

## Molecular Dynamics Simulation of a Small Drop of Liquid Argon

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Results for molecular dynamics simulation method of small liquid drops of argon ( $N = 1200$ – $14400$  molecules) at  $94.4$  K through a Lennard-Jones intermolecular potential are presented in this paper as a preliminary study of drop systems. We have calculated the density profiles  $\rho(r)$ , and from which the liquid and gas densities  $\rho_l$  and  $\rho_g$ , the position of the Gibbs' dividing surface  $R_o$ , the thickness of the interface  $d$ , and the radius of equimolar surface  $R_e$  can be obtained. Next we have calculated the normal and transverse pressure tensor  $p_N(r)$  and  $p_T(r)$  using Irving-Kirkwood method, and from which the liquid and gas pressures  $p_l$  and  $p_g$ , the surface tension  $\gamma_s$ , the surface of tension  $R_s$ , and Tolman's length  $\delta$  can be obtained. The variation of these properties with  $N$  is applied for the validity of Laplace's equation for the pressure change and Tolman's equation for the effect of curvature on surface tension through two routes, thermodynamic and mechanical.

**Key Words** : Drop of liquid argon, Irving-Kirkwood pressure, Surface tension, Molecular dynamics simulation

## Introduction

The investigation of mechanical or thermodynamic properties of small systems is of great scientific and practical interest. When considering liquid drops in the theory of surface phenomena, a most important effect is the dependence of the surface tension on the drop size. The thermodynamic analysis of Gibbs<sup>1</sup> and the older mechanical ideas of Young, Laplace, and others<sup>2-7</sup> lead to several widely used formulas for droplets.

Laplace<sup>2</sup> considered a liquid droplet floating in a vapor phase and noticed that the surface tension of the liquid-vapor interface tries to contract the spherical surface of the droplet. The droplet must therefore be stabilized by a pressure difference over the interface that balances the contracting force. The Laplace equation expresses this condition for mechanical equilibrium for a three dimensional fluid:

$$\Delta p = \frac{2\gamma_s}{R_s}, \quad (1)$$

where  $\Delta p = p_l - p_g$  is the pressure difference between the interior of the drop ( $p_l$ ) and the gas ( $p_g$ ) and  $\gamma_s$  is the surface tension referred to the surface of tension  $R_s$  (radius of tension).

The Tolman equation for the variation of the surface tension with drop size is given by

$$\frac{\gamma_s}{\gamma_\infty} = 1 - \frac{2\delta}{R_s} + \dots, \quad (2)$$

where  $\gamma_\infty$  is the surface tension for the planar interface and  $\delta = R_e - R_s$  is called Tolman's length after Tolman<sup>3</sup> with  $R_e$  the radius for the equimolar surface. Using Eqs. (1) and (2), the thermodynamic route leads to

$$R_s = \frac{3 - [9 - 4R_e \frac{\Delta p}{\gamma_\infty}]^{1/2}}{\Delta p / \gamma_\infty}. \quad (3)$$

The equimolar dividing surface at radius  $R_e$  is defined so that the system would contain an equal number of molecules where the density remains constant at its two respective limiting value on either side of the surface, with a discontinuous change at the surface itself. For a spherical drop,  $R_e$  is given by

$$R_e^3 = \frac{1}{\rho_g - \rho_l} \int_0^\infty dr \, r^3 \frac{d\rho(r)}{dr}. \quad (4)$$

The local pressure tensor  $\mathbf{p}(r)$  for drops can be defined<sup>8,9</sup> in terms of the pair-correlation function of the fluid and although this definition is not unique, all tensors have in common that they satisfy the condition

$$\nabla \cdot \mathbf{p}(r) = 0 \quad (5)$$

in the absence of an external field. Furthermore, all tensors become isotropic in a bulk phase with diagonal components  $p$ , the pressure in the bulk. In a spherical symmetry, the pressure tensor has only two independent components

$$\mathbf{p}(r) = p_N(r)\hat{\mathbf{r}}\hat{\mathbf{r}} + p_T(r)(\mathbf{I} - \hat{\mathbf{r}}\hat{\mathbf{r}}) \quad (6)$$

where  $\hat{\mathbf{r}}$  is a unit vector in the direction  $\mathbf{r}$ ,  $\mathbf{r}$  is the distance from the origin, and  $\mathbf{I}$  is the unit tensor.  $p_N(r)$  and  $p_T(r)$  are the normal and transverse components of the pressure tensor at position  $\mathbf{r}$ , respectively.

