc}} / [\text{PFT}]_{\text{conc}})$ is the concentration ratio measured in downwind samples and $[\text{PFT}]_{\text{flux}}$ is the known PFT emission flux at the plant. This assumes that the emission sources of the reactive alkenes and PFTs are collocated. Concentrations of PFTs and reactive alkenes measured downwind were corrected for background concentrations measured upwind. Measurements were made in the fall of 2003. The experimental approach is detailed in the following sections.

PFT Emission Flux

The PFT emission flux from the plant must be sufficient so that PFT concentrations are quantifiable in 6-L canister samples collected in downwind plume. The dilution factor was estimated from measurements downwind of the Sweeny plant made during the TexAQS 2000 experiment. Typical NO_2 concentrations were 3 ppb(v). From an NO_2 emission of 5108 tons/y as given in an 1999 EPA AIRS inventory, the NO_2 emission rate is equivalent to 4700 L(gas phase)/min. Thus, an emission of 4700 L/min yielded 3 ppb(v) in aircraft sampling. We chose a PFT emission rate to yield a concentration well above the background. PFTs chosen for this experiment were perfluorodimethylcyclobutane, commonly called PDCB and perfluoromethylcyclopentane, commonly called PMCP. The PDCB is composed of two isomers and the gas chromatographic (GC) system used to analyze PFTs can be set to separate these isomers. PDCB has a background of 2.0 ppq (parts per quadrillion or parts per 10^{15}), composed of about 72.5% 1,2 PDCB and 27.5% 1,3 PDCB. PMCP has an ambient background of 9.5 ppq. A possible advantage of using PDCB is that it is composed of two resolvable PFTs (equivalent to two tracers) whereas PMCP is a single component PFT.

PFT Release Cylinder Preparation

Based on the above preliminary transport and dilution calculation two cylinders of PFT release gases were prepared, one with PDCB and one with PMCP. The aluminum cylinders have a capacity of 137 cu feet at 1800 psi. Based on dew point considerations it was decided to prepare the cylinders with a total pressure of 200 psi, in order to avoid condensing liquid PFT as the cylinder pressure dropped. Consequently, only 15.2 cu ft or 430 liters of release gas were prepared for each tracer.

The PFT release gases were prepared by first by removing dissolved gases from the liquid PFTs. The PFT can dissolve about an equal volume (STP) of air per volume of liquid PFT. The dissolved air was removed by repeated freeze-thaw cycles until the vapor pressure of the PFT was reached. For PDCB, 126.6 grams (PCR lot 5479) were volatilized into a pre-evacuated (less than 0.2 torr) cylinder (Cylinder ID CC15276) and pressured with 99.9% nitrogen for a design concentration of 24,200 ppm. Likewise, 114 grams of PMCP (3 bottles of PCR >90% PMCP, lot 12483-4, and remainder Flutec PP1/2, 2/23/88 PP1/2(B)) were volatilized into cylinder CC4921 for a design concentration of 20,990 ppm.

The PFT release gases were analyzed on a HP 5890 gas chromatograph, with a Carbochrom capillary column with a thermal conductivity detector. Analysis of the prepared cylinders with both pure liquid PFTs and earlier analyzed standards indicated a measured concentration for PDCB of 22,212 ppm and 21,415 ppm for PMCP.

The PFT release cylinders contained 430 L (STP) of PFT tagged gas. The release at the Sweeny Plant was chosen to be 50 mL/min which was sufficient to provide 18 eight-hour-days of release for both PFTs.

PFT Release Deployment

The PFT release cylinders were shipped to the Sweeny plant in Old Ocean, Texas with regulators and calibrated flow restrictors. The regulator output pressure was set to provide 50 mL/min of flow through the flow restrictor. An electronic flowmeter was also sent to Sweeny for measurement of the PFT release rate on flight days.

During a July 2003 visit to Sweeny plant, two release sites were selected. The first site was near the compressors, the GPS coordinates were 29° 04.640'N and 95°44.683'W. This site was chosen since the compressors were identified as a possible source of leaking alkene. The PDCB source was placed at this site. The release cylinder was mounted at ground level and 10 foot section of 1/8 inch polyurethane tubing was used to raise the release height. The PFT release flow rate was checked at the flow restrictor and at the end of the 10 foot section and were found to be the same. The inlet of the water chiller was chosen as the release site for the PMCP tracer. The GPS coordinates were 29° 04.686'N and 95° 44.718'W. Again, it was thought the water chiller was possibly a source of alkene. At this site the cylinder was placed at ground level and

again about 20 foot of polyurethane tubing was used to position the release as close as possible to the water chiller inlet. During setup, the flow measured at the flow restrictor and the release point at the end of the 20 feet of tubing, were identical.

