

Multifunctional glass fiber/polyamide composites with thermal energy storage/release capability

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Abstract. Thermoplastic composite laminates with thermal energy storage (TES) capability were prepared by combining a glass fabric, a polyamide 12 (PA12) matrix and two different phase change materials (PCMs), i.e. a paraffinic wax microencapsulated in melamine-formaldehyde shells and a paraffin shape stabilized with carbon nanotubes. The melt flow index of the PA12/PCM blends decreased with the PCM concentration, especially in the systems with shape stabilized wax. Differential scanning calorimetry showed that, for the matrices with microcapsules, the values of enthalpy were approximately the 70% of the theoretical values, which was attributed to the fracture of some microcapsules. Nevertheless, most of the energy storage capability was preserved. On the other hand, much lower relative enthalpy values were measured on the composites with shape stabilized wax, due to a considerable paraffin leakage or degradation. The subsequent characterization of the glass fabric laminates highlighted that the fiber and void volume fractions were comparable for all the laminates except for that with the higher amount of shape stabilized wax, where the high viscosity of the matrix led to a low fiber volume fraction and higher void content. The mechanical properties of the laminates were only slightly impaired by PCM addition, while a more sensible drop of the elastic modulus, of the stress at break and of the interlaminar shear strength could be observed in the shape stabilized wax systems.

Keywords: polymer composites, polyamide 12, thermal energy storage, phase change materials, multifunctional composites

1. Introduction

The growing increase in greenhouse gases emissions and high cost of fossil fuel are the main reasons for the need of a more effective use of energy in all the domestic and industrial activities. Thermal energy storage (TES) consists in storing heat for a later use thus reducing the discrepancy between energy availability and demand with beneficial effects on thermal management processes [1–3]. TES systems currently find employment in many applications, such as in power generation systems [4, 5] and in construction [6, 7], applications where the need for thermal energy is considerable and varies noticeably on a daily and seasonal basis [8].

Thermal energy can be stored and released as sensible heat, through a thermochemical reaction, or as

latent heat by using phase change materials (PCMs). These materials generally undergo reversible solid/solid or solid/liquid phase transitions and can be classified as organic, inorganic or eutectic [1]. PCMs can accumulate a large amount of thermal energy per unit mass, at a nearly constant temperature, with a low change in volume [9]. Organic PCMs, and paraffin waxes in particular, are the most widely used materials for TES applications [1, 10, 11]. They present considerable advantages over other PCMs, such as high energy density, small volume change over phase transition, narrow working temperature range, tunable operating temperature, low density and cheapness [12, 13]. On the other hand, organic PCMs have some drawbacks, such as low thermal conductivity and need for confinement to avoid leakage above the

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melting temperature [14]. The leakage issue can be tackled in two main ways. The first is the encapsulation of the PCMs in organic or inorganic micro- or nano shells, which also protect the PCM from the external environment and may increase its thermal stability [15–17]. The second method is called ‘shape stabilization’, and involves the confinement of the PCM using a polymer matrix [18–21], a porous or layered material [22, 23] or an inorganic nanofiller [24–26]. If the shape stabilization is performed with a metallic or a carbon based material, this also leads to an increase of the overall thermal conductivity [27, 28].

TES systems based on PCMs find applications in buildings [29, 30], hot/cold water storage [31], solar thermal power plants [32], smart thermoregulating textiles [25, 33], and thermal management of electronic devices [22]. In most of these applications, the TES function is performed by a dedicated added module, containing PCMs. However, there are some fields where the addition of a new part performing the thermal management would lead to an unacceptable increase in mass and volume. In these cases, it would be advantageous to have a multifunctional structure that also contributes to the thermal management.

The most suitable materials that can be designed as multifunctional are the composite materials [34–36]. Being composed of two or more phases with different properties [37, 38], they could be designed to combine load bearing properties and functional capabilities. Particularly, lightweight polymer matrix composites performing TES functions and a structural/semi structural role could be usefully employed in fields where weight and volume savings are crucial design parameters but the temperature control is also important. Examples of such fields can be the automotive, aerospace, portable electronics and technical garments industries. However, even though there are many examples in the literature of encapsulated and shape stabilized PCMs embedded in a polymer matrix [5, 12, 17, 29, 39–42], only few papers can be found that deal with the development of polymer composites merging structural and TES functions. Most of the examples of such composites regard sandwich structures that have functions of thermal management with [22] or without [43, 44] the use of a PCM. More recently, Yoo and coworkers [45, 46] developed a glass fiber/epoxy composite including a commercial microencapsulated PCM and characterized its thermal [45], mechanical and viscoelastic [46] properties. Moreover, our group is currently

preparing and characterizing multifunctional epoxy/carbon fiber composites containing various percentages of a paraffin shape stabilized with carbon nanotubes (CNTs) [47].

In a polymer composite, the matrix can be a thermoplastic or a thermosetting polymer. Thermoplastic composites reinforced with long and short fibers (fiber reinforced thermoplastics, FRTs) are attracting increasing attention because of their advantages over their thermosetting counterpart. They provide higher toughness, higher strain to failure, superior impact resistance and high fracture resistance, which impart outstanding damage tolerance properties [48]. Moreover, thermoplastics have unlimited shelf life at room temperature, lower cost and shorter fabrication time, since they do not have to be cured. They can be easily reprocessed, post thermoformed, joined and repaired by welding or solvent bonding [48–50]. Because of all these features, thermoplastic composites are widely employed in many fields, such as the transportation industry, where they are used to realize structural/semi structural parts like bumpers, front end modules and dashboard frames [51, 52]. Among all the FRTs, those having a polyamide (PA) based matrix and a long (continuous or discontinuous) fiber reinforcement are the most widely used today, thanks to their high mechanical properties and relatively low cost [52].

To the best of our knowledge, no papers dealing with the development of structural thermoplastic composites with TES capability can be found in the open scientific literature, since the small number of research works on multifunctional structural composites with TES properties focus on composites with a thermosetting matrix. On the basis of these considerations, the objective of the present work is to develop and characterize multifunctional composite laminates based on polyamide 12 (PA12) and an E-glass fabric, in which the TES function is achieved by adding two different paraffinic PCMs, able to store and release latent heat in the temperature range 40–50 °C. The aim and the novelty of this work is to produce new composite materials able to exploit all the aforementioned advantages of thermoplastic composites, as well as combine good mechanical properties and thermal energy storage/release capability. PA12 was chosen as a matrix because, due to a relatively high methylene/amide ratio (11/1), it presents a lower moisture sensitivity and a lower melting temperature than the more common PA6 and PA66

[53–55]. Additionally, there are many examples in the literature of PA12 reinforced with continuous and discontinuous glass fibers [49, 56–59]. PA12 was blended with two selected PCMs, namely (1) a commercial microencapsulated PCM, in which the paraffinic core is embedded in melamine-formaldehyde shells; and (2) a shape stabilized PCM, where the leakage of paraffin above the melting temperature is prevented by the presence of CNTs. The most promising PA12/PCM compositions were then chosen to prepare composite laminates through the addition of a glass fiber fabric. The resulting laminates were thermally and mechanically characterized, and the properties were then correlated to their microstructure.