The general condition of mechanical equilibrium, Eq. (5), leads to

$$\frac{dp_N(r)}{dr} = -\frac{2}{r}[p_N(r) - p_T(r)]. \quad (7)$$

Note that  $p_N(r)$  and  $p_T(r)$  both become equal to the bulk pressure  $p$  in a bulk phase. Integrating Eq. (7) from  $0$  to a position  $R_v$  (or  $\infty$ ) sufficiently deep in the vapor phase gives the pressure difference  $\Delta p$ ,

$$\Delta p = 2 \int_0^\infty dr \frac{1}{r} [p_N(r) - p_T(r)]. \quad (8)$$

Combining to the Laplace Eq. (1), we obtain for the surface tension

$$\gamma_s = \int_0^\infty dr \frac{R_s}{r} [p_N(r) - p_T(r)] . \quad (9)$$

From mechanical arguments for the force and torque on a hypothetical strip cutting the surface of the drop, Bakker<sup>10</sup> and Buff<sup>11</sup> obtained the equation

$$\gamma_s = \int_0^\infty dr \left( \frac{r}{R_s} \right)^2 [p_N(r) - p_T(r)] . \quad (10)$$

Eq. (9) is invariant to the form of the pressure tensor, whereas Eq. (10) is not. Combining Eqs. (7) and (10), using Eq.(1), gives for  $\gamma_s$

$$\gamma_s^3 = -\frac{1}{8}(p_l - p_g)^2 \int_0^\infty dr r^3 \frac{dp_N(r)}{dr} . \quad (11)$$

**Molecular Dynamics Simulation and Irving-Kirkwood Pressure Tensor.** The usual Lennard-Jones (LJ) 12-6 potential for the interaction between argon molecules is used with LJ parameters,  $\sigma = 0.34$  nm and  $\varepsilon/k_B = 120$  K, where  $k_B$  is the Boltzmann constant. The inter-atomic potential is truncated at  $r_c = 4\sigma$  and long-range corrections are applied to the energy, pressure, *etc.* due to the potential truncation.<sup>12</sup> The time integrations for the equation of translational motion is solved using the velocity-Verlet algorithm<sup>13</sup> with a time step of  $5 \times 10^{-15}$  second (5 fs). The temperature (94.4 K) is kept constant by using a Nose-Hoover<sup>14,15</sup> thermostat. These systems of  $N = 1200, 1800, 3600, 7200, 10800$ , and 14400 molecules of argon are fully equilibrated in cubic boxes with spherical boundary conditions<sup>16</sup>:

$$\begin{aligned} u_k &= k(r_i - r_o)^2, & r_i > r_o \\ &= 0, & r_i < r_o \end{aligned} \quad (12)$$

where  $k = 25$  cal/mol and  $r_o$  is given in Table 1 for each system of  $N$ . This external repulsive potential serves to prevent molecules from leaving the spherical cell. The values of  $k$  and  $r_o$  have to be chosen with care. The value of  $r_o$  must not be so small that the potential interferes the drop, nor so large that the vapor phase is very large or that the drop evaporates.

The Irving-Kirkwood (IK) pressure tensor is calculated by an extension to a spherically symmetric system of the method described by Tsai.<sup>17</sup> Details of the calculation of

$p_N^{IK}(r)$  is are given in the appendix of Ref. 16 and we describe the brief calculation here. The normal component  $p_N(r)$  is the sum of kinetic and configurational terms

$$p_N(r) = p_K(r) + p_U(r) , \quad (13)$$

where  $p_K(r) = k_B T \rho(r)$  is the kinetic term. The configurational term is given by

$$p_U(r) = S^{-1} \sum_k f_k , \quad (14)$$

where  $S = 4\pi r^2$  is the area of a spherical surface of radius  $r$  and the sum over  $k$  is over the normal components of all the pair forces  $f_k$  acting across the surface. For a single surface  $S$  and one pair of molecules, the relevant geometry is given in Figure 1. Depending on the location of molecule  $i$  and  $j$ , the force acts across no [Fig. 1(a)], only one [Fig. 1(b)], or two intersection(s) [Fig. 1(c)]. The force vector  $f(r_{ij})$  is given by

$$f(r_{ij}) = \hat{r}_{ij} f(r_{ij}) = -\hat{r}_{ij} \frac{du(r_{ij})}{dr_{ij}} \text{ and } f_k = |\hat{r} \cdot \hat{r}_{ij}| f(r_{ij}) = |\mathbf{r} \cdot \mathbf{r}_{ij}| f(r_{ij}) / r r_{ij}$$

