

# Dynamic simulation in the process of pressurized denitration based on oxy-fuel combustion

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**Abstract.** Oxy-fuel combustion is considered as one of the most promising technologies for capturing CO<sub>2</sub> from coal-fired power plants. It will greatly reduce the cost of gas purification if we remove NO<sub>x</sub> in the process of compression, which is the characteristic of oxy-combustion. In this paper, simulation of denitration process of oxy-fuel combustion flue gas was realized by the Aspen Plus software, systematically analyzed the effect of temperature, pressure, initial concentration of O<sub>2</sub> and NO in the denitration process. Results show that the increasing of pressure, initial concentration of O<sub>2</sub>, initial concentration of NO and the decrease of temperature are all beneficial to the denitration process.

## 1. Introduction

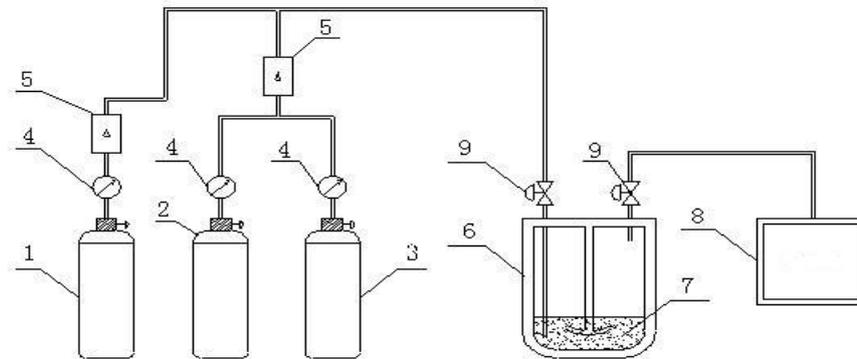
NO<sub>x</sub> can be removed effectively in the process of compression in oxy-fuel combustion, thus this method can save the cost of denitration equipment. However, most of current studies are experimental researches. The object of study has some limitation due to the limitation of experimental conditions. Besides, the reaction mechanism of removal process of NO<sub>x</sub> is comprehensive, the specific reaction mechanism has not yet been determined. Besides, current studies always focus on studying the effects of different reaction conditions on the removal of NO<sub>x</sub>, but the research of integrated optimization choice of optimum research conditions is relatively less[1,2]. In this paper, a reliable model is established by Aspen Plus software according to dynamic data existed in the literature and some experimental data. Then by monitoring gas-phase NO<sub>x</sub> concentration, we analyze the effect of different reaction pressure, temperature, initial O<sub>2</sub> and NO concentration on the process of NO<sub>x</sub> absorption[3-5].

## 2. Experimental and system flow set-up

The experiment apparatus is shown in Figure 1. This apparatus can be divided into three parts: the synthetic flue gas system, the reaction system and the gas analysis system.

Synthetic flue gas system is made up of gas cylinders, pressure- reducing valve and mass flow controllers. Flue gas mainly consists of CO<sub>2</sub>, O<sub>2</sub>, NO and SO<sub>2</sub>. The gas flow is controlled by using a mass flow controller to realize precise control and maintain the stable of system flow[6-8]. The body of reaction system is a flip-style magnetic seal lifting autoclave. Temperature and pressure of autoclave are monitored by the external pressure gauge and thermometer. In order to control the flue gas entering or leaving the autoclave, some stop valves are provided in import and export. Synthetic flue gas enters the bottom of the autoclave to react with the deionized water which is pre-loaded[9,10]. The composition of export flue gas is tested by multifunction flue gas analyzer.





**Figure 1.** Simplified process flow diagram of the experimental apparatus.

1 O<sub>2</sub> cylinder; 2 CO<sub>2</sub> (or N<sub>2</sub>) cylinder; 3 mixed gases cylinder; 4 pressure reducing valve; 5 MFC; 6 autoclave; 7 deionized water; 8 flue gas analyzer; 9 stop valve.

According to the apparatus or conditions, a series of RBATCH module based on principle of dynamic are used to realize the simulation. The three RBATCH modules are used to simulate the processes of CO<sub>2</sub> cleaning, flue gas booster and constant pressure reaction respectively. Export gas of RBATCH3 occurs flash in the circumstance of export pressure and temperature, and the concentration of NO can be test in gaseous after dehydration.

