

# A study on the effects of graphene nano-platelets (GnPs) sheet sizes from a few to hundred microns on the thermal, mechanical, and electrical properties of polypropylene (PP)/GnPs composites

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**Abstract.** Polypropylene (PP) is incorporated with four different grades (H100, M25, M5, and C300) of graphene nano-platelets (GnPs) via twin screw extrusion followed by injection moulding. The composites' thermal stability, crystallization behaviour, tensile strength, and electrical property are carefully examined. The thermal stability is significantly enhanced with the incorporation of small-sized GnPs as shown by the 11.2% improvement in  $T_{5\%}$  (the temperature at which 5 wt% of the mass loss occurs) and 5.1% improvement in  $T_{\max}$  (the temperature at which the maximum loss rate occurs). The thermal stabilizing effect of fillers can be significantly enhanced when they are well distributed with less aggregation as is the case for small-sized GnPs. The GnPs show a considerable nucleating effect on PP by increasing the crystallization temperature ( $T_c$ ). The greatest improvement in tensile property is achieved with the use of small-sized GnPs. A 33.0% enhancement in tensile strength and 59.1% improvement of tensile modulus are obtained with the use of C300 and M5, respectively. The significantly increased thermal stability and mechanical property with small-sized GnPs are due to the fact that these small-sized fillers achieve a high degree of dispersion with less agglomeration as shown in the scanning electron microscope (SEM) images. However, the fillers with a large sheet size are still beneficial for purposes concerning electrical conductivity since the lowest percolation is obtained with H100. The greater the size of the GnPs, the smaller the percolation threshold of composites is exhibited.

**Keywords:** polymer composites, polypropylene, graphene nano-platelets, electrical conductivity, tensile property

## 1. Introduction

Graphene is a single layer of carbon atoms packed in a honeycomb structure [1]. Upon the discovery of free standing graphene in 2004, a revolutionary amount of research has been conducted to fully exploit the exceptional properties of graphene [2–9]. However, it has been considered extremely challenging to commercialize advanced products fabricated with graphene due to inability in mass production of high-quality graphene at low cost. Recently, graphene nano-platelets (GnPs) have been recognized as an

inexpensive alternative to graphene due to its possibility of mass production at low cost [10, 11]. GnPs are layered graphene nano-crystals in the structure of platelets stacked by van der Waal's forces [12]. The incorporation of GnPs into conventional polyolefins has promising potential in a vast array of applications due to its excellent thermal, mechanical, and electrical properties. Such composites can be employed in the fields of electronics, automobile, aerospace, sensors, and many more [13, 14]. Among many polymers, polypropylene (PP) is one of the

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most widely used thermoplastics owing to its great physical and mechanical properties, chemical resistance, recyclability, high processability, and low cost [15]. The field of applications for PP includes packaging, textiles (ropes and carpets), automotive components, etc. [16].

Due to the high potential of the PP composites incorporated with GnPs, researchers have extensively studied the various properties of the composites [17–20]. It was revealed that the performance of the composites is highly dependent upon the physical characteristics of GnPs. For example, Liang *et al.* [17] showed that the tensile modulus of neat PP (1.25 GPa) was 100% improved and reached up to 2.5 GPa with the use of GnPs with diameters less than 10 microns and thickness smaller than 5 nm. However, less reinforcement was achieved (tensile modulus reached 1.9 GPa) when greater-sized GnPs (with a diameter between 10 and 50 microns and thickness between 3.4 and 7 nm) was employed. Kalaitzidou *et al.* [21] revealed that neat PP with initial flexural modulus of ~1.2 GPa reached a flexural modulus of 9 GPa with the addition of 20 vol% GnPs with a diameter of 1  $\mu\text{m}$  whereas 5 GPa was obtained when 5  $\mu\text{m}$  diameter GnPs were used. Chunhui *et al.* [22] also revealed that the flexural strength is inversely proportional to the size of graphite. The incorporation of GnPs also significantly influences the thermal properties of polymeric materials. For instance, Bafana *et al.* [23] demonstrated that the addition of 1.5 wt% of GnPs increased  $T_{10\%}$  (temperature for 10% weight loss) by 29 °C. The crystallization behaviour of polymer matrix is also influenced when GnPs are present. For example, Pedrazzoli *et al.* [24] showed that the crystallization rate of the PP/GnPs was increased by 380% with an amount of 0.01 wt% of GnPs during isothermal crystallization at 145 °C. They also reported that the growth of  $\beta$ -crystals of PP was promoted up to 11% with an amount of 1 wt% of GnPs. However, the studies that compare and reveal the relation between the GnPs sheet size and thermal properties are rather sparse. Moreover, the percolation threshold of PP/GnPs composites is also closely associated with the sheet size of GnPs. Park *et al.* [25] showed that the exfoliated graphite nanoplatelets with sheet size of 1 micron gave a percolation threshold of 15 wt%. It was also reported that the use of GnPs with 5 and 10  $\mu\text{m}$  in the diameter exhibited a percolation threshold of 6 and 4 vol%, respectively [26].