2. Experimental

2.1. Materials

Two paraffinic PCMs were considered, namely a microencapsulated one and a shape stabilized one. Since one of the main goals of this work was to compare a system with microencapsulated paraffin with a system with shape stabilized paraffin, two paraffin waxes with approximately the same melting/crystallization temperatures and enthalpies were selected.

The utilized microencapsulated PCM was the Microtek MPCM43D, provided by Microtek Laboratories Inc. (Dayton, OH, USA). In this system, the PCM phase, i.e. a paraffin wax, had a melting temperature of 43 °C and it was encapsulated inside a stable melamine-formaldehyde based shell, which constitutes the 10–15% of the mass. These microcapsules were characterized by a mean diameter of 17–20 µm, and the melting enthalpy declared by the producer was 190–200 J/g.

The shape stabilized PCM was made by mixing a paraffin wax with carbon nanotubes, following the approach recently reported in [47]. RT44HC paraffin wax (melting temperature = 44 °C, melting enthalpy = 240 J/g) was supplied by Rubitherm Technologies GmbH (Berlin, Germany). Multi-walled carbon nanotubes NC7000® (average diameter 9.5 nm, average length 1.5 µm, BET surface area 250–300 m²/g) were purchased from Nanocyl SA (Sambreville, Belgium).

The thermoplastic matrix was a Rilsan® PA12, supplied by Arkema Group (Lyon, France) in form of polymer chips (density 1.01 g/cm³, melting temperature 174 °C).

The glass fiber (GF) fabric was a bi-directional crimped roving fabric made of E-glass fibers (fiber

diameter 12 µm), supplied by Angeloni Srl (Venice, Italy). All the materials were used as received.

2.2. Sample preparation

2.2.1. Preparation of PA12/PCM blends

The microencapsulated system was ready to use as received, while the shape stabilized PCM was prepared as described in reference [47] and briefly reported here. CNTs were added to the molten paraffin in a weight ratio of 15:85 and vigorously mixed for 5 minutes at 500 rpm at 80 °C with a Dispermat mechanical mixer. As reported in our previous work, this specific CNT weight fraction was chosen because it guaranteed an optimal shape stabilization with no leakage above the melting temperature of the paraffin [47]. The mixture was then cooled down to room temperature and grinded in a cryogenic blade miller Ika Labortechnik M20, to obtain a fine powder denoted as ParCNT in the text.

The PA12/PCM blends were prepared by melt compounding and hot pressing. PA12 granules and the PCMs (either the microcapsules or the ParCNT powder) were melt compounded in a Thermo Haake Rheomix 600 internal mixer, equipped with counter-rotating rotors, at different PCM concentrations (ranging from 15 to 60 wt%). The materials were mixed at 200 °C at 60 rpm for 5 minutes. The resulting compounds were molded through a Carver hot-plate press at 200 °C for 5 minutes under an applied pressure of 1.75 MPa. In this way, neat PA12 and PA12/PCM blends at different concentrations were obtained in form of square sheets of 120×120 mm², with a thickness of approximately 2 mm. The prepared matrices are listed in Table 1. The neat PA12 was called PA12-N, the blends with capsules were designed as PA12-Cx and the blends with ParCNT were denoted as PA12-Px (x = 15, 30, 45, 60).

Table 1. list of the prepared matrices

Sample	PA12 [wt%]	Paraffin RT44HC [wt%]	CNTs [wt%]	Microcapsules M43D [wt%]
PA12-N	100	–	–	–
PA12-C15	85	–	–	15
PA12-C30	70	–	–	30
PA12-C45	55	–	–	45
PA12-C60	40	–	–	60
PA12-P15	85	12.8	2.2	–
PA12-P30	70	25.5	4.5	–
PA12-P45	55	38.3	6.7	–
PA12-P60	40	51.0	9.0	–

2.2.2. Preparation of the PA12/PCM-GF laminates

The prepared PA12/PCM blends were used to fabricate composite laminates with E-glass fiber fabric. Five matrix compositions were chosen, namely PA12-N, PA12-C30, PA12-C60, PA12-P30 and PA12-P60. PA12/PCM sheets were prepared through melt compounding and hot-plate pressing, in the way described in Section 2.2.1. These sheets had a smaller thickness than those described before, of approximately 0.3 mm, to ease the process of lamination. They were alternated to the glass fiber fabric to prepare laminates consisting of 5 laminae with surface dimensions of 120×120 mm², via hot pressing at 200 °C for 5 minutes under an applied pressure of 3.4 MPa. The resulting laminates had a thickness of approximately 2 mm. The laminates were designated as GF-N, GF-C30, GF-C60, GF-P30 and GF-P60.

2.3. Experimental techniques

2.3.1. Characterization of the matrices

Melt flow index (MFI) tests at 230 °C and with a weight of 2.16 kg were performed on all the prepared matrices with a Dynisco LMI D4000 machine.

The density of the matrices was measured with a helium pycnometer Micrometrics AccuPyc 1330TC, at 23 °C. In order to reach stationary conditions, the density of each sample was the average of 99 consecutive measures.

Scanning electron microscopy (SEM) images of the cryofractured surfaces of all the matrices were acquired through a Jeol IT300 scanning electron microscope at an accelerating voltage of 10 kV, after Pt-Pd sputtering.

Differential scanning calorimetry (DSC) was performed with a Mettler DSC30 machine under a nitrogen flow of 150 mL/min, in a temperature range between 0 and 230 °C, at a heating/cooling rate of 10 °C/min. All the specimens had a mass of approximately 15 mg and were subjected to a first heating scan, a cooling scan and a second heating scan. In this way, melting/crystallization temperatures (T_m , T_c), and melting/crystallization enthalpies (ΔH_m , ΔH_c) of the PCMs were determined. Moreover, relative melting/crystallization enthalpies (ΔH_m^{rel} , ΔH_c^{rel}) were obtained by dividing the ΔH_m and ΔH_c values for the melting/crystallization enthalpy of the capsules or the ParCNT powder, considering the nominal PCM content in the blends. The melting and crystallization

temperatures and enthalpies of the PA12 (T_m^{PA} , T_c^{PA} , ΔH_m^{PA} , ΔH_c^{PA}) were also recorded.

Thermogravimetric analysis (TGA) was carried out by using a Mettler TG 50 machine under a nitrogen flow of 200 mL/min, in a temperature interval between 30 and 700 °C, at a heating rate of 10 °C/min. The test allowed the determination of the temperatures associated to a mass loss of the 1% ($T_{1\%}$), of the 5% ($T_{5\%}$), and the decomposition temperature (T_d), taken as the temperature associated to the maximum mass loss rate.

To evaluate the dimensional stability of the resulting matrices, Vicat tests were performed according to ASTM D 1525 standard at a heating rate of 120 °C/h and under an applied load of 10 N, in a silicone oil bath. The nominal dimensions of the samples were 10×10×5 mm³.