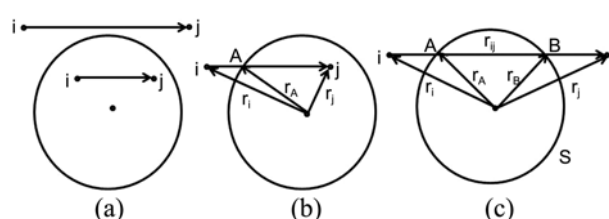
so that

$$p_U(r) = -(4\pi r^3)^{-1} \sum_k |\mathbf{r} \cdot \mathbf{r}_{ij}| \frac{1}{r_{ij}} \frac{du(r_{ij})}{dr_{ij}} . \quad (15)$$

Since the end of  $\mathbf{r}$  ( $\mathbf{r}_A$  or  $\mathbf{r}_B$ ) lines on  $S$  and is between  $i$  and  $j$ , we can write in Figure 1(c)

$$\mathbf{r} = \frac{1}{2}(\mathbf{r}_i + \mathbf{r}_j) + \lambda \frac{1}{2} \mathbf{r}_{ij} , \quad (16)$$

where  $\lambda$  is an undetermined constant in the range  $-1 \leq \lambda \leq 1$  so that  $\mathbf{r} = \mathbf{r}_A$ ,  $\lambda < 0$  and  $\mathbf{r} = \mathbf{r}_B$ ,  $\lambda > 0$ . We can find the two  $\lambda$  values for  $\mathbf{r}_A$  and  $\mathbf{r}_B$  for a given surface,  $\lambda_+$  and  $\lambda_-$ , so that the  $f_k$  acts across the surface by squating Eq. (16) and solving the resulting quadratic:



**Figure 1.** Geometry for calculating the contribution to the pressure tensor from a pair of molecules  $i$  and  $j$  with (a) no, (b) only one, (c) or two intersection(s).

**Table 1.** The parameter of external repulsive potential in Eq. (12)  $r_o$ , the liquid and gas densities  $\rho_l$  and  $\rho_g$ , the position of the Gibbs' dividing surface  $R_o$ , the thickness of the interface  $d$ , the radius of equimolar surface  $R_e$ , number of molecules in the drop  $N_d$ , and the percentage of  $N_d/N$  obtained from this work

N	$r_o$ (nm)	$\rho_l$ (g/cm <sup>3</sup> )	$\rho_g$ (g/cm <sup>3</sup> )	$R_o$ (nm)	$d$ (nm)	$R_e$ (nm)	$N_d$	$N_d/N$ (%)
14400	10.99	1.360	0.008	5.47	0.77	5.48	13985	97.1
10800	9.99	1.364	0.010	4.96	0.80	4.99	10464	96.9
7200	8.72	1.365	0.014	4.31	0.79	4.34	6910	96.0
3600	6.92	1.371	0.020	3.38	0.80	3.43	3375	93.8
1800	5.50	1.384	0.031	2.40	0.76	2.45	1625	90.2
1200	4.80	1.403	0.044	2.02	0.80	2.08	1033	86.1

$$\lambda_{\pm} = \frac{r_i^2 - r_j^2}{r_{ij}^2} \pm \left[ \left( \frac{r_i^2 - r_j^2}{r_{ij}^2} \right)^2 + 1 - \left( \frac{r_i^2 - r_j^2}{r_{ij}^2} \right) + \frac{4r^2}{r_{ij}^2} \right]^{1/2} \quad (17)$$

and so for both intersection the scalar product that appears in Eq. (15) has the same value as required by symmetry. The final result is obtained from  $\mathbf{r}$  in Eq. (17):

$$|\mathbf{r} \cdot \mathbf{r}_{ij}| = \frac{1}{2} r_{ij}^2 \left[ \left( \frac{r_i^2 - r_j^2}{r_{ij}^2} \right)^2 + 1 - \left( \frac{r_i^2 - r_j^2}{r_{ij}^2} \right) + \frac{4r^2}{r_{ij}^2} \right]^{1/2}. \quad (18)$$

