

Investigationsof Nanocrystalline Alloy Electrosark Coating Madeof Nanocrystalline Alloy Based on 5БДCP Ferrum

A V Kolomeichenko¹, I S Kuznetsov¹, A Yu Izmaylov², R Yu Solovyev², S N Sharifullin^{2,3}

¹Federal State Budgetary Educational Establishment of Higher Education „Orel State Agrarian University named after N.V. Parakhin”, Russia

²Federal State Budgetary Scientific Institution “Federal Scientific Agroengineering Center of All-Russian Institute of Mechanization”, Russia

³Kazan Federal University, 18 Kremlyovskaya street, Kazan, 420008, Russian Federation

Ivan-654@yandex.ru

Abstract. The article describes the properties of wear resistant electrosark coating made of nanocrystalline alloy of type 5БДCP (Finemet). It is proved that electrosark coating has nanocrystalline structure which is like amorphous matrix with nanocrystals α – Fe. Coating thickness is 33 μm , micro-hardness is 8461 - 11357 MPa, wear resistance is $0,55 \times 10^4 \text{s/g}$. Coating ofnanocrystalline alloy of type 5БДCP can be used to increase wear resistance of machinery working surfaces.

1. Introduction

One of the promising directions of improving the wear resistance of working surfaces of details is their hardening due to the creation of surface layers with high physical-mechanical properties. Analysis of scientific and technical information showed that among the commonly used methods of hardening of working surfaces can distinguish heat treatment, chemical heat treatment, laser and plasma hardening and others. A promising method of hardening the working surfaces with complex geometric form, is an electro spark processing (ESP) [1]. There are many different ways to method development ESP. One of the ways is the use of new materials with nanocrystalline structure. The use of such materials will allow to obtain multifunctional electro spark coating, can improve wear resistance of working surfaces of parts [2-12].

2. Obiectiv.

Explore the properties of electric-reinforcing coating made of nanocrystalline alloy (NCA).

3. Methods.

As an electrode material 5BDSR nanocrystalline alloy was selected mark (Finemet) (Fe-70% B - 9.2%, Si- 6.3% Nb- 2.21%, 0.8% Cu-, Mo- 0.2%). The structure of the resulting coatings was investigated with a scanning electron microscope Hitachi TM - 1000. The reinforcing coating is applied to the samples of steel 65G install EDM brand BIG - 4 (mode: №2, K = 0.8). The thickness of



the experimental electric-spark coatings was measured on transverse sections. The measurements were performed on a microscope MIM-8. Base surface served as the boundary between the coating and the substrate. Microhardness was measured at a load of 50 g indentation of diamond tips on a computerized Hardness PMT-3M-01. Process studied mass transfer was investigated by measuring geometric parameters of single erosion marks left electrode. Hardness measurements were performed PMT-3M. Microhardness was equipped with a screw ocular micrometer MOV-1-16H, and MA-25 lens (epiobektiv plan-achromatic $F = 25,0$ mm, $A = 0,17$). Tribotechnicheskie tests performed on the machine friction MTU-01, at the outer load of 2.5 N, with relative sliding speed - 1.0 m / s. Material for manufacturing served kontrobraztsa steel grade 65G, hardened to HRC 58 ... 60. Depreciation is determined by gravimetric method using weights Sartorius Competence CP64 with an accuracy of 0.0001 g.

4. The results of the research.

Scanning electron microscopy made it possible to state that-tension coating obtained by treating the steel substrate electrode of the NCA brand 5BDSR, it has a homogeneous structure to the level of 1 micron. However, in the transition zone between the coating and the substrate are microcrystalline incorporating substrate material (Fig. 1). X-ray studies have shown that the coating alloy 5BDSR has a nanocrystalline structure, is an amorphous matrix with nanocrystals α - Fe. It can be seen from Figure 2, in which there is reflection from the crystal phases α -Fe [10].

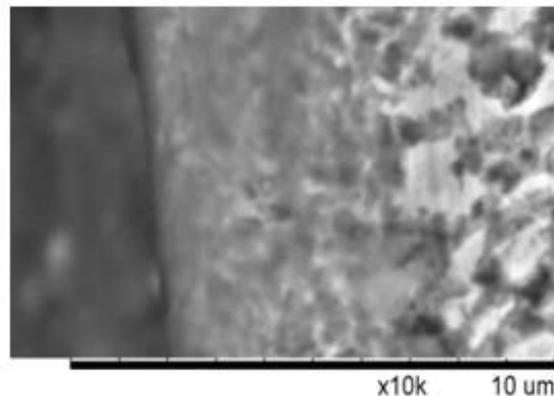


Figure1. Electrospark coating structure

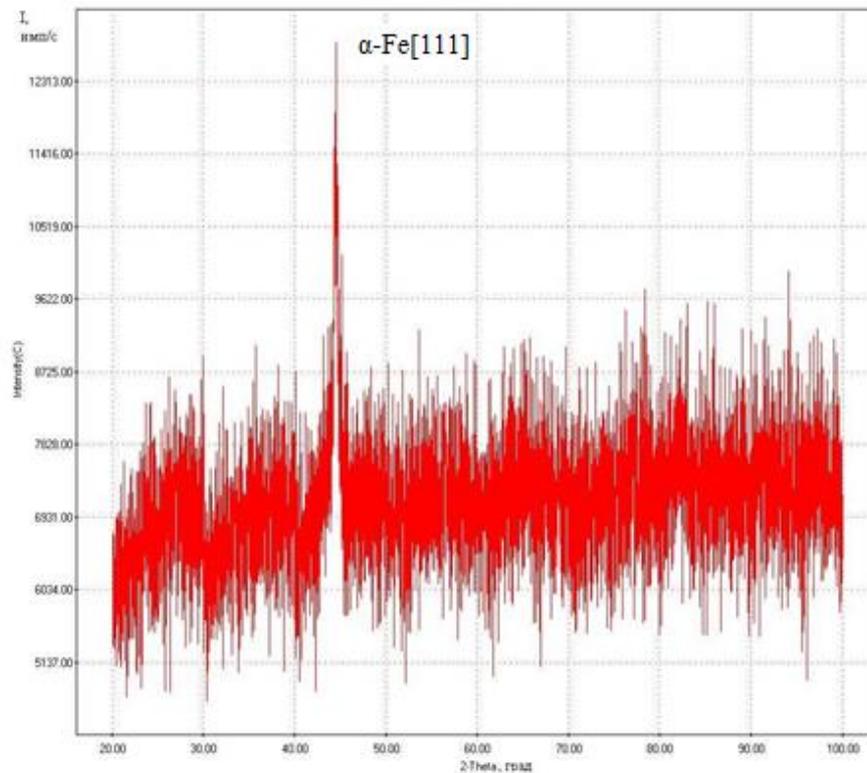


Figure2. Diffraction pattern of electric spark coating

The thickness of the electric-cover changes nonlinearly. The experimental dependence of the thickness of the specific processing time provided in Figure 3 As it set the threshold of brittle fracture is 2.1 min / cm^2 critical threshold of brittle fracture is equal to 5.2 min / cm^2 . In ESP at № mode 2, $k = 0.8$ of the maximum thickness of coating grade 5BDSR NCA - $h = 33 \mu\text{m}$, which is approximately 1.5 times greater than the thickness of the alloy coating-grade VK6 OM obtained in a similar mode.

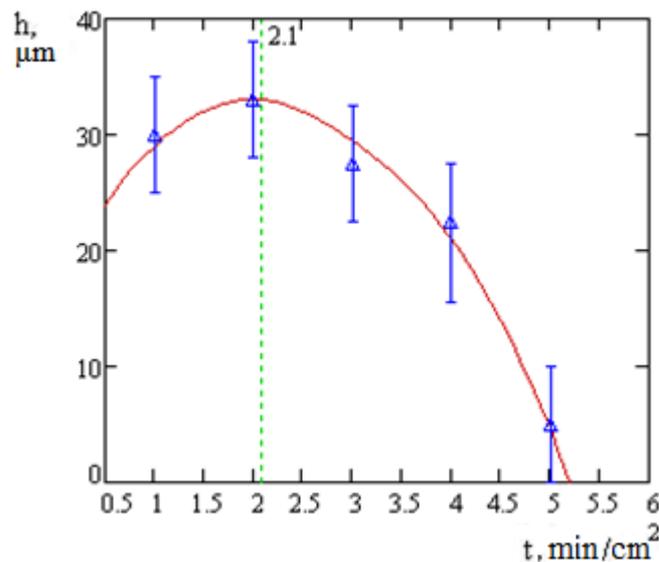


Figure3. The dependence of the film thickness h of the specific processing time t

Microhardness strengthening coating is largest dispersion. The maximum value of the microhardness of coatings NCA brand 5BDSR - $N_{\mu\text{max}} = 11357 \text{ MPa}$ minimum - $N_{\mu\text{min}} = 8461 \text{ MPa}$. A

characteristic feature indicative of plastic deformation of the coating is the presence of "crown" on the printout of the indenter [1, 8].

During the mass transfer studies have demonstrated the dependence of the mass of the electrode material transported from the anode to the cathode, the initial stress - one of the main technological parameters of ESP. Figure 4 shows the regression power law, which can be used to develop the process of hardening of details. Using the gravimetric method was established and mass transfer direction generally ESP efficiency. This method allowed us to determine a number of mass transfer parameters necessary for the process to ensure ESP process (Table. 1).

Table 1. Mass-transfer parameters

Mass-transfer average ratio	Threshold fragile destruction coatings, $t_x, \text{min/cm}^2$	The critical threshold brittle fracture surfaces, $t_{kp}, \text{min/cm}^2$
0,54	4,0	6,5

Endurance tests yielded dependence on wear test duration, represented as a function of logarithmic regression. After differentiation its wear rate dependence on the time (Fig. 5) was obtained.

Tribological tests found that the hardening electric spark coating NCA brand 5BDSR has wear rate $W_{sr} = 18 \times 10^{-5} \text{ g/s}$ and wear resistance $U = 0,55 \times 10^4 \text{ s/g}$. Low wear rate and high wear resistance indicate that the considered electric spark coating should be used in hardening of working surfaces of parts.

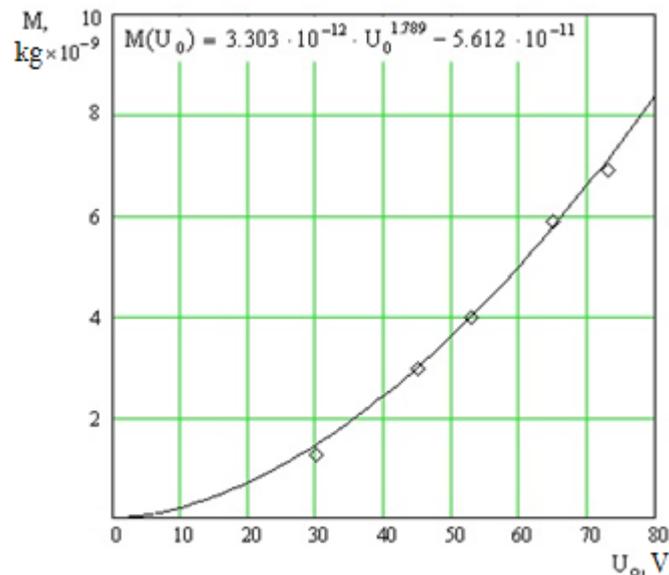


Figure 4. The dependence of the mass of the electrode material is transferred from the anode to the cathode, the initial voltage for ESP

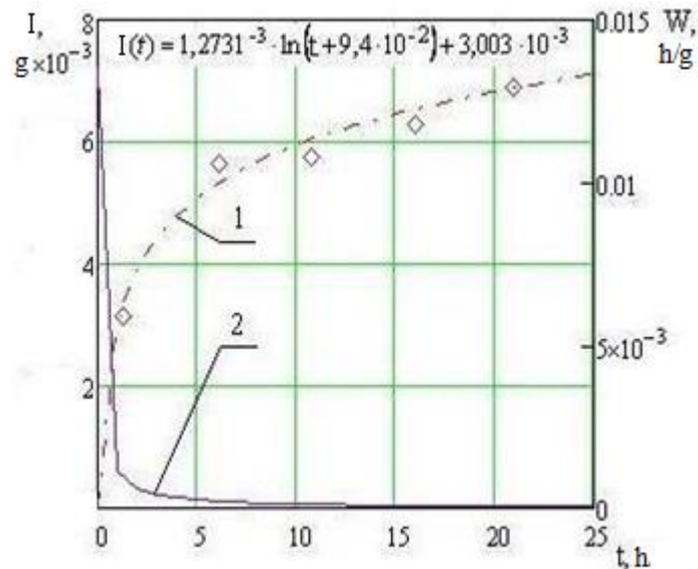


Figure 5. Dependencies wear (1) and wear rate (2) electric spark coating on the duration of the test

5. Conclusion.

Dura-tension coating of nanocrystalline alloy brand 5BDSR a nanocrystalline structure, the thickness of 33 microns, the maximum microhardness of 11357 MPa, the wear resistance of 0.55×10^4 s / g. Coverage of this alloy can be used to improve the wear resistance of working surfaces of machine parts.

References.

- [1] Kolomeychenko A V, Kuznetsov I S 2015 Theory and practice of electric-hardening cutting machine parts amorphous and nanocrystalline alloys Monograph *Eagle. Publishing house Orel State Agrarian University* pp 174
- [2] Ageev E, Mizobata K, Nakajima T, Zen H, Kii T and Ohgaki H 2015 Time-resolved detection of structural change in polyethylene films using mid-infrared laser pulses *Applied Physics Letters* V 107 No 4 **041904**
- [3] Ageeva E V, Khor'yakova N M, Ageev E V 2015 Morphology and composition of copper electrospark powder suitable for sintering *Russian Engineering Research* V 35 No 1 pp 33-35
- [4] Cadney S, Brochu M 2008 Formation of amorphous Zr_{41.2}Ti_{13.8}Ni₁₀Cu_{12.5}Be_{22.5} coatings via the electrospark deposition process *Intermetallics* Vol 16 No 4 pp 518-23
- [5] Brochu M, Heard D W, Milligan J, Cadney S 2010 Bulk nanostructure and amorphous metallic components using the electrospark welding process *Assembly automation* Vol 30 No 3 pp 248-56
- [6] Milligan J, Heard D W, Brochu M 2010 Formation of nanostructured weldments in the Al-Si system using electrospark welding *Applied surface science* Vol 256 No 12 pp 4009-16
- [7] Cadney S, Goodall G, Kim G, Moran A, Brochu M 2009 The transformation of an al-based crystalline electrode material to an amorphous deposit via the electrospark welding process *Journal of alloys and compounds* Vol 476 No 1-2 pp 147-51
- [8] Kolomeichenko A V, Kuznetsov I S, Kravchenko I N 2015 Investigation of the thickness and microhardness of electrospark coatings of amorphous and nanocrystalline alloys *Welding International* Vol 29 No 10 pp 823-25
- [9] Kolomeichenko A V, Kuznetsov I S 2014 Tribotechnical properties the electrospark coating of amorphous and nanocrystalline alloys based on iron *Friction and wear* Vol 35 No 6 pp 501-504
- [10] Kolomeychenko A V, Kuznetsov I S, Rodichev A Y, Penyashki T G 2015 On the question of getting in electric-spark coatings of amorphous and nanocrystalline structures *Repair. Recovery. Modernization* No 5 pp 33-36

[11] Adigamov N R, Sharifullin S N, Podgaraya K S 2013 Efficient technology for the modernization of the high-pressure fuel pumps, automotive diesel engines *Proceedings GOSNITI V* 113 pp 206-14

[12] Adigamov R N, Lyalyakin V P, Soloviev R Y, Sharifullin S N 2016 Plasma technology in improving the efficiency of the diesel engine high pressure fuel pumps *Welding Engineering* No 2 pp 49-51