

# Synthesis Oxide Dispersion Strengthening Stainless Steel doped with Nano Zirconia by Mechanical Alloying

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**Abstract.** The oxide dispersion strengthening stainless steel of Fe-11.5wt%Cr and Fe-11.5wt%Cr-1%ZrO<sub>2</sub> alloy by mechanical alloying method were synthesized by planetary ball milling. The methods employed for study were designing of Fe-11.5wt%Cr and Fe-11.5wt%Cr-1%ZrO<sub>2</sub> proportion of composition alloy which is plotted to *Schaffler* diagram to get ferritic/martensitic stainless steel. After MA the ODS powders were compaction with pressure 80kg/mm<sup>2</sup> and followed by sintering at the temperature of 900,1000 and 1100° C under high purity argon atmosphere for 1 hour. Characterization by XRD is used to examination phase present. Optical microscopy and SEM is used to get image microstructures. XRD analysis resulting the ferritic and martensitic is a major and minor phase respectively. There are not significant differences in the microstructure between Fe-11.5wt%Cr and Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>. An increase in the sintering temperature shift the microstructure from dendritic to equiaxed. EDS examination showed that zirconia exit in the alloy Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>. The addition of 1 % nano-zirconia (ZrO<sub>2</sub>) into Fe-Cr alloy while milling process was resulted a higher Hardness Vickers Values rather than without zirconia addition. Average value of Hardness Vickers values was resulted 135.5 HV for Fe-11.5wt%Cr whereas 138.4 HV for Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>.

## 1. Introduction

Current development of high-performance nuclear structural materials for breeding-blanket structural components, which will be exposed to high fluxes neutrons is one of the major challenges in future fusion reactors materials. The requirement of structural materials for the blanket components to a large degree dictates the design of the reactor systems. The selection of suitable structural materials is based on mechanical, thermophysical, corrosion and compatibility, low neutron induced radioactivity, and resistance to radiation-induced damage phenomena like material hardening embrittlement [1].

Oxide-dispersion strengthened (ODS) stainless steels have been considered as promising high-temperature materials such as nuclear materials. High-chromium ferritic/martensitic steels are considered for the Generation IV nuclear reactors operated at elevated-temperature in-core applications. Basically, these steels contain 9–12% Cr to improve high temperature oxidation. [2,3] Mechanical alloying (MA) is one of the methods to synthesize material uniformly by disperse nano-sized oxide particles such as yttria (Y<sub>2</sub>O<sub>3</sub>) in the metal matrix. This technique can be also employed to fabricate nano Fe alloys with the oxide dispersion [4,5,6].



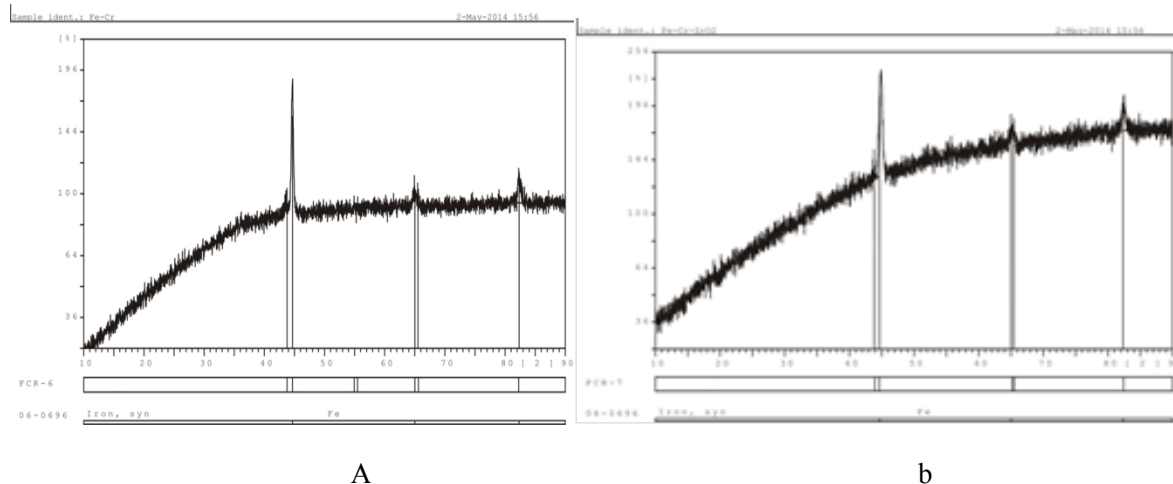
The purpose of this paper is to characterize the microstructural and mechanical properties (hardness) of ferritic/martensitic stainless steel of Fe-11.5wt%Cr and Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub> as a candidate structural material for nuclear reactors application [7,8].