The components of flue gas are defined in simulation under the same components of experiment, and the productions are HNO<sub>2</sub> and HNO<sub>3</sub>. We use the model of ELECNRTL to consider the effect of molecules-molecules, electrolyte-electrolyte and electrolyte-molecules, due to the electrolyte in system participated in the reaction. Aspen Plus automatically calls the internal parameters. In the method of calculating gas-liquid balance activity coefficient, Henry's law can be used to describe the condition of dissolved gas or other supercritical components. The specified Henry components of simulation process contain NO, NO<sub>2</sub>, O<sub>2</sub>, CO<sub>2</sub>, HNO<sub>2</sub> and HNO<sub>3</sub>.

### 3. Simulation verification

The flue gas and operating conditions of experiment are consistent with the simulation. The experimental research and process simulation based on Aspen of pressurized denitration process at different conditions in reaction kettles, Denitration conditions and the experiment and simulation results are shown in Table 1.

We can find that the NO removal rates in simulation results coincide well with the experiment. The maximum relative error is only 1%, so the model and mechanism used in simulation is reliable and feasible. Theoretical support is provided to promote the industrial application of denitration way.

**Table 1.** The simulation results compared with the experimental results.

Initial concentration		Temperature /°C	Pressure /bar	Residence time /min	Simulation removal ratio of NO /%	Experimental removal ratio of NO /%	Relative error of removal ratio of NO/%
NO /ppm	O <sub>2</sub> /%						
279	5	25	10	5	76.0	76.0	0
836	5	25	6	5	83.5	82.7	1.0
836	5	25	10	5	92.5	92.2	0.3
836	5	25	10	10	95.9	95.2	0.7
836	5	30	10	5	91.1	91.0	0.1
836	10	25	10	5	94.4	93.5	1.0
836	5	25	14	5	94.9	95.3	-0.4

3.1. Effect of pressure on the removal of NO

In the process, the absorption reactor temperature is 25°C, initial concentration of O<sub>2</sub> is 5%, residence time of constant pressure in RBATH3 is 5min, initial concentration of NO is 836ppm. The effect of pressure on the absorption of NO is studied by changing the stop pressure of Rbatch2. Pressure range is 4bar to 20bar, the simulation results are shown in Figure 2 and Figure 3.

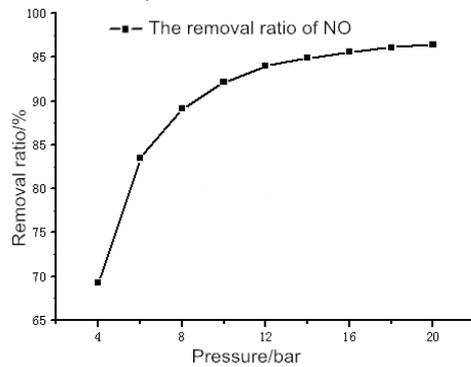


Figure 2. The removal rate of NO varied with pressure.

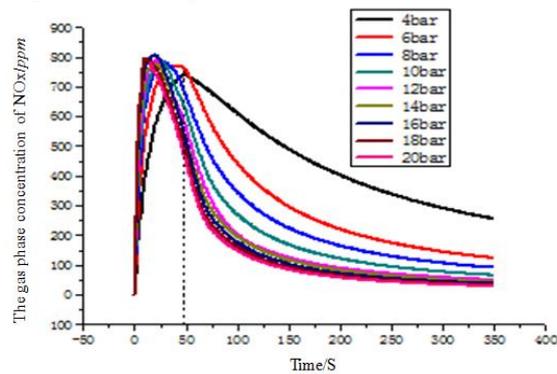


Figure 3. The relationship between gas phase NO<sub>x</sub> concentration and time in reactor.

Figure 2 shows that removal rate of NO increases with the increase of pressure. And removal rate of NO reaches 96.4% under the pressure of 20bar, so the increase of NO will be conducive to the removal of NO. But the effect of increased removal rate of NO is different under different pressure range, the effect is obvious in low pressure, while it becomes more slowly if the pressure is higher than 12bar. Figure 3 shows the relationship between gas phase NO<sub>x</sub> concentration and time in reactor, the concentration of NO<sub>x</sub> increases with pressure at preliminary stage. When the pressure is higher than 12bar, the concentration of NO<sub>x</sub> begins to drop.

NO<sub>x</sub> is absorbed quickly in early stage of constant pressure reaction, and concentration of NO<sub>x</sub> gradually reduces with the time. Under the condition of 5min residence time, concentration of NO<sub>x</sub> is stable in high pressure, but a decline exists in low pressure. So the increase of pressure is conducive to the denitration process of flue gas. But enough residence time is required to reduce the NO<sub>x</sub> concentration to a certain extent, and residence time becomes shorter with the increase of pressure.