Quasi-static tensile tests were performed according to the ASTM D638-10 standard, with a universal testing machine Instron 4502, equipped with a 1 kN load cell. Dumbbell 1BA specimens (standard UNI EN ISO 527-2) were cut by means of a specimen cutter Ceast 6051. The dimensions of the specimens were the following: length of the narrow parallel sided portion = 30±0.5 mm, width of the narrow portion = 5±0.5 mm, thickness ≥ 2 mm, gauge length = 25±0.5 mm. For each composition, five specimens were tested at 0.25 mm/min for the measurement of the elastic modulus, using a resistance extensometer Instron 2620 with a gauge length of 12.5 mm. The elastic modulus (E) was measured as the secant modulus on the stress-strain curve between strain values of 0.05 and 0.25%. Five additional specimens were tested until failure, at a crosshead speed of 10 mm/min. The stress and strain at the yield point (σ_y , ϵ_y) and at break (σ_B , ϵ_B) were thus determined.

2.3.2. Characterization of the laminates

Optical microscope observations of the composites were made with a Leica DM6000M optical microscope. The samples were englobed, lapped and observed to investigate the disposition of the fibers and the distribution of the components in the matrices. The density of the laminates was measured with a He pycnometer Micrometrics AccuPyc 1330TC at 23 °C. The density of each sample was the average of 99 measures. The density of neat glass fibers was also measured.

DSC and TGA tests were performed in the same experimental conditions utilized for the matrices (see

Section 2.3.1). These tests were carried out also on the neat glass fibers. TGA measurements allowed the calculation of an experimental weight fraction of fibers (ω_f), from which a theoretical density of the laminates was computed. By a comparison with the experimental density obtained via pycnometer measures, the volume fraction of voids (ϕ_v) was calculated. Then, the volume fraction of the fibers (ϕ_f) and the matrix (ϕ_m) could be computed.

Quasi-static tensile tests were performed on the laminates, according to the ASTM D3039 standard. Tests were performed with a universal testing machine Instron 4502 equipped with a 10 kN load cell. Rectangular specimens with surface dimensions of $100 \times 10 \text{ mm}^2$ (and the thickness of the laminate) were cut from each laminate with a diamond wheel. The specimens were tabbed at both ends with glass fiber composite tabs, to avoid damages in the gripping zone. In this way, the elastic modulus (E) and the tensile properties at break (σ_B , ϵ_B) of the laminates were determined.

Short beam shear tests were carried out according to the ASTM D 2344 standard, to evaluate the interlaminar shear strength of the prepared laminates. The tested specimens were cut out of the prepared laminates with a diamond wheel and had nominal dimensions of $15 \times 5 \times 2 \text{ mm}^3$. Tests were performed using an Instron 5969 universal testing machine, equipped with a 50 kN load cell. The span length was fixed at 8 mm and the crosshead speed was fixed at 1 mm/min. The interlaminar shear strength ($ILSS$) was calculated with the Equation (1):

$$ILSS = \frac{3}{4} \frac{P_m}{b \cdot h} \quad (1)$$

where P_m is the maximum load observed during the test and b and h are the specimen width and thickness, respectively. At least five specimens were tested for each sample.

3. Results and discussion

3.1. Characterization of the matrices

Table 2 reports the results of the MFI tests on the matrices. For the matrices with microcapsules, as the capsule content increases the MFI decreases, reaching a minimum of 5.2 g/10 min for the PA12-C60 sample. Also for the matrices with CNT-stabilized paraffin, the MFI decreases with an increase of ParCNT, but in a more dramatic way. Compared to the MFI value of the neat PA12, the MFI is halved with a ParCNT

Table 2. Results of MFI tests on the prepared matrices

Sample	Load [kg]	T [°C]	MFI [g/10 min]
PA12-N	2.16	230	10.3±0.6
PA12-C15	2.16	230	9.2±0.3
PA12-C30	2.16	230	6.9±0.6
PA12-C45	2.16	230	6.1±0.6
PA12-C60	2.16	230	5.2±0.6
PA12-P15	2.16	230	5.2±0.8
PA12-P30	2.16	230	0.7±0.1
PA12-P45	5.00	230	0.7±0.1
PA12-P60	10.00	230	0.5±0.1

content of only 15 wt% and is close to 0.7 g/10 min for a ParCNT content of 30 wt%. Further increases of the ParCNT concentration decrease the fluidity in such a way that the measures could not be performed with a mass of 2.16 kg, but a heavier weight had to be used to obtain a reliable MFI result (see Table 2). This is probably due to the increasing CNT content, since these nanofillers are well known to heavily increase the viscosity of molten polymers. Because of the change in the applied load, it is not possible to draw a trend of the MFI, but these results suggest that it may be difficult to obtain a composite without pores at elevated ParCNT contents. This also implies that, although both PCMs types decrease the fluidity of the PA12, the effect of the capsules is less intense than that of the ParCNT, which indicates a better processability of this PCM during the fabrication of laminates.

Figure 1 shows the SEM micrographs of some prepared matrices, namely PA12-C15, PA12-C60, PA12-P15 and PA12-P60, taken at the same magnification ($1000\times$). For each system, only the SEM images of the matrices with the lower and the higher PCM content (15 and 60%) are reported, for the sake of brevity. In the PA12-C15 and PA12-C60 samples (Figure 1a, 1b), capsules with dimensions ranging from 5 to 20 μm can be observed, and a good adhesion between PA12 and the melamine-formaldehyde shells can be detected. Some capsules are broken, which can be due to the production process or to the cryofracture operations. No microcapsule agglomerates are visible, and the uniform distribution of the capsules determines a morphological continuity of the matrix, which is important for the mechanical performance of the blends. In the sample with 15% of ParCNT (Figure 1c), small domains of ParCNT are visible, but the interfacial adhesion is poorer than