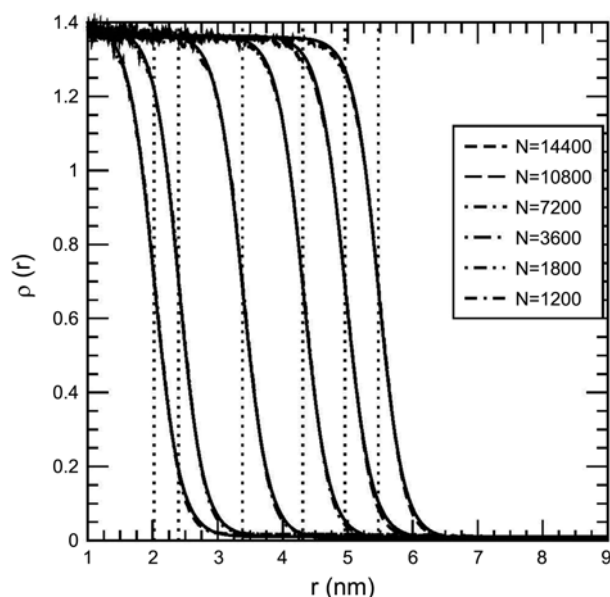
If both  $|\lambda_{+}| \leq 1$  and  $|\lambda_{-}| \leq 1$ , there are two intersection [Fig. 1(c)]. If both  $|\lambda_{+}| > 1$  and  $|\lambda_{-}| > 1$ , there is no intersection [Fig. 1(a)]. For the other cases, there is only one intersection [Fig. 1(b)]. The following two equalities are used:  $(\mathbf{r}_i + \mathbf{r}_j) \cdot \mathbf{r}_{ij} = r_j^2 - r_i^2$  and  $2\mathbf{r}_i \cdot \mathbf{r}_j = r_i^2 + r_j^2 - r_{ij}^2$ .

## Results and Discussion

Typical density profiles for different numbers of argon molecules ( $N$ ), obtained from simulations, are shown in Figure 2 as dashed lines. A hyperbolic tangent function of the form<sup>18</sup>

$$\rho(r) = \frac{1}{2}(\rho_l + \rho_g) - \frac{1}{2}(\rho_l - \rho_g) \tanh[2(r - R_0)/d] \quad (19)$$

is fitted to the simulation results where  $R_0$  is the position of the Gibbs' dividing surface and  $d$  is a parameter for thickness of the interface. In the drop center the counting statistics are so poor because of the low volume of each shell in this region that the density profile of the central part is artificially flat. The fitted  $\rho(r)$  and the positions of  $R_0$  are shown as solid lines and as dotted lines in Figure 2, respectively. The values



**Figure 2.** Density profiles for different numbers of argon molecules ( $N$ ) at 94.4 K, obtained from simulations, are shown as dashed lines. The fitted  $\rho(r)$  as Eq. (19) are shown as solid lines and the straight dotted lines represent the positions of  $R_0$ .

of  $R_0$  and  $d$  used in Eq. (19) with  $\rho_l$  and  $\rho_g$  are given in Table 1 for different numbers of argon molecules ( $N$ ). Both densities strongly increase with decreasing  $N$ . Using Eq. (4) and the obtained density profiles  $\rho(r)$ , the radii  $R_e$  for the equimolar surface for different numbers of argon molecules ( $N$ ) are calculated and also listed in Table 1. The values for  $R_0$  and  $R_e$  are very close each other and they increase with increasing  $N$ .

To estimate a measure of the average drop size, the number of molecules  $N_d$  in the drop is defined as<sup>16</sup>

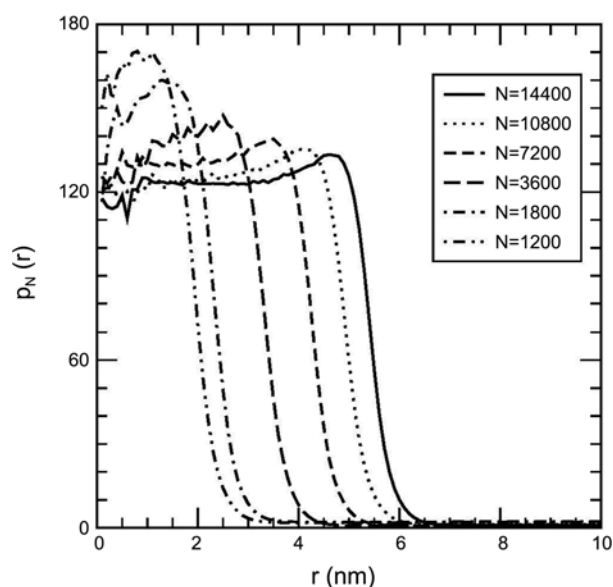
$$N_d = 4\pi \int_0^{R_{10}} dr r^2 \rho(r), \quad (20)$$

where

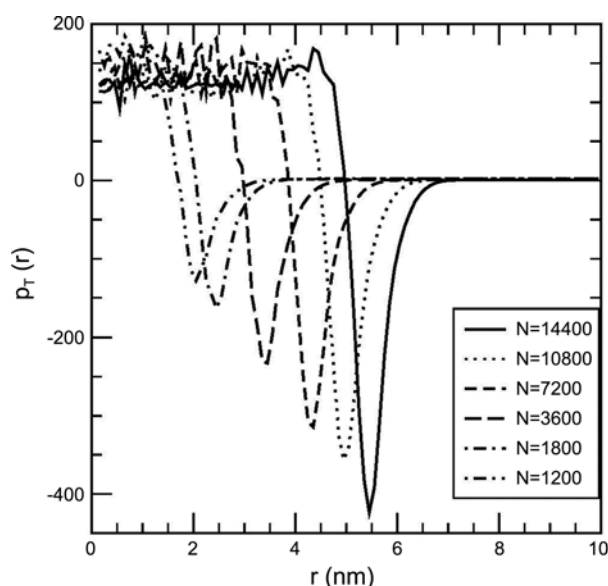
$$\rho(R_{10}) = \rho_g + 0.10(\rho_l - \rho_g). \quad (21)$$

The drop contains molecules out to a radius  $R_{10}$  where the local density has fallen to the gas density plus 10% of the difference between  $\rho_l$  and  $\rho_g$ . The values of  $N_d$  obtained from the simulation are listed in Table 1. The percentage of  $N_d/N$  (Table 1) strongly decreases with decreasing  $N$ , in accord with the strong increment of  $\rho_g$  with decreasing  $N$ , indicating that small drops are only stable in surroundings of a high pressure gas phase. Or it might be related to artificially the volume of the cubic simulation box in which the drop of liquid argon is immersed.

Figures 3 and 4 show the normal and transverse components of the pressure tensor. First,  $p_N^{\text{IK}}(r)$  are obtained from the simulation according to the Irving-Kirkwood (IK) method, Eqs. (13)-(18), and then  $p_T^{\text{IK}}(r)$  are derived from these by Eq. (7). The central part of the kinetic term  $p_T^{\text{IK}}(r)$  in Eq. (13) is flat because of poor statistics for  $\rho(r)$  in the drop center, while the configurational term  $p_U^{\text{IK}}(r)$  is not since many pairs of molecules  $i$  and  $j$  give contribution to the pressure tensor in the drop center. The central part of the



**Figure 3.** The Irving-Kirkwood (IK) normal pressure tensor at 94.4 K.



**Figure 4.** The Irving-Kirkwood (IK) transverse pressure tensor at 94.4 K.

final  $p_N^{\text{IK}}(r)$  is not flat unlike the earlier study.<sup>16</sup> It increases with  $r$  and decreases after a maximum at  $r_{\text{max}} < R_c$ .

The values of  $p_l$  and  $p_g$  in Table 2 are obtained by averaging  $p_N^{\text{IK}}(r)$  from  $r = 0$  to  $r_{\text{max}}$  and from  $r = R_c + d/2$  to  $r = \infty$ , respectively, instead of using Eq. (19) with  $\rho$  replaced by  $p_N^{\text{IK}}$  as reported in Ref. 16. Both  $p_l$  and  $p_g$  decrease with increasing  $N$  indicating high  $p_l$  and  $p_g$  at small  $N$ . The value of  $\Delta p = p_l - p_g$  may be different from  $\Delta p = p_N^{\text{IK}}(0) - p_N^{\text{IK}}(\infty)$  which is obtained from Eqs. (7) and (8). The values of  $\frac{\Delta p}{\gamma_\infty}$  in Eq. (3) with  $\gamma_\infty = 10.77 \text{ mN/m}$ <sup>19</sup> ranged in 1.1–1.5  $\text{nm}^{-1}$  are normal but  $R_c$  in Table 1 are large, which results in  $4R_c \frac{\Delta p}{\gamma_\infty} > 9$  for all the cases of  $N$ . This concludes that Eq. (3), the thermodynamic route, is unable to calculate  $R_s$ . The criterion for the thermodynamic route,  $R_c \frac{\Delta p}{\gamma_\infty} < 9/4$ , is somewhat irrational since  $R_c$  increases with increasing  $N$  as seen in Table 1, showing that Eq. (3) is unsuccessful for large  $R_c$  and therefore for large  $N$ .