## 2. Experimental methods

The powder mixture with the nominal composition of Fe-11.5wt%Cr and Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub> alloy was mechanically alloyed using Planetary Ball Milling (PBM) equipped with stainless steel vial for 2 hours. The milling balls were made of Zirconia with diameter of 2 mm. Ball-to-powder weight ratio was 10:1. The speed of rotating arm was 580 r.p.m. After MA the ODS powders were compaction with pressure 80kg/mm<sup>2</sup> and followed to sintering at the temperature of 900,1000 and 1100° C under high purity argon atmosphere for 1 hour. Micro hardness measurements were performed by using micro hardness tester HV 1000 equipped with a Vickers diamond pyramid and applying load of 0.98N for 15s. Each result is the average of at least 5 measurements. Characterization XRD by PHILIPS type PW 1835 device, using the Cu-K<sub>α</sub> radiation with  $\lambda=0.15406$  nm. Optical microscopy and SEM is used to get image microstructures.

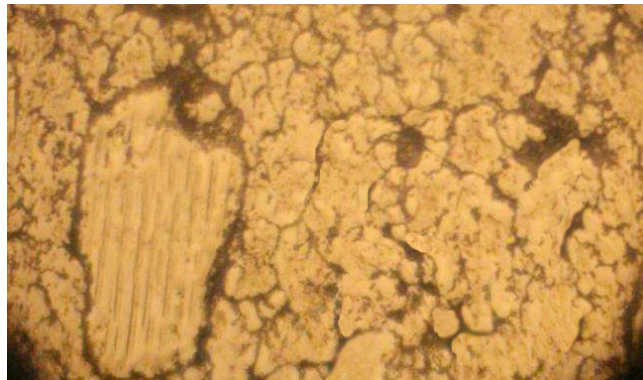
## 3. Result and discussions

X-ray diffraction patterns of the Fe-11.5wt%Cr and Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub> alloy after sintering from planetary ball mill are shown in Figs. 1a and b, respectively. The peaks of elemental powder ZrO<sub>2</sub>, was not appeared in the diffraction pattern. The phase present is dominated by ferritic phase and martensitic is minor phase.