A secondary effort in this study was to estimate the NO_y emission flux, the GPS coordinates of the power plant, emitting the majority of the NO_y was $29^\circ 04.368' \text{N}$ and $95^\circ 44.732' \text{W}$, about 1933 feet from the PDCB release site.

A release protocol was developed and implemented. The sampling aircraft flew on days with appropriate wind direction and speed. On favorable days a call was placed to Sweeny before 11 AM. The two PFT release cylinders were opened at the cylinder head at least two hours before the aircraft arrived to assure that the tracer was transported downwind to the sampling area. An electronic flowmeter was used to control the flowrate to $50 \pm 5 \text{ mL/min}$; it only had to be adjusted once during the study. At the end of the sampling day, the flow was again measured and both cylinders were turned off.

Aircraft PFT Sampling Protocol

Replicate 6-L samples were taken aboard the Piper-Aztec, one for PFT analyses and the other for alkene and other hydrocarbon analyses. The aircraft sampling was a Texas Commission on Environmental Quality (TCEQ)/Baylor University effort. The aircraft flew four sampling runs under favorable synoptic conditions. The wind had to be from the SE to S to ensure that there was minimal background concentration of alkenes from upwind sources. Winds had to range from 5 to 10 mph to produce a well-defined downwind plume. On these days, a call was made to Sweeny to turn on the release cylinders and the aircraft air sampling instruments were turned on and calibrated. The aircraft also measured NO , NO_2 , NO_y , ozone, and the standard meteorological variables. A RAD monitor (Reactive Alkene Detector), provided a measure of the total alkene concentration and was used to locate the alkene plume and to determine when to open the sampling canisters(3).

Table 1 lists the dates of the four sampling flights. On each of these flights, samples were taken both upwind and downwind of the Sweeny plant. The upwind sample was used to measure the background PFT and alkene concentrations. The downwind plume samples were expected to contain both the emitted alkene and PFT. The sample time and aircraft event number is given for each sample. The GPS location of the aircraft at the start of sampling and the downwind distance from the PMCP tracer release site is also given. Note that there is only one downwind sample in the 11/20/2003 flight, because the plume could not be located according to the real time RAD monitor. After this flight, the flight plan was revised to increase the probability of locating the alkene plume. Generally the first downwind sample was about 1.5 miles downwind of Sweeny, and the second about 4 miles downwind.

Table 1

Date	Event	Sample	Sampling		Location		Distance to	
Number		Type	Start	End	Lat.(N)	Long.(W)	PMCP release	
							km	miles
11/20/2003	10	Upwind	14:49:08	14:49:29	29.042212	95.75304413	4.06	2.52
	15	Downwind	15:14:53	15:15:14	29.105884	95.75960159	3.38	2.10
11/25/2003	21	Upwind	14:24:03	14:24:24	29.039551	95.76618576	4.74	2.95
	27	Downwind	14:54:50	14:55:11	29.098845	95.76366425	2.91	1.81
	34	Downwind	15:17:30	15:17:51	29.105448	95.72710800	3.52	2.18
12/07/2003	6	Upwind	13:59:01	13:59:22	29.034008	95.72785568	5.19	3.22
	25	Downwind	14:54:03	14:54:24	29.100316	95.74945323	2.50	1.55
	30	Downwind	15:09:45	15:10:06	29.136886	95.74980164	6.55	4.07
12/14/2003	11	Upwind	14:25:50	14:26:11	29.035739	95.71270498	3.51	2.18
	27	Downwind	15:16:24	15:16:45	29.100049	95.75495529	2.61	1.62
	32	Downwind	15:43:16	15:43:37	29.132086	95.76791763	6.39	3.97
			PMCP Release Site		29.07810	95.745300		
			PDCB Release Site		29.07733	95.744717		

PFT Analysis

PFT canister samples were returned to the TTC at BNL for analysis. Table 2 gives the sampling date, event number, canister ID, and the initial canister pressure. The canisters were at sub-ambient pressure. Samples were extracted from canisters by pressurizing to two atmospheres with nitrogen. The last column is the amount of added nitrogen. This nitrogen had been previously analyzed on the PFT analysis system and verified as being free of PFT.