The mechanical route for  $\gamma_s$ , Eq. (10), has an analogy to  $\gamma_\infty$  for the planar interface:

$$\gamma_\infty = \frac{1}{2} \int_0^\infty dz [p_N(z) - p_T(z)] = \frac{1}{2} L_z [\bar{p}_N - \bar{p}_T], \quad (22)$$

where  $p_N(z)$  and  $p_T(z)$  are the normal and transverse

components of the pressure tensor at position  $z$ , respectively, with  $L_z$  the length of  $z$ -side of simulation box. Recent studies for vapor-liquid interface at 94.4 K using a test-area molecular dynamics simulation method have reported an excellent agreement with the experimental data for  $\gamma_\infty$ .<sup>20,21</sup>

The values of the surface tension  $\gamma_s$  using Eq. (11), the mechanical route plus the Laplace equation, obtained from the simulation are listed in Table 2 for different numbers of argon molecules ( $N$ ).  $\gamma_s$  increases with increasing  $N$ , and gives the exact value of  $\gamma_\infty$  for  $N = 3600$  so that Tolman's length  $\delta$  in this case is 0 according to Eq. (2). Generally  $\gamma_s$  is less than  $\gamma_\infty$  due to  $\delta > 0$  [Eq. (2)], but  $\gamma_s$  obtained from simulations are larger than  $\gamma_\infty$  for  $N > 7200$ . This is also reported in the other study. For example,  $\gamma_s^*$  is 0.85 for the thermodynamics route and 0.74 for the mechanical route in the case of  $N = 2048$  (the largest  $N$  in Ref. 16) with  $\gamma_\infty^* = 0.75$  where the reduced  $\gamma^*$  is defined as  $\gamma \frac{\sigma_\epsilon}{\epsilon}$ . This indicates that the liquid drops of argon in this study are somewhat large.

The values of  $R_s$  and  $\delta$ , calculated from the values of  $\gamma_s$  using Eqs. (1) and (2), are listed in Table 2. The results from Eq. (1) are reasonable, while those from Eq. (2) are somewhat unacceptable except the cases of small  $N$ . The Tolman's lengths are negative for large  $N$ . The failure of the thermodynamic route for  $R_s$ , Eq. (3), is originated from the Tolman equation, Eq. (2), for large  $N$ . Note that the Laplace equation, Eq. (1),  $\gamma_s = \frac{1}{2} R_s \cdot \Delta p$  is very similar to Eq. (22) for  $\gamma_\infty$ .

In summary, we have carried out molecular dynamics simulations of small liquid drops of argon (1200–14400 molecules) at  $T = 94.4 \text{ K}$  in which the atoms interact with a Lennard-Jones intermolecular potential cutoff at  $4\sigma$  with spherical boundary conditions. The obtained surface tension  $\gamma_s$  using the mechanical route increases with increasing  $N$ , and gives the exact value of  $\gamma_\infty$  (surface tension for the planar interface) for  $N = 3600$  so that Tolman's length  $\delta = 0$  in this case. Generally  $\gamma_s$  is less than  $\gamma_\infty$  due to  $\delta > 0$  (the Tolman equation), but  $\gamma_s$  obtained from simulations are larger than  $\gamma_\infty$  for  $N > 7200$ . The thermodynamic route, combining the Laplace equation and the Tolman equation, is failed for large radii of the equimolar surface  $R_c$  and therefore for large  $N$  which is originated from the Tolman equation for large  $N$ . This result restricts the size of liquid drop of argon to be less than  $N = 3600$ .

**Acknowledgments.** This research was supported by

**Table 2.** The liquid and gas pressures  $p_l$  and  $p_g$ , the surface tension  $\gamma_s$ , the surface of tension  $R_s$ , and Tolman's length  $\delta$  obtained from this work

$N$	$p_l$ (bar)	$p_g$ (bar)	$\gamma_s$ (mN/m)	$R_s$ (nm), Eq. (1)	$\delta$ (nm), Eq. (1)	$R_s$ , Eq. (2)	$\delta$ , Eq. (2)
14400	123.5	1.1	15.8	2.58	2.90	7.15	-1.67
10800	125.1	1.2	14.6	2.36	2.63	6.07	-1.08
7200	131.0	1.3	13.3	2.05	2.29	4.92	-0.58
3600	135.1	1.6	10.8	1.62	1.81	3.43	0.00
1800	147.8	2.0	8.24	1.13	1.32	2.19	0.26
1200	163.8	2.1	6.47	0.80	1.28	1.73	0.35

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