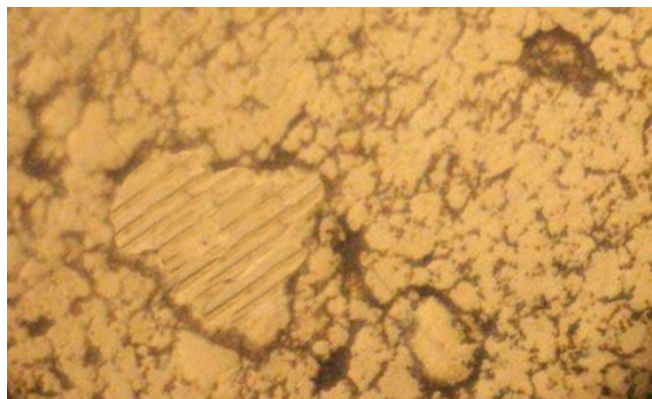


**Figure 1.** a) Fe-11.5wt%Cr b) Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub> sinter at 11000C

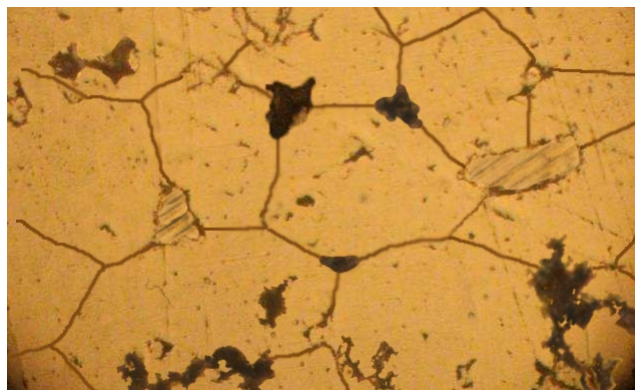
Figure 2,3, and 4 shows representative optical and SEM-EDS micrographs of this Fe-11.5wt%Cr and Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub> stainless steel after sintering at 900° C,1000° C and 1100° C. According to optical microscopy, there are not significant differences in the microstructure between Fe-11.5wt%Cr and Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>. After sintering at temperature 900° C and 1000° C. But an increase in the sintering temperature shift microstructure significantly at 1100° C. The microstructure changed from dendritic to equiaxed. Fig.4 showed that EDS examination depicted that zirconia exit in the alloy Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>.



a

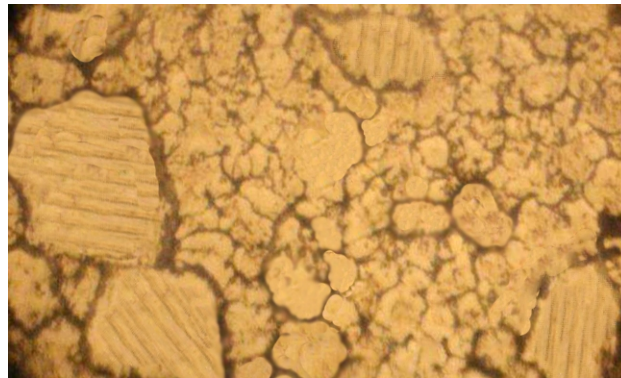


b

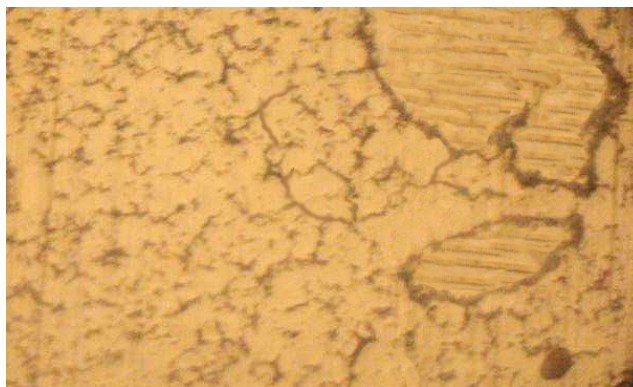


c

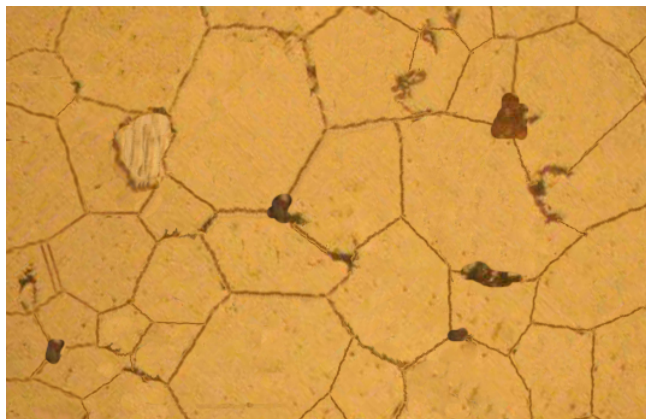
**Figure 2.** Microstructures of Fe-11.5wt%Cr sinter at a) 9000C b) 10000C c) 11000C, 25x