Three samples from each PFT canister were trapped on a CATS (Capillary Adsorbent Tracer Sampler), which is a small tube containing Ambersorb, a carbonaceous adsorbent which quantitatively collects any PFT in an air sample that is passed through it. The sample was withdrawn from the canister into a clean 1 liter sampling bag; which was then pumped through a CATS. After each sample the bag was purged with clean nitrogen and evacuated with a pump. This procedure was first tested with a blank canister filled with ambient air. The PFTs on the CATS were then thermally desorbed, separated by high-resolution GC and quantified by an ECD (electron capture detector). An exact transfer volume in this procedure need not be measured since the ambient background concentration of PMCH (perfluoromethylcyclohexane) in samples serves as an internal standard as explained below. After each sample, the bag was purged with clean nitrogen and evacuated with a pump. Chromatographic conditions were set to analyze only PDCB, PMCP and PMCH (perfluoromethylcyclohexane), the first two were released from the

Table 2

Date	Event Number	Sample Type	Canister ID	Sample Pressure Torr	Added Nitrogen psi
11/20/2003	10	Upwind	A-61	613	14.2
	15	Downwind	N-79	611	14.1
11/25/2003	21	Upwind	SJV-120	607	14.1
	27	Downwind	H-179	608	14.1
	34	Downwind	29	617	14.2
12/07/2003	6	Upwind	I-53	614	14.1
	25	Downwind	K-151	602	14.1
	30	Downwind	102	583	14.4
12/14/2003	11	Upwind	H-102	622	14
	27	Downwind	S-131	607	14.5
	32	Downwind	DU98102	604	14.5

plant; PMCH was not released but is has a constant, well measured ambient background concentration and is used here as an internal standard to account for dilution of the samples and enable the calculation of the actual PDCB and PMCP concentrations in the plume.

Figure 1 is a chromatogram of a nominal 100 femtoliter PFT standard which contains the first three PFTs. There are four peaks, the first two being the two isomers of PDCB, the third is PMCP and the last is PMCH, the internal standard. The numbers in green at the top are the retention times and the red ticks on the baseline are integration events. The analysis is complete in about 14 minutes, and is automated in batches of 23 analyses. Typically, a few of these 23 are PFT standards (as in Figure 1) and others are of ambient air (a chromatogram of the PFTs at their ambient concentrations). Such samples provide the necessary checks on the analysis system.

The results of the PFT analysis are given in Table 3. The first column gives the sample name and event number (see Table 2). The second column is a CATS ID, a unique number to track the samples. The last 8 columns are the retention times and area counts for the four peaks as illustrated in Figure 2. Each canister has three rows in this table since each canister yielded three samples; the third sample was generally the largest in volume. This is because it was initially expected that the PFT concentrations would be higher for the first two samples, more or less one liter samples. After the first two analyses for each canister was completed it was decided, based on the results to analyze the remainder as one sample. Note that several PFT standards and ambient air standard are included in these tables, since they are associated with this grouping of samples.