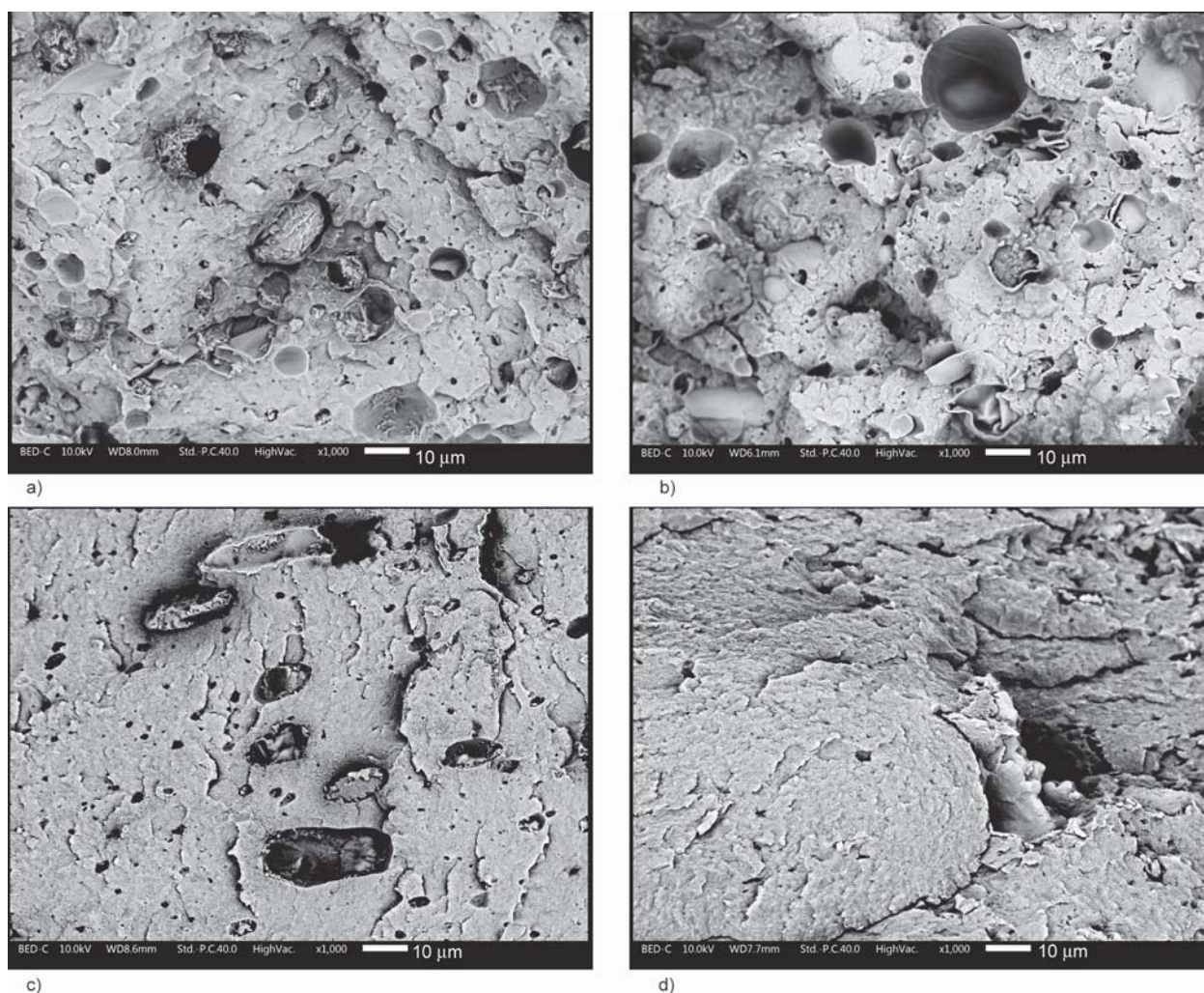


Figure 1. SEM micrographs of the cryofractured surface of some of the prepared matrices. (a) PA12-C15; (b) PA12-C60; (c) PA12-P15; (d) PA12-P60.

that observed with capsules. Conversely, the PCM domains are not visible in the PA12-P60 sample (Figure 1d). A non uniform distribution of the ParCNT was observed in the micrographs of other specimens with the same composition, with the presence of large (500 μm) domains. Also in this case, the results suggest that it could be easier to process the matrices with capsules than those blended with ParCNT powder. Figure 2 shows the DSC thermograms relative to the first heating scan of the matrices with capsules and with ParCNT, respectively. The most important DSC results are summarized in Table 3. The data of the second heating scan are not reported for the sake of brevity, as no important differences were detected between the first and the second heating scan. For the sample PA12-N, an endothermic melting peak can be observed in the heating scan at approximately 180 $^{\circ}\text{C}$. The same peak is visible also for the other samples, where an additional endothermic peak is visible at approximately 40–50 $^{\circ}\text{C}$. This last peak is associated

to the melting of the PCM, either in the capsules (Figure 2a) or in the ParCNT (Figure 2b) blends. Corresponding crystallization peaks have been observed in the cooling scans (not reported here for the sake of brevity). For the matrices with capsules, the melting enthalpy of the PCM increases with an increase of capsules content, and the relative developed enthalpy is approximately 70% of the expected one, according to the nominal capsules content. These values of relative melting and crystallization enthalpy of the PCMs are comparable with those observed in the literature for blends with paraffin microcapsules embedded in a thermoplastic polymeric matrix [60, 61]. This suggests that, during the processing steps, some capsules were broken, and the paraffin leaked out of the blend. Nevertheless, most of the thermal energy storage/release capability is retained. Conversely, for matrices with ParCNT (Figure 2b), the PCM melting enthalpy does not follow a trend with the ParCNT content and enthalpy values are in the

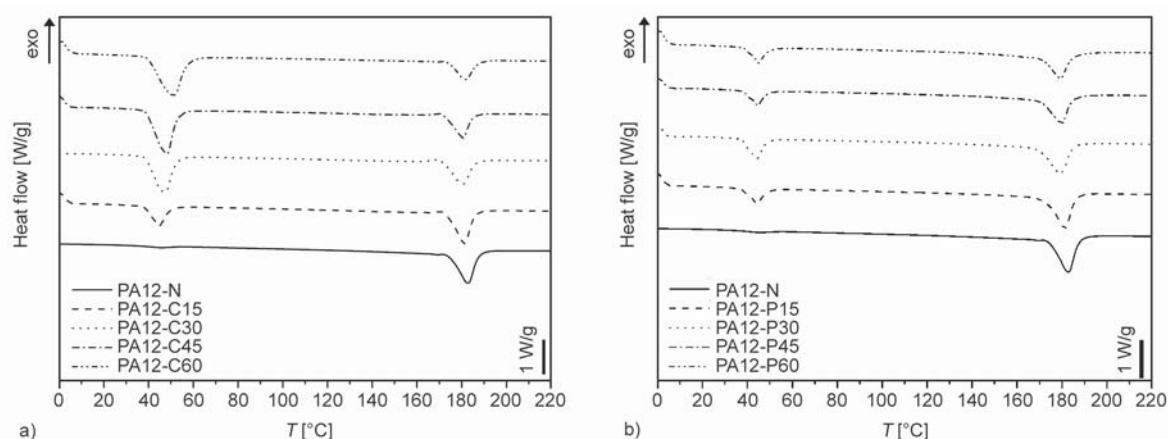


Figure 2. DSC thermograms of the prepared matrices. (a) Matrices with microcapsules; (b) matrices with paraffin and CNTs.

Table 3. Results of the DSC tests on the prepared matrices

Sample	T_m [°C]	ΔH_m [J/g]	ΔH_m^{rel} [%]	T_m^{PA} [°C]	ΔH_m^{PA} [J/g]	T_c [°C]	ΔH_c [J/g]	T_c^{PA} [°C]	ΔH_c^{PA} [J/g]
PA12-N	—	—	—	181.2	47.9	—	—	155.7	52.0
PA12-C15	43.9	20.5	68.3	179.8	40.9	32.4	18.1	153.2	40.8
PA12-C30	45.9	46.8	77.9	179.3	35.6	23.0	46.8	152.0	36.0
PA12-C45	46.2	61.2	67.9	172.2	31.0	24.7	61.2	155.7	31.1
PA12-C60	49.1	76.2	63.8	180.2	25.9	21.8	71.7	152.6	23.8
PA12-P15	43.3	16.1	57.3	172.2	46.6	33.2	11.3	160.5	46.3
PA12-P30	43.1	21.1	37.6	177.7	42.6	32.6	15.6	165.4	42.8
PA12-P45	43.5	14.0	16.7	178.4	42.8	29.2	8.6	158.7	41.3
PA12-P60	44.0	16.4	14.6	178.0	46.4	30.4	12.2	160.7	46.1

T_m melting temperature of the PCM [°C]
 ΔH_m PCM melting enthalpy [J/g]
 ΔH_m^{rel} relative PCM melting enthalpy [%]
 T_m^{PA} melting temperature of PA12 [°C]
 ΔH_m^{PA} melting enthalpy of PA12 [J/g]
 T_c crystallization temperature of the PCM [°C]
 ΔH_c PCM crystallization enthalpy [J/g]
 T_c^{PA} crystallization temperature of PA12 [°C]
 ΔH_c^{PA} crystallization enthalpy of PA12 [J/g]

range 14–21 J/g, well below the expected values (see Table 3). This suggests that most of the paraffin was degraded or leaked out of the matrix during the production process. Interestingly, the crystallization temperature of PA12 matrix is increased of about 5 °C in the ParCNT based blends. As already observed in our previous papers on polyamide 6-clay nanocomposites [62], this is probably due to the nucleating effect played by CNTs within the matrix.