3.2. Effect of temperature on the removal of NO

In the process, the stop pressure in Rbatch2 is 10bar, initial concentration of O<sub>2</sub> is 5%, residence time of constant pressure in RBATH3 is constant, initial concentration of NO is 836ppm. The effect of temperature on the absorption of NO is studied by changing temperature from 10°C to 85°C.

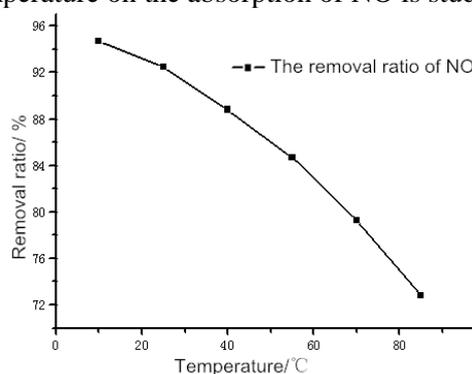


Figure 4. The removal rate of NO varies with temperature.

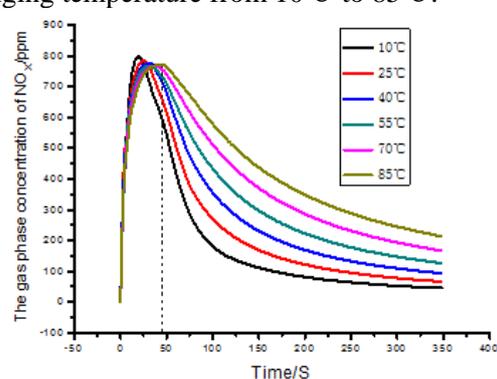
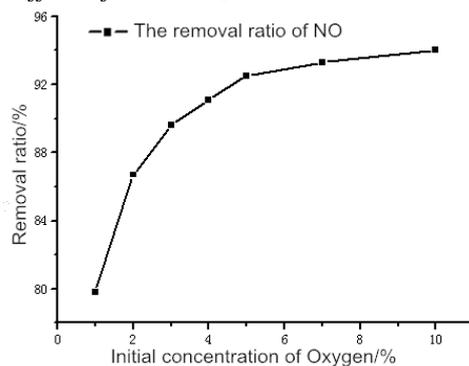


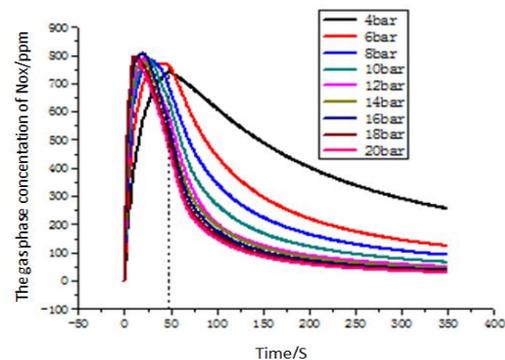
Figure 5. The relationship between gas phase NO<sub>x</sub> concentration and temperature.

Figure 4 shows that removal rate of NO decreases with the gradually increase of temperature. So the decrease of temperature is conducive to the absorption of NO. The remove rate of NO reduces by 22% while the temperature rises from 10°C to 85°C. Figure 5 shows the concentration variety of NO<sub>x</sub> in the process of absorption. The gas phase concentration of NO<sub>x</sub> almost maintains the stability at the preliminary stage. But in the later stage, the NO<sub>x</sub> concentration in high temperature is higher than lower temperature's. The export gas phase NO<sub>x</sub> concentration of Rbatch 2 has a certain decline compared with entrance, and the export gas phase NO<sub>x</sub> concentration declines with the decrease of temperature, but the amplitude of decrease is not obvious. NO<sub>x</sub> is absorbed quickly in early constant pressure reaction stage, and the export NO<sub>x</sub> concentration decreases with the increasing of time. NO<sub>x</sub> concentration in low temperature is lower than high temperayure's in constant pressure reaction stage. Under the condition of 5min residence time, the NO<sub>x</sub> concentration in low temperature has tended balance, while the NO<sub>x</sub> concentration in high temperature continues to drop. So the decrease of temperature is conducive to the pressurized denitration process of flue gas. But if we want to reduce NO<sub>x</sub> concentration to a certain extent, the enough residence time should be ensured, which will be longer with the increase of temperature.