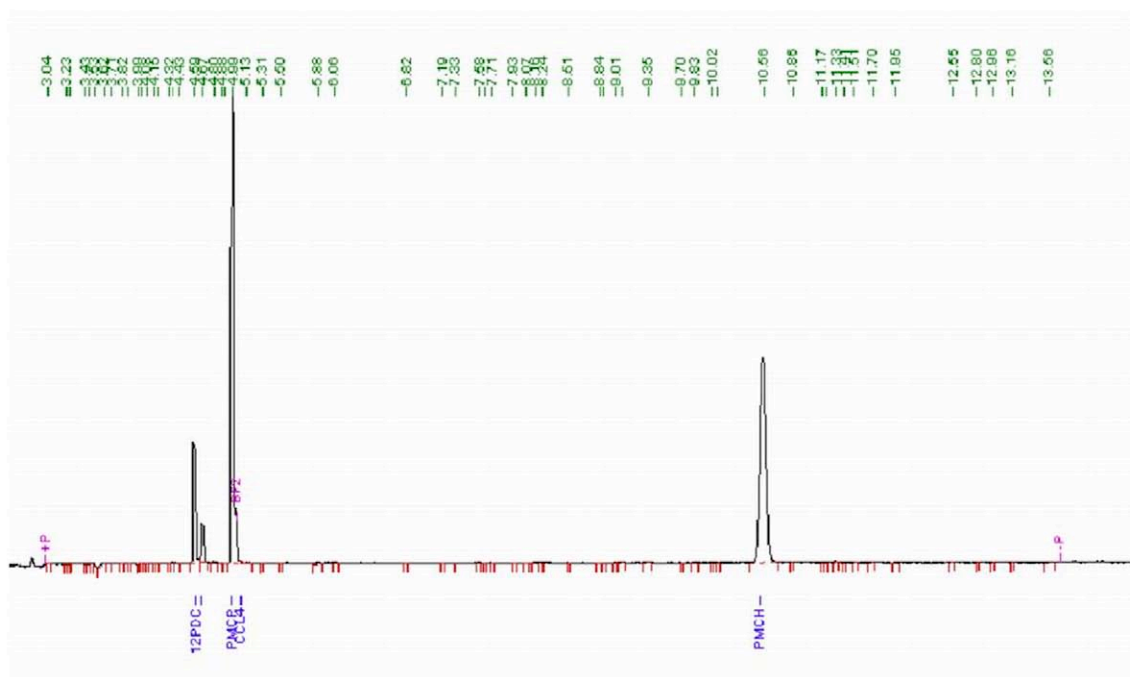


Figure 1

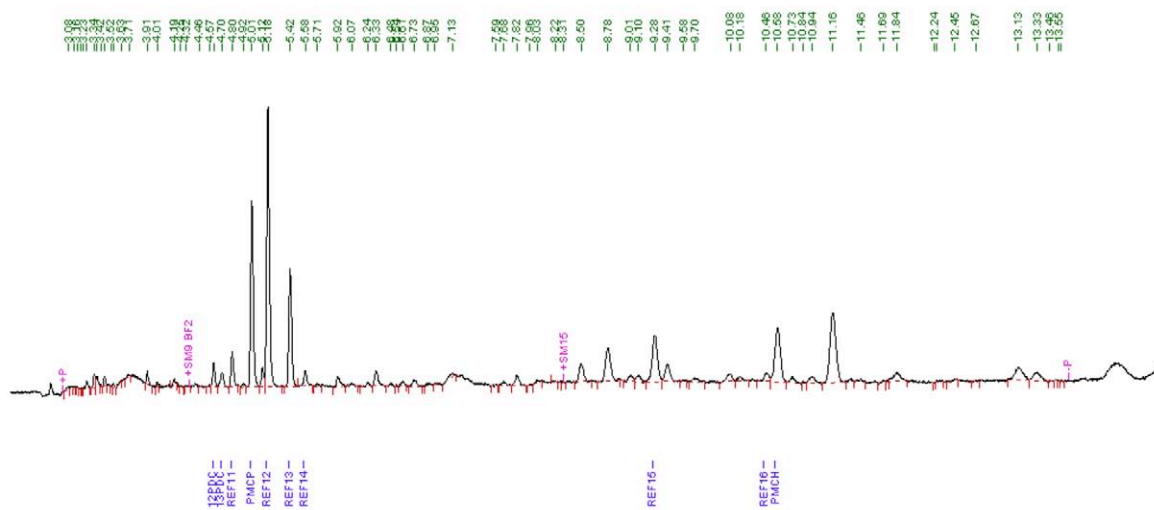


Figure 2

Table 3

Sample Name	ID	PDCB				PMCP		PMCH	
		1,2		1,3		ret time	area	ret time	area
		ret time	area	ret time	area				
A-61	#12610	4.566	274.86	4.663	632.35	4.966	2022.66	10.476	934.82
A-61	#1014	4.571	222.29	4.667	592.75	4.971	1864.75	10.486	863.17
A-61	#2129	4.609	1233.23	4.706	2687.02	5.012	7596.35	10.57	4283.07
H-102	#1591	4.565	240.61	4.661	525.5	4.964	2221.37	10.477	1058.16
H-102	#12851	4.604	1080.2	4.701	1970.75	5.007	7711.8	10.56	4370.77
I-53,	#4406	4.570	235.89	4.666	620.94	4.970	2230.74	10.491	1004.74
I-53	#2129	4.564	257.51	4.66	414.46	4.965	1769.44	10.49	875.27
I-53	#1591	4.596	1035.08	4.692	1542.25	4.998	6751.37	10.548	3723.89
SJV-120	#8113	4.567	943.96	4.663	4430.5	4.966	3795.39	10.484	1158.21
SJV-120	#12851	4.577	1483.96	4.674	5861.5	4.977	4624.36	10.496	1598.76
SJV-120	#866	4.616	4368	4.715	16814.56	5.020	13331.84	10.59	5105.14
25 uL EI8	25 fL	4.595	24045	4.68	9256	4.997	102056	10.551	99305
N-79	2129	4.595	319.3	4.68	1008.9	4.993	2964.2	10.52	1388.8
N-79		4.587	466.6	4.683	1153.3	4.987	3247.5	10.526	1802.6
N-79	1607	4.595	883.5	4.691	2128.4	4.996	8695	10.54	2901.05
H-179	12851	4.601	1832.2	4.698	6152.1	5.003	4699	10.527	1762.6
H-179		4.593	2219.4	4.69	7657.1	4.995	6484.2	10.549	1884.5
H-179	4406	4.582	5145.8	4.679	15320.7	4.982	14044	10.501	3931.46
K-151	1591	4.608	508	4.705	1037	5.010	3472	10.561	1562.74
K-151		4.599	417.4	4.695	1009.9	5.001	3320.5	10.537	1600.65
K-151	8113	4.605	734.22	4.7	1499.61	5.006	8563.87	10.557	2409.07
S-131	10325	4.605	478.4	4.702	992.2	5.007	3275	10.562	1729.6
S-131	907	4.592	539.2	4.688	1003.6	4.993	3394	10.54	1681.2
S-131	12610	4.608	1058.14	4.704	1749.72	5.011	9607	10.566	3206.1
29	12610	4.562	2414	4.657	10391	4.959	5619	10.46	2386.7
29	9928	4.594	2717.9	4.69	12523.5	4.994	6008.3	10.53	1972.06
29	3516	4.570	1376.9	4.664	6160.9	4.957	4798.5	10.47	1011.44
DU98102	11406	4.564	598	4.659	1000.2	4.983	3514	10.47	1573.3
DU98102	11036	4.569	673.1	4.662	1196	4.968	4258.3	10.493	2154.4
DU98102	5337	4.608	1209.52	4.704	1772.22	5.011	10097.3	10.569	3402
102	5337	4.570	470	4.665	1043	4.989	3272	10.48	1706.1
102	12043	4.548	538.7	4.644	1028.7	4.947	3216.95	10.447	1497.22
102	11406	4.601	620.66	4.696	1699.21	5.001	5208.47	10.545	2703.2
1 Liter BNL air		4.570	477.6	4.652	158.99	4.969	2527.7	10.469	2444.7
1 Liter BNL air		4.573	472.78	4.656	331.5	4.973	4512.4	10.497	2275.4
1 Liter BNL air		4.594	449.61	4.675	297.22	4.994	4730.85	10.535	2399.09
1 Liter BNL air		4.567	482.2	4.651	488.1	4.968	4361.4	10.51	2470.63
1 Liter BNL air		4.576	459.46	4.663	341.18	4.977	5474.91	10.495	2452.69