The paraffin leakage/degradation effect is visible also in the TGA results, reported in Figure 3 and in Table 4. The residual mass and the mass loss derivative of the systems with capsules as a function of temperature are reported in Figure 3a, 3b. As the capsule content increases, the curves shift to lower temperatures and the values of $T_{1\%}$ and $T_{5\%}$ decrease, thus indicating a lower thermal resistance. This was expected,

since the degradation temperature of the neat PA12 is higher than that of the PCM capsules. The blends show two distinct degradation steps; the first is associated to the degradation of the capsules and proportional to the capsules content (300–400 °C), and the second is related to the degradation of the PA12 (450–500 °C). The TGA thermograms of the blends with paraffin are reported in Figure 3c, 3d. The ParCNT powder presents a degradation peak temperature T_d of approximately 210 °C, well below that of the capsules. Considering that the PCM concentration within the capsules is not different from the paraffin content in the CNT stabilized systems, it can be concluded that the PCM encapsulation delays the degradation of the PCM and improves the overall thermal resistance, while CNTs do not perform any thermal barrier effect. This implies that the capsules are more suitable

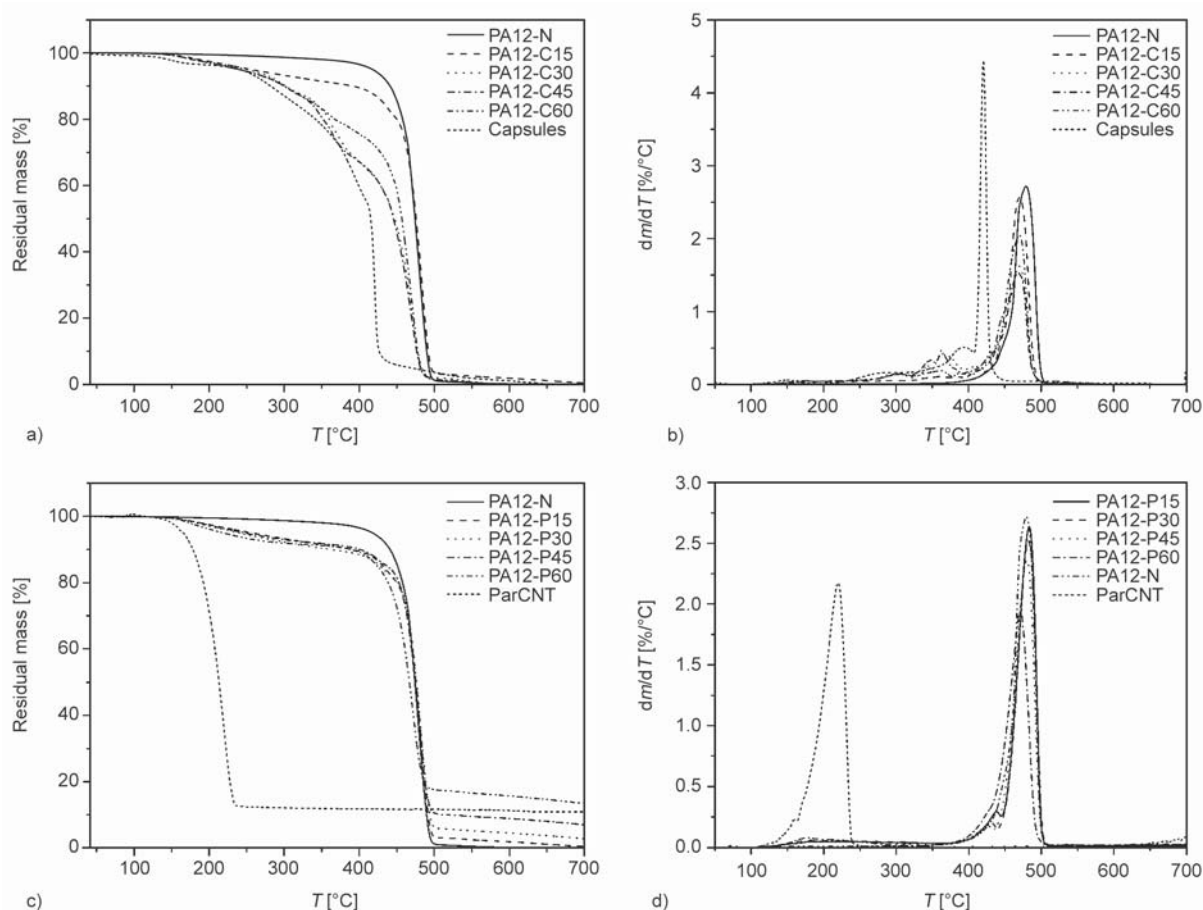


Figure 3. TGA thermograms of the prepared matrices. (a) Matrices with microcapsules, residual mass; (b) matrices with microcapsules, derivative of the mass loss; (c) matrices with paraffin and CNTs, residual mass; (d) derivative of the mass loss.

as PCM coupled with a polymer system as PA12, which has to be processed at a temperature around 200 °C. Also for the systems with ParCNT, the blends show a first degradation step in correspondence of the degradation of the PCM, and a second one where the PA12 degrades, but the mass loss associated to

the PCM degradation step is not proportional to the nominal ParCNT content, since it is nearly constant, being approximately 9%. This is in good agreement with the DSC results and suggests that the majority of the PCM leaked out of the matrix during the production process. On the other hand, the residue at the end of the test is proportional to the ParCNT content. The residue is mostly due to the CNTs, whose degradation in N₂ atmosphere can be considered negligible in this case, and thus it can be assumed that, unlike the paraffin, the CNTs do not leave the blends during the production process. This is consistent with the MFI results, since the CNTs are considered as the major responsible for the dramatic increase in viscosity observed for the matrices with ParCNT. Figure 4 shows representative stress-strain curves obtained during quasi-static tensile tests, while the most important mechanical parameters are reported in Table 5. All the considered mechanical properties of the blends are lower than that of PA12-N. For both systems, all the properties have a negative trend with the PCM content, which can be due to the poor