**a**



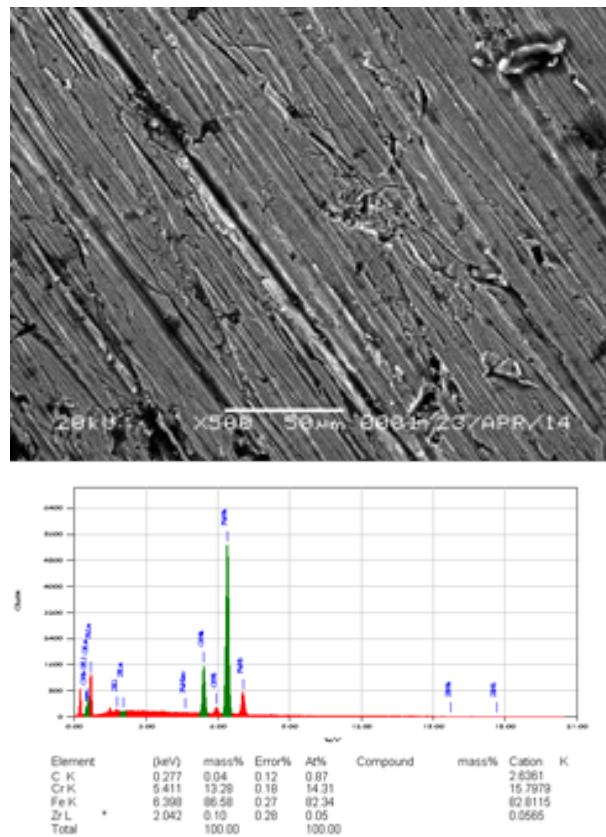
**b**



**c**

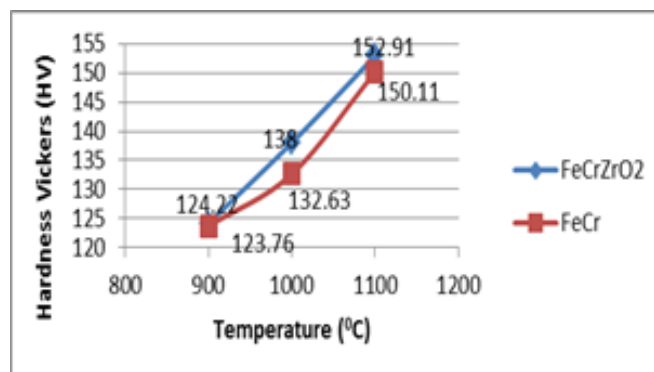
**Figure 3.** Microstructures of Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub> sinter at a)900<sup>0</sup>C b)1000<sup>0</sup>C c)1100<sup>0</sup>C, 25x





**Figure 4.** SEM-EDS Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>

Micro Vickers hardness measurements performed on Fe-11.5wt%Cr and Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub> have shown in figure 5. It was found that the micro hardness value of Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub> highest compare with micro hardness value of Fe-11.5wt%Cr. Average value of Hardness Vickers values was resulted 135.5 HV for Fe-11.5wt%Cr whereas 138.4 HV for Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>. It can be concluded that the addition nano zirconia increase micro hardness Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>. Sintering temperature is also increasing hardness of Fe-11.5wt%Cr and Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>. Due to increasing density of the specimen.



**Figure 5.** Micro Vickers hardness measurements

#### 4. Conclusion

On the basis of the results the following conclusions can be as followed:

1. There are not significant differences in the microstructure between Fe-11.5wt%Cr and Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>. EDS examination showed that zirconia exit in the alloy Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>
2. An increase in the sintering temperature shift the microstructure from dendritic to equaxed.
3. The XRD pattern was found that ferritic and martensitic were the major phase and minor phase, respectively.
4. It was found that the highest micro hardness value was achieved by addition nano zirconia. Average value of Hardness Vickers values was resulted 135.5 HV for Fe-11.5wt%Cr whereas 138.4 HV for Fe-11.5wt%Cr-1%wtZrO<sub>2</sub>. wtZrO<sub>2</sub> Sintering temperature is also increasing hardness of Fe-11.5wt%Cr and Fe-11.5wt%Cr-1wt%ZrO<sub>2</sub>. Due to increasing density of the specimen.

#### Acknowledgments

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