The chromatogram in Figure 1 is from a PFT standard. Figure 2 shows the chromatogram of canister sample H-102. Note that there are more peaks in this chromatogram than can be attributed to the released PFTs, or the internal standard. The identification in blue, below the baseline, gives the location of the PFTs and of peaks that always appeared in the ambient air chromatograms, labeled with a reference number. There are some unexpected peaks, and these are most likely compounds unique to the sampling region as they were consistently found in all of the samples. These are most likely, higher than ambient concentrations of chlorofluorocarbons and elevated hydrocarbons. No attempt was made to identify these compounds. Unfortunately, one of these unexpected peaks was unresolvable from 1,3 PDCB, one of the two isomers of PDCB, consequently the 1,3 PDCB results cannot be used. But 1,2 PDCB, PMCP and PMCH are all fully resolved as verified by carefully measuring the widths of the peaks and comparing them with those in the PFT standard. Any increased in width is due to a coincidence with an unresolved compound. The chromatographic integration technique was refined with several iterations because of the increased in the number of “new” peaks in the samples. The chromatograms were inspected to verify correct integration of the peaks.

To factor out the sample dilution the area counts for PDCB and PMCP were divided by the PMCH area counts. The resulting values were then averaged for the triplicate PFT analysis for each canister, and the results are given in Table 4.

Table 4

Date	Event Number	Sample Type	Canister ID	PDCB/PMCH area ratio	PMCP/PMCH area ratio
11/20/2003	10	Upwind	A-61	0.285 ± 0.019	1.888 ± 0.22
	15	Downwind	N-79	0.274 ± 0.038	2.447 ± 0.62
11/25/2003	21	Upwind	SJV-120	0.864 ± 0.057	2.767 ± 0.336
	27	Downwind	H-179	1.214 ± 0.135	3.329 ± 0.486
	34	Downwind	29	1.212 ± 0.210	3.059 ± 1.220
12/07/2003	6	Upwind	I-53	0.273 ± 0.030	1.919 ± 0.21
	25	Downwind	K-151	0.298 ± 0.032	2.756 ± 0.81
	30	Downwind	102	0.276 ± 0.066	1.980 ± 0.13
12/14/2003	11	Upwind	H-102	0.243 ± 0.014	1.830 ± 0.24
	27	Downwind	S-131	0.314 ± 0.028	2.460 ± 0.60
	32	Downwind	DU98102	0.348 ± 0.034	2.506 ± 0.51

Results and Discussion

Alkene and NO_y Emission Rate Calculation

A. Comparison of PMCP and PDCB Tracer Results

An examination of the results in Table 4 shows that there are three instances when the PMCP downwind concentration is elevated but the PDCB is not. If we plot the data, eliminating these three points (events, 15, 25, and 30 in Table 4), we get the plot shown in Figure 3. A regression analysis of the data yields a slope of 1.41 ± 0.08 . But the PDCB value used here is only first isomer of PDCB which is only 72.5 % of the released PDCB (the other isomer is being omitted due to chromatographic interference). If this is taken into account, the slope is 1.02 ± 0.06 which is comparable to an expected 1.037 based on the PFT flux rate and the measured PFT concentrations in the release cylinders.

The elevated PFT background in event 21 is due to changing winds. Until about 12 noon, the winds had been changing from northerly to the preferred S-SE direction. Tracer had been released since mid-morning and most likely the higher PFT background is from tracer that had been released when the winds were northerly and transported back towards the plant when the winds turned south.

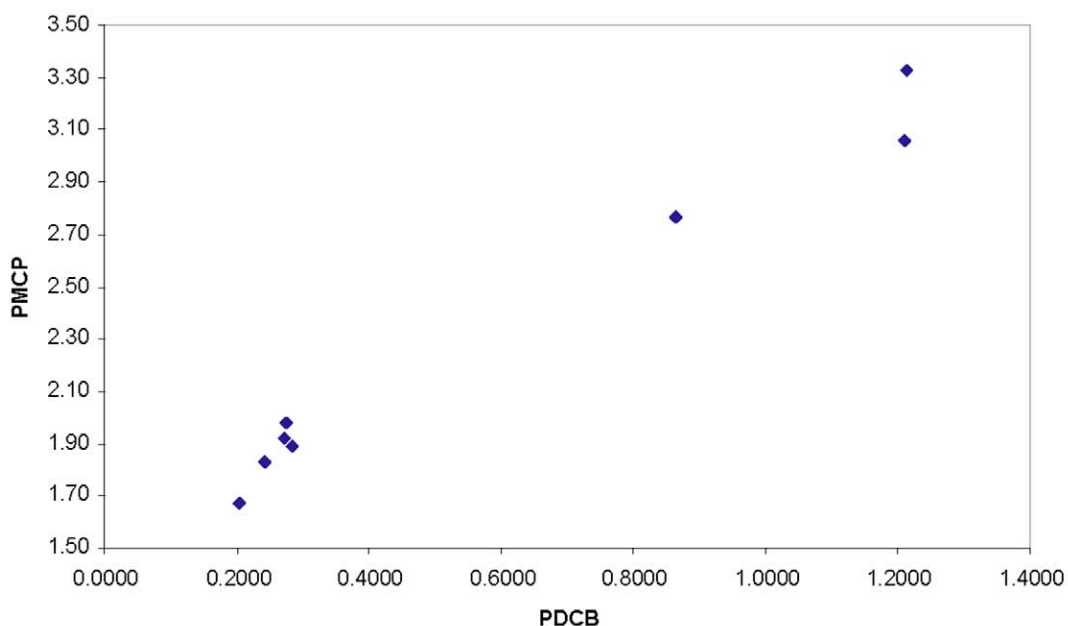


Figure 3. PMCP and PMCH correlation

The three downwind points that were eliminated from Figure 3 are interesting. The fact that PMCP was measurable and PDCB was not implies that there was a difference transport mechanisms for PDCB and PMCP. PDCB was released near the compressor in thermally hot core of the plant; PMCP was released at the water chiller inlet into a cooler plume. One interpretation is that there were two transport plumes, one straight up from the plant and at a higher elevation and the water chiller plume at a lower altitude. The water chiller plume is visible close to the plant and the sampling aircraft was visually biased to following this plume. Consequently, the remaining analysis will only use PMCP which was always in the plume that the aircraft was sampling. Most of the plume sampling was done at 1000 ft MSL.

B. Calculation of alkene emission flux from the Sweeny plant

The calculation of the alkene fluxes requires the PMCP concentration, which is obtained from the PMCP/PMCH ratio, using a value of 5.0 ppq for the concentration of PMCH.

The first calculation is for ethene; the ethene concentrations are from the replicate canisters sent for hydrocarbon analysis. The results are given in Table 5. In some instances the ethene concentration is missing or is negative when the upwind background concentration is subtracted. Nonetheless, four ethene fluxes can be calculated and the average is 106 ± 29 kg/hr. This can be compared to Sweeny estimate of 18 kg/hr in (1); this estimate is based on summing emission factors in the Sweeny plant. The ethene 106 ± 29 kg/hr emission flux calculated here is only dependent on the accurately calibrated PFT emission flux and measured PFT concentration and is about 6 times higher than the Sweeny estimate.

Table 5

Date	Event Number	Sample Type	Ethene		PMCP conc		Ethene flux	
			$\mu\text{g}/\text{m}^3$	bkg corr	ppq	bkg corr	kg/min	kg/hr
11/20/2003	10	Upwind	0.3		9.44	0.00	2.80	0.00
	15	Downwind			12.24			
11/25/2003	21	Upwind	0.8	0.0	13.84			
	27	Downwind	5.8	5.0	16.65	2.81	1.90	114
	34	Downwind	2.5	1.7	15.30	1.46	1.25	75
12/07/2003	6	Upwind	0.8	0.0	9.60	0.00		
	25	Downwind	6.8	6.0	13.78	4.19	1.53	92
	30	Downwind	5.7	4.9	9.90	0.31		
12/14/2003	11	Upwind	2.5	0.0	9.15	0.00		
	27	Downwind	0.8	-1.7	12.30	3.15		
	32	Downwind	10.0	7.5	12.53	3.38	2.37	142
			PMCP flux 1070×10^{-6} L/min					
			Ethene flux 106 ± 29 kg/hr					

The propene fluxes are similarly calculated and are given in Table 6. Again note the appearance of negative concentrations for propene when the background concentration is subtracted. For propene the calculated emission flux appears to vary by a factor of 4 to 6 over the different sampling dates, but are consistent in the two downwind samples taken on each

sampling date. The propene flux on 11/25/2003 averaged 82 ± 1 kg/hr and on 12/7/2003, averaged 277 ± 55 kg/hr; clearly these are statistically different. Correspondingly, the ethene fluxes are more or less the same for these two dates, implying that the PFT analyses are not at fault. Two interpretations are

- The propene hydrocarbon analyses are at fault, perhaps on 12/7/04 there was an unresolved compound interfering with the quantification of propene.
- There was an actual change in propene emission flux at the plant. The sampling protocol required the operators at the Sweeny plant to immediately inform the flight crew of any unexpected outages; allowing the flight crew to cancel the sampling run. No outages were reported by the Sweeny plant operators.

The propene fluxes of 82 ± 1 kg/hr on 11/25/2003 and 277 ± 55 kg/hr on 12/3/2003 can be compared to Sweeny summed emission factors estimate of 17 kg/hr (1).

Table 6

Date	Event Number	Sample Type	Propene		PMCP conc		Propene flux	
			$\mu\text{g}/\text{m}^3$	bkg corr	ppq	bkg corr	kg/min	kg/hr
11/20/2003	10	Upwind	0.4	0.0	9.44	0.00		
	15	Downwind	0.8	0.4	12.24	2.80		
11/25/2003	21	Upwind	0.8	0.0	13.84	0.00		
	27	Downwind	4.4	3.6	16.65	2.81	1.37	82
	34	Downwind	2.7	1.9	15.30	1.46	1.39	84
12/07/2003	6	Upwind	0.6	0.0	9.60	0.00		
	25	Downwind	16.1	15.5	13.78	4.19	3.96	238
	30	Downwind	2.1	1.5	9.90	0.31	5.26	316
12/14/2003	11	Upwind	1.6	0.0	9.15	0.00		
	27	Downwind	0.6	-1.0	12.30	3.15		
	32	Downwind	4.3	2.7	12.53	3.38	0.85	51
PMCP flux 1070×10^{-6} L/min								

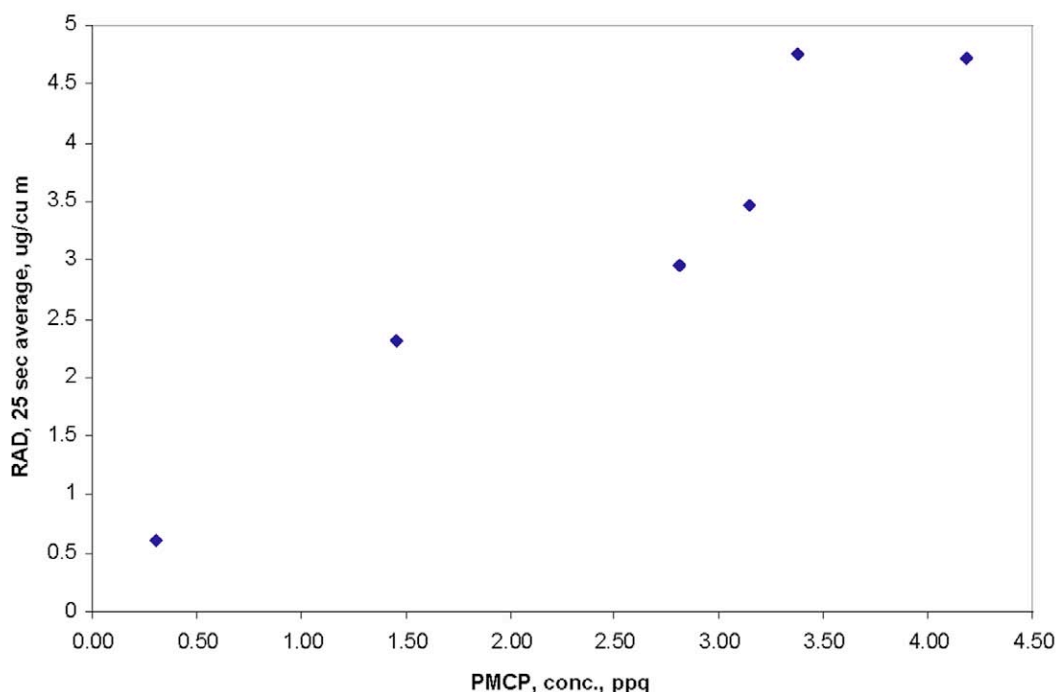


Figure 4

Further insight is seen in the additional plot given as Figure 4. This is plot of the PMCP concentration in the downwind samples for all of the runs versus the corresponding RAD measurement. Since the RAD is a real time monitor it was necessary to average the data; the RAD measurement in the plot is a 25 second average of 5 second data since the canister sampling time was 25 seconds. There is a very good correlation (r^2 is 0.92) and the intercept is 0.42 ± 0.44 (it should be zero). The RAD measurement is a weighted sum of the ethene and propene concentrations. Guenther et al. (3) measured the relative ethene response as 15% of the propene response. If there had been a factor of 3 change in the propene emission between 11/25 and 12/7 sampling dates, then this would have been apparent in this plot of all of the data, but this plot has a very good correlation implying that the propene concentrations are possibly in error.

C. Calculation of the NO_y emission flux from the Sweeny plant

Aboard the sampling aircraft was a real-time NO , NO_2 and NO_y monitor. The NO_y emission flux was calculated from a 25 second average of 5 second NO_y concentration data; the results are given in Table 7. Disregarding the flux determined on 12/7/03, the average flux is calculated as 230 ± 40 kg/hr and can be compared to 2000 TRNCC estimate of 554 kg/hr (1). The estimate based on the PFT flux measurement is expected to be less accurate than the ethene and propene flux estimates, since the NO_y concentration is not replicate canister based but rather an 25 second average of real-time data. Nonetheless, it has the right magnitude compared to the 2000 inventory estimate.

Table 7

Date	Event Number	Sample Type	NO _y conc.			PMCP conc		NO _y flux	
			ppb	µg/m ³	bkg corr	ppq	bkg corr	kg/min	tonnes/yr
11/20/2003	10	Upwind	4.91			9.44	0.00		
	15	Downwind	4.91			12.24	2.80		
11/25/2003	21	Upwind	3.43	6.46	0.00	13.84	0.00		
	27	Downwind	9.51	17.90	11.45	16.65	2.81	4.36	2292
	34	Downwind	6.13	11.54	5.09	15.30	1.46	3.73	1961
12/07/2003	6	Upwind	3.90	7.35	0.00	9.60	0.00		
	25	Downwind	4.73	8.92	1.57	13.78	4.19	0.40	211
	30	Downwind	3.57	6.72	-0.63	9.90	0.31		
12/14/2003	11	Upwind	7.16	13.48	0.00	9.15	0.00		
	27	Downwind	11.82	22.26	8.77	12.30	3.15	2.98	1567
	32	Downwind	14.80	27.87	14.38	12.53	3.38	4.55	2395
			PMCP flux 1070 x 10 ⁻⁶ L/min						
			NO _y flux 2050 ± 370 tonnes/yr						

A possible explanation for the unrealistic results on 12/7/03 is that the NO_y plume was not coincident with PFT/ethene/propene plume; the NO_y source at the power plant is 1900 feet away from the PFT/ethene/propane sources.

Conclusions

1. The use of PFTs for the determination of fugitive emission fluxes has been successfully demonstrated in this field study. The two PFTs used in this study were well correlated in the canister samples when the two PFTS were in the same emission plume.
2. During certain meteorological conditions, two plumes were emanating from the Sweeny plant, one from the relatively hot core of the plant and other from the relatively cooler water chiller. The aircraft samples were more often from the cooler water chiller plume.
3. The ethene emission flux has been measured as 106 ± 29 kg/hr, based on the ethene and PFT concentrations in the downwind aircraft canister samples and known PFT emission flux released inside the Sweeny plant. This is the average of three sampling dates, 11/25, 12/7, and 12/14/2003. This is 6 times higher than the 2000 TRNCC estimate.

4. The propene emission flux has similarly been measured as 82 ± 1 kg/hr on 11/25, 277 ± 55 kg/hr on 12/7 and 51 kg/hr on 12/14/2003. The varying results from different sampling dates is either a genuine variation in the plant propene emission rate or due to a large variability in the propene concentration in the hydrocarbon analyses. The high correlation between the PMCP and the RAD measurement of reactive alkenes, implies there are variabilities in the hydrocarbon analyses. The propene flux measurements are respectively 4.8, 16.2 or 3 times larger than the 2000 TRNCC estimate.
5. The NO_y emission flux has been estimated as 230 ± 40 kg/hr based on the PMCP concentration in the aircraft sampled canister and a 25 second average of the NO_y real-time concentration. It can be compared to the 2000 TRNCC estimate of 554 kg/hr.

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