### 3.3. Effect of initial O<sub>2</sub> concentration on the removal of NO



**Figure 6.** The removal rate of NO varies with initial O<sub>2</sub> concentration.



**Figure 7.** The relationship between gas phase NO<sub>x</sub> concentration and time.

The stop pressure in Rbatch2 is 10bar, the absorption reactor temperature is 25°C, residence time of constant pressure in RBATH3 is constant, initial concentration of NO is 836ppm. The effect of initial O<sub>2</sub> concentration on the absorption of NO is studied by changing the downtime. Initial O<sub>2</sub> concentration range is 1% to 10%, the simulation results are shown in Figure 6 and Figure 7.

Figure 6 shows that removal rate of NO gradually increased with the increase of initial O<sub>2</sub> concentration, so the increase of O<sub>2</sub> concentration in flue gas is conducive to the removal of NO. But the effect of increased removal rate of NO is different under different initial O<sub>2</sub> concentration. The removal rate of NO increases rapidly with the increase of initial O<sub>2</sub> concentration when the initial O<sub>2</sub> concentration is lower than 5%. In contrast, the effect of initial O<sub>2</sub> concentration on the removal ratio of NO is weak, if the initial O<sub>2</sub> concentration is more than 5%. So when the initial O<sub>2</sub> concentration is 3% to 5%, it is more suitable for pressurized denitration process.

Figure 7 shows the change of NO<sub>x</sub> concentration with the absorption time. Concentration of NO<sub>x</sub> decreases at preliminary stage, the effect of O<sub>2</sub> concentration on the NO<sub>x</sub> is obvious when the initial O<sub>2</sub> concentration is 1% to 5%, while it is more slowly if the initial O<sub>2</sub> concentration is more than 5%. It is accordance with that in Fig.7. Under the condition of 5min residence time, the NO<sub>x</sub> concentration in high initial O<sub>2</sub> concentration tends balance, while the NO<sub>x</sub> concentration in low O<sub>2</sub> concentration continues to drop. So increase of initial O<sub>2</sub> concentration is conducive to the pressurized denitration

process of flue gas. But if we want to reduce NO<sub>x</sub> concentration to a certain extent, the enough residence time should be ensured, which will be longer with the decrease of initial O<sub>2</sub> concentration.

#### 4. Summary

In this paper, simulation of the pressurized denitration process of oxy-fuel combustion flue gas is provided based on the principle of Aspen Plus intermittent reactors. Results are shown as follows:

(1) Increase of pressure, initial O<sub>2</sub> concentration, initial NO concentration and decrease of temperature are all conducive to the pressurized denitration process of flue gas. The maximum of removal can reach 96.4% in the experimental conditional.

(2) The 3%-5% content of O<sub>2</sub> in flue gas is good for the pressurized denitration process of flue gas. And this concentration range is also the allowable range of O<sub>2</sub> in actual flue gas.

(3) The pressurized process can remove only a little NO, so enough residence time is required to meet the requirement of NO<sub>x</sub> removal rate. The residence time increases with the decrease of pressure, initial O<sub>2</sub> concentration, initial NO concentration and the increase of temperature.

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#### References

- [1] Wall T, Stanger R, Santos S 2011 *Netherlands. Int. J. of Greenhouse Gas Control* **5** L5
- [2] Ikeda M, Toporov D, Christ D 2012 *United States. Energy & Fuels* **26** L3141
- [3] Timothy T, Rohan S, Terry W 2013 *Netherlands. Int. J. of Greenhouse Gas Control* **18** L15
- [4] England E, Corcoran W 2012 *Industrial & Engineering Chemistry Fundamentals* **4** L65
- [5] Murciano L T, White V, Petrocelli F 2011 *United Kingdom. J. Energy Procedia* **4** L9
- [6] Huang Y, Wang M, Stephenson P 2012 *Netherlands. Fuel* **101** L244
- [7] Krzywański J, Rajczyk R, Nowak W 2014 *Chemical and Process Engineering* **35** L217
- [8] Jia L, Tan Y, Wang C. 2010 *United States. Energy & Fuels* **24** L910
- [9] Gungor A, Eskin N 2008 *Netherlands. Int. J. Thermal Sci.* **47** L157
- [10] Isabelle L, Nruno A, Jean-Pierre T 2011 *United Kingdom. J. Energy Procedia* **4** L2847