Table 4. Results of the TGA tests on the prepared matrices

Sample	T _{1%} [°C]	T _{5%} [°C]	T _d [°C]
PA12-N	269	418	479
PA12-C15	164	256	470
PA12-C30	160	250	470
PA12-C45	160	244	470
PA12-C60	159	243	469
PA12-P15	164	256	483
PA12-P30	162	239	482
PA12-P45	165	247	480
PA12-P60	159	219	479

T_{1%} temperature corresponding to a mass loss of 1% [°C]

T_{5%} temperature corresponding to a mass loss of 5% [°C]

T_d degradation temperature, associated to the maximum mass loss rate [°C]

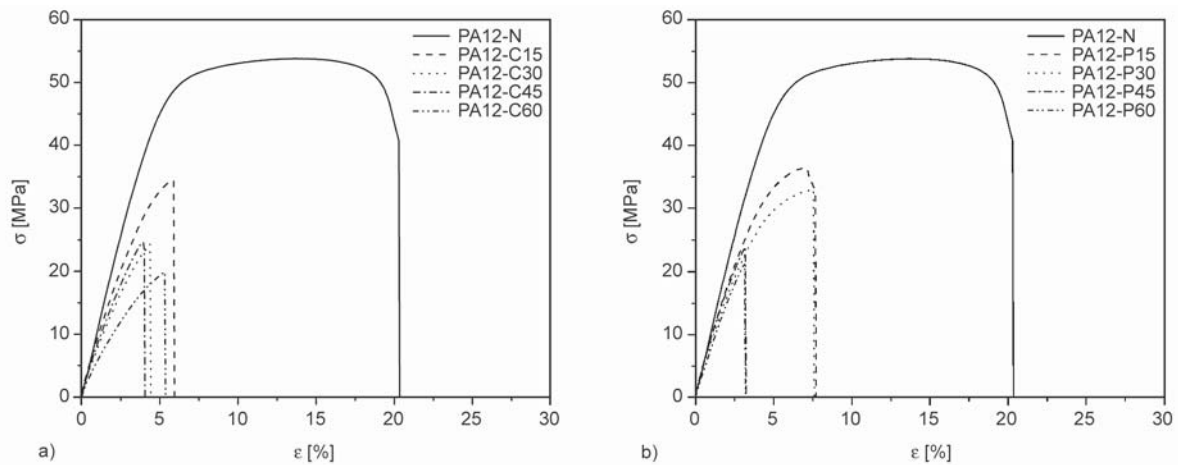


Figure 4. Representative stress-strain curves of the prepared matrices in the quasi static tensile tests. (a) Matrices with capsules; (b) matrices with paraffin and CNTs.

mechanical properties of the PCMs themselves. The only exception is represented by the elastic modulus in the matrices with ParCNT, increasing as the ParCNT content increase, which could be due to the increasing amount of CNTs within the matrix. This conclusion is in good agreement with the results of the thermal characterization and with those of the Vicat tests, reported in Table 5. The values of Vicat softening temperature (VST) of the blends are close to that of the PA12-N, which indicates that the melting of both PCMs does not lead to a remarkable softening of the matrix. For the matrices with ParCNT, the VST slightly increases with the PCM content, which can be once again due to the presence of CNTs.

The physical, thermal and mechanical characterization of the matrices highlighted that the capsules may be most suitable than ParCNT in combination with the PA12, in the perspective of producing long fiber multifunctional composites, if both the processability and the thermo mechanical properties are considered. However, laminates were produced with both matrix systems as well, at two different PCM

fractions (30 and 60 wt% respect to the matrix), and compared with the laminate without PCM. The results of the characterization are reported hereafter.

3.2. Characterization of the laminates

Figure 5 shows the optical microscope images of the polished surface of the produced laminates. Observing the images at lower magnification (Figure 5a–5c, 5e, 5f) it can be seen that the fibers in all the laminates are wetted homogeneously and kept the orientation set in the die during the preliminary operation of the hot pressing. The proper fiber wetting can be better appreciated in the high magnification image of GF-C60 (Figure 5d), where also the capsules can be observed in the interlaminar region. The only exception is GF-P60 (Figure 5f), in which the fibers are not properly wetted and the weaving of the fabric seems distorted. A non homogeneous distribution of the matrix across the thickness of the laminate and an incomplete wetting of the fabric can be easily observed, and it was probably due to the high viscosity of the matrix (see MFI results in Section 3.1).

Table 5. Results from quasi static tensile tests and Vicat tests on the prepared matrices

Sample	E [MPa]	σ_y [MPa]	ϵ_y [%]	σ_B [MPa]	ϵ_B [%]	VST [°C]
PA12-N	1794±91	52.5±1.4	13.4±1.6	40.3±1.9	20.0±1.3	175.3
PA12-C15	1340±73	34.7±1.2	5.7±0.2	34.7±1.2	5.7±0.2	172.5
PA12-C30	1007±49	24.6±1.5	5.3±0.7	24.6±1.5	5.7±0.2	173.2
PA12-C45	1027±29	24.8±4.5	4.2±1.0	24.6±1.5	4.2±1.0	172.5
PA12-C60	973±39	20.0±2.2	5.6±0.8	20.0±2.2	5.6±0.8	173.2
PA12-P15	1316±67	29.8±4.6	5.1±1.4	27.5±3.4	5.5±1.6	173.2
PA12-P30	1345±17	32.3±2.4	6.4±1.3	31.8±2.7	6.7±1.3	174.6
PA12-P45	1378±38	27.6±2.5	4.2±0.7	22.7±6.6	4.2±0.6	175.7
PA12-P60	1529±55	24.1±6.5	3.3±1.3	23.2±7.3	3.3±1.2	179.4

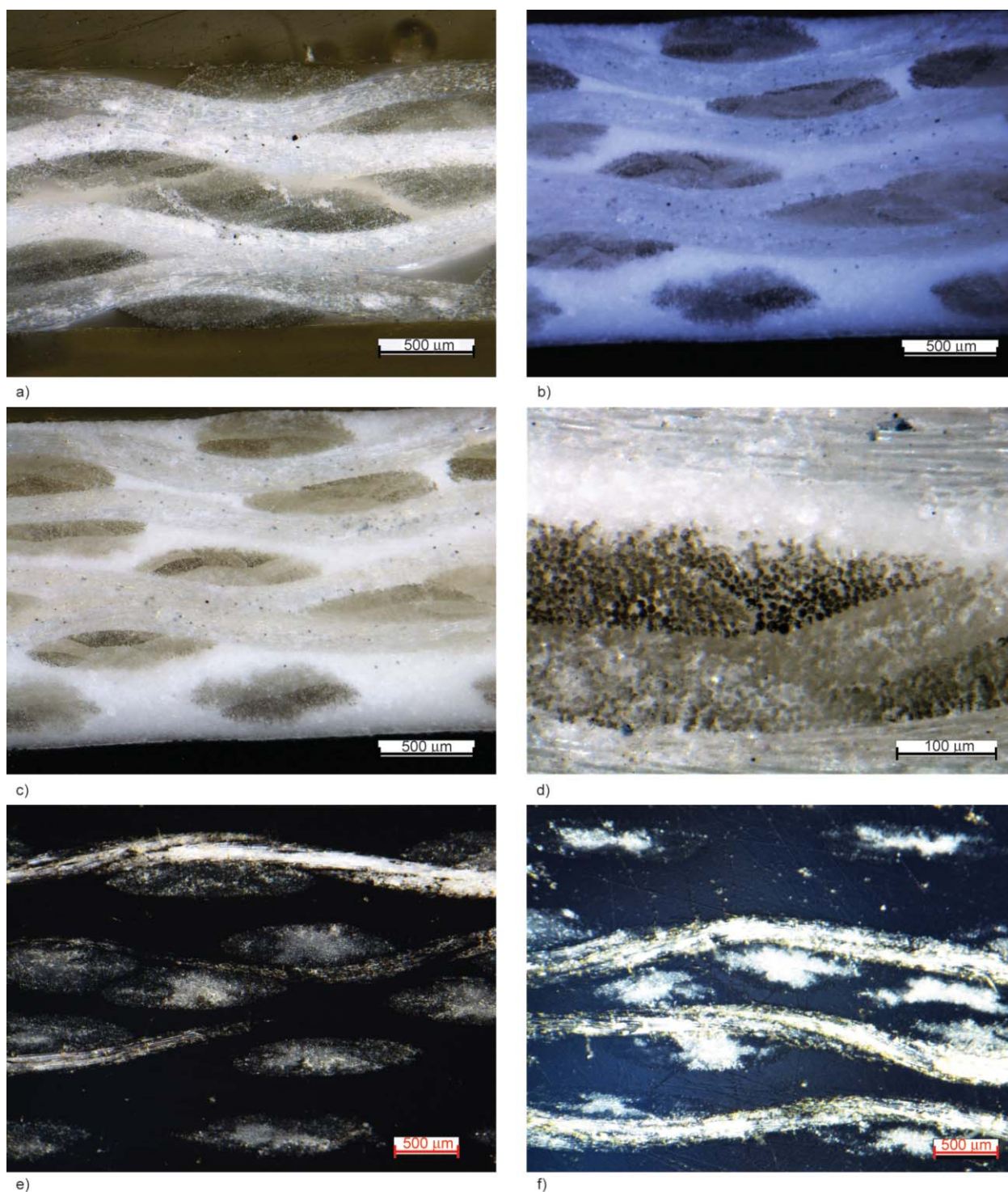


Figure 5. Optical microscope images of the polished surface of the prepared laminates (a) GF-N, 48 \times ; (b) GF-C30, 48 \times ; (c) GF-C60, 48 \times ; (d) GF-C60, 256 \times ; (e) GF-P30, 48 \times ; (f) GF-P60, 48 \times .

After the production of the laminates, it is important to evaluate the real weight and volume fractions of fibers and matrix, and the volume fraction of voids. This was performed through TGA measurements, which allowed an evaluation of the fiber weight fraction and the calculation of a theoretical density, and through He pycnometry, which led to the measurement of an experimental density and to the calculation

of the volume composition. The results of this analysis are reported in Table 6. The fiber volume fraction is nearly the same for the laminates GF-N, GF-C30, GF-C60 and GF-P30, being around 50–55 vol%, and also the volume fraction of voids is similar in these samples (around 2 vol%). This means that the properties of these laminates can be directly compared. On the other hand, in the GF-P60 laminate the void

Table 6. Volume fractions of the constituents of the prepared laminates

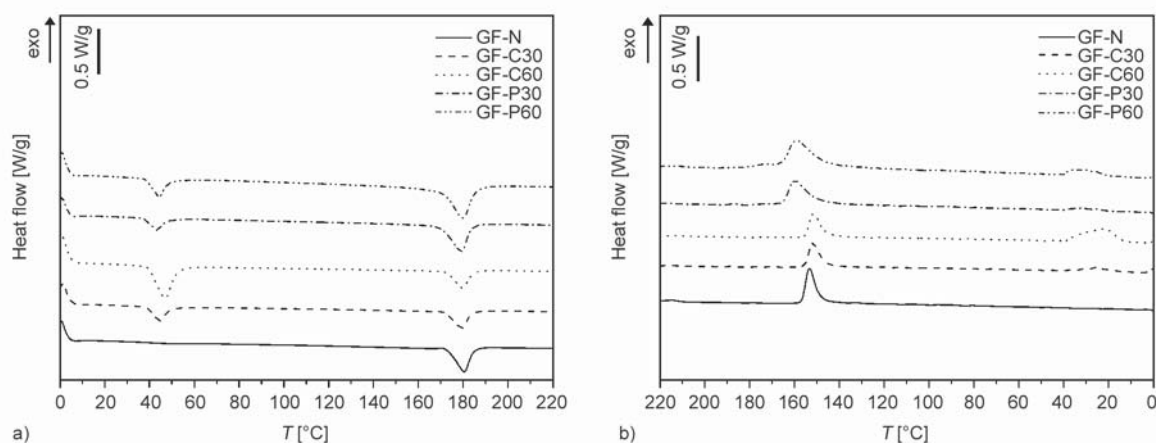
Sample	ϕ_f [vol%]	ϕ_m [vol%]	ϕ_v [vol%]
GF-N	53.4	44.5	2.1
GF-C30	55.5	42.2	2.3
GF-C60	53.2	44.3	2.5
GF-P30	50.5	47.7	1.8
GF-P60	32.4	57.8	9.8

 ϕ_f fiber volume fraction [vol%] ϕ_m matrix volume fraction [vol%] ϕ_v voids volume fraction [vol%]

volume fraction is considerably higher (9.8 vol%), in accordance with the optical microscope results, and the fiber volume content is noticeably lower (i.e. 32.7 vol%). This does not allow a proper comparison of this sample with the others.

Figure 6 shows the DSC thermograms relative to the first heating and the cooling scan of the prepared laminates, respectively. In Figure 6b, the temperature

axis decreases from 220 to 0 °C to better present the cooling scan results. The most important DSC results are summarized in Table 7. As for the matrices (see Section 3.1), the data of the second heating scan are not reported for the sake of brevity, as no important differences were detected between the first and the second heating scan. The aim of this analysis was to investigate if the additional hot pressing thermal cycle required to produce laminates further deteriorates the PCM energy storage/release capability. As observed for the matrices, in the heating scan (Figure 6a) two endothermic peaks are present, which are associated to the melting of the PCM and of the PA12, respectively. As reported in Table 7, the composite with the best thermal performance is GF-C60, developing a melting enthalpy of 17.1 J/g ($\Delta H_m^{\text{rel}} = 53\%$). However, the values of relative enthalpies are lower than those of the corresponding matrices, which indicates that the lamination process further decreases the thermal energy storage/release capability,

**Figure 6.** DCS thermograms of the prepared laminates. (a) first heating scan; (b) cooling scan.**Table 7.** Results of the DSC tests on the prepared laminates

Sample	T_m [°C]	ΔH_m [J/g]	ΔH_m^{rel} [%]	T_m^{PA} [°C]	ΔH_m^{PA} [J/g]	T_c [°C]	ΔH_c [J/g]	T_c^{PA} [°C]	ΔH_c^{PA} [J/g]
GF-N	—	—	—	179.9	11.5	—	—	154.2	11.4
GF-C30	43.9	6.5	44.2	178.8	8.7	25.2	3.1	152.4	8.3
GF-C60	46.3	17.1	52.7	178.9	8.5	23.2	13.8	152.4	8.0
GF-P30	43.0	5.3	31.9	178.5	16.2	39.7	2.0	160.3	16.1
GF-P60	43.5	8.4	15.8	178.7	21.0	31.3	5.6	160.1	21.0

 T_m melting temperature of the PCM [°C] ΔH_m PCM melting enthalpy [J/g] ΔH_m^{rel} relative PCM melting enthalpy [%] T_m^{PA} melting temperature of PA12 [°C] ΔH_m^{PA} melting enthalpy of PA12 [J/g] T_c crystallization temperature of the PCM [°C] ΔH_c PCM crystallization enthalpy [J/g] T_c^{PA} crystallization temperature of PA12 [°C] ΔH_c^{PA} crystallization enthalpy of PA12 [J/g]

causing additional breaking of capsules and degradation of paraffin. Further efforts will be made in the future to prevent microcapsule damage and improve the thermal energy storage/release properties of the prepared composites. The composites with ParCNT present a much greater decrease of relative melting enthalpy respect to the matrices, and the values of ΔH_m^{rel} are not even proportional to the ParCNT fraction. This suggests that, during the process, the ParCNT degrades more than the microencapsulated PCM, which is in good agreement with the TGA results (see Figure 3). This suggests that, considering the processing conditions, the microcapsules can be more easily incorporated in a glass fiber/PA12 laminate. As already observed in the matrices (see Table 3) the crystallization temperature of PA12 matrix is increased of about 5 °C in the ParCNT based laminates, because of the nucleating effect played by CNTs in the matrix.

Finally, the mechanical properties of the laminates were evaluated through tensile tests and short beam shear tests. Figure 7 shows representative stress-strain curves of the tensile tests on the prepared laminates, while the most important results are summarized in Table 8. The stress at break decreases upon PCM addition, and this effect is more evident for the laminates with ParCNT, in which also the elastic modulus decreases compared to the laminate without PCM (GF-N). Conversely, the elastic moduli of both laminates with capsules are not significantly different from that of GF-N, indicating that in these laminates the stiffness is determined essentially by the elastic properties of the reinforcement, and the matrix properly fulfils the role of transferring the load to the

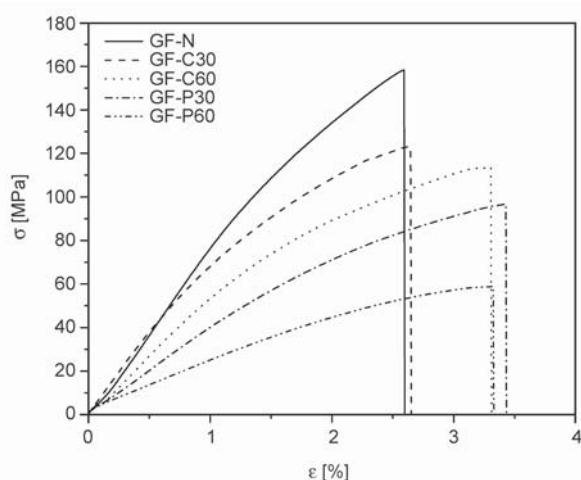


Figure 7. Representative stress-strain curves obtained during quasi static tensile tests on the prepared laminates

Table 8. Results of the quasi static tensile tests and short beam shear tests on the prepared laminates

Sample	E [GPa]	σ_B [MPa]	ε_B [%]	$ILSS$ [MPa]
GF-N	13.1±0.3	160±29	2.7±0.3	11.2±1.7
GF-C30	12.7±0.9	124±18	3.0±0.4	9.8±1.7
GF-C60	13.3±0.7	114±10	3.0±0.7	9.4±2.1
GF-P30	9.9±0.4	92±9	3.5±0.1	6.7±0.3
GF-P60	6.5±0.1	56±15	3.5±1.1	5.5±1.8

fibers. Additionally, also the strain at break values are not negatively affected by the PCM addition, and thus it can be concluded that the mechanical properties of the resulting laminates are only marginally influenced by microcapsules addition within the materials, while a sensible drop of the mechanical performances can be observed with ParCNT addition.

As mentioned before, the interlaminar properties of the laminates were investigated through a short beam shear test. Values of interlaminar shear strength ($ILSS$) are reported in Table 8. Once again, if the standard deviations are considered, the laminates with capsules do not show a significantly different performance with respect to the laminate without PCM (GF-N), while the interlaminar properties of the laminates with ParCNT sharply decrease, proportionally to the PCM concentration. This can be attributed to the poor adhesion, as a result of the high viscosity of the matrices involved, and to the lower mechanical properties of the matrices with ParCNT.

4. Conclusions

In this work, glass fiber reinforced thermoplastic composite laminates with thermal energy storage/release capability were prepared by combining a PA12 matrix with two different paraffin based PCMs (microcapsules and ParCNT), and the physical properties of the resulting materials were thoroughly characterized.

MFI tests on the matrices showed that the fluidity of the PA12 decreased with an increase of the PCM content. For the system with ParCNT this decrease was more evident than for the systems with microcapsules, which suggests that the latter could be processed more easily. DSC analysis revealed that, for the systems with capsules, the melting enthalpy increased with the PCM content. These systems developed a melting enthalpy which was approximately 70% of the expected one, and the enthalpy loss was attributed to the breaking of some capsules and the

leakage/degradation of the PCM. The drop of the melting/crystallization enthalpy was heavier for the systems with ParCNT, due to a greater paraffin degradation and leakage during the production process, as a consequence of the lower thermal stability of ParCNT compared to the capsules. For both systems, the Vicat softening temperature was almost not affected by the presence of the PCMs, nor did the PCM melting determine a loss in the dimensional stability. Quasi static tensile tests showed that the mechanical properties of the blends were lower than those of the neat PA12, probably because of the lower mechanical properties of the PCM and/or the not perfect adhesion with PA12. Only a slight increase of elastic modulus at elevated ParCNT concentrations was observed, due to the considerable percentage of CNTs, but the modulus was always lower than that of the neat PA12.

The subsequent characterization of the laminates highlighted that the fiber and void volume fractions were comparable for all the laminates except for that with the higher amount of ParCNT, where the high viscosity of the matrix led to a lower fiber volume fraction and a higher void content. DSC tests showed that the relative enthalpy values of the laminates were lower than those of the corresponding matrices, which indicates that the lamination process probably determined a further breaking of capsules and degradation of paraffin. The mechanical properties of the laminates were only slightly impaired by microcapsules addition, while a more sensible drop of the elastic modulus, of the stress at break and of the interlaminar shear strength could be observed in the systems with ParCNT.

The results of this work indicated that the microencapsulated PCM was more suitable to produce structural TES composites in combination with a PA12 matrix and glass fibers, since it showed a greater thermal stability and did not impair the mechanical properties of the laminates. The performed experiments are a good starting point for the design and fabrication of thermoplastic composites with TES capability, and further efforts will be made to improve the processing conditions and limit damage of microcapsules, thus increasing the thermal energy storage/release properties of the prepared composites.

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