As described above, when GnPs are incorporated, a variety of properties are improved, and this improvement is significantly dependent upon the sheet size of GnPs. Therefore, the size of GnPs should be carefully chosen to maximize the performance. For instance, relatively small sized GnPs should be incorporated when lightweight GnPs-reinforced composites are considered for automotive parts for an improved fuel economy in the future. GnPs can also be utilized for high barrier performance packaging materials for chemical, solvent, and fuel containers. For safety issues, relatively large sized GnPs can be used to improve electrical conductivity for prevention of electrostatic discharge. Therefore, it is essential to understand the effects of the GnPs' physical properties on the performance of the composites from a manufacturing point of view when the composites are fabricated via conventional industrial machines. However, few studies systematically investigate the influences of a wide range of the GnPs' sheet size spanning from a few to hundreds of microns on the various properties of the composites. Hence the objectives of this study were to investigate the effects of physical property of GnPs on the thermal stability, crystallization behaviour of PP, tensile strength, and electrical conductivity of PP/GnPs composites. The size of the GnPs used in this study spanned from a few microns to several hundred microns in diameter. Several physical properties, such as the number of particles per unit volume and surface area, vary with the GnPs' sheet size and therefore will also be considered when discussing various properties of the composites.

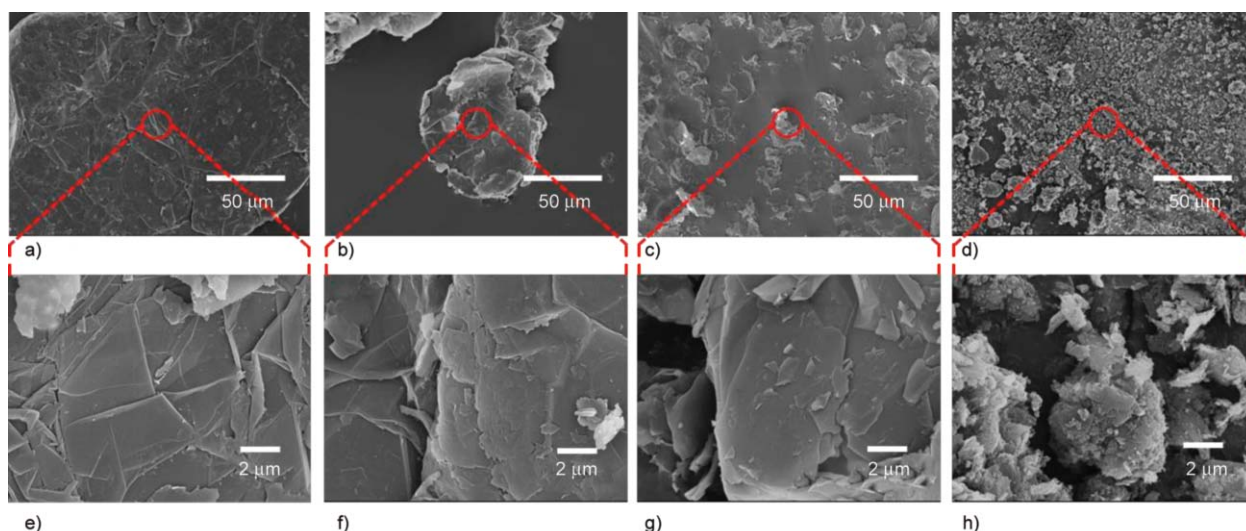
## 2. Materials and methods

### 2.1. Materials

PP (HM20/70P) was obtained from Goonvean Fibres Ltd. and used as received. The average size of this powder type PP for this grade falls in a range of 0.055 to 0.077 mm with a density of 0.90 to 0.91 g/cm<sup>3</sup>. The melt flow index was measured to be 19.4 g/10 min at 230 °C and 2.16 kg (D4002, Dynisco Polymer Test

**Table 1.** Dimensions and physical properties of GnPs used in this study. These values were provided in the technical sheet from XG science.

Grades of GnPs		H100	M25	M5	C300
Diameter	[ $\mu\text{m}$ ]	>150	>25	>5	>2
Thickness	[nm]	~15	~6–8	~6–8	~5
Surface area	[m <sup>2</sup> /g]	50–80	120–150	120–150	~300



**Figure 1.** The SEM images of GnPs for each grade: (a and e) H100, (b and f) M25, (c and g) M5, and (d and h) C300.

Systems). Three different grades (Grade M, C, and H) of GnPs and two different sizes of grade M (5 and 25  $\mu\text{m}$ ) were purchased from XG Science. The dimensions and physical properties of GnPs were determined and detailed in Table 1. The SEM images of each grade of the GnPs are provided in Figure 1.

## 2.2. Composites preparation

PP was compounded with grade M25, M5, and C300 GnPs with desired mass fractions ranging from 5 to 20 wt%. The mass fraction was converted to volume fraction, and the compositions of all the samples are summarized in Table 2. The data for PP composites with H100 was reproduced from our previous study [27]. Both PP and GnPs were suspended in ethanol and mechanically stirred for an improved dispersion. The mixture was dried in a vacuum oven at 60 °C for 24 hours and fed into the counter-rotating conical micro-compounder (Ruiming, SJZS-07A). The temperature setting from the hopper to the die was 165/ 170/175/185. The mixture of PP and GnPs was circulated for 5 min and extruded. The screw speed was 24 rpm. The compounded strands were pelletized by a pelletizing machine and desiccated again at 60 °C for 12 hours to avoid moisture inclusion. The dried and pelletized extrudates were then added into an injection moulding machine.

## 2.3. Characterizations

### 2.3.1. Thermal behaviour and stability

The thermal behaviour of the PP/GnPs composites were examined by means of differential scanning calorimeter (DSC) using a thermal analyser (TA

**Table 2.** Summary of composite compositions and corresponding volume percent.

Filler		PP	
[wt%]	[vol%]	[wt%]	[vol%]
<b>H100</b>			
0.0	0.0	100.0	100.0
3.0	1.3	97.0	98.7
7.5	3.2	92.5	96.8
10.0	4.4	90.0	95.6
20.0	9.3	80.0	90.7
<b>M25</b>			
5.0	2.1	95.0	97.8
10.0	4.4	90.0	95.6
15.0	6.7	85.0	93.3
20.0	9.3	80.0	90.7
<b>M5</b>			
5.0	2.1	95.0	97.8
10.0	4.4	90.0	95.6
15.0	6.7	85.0	93.3
20.0	9.3	80.0	90.7
<b>C300</b>			
5.0	2.1	95.0	97.8
10.0	4.4	90.0	95.6
15.0	6.7	85.0	93.3
20.0	9.3	80.0	90.7

Q2000, USA). The samples were scanned from –30 to 250 °C under nitrogen atmosphere with ramping rates of 10 °C/minute. The specimens were treated at 250 °C for 3 minutes to eliminate the thermal history. The thermal stability was studied by means of thermogravimetric analysis (TGA) using a thermal analyser (TA Q500, USA). The samples were treated from 20 to 800 °C with a heating rate of 10 °C/minute under a nitrogen condition.

### 2.3.2. Structural and morphological measurements

The structural analysis of PP/GnPs composites were conducted by means of X-ray diffraction (XRD) using Rigaku Miniflex (Cu-K $\alpha$  radiation,  $\lambda = 1.54184$  Å). The morphology of the composites was investigated by a scanning electron microscope (SEM) (Zeiss Leo 1550).

### 2.3.3. Tensile strength measurement

Dog bone tensile specimens were prepared by our injection moulding machine, and each specimen had a length of 75 mm, a thickness of 2 mm, and a parallel length of 30 mm. Five samples were tested on a universal testing machine (4.4 kN, eXpert 7603, ADMET, USA) with a cross-head speed of 5 mm/minute at an ambient atmosphere in accordance to ASTM D638-14.

### 2.3.4. Electrical conductivity measurement

In-plane electrical conductivity ( $\sigma_I$ ) was measured by a four-point probe method. Specimens were trimmed into dimensions of 15 mm $\times$ 10 mm $\times$ 2 mm, and the polymer-rich surface was removed prior to measurement. The in-plane conductivity was calculated by Equation (1):

$$\sigma_I = \frac{1}{\rho} = \frac{1}{R \cdot t} = \left( \frac{\ln 2}{\pi \cdot t} \right) \frac{I}{V} [\text{S} \cdot \text{cm}^{-1}] \quad (1)$$

where  $\rho$  is the electrical resistivity,  $R$  is the electrical resistance,  $t$  is the specimen thickness,  $I$  is the applied current, and  $V$  is the detected voltage drop. The four-point measurement setup was described elsewhere [27].

Through-plane conductivity ( $\sigma_T$ ) was measured by placing the specimen in a house-built fixture under

constant pressure. The samples were positioned between copper foil electrodes, and silver paste was employed to minimize the contact resistance between the samples and electrodes. The through-plane electrical conductivity was determined by Equation (2):

$$\sigma_T = \frac{t}{R \cdot A} [\text{S} \cdot \text{cm}^{-1}] \quad (2)$$

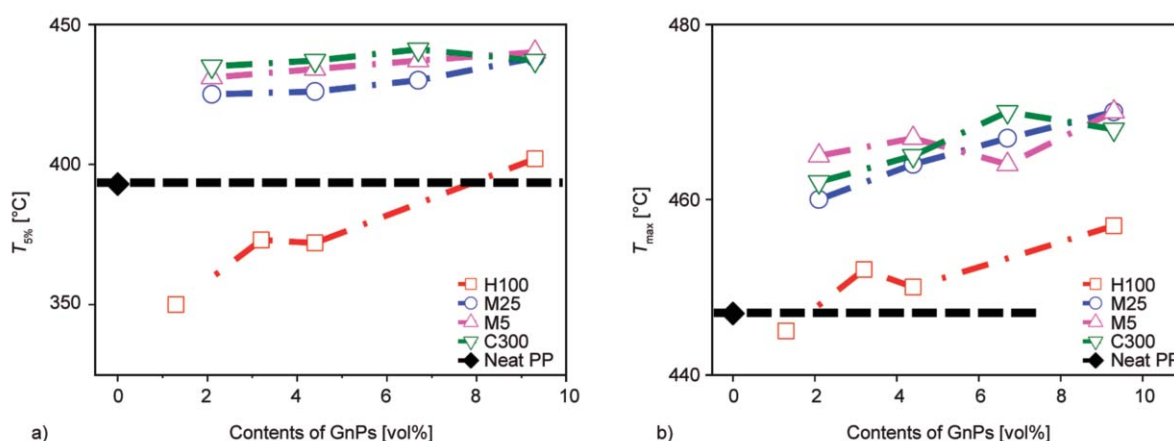
where  $R$  is the electrical resistance,  $t$  is the specimen thickness, and  $A$  is the area of the sample. The schematic representation of through-plane setup was described elsewhere [27].

## 3. Results and discussion

### 3.1. Thermal stability

The thermal stability parameters estimated from TGA are provided in Table 3, and  $T_{5\%}$  (5% weight loss temperature) and  $T_{\max}$  (the maximum mass loss temperature) are shown in Figure 2 with respect to the grade of each GnPs.

Figure 2 illustrates an improved thermal stability as the contents of the GnPs increase within the composite for all the grades. It is evident that the GnPs with a diameter less than 25  $\mu\text{m}$  (M25, M5, and C300) show superior effectiveness when compared to H100. While  $T_{\max}$  is heightened with the addition of any grade of GnPs, the composites incorporated with very large-sized GnPs (H100) exhibited inferior thermal stability at the initial stage of thermal decomposition in comparison to neat PP as indicated by  $T_{5\%}$  (Figure 2a). In general, GnPs are known to improve a thermal stability due to its barrier effect and removal of free-radicals initiating the decomposition of polymers [28, 29]. In addition, the dispersed GnPs sheets allow the thermal conduction and uniform



**Figure 2.** The variations of (a)  $T_{5\%}$  and (b)  $T_{\max}$  with increasing amount of GnPs with respect to each grade.



**Table 3.** Parameters extracted from TGA with respect to GnPs grades and their contents in the composites. The PP/H100 data were adapted from [27] with permission from Elsevier.

	Neat PP	H100				M25				M5				C300			
Contents of GnPs [vol%]	0.0	1.3	3.2	4.4	9.3	2.1	4.4	6.7	9.3	2.1	4.4	6.7	9.3	2.1	4.4	6.7	9.3
Contents of GnPs [wt%]	0.0	3.0	7.5	10.0	20.0	5.0	10.0	15.0	20.0	5.0	10.0	15.0	20.0	5.0	10.0	15.0	20.0
Residual amount [wt%]	0.0	3.1	6.9	9.5	18.9	4.5	10.4	14.2	19.5	4.1	8.5	13.6	19.2	5.9	8.9	14.7	19.3
$T_{5\%}$ [°C]	393	350	373	372	402	425	426	430	438	431	434	437	440	435	437	441	437
$T_{max}$ [°C]	447	445	452	450	457	460	464	467	470	465	467	464	470	462	465	470	468

distribution of heat spread in the polymer matrix, leading to an improved thermal stability. However, the SEM images show that H100 GnPs are highly re-stacked and agglomerated when compared to other small-sized GnPs (Figure 6), and this inferior dispersion of H100 could result in a reduced thermal stability. Since the advanced distribution of fillers within the matrix is achieved with smaller-sized GnPs, a significantly increased thermal stability is observed with these fillers such as M25, M5, and C300.

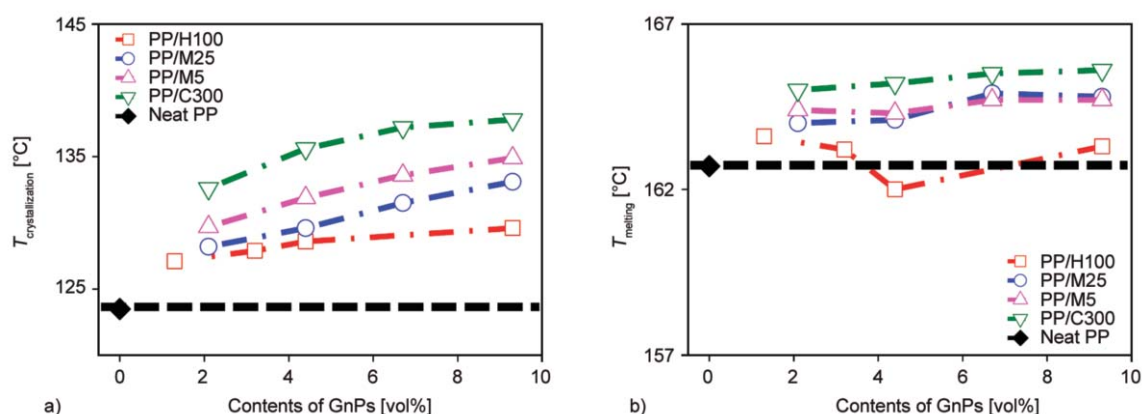
### 3.2. Effect of GnPs on the crystallization of PP

Crystallization ( $T_c$ ) and melting temperatures ( $T_m$ ) of PP composites with each grade of GnPs were measured by means of DSC and described as a function of GnPs contents in Figure 3. The crystallization parameters extracted from DSC are detailed in Table 4.

It is evident that the addition of GnPs considerably increases  $T_c$ , indicating that the GnPs serve as nucleating agents [24]. This nucleating effect is amplified as the size of GnPs decreases.  $T_c$  increased by 14.3 °C with the addition of 9. vol% of C300 whereas the addition of 9.3 vol% H100 only escalates  $T_c$  by 6.1 °C. This is likely due to the well-dispersion and large surface area of C300. Since the GnPs fillers act as seeds for heterogeneous nucleation, crystallization can be facilitated at relatively higher temperatures when larger surface areas are available from small sized GnPs. While the crystallization temperature is largely influenced by addition of GnPs, the degree of crystallinity ( $X_c$ ), calculated by melting enthalpy ( $\Delta H_m$ ) measured from DSC, of the composites was not changed significantly with the addition of any size of GnPs as shown in Table 4.

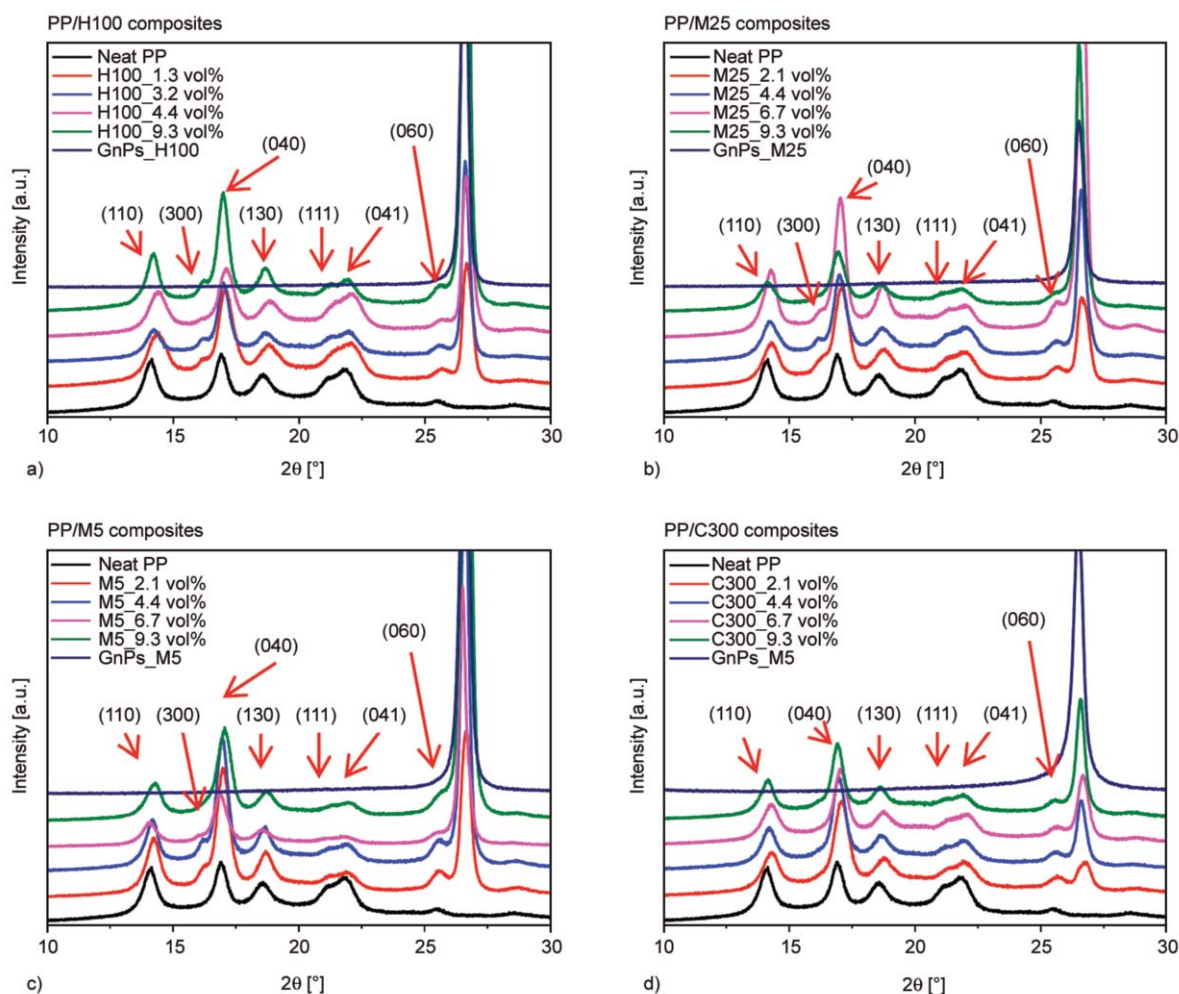
**Table 4.** The crystallization parameters extracted from DSC. The PP/H100 data were adapted from [27] with permission from Elsevier.

	Neat PP	PP/H100 [vol%]				PP/M25 [vol%]				PP/M5 [vol%]				PP/C300 [vol%]			
		1.3	3.2	4.4	9.3	2.1	4.4	6.7	9.3	2.1	4.4	6.7	9.3	2.1	4.4	6.7	9.3
$T_{cry}$ [°C]	123.5	127.1	127.9	128.6	129.6	128.2	129.6	131.5	133.1	129.7	131.9	133.6	134.9	132.6	135.6	137.2	137.8
$T_m$ [°C]	162.7	163.6	163.2	162.0	163.3	164.0	164.1	164.9	164.8	164.4	164.3	164.7	164.7	165.0	165.2	165.5	165.6
$\Delta T$ [°C]	39.2	36.5	35.3	33.4	33.7	35.8	34.5	33.4	31.7	34.8	32.4	31.1	29.8	32.4	29.6	28.3	27.8
$\Delta H_{cry}$ [J·g <sup>-1</sup> ]	171.5	166.6	162.7	150.5	133.5	119.0	115.9	111.1	104.0	124.1	118.9	112.2	105.4	122.9	121.0	109.4	103.6
$\Delta H_m$ [J·g <sup>-1</sup> ]	124.8	122.5	117.3	113.1	100.6	123.1	116.4	112.3	105.7	122.0	116.2	110.7	105.5	122.4	117.8	108.6	103.5
$X_c$ [%]	60	60	60	60	59	62	62	63	63	62	62	62	62	62	62	61	61

**Figure 3.** (a) Crystallization ( $T_c$ ) and (b) melting temperatures ( $T_m$ ) of PP/GnPs composites as a function of GnPs contents.

The degree of crystallinity of neat PP was 60%, and it increased up to 63% with 9.3 vol% of M25 GnPs, and up to 62% with 9.3 vol% of M5 GnPs. This enhancement is rather insignificant considering the amount of fillers incorporated into the PP matrix. Moreover, unlike the  $T_c$ ,  $T_m$  of composites does not deviate considerably from that of neat PP (Figure 3b). Addition of 9.3 vol% of H100 only increases  $T_m$  by 0.6 °C, and only 2.9 °C rises with 9.3 vol% of C300. The lesser degree of variation in  $T_m$  indicates that the crystal types of PP remain invariant with the addition of all the different grades of the GnPs.  $T_m$  is largely dependent upon the forms of crystals. For instance,  $\alpha$ -crystals show a melting point around ~165 °C and  $\beta$ -crystals around 150–160 °C, respectively [30]. In the XRD analysis below (Figure 4),  $\beta$ -crystals are observed from the composites with H100, M25, and M5, but it can be seen that the amount of  $\beta$ -crystals formed is insignificant and hence does not affect  $T_m$ . The investigation on crystallization of PP by means of XRD illustrates that neat PP exhibits five main

peaks at 14.08, 16.95, 18.5, 21.2, and 21.85°, which are responsible for (110), (040), (130), (111), and (041) of  $\alpha$ -crystals, respectively. Upon addition of GnPs, (040) plane at 16.95° become significantly dominant, and the growth of the (060) plane peak is also observed. Further, the (300) plane of  $\beta$ -crystals also appeared for the composites incorporated with H100, M25, and M5. It should be noted that all the planes that showed significant peak growth with the presence of GnPs are in the general form of (00x) type, which is crystallographically in line with the GnPs (002) plane. It was shown that the GnPs may serve as a nucleation site and the nucleation begins around the GnPs [24, 31]. When this occurs, it is possible that the PP chains can exhibit epitaxial growth on GnPs as  $c$ -axis of GnPs is merged with  $b$ -axis of PP, indicating that (002) plane of GnPs is matched with (040) plane of PP. Similar phenomena were also reported in several other studies [13, 31, 32]. The appearance of  $\beta$ -crystals is not observed with the composites with C300, and this could be due to



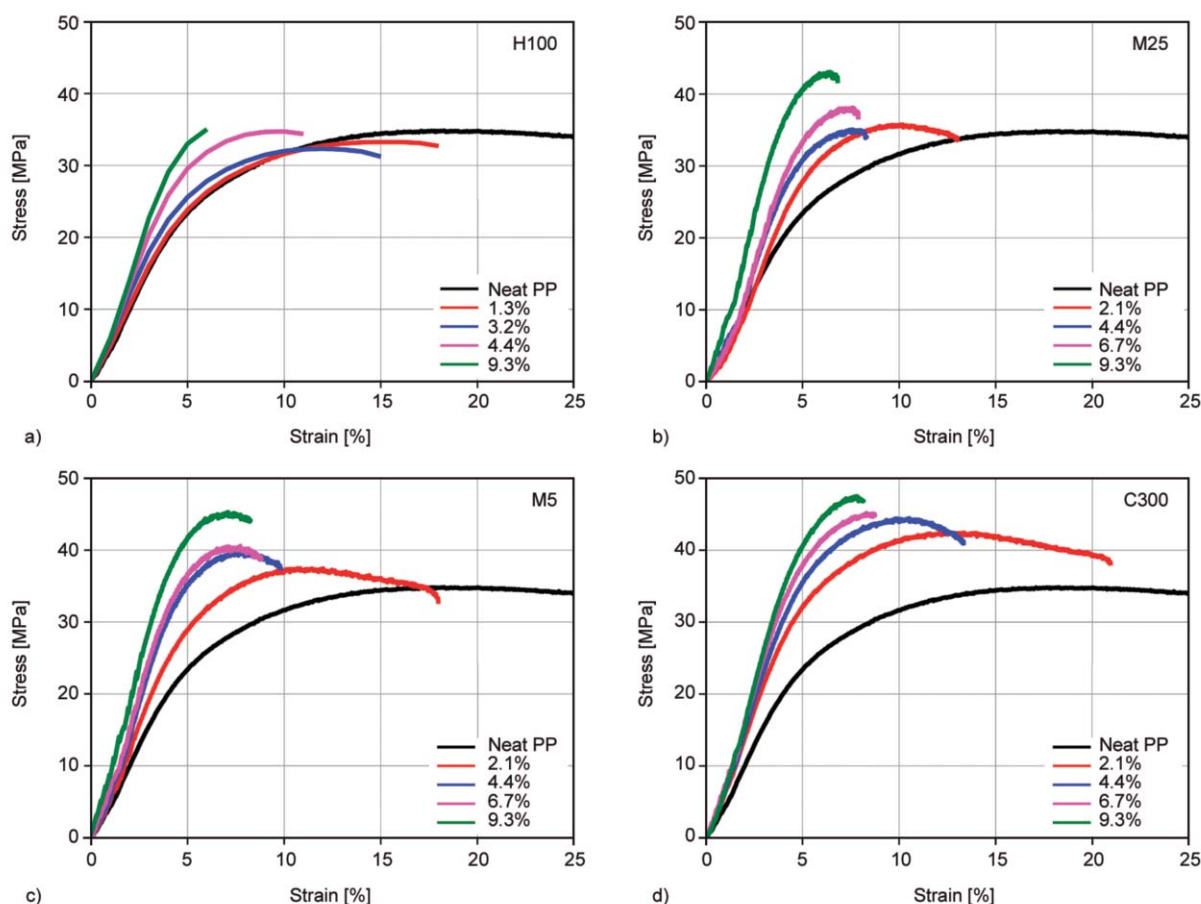
**Figure 4.** XRD curves of neat PP and PP composites compounded with (a) H100, (b) M25, (c) M5, and (d) C300, respectively. Figure 4a is adapted from [25] with permission from.

the saturation effect associated with the small size of C300. When the size of GnPs is small, the greater number of GnPs particles will be present per unit volume when compared to larger-sized GnPs for the same loading. In this case, there might not be enough polymer chains that can orient and align along with all the GnPs particles when a large amount of GnPs within the composite is present. Kalaitzidou *et al.* [31] showed that this saturation occurred with only 1 vol% of GnPs with sheet size of 1  $\mu\text{m}$ . The saturation effect diminishes as the size of GnPs increase, and the particular plane induced by GnPs can be observed with the high contents of GnPs. For example, the (300) plane was observed from PP/M5 composites with 4.4 vol% and PP/M25 composites with 6.7 vol%, respectively, and the (300) plane detected from all the PP/H100 composites with up to 9.3 vol%. This saturation was also observed from PP composites incorporated with carbon nanotubes [33]. It has been known that  $\beta$ -crystals of PP give enhanced impact strength [34]. Since GnPs promote the formation of  $\beta$ -crystals of PP, the impact strength will increase with the addition of GnPs and the highest

impact strength will be obtained at a GnPs' loading that saturates the  $\beta$ -crystal formation. Therefore, the particular GnPs' loading that shows the maximum impact strength will vary with different sizes of GnPs due to the saturation effect. A trend such as this has been observed elsewhere as well [35].

### 3.3. Tensile strength

Tensile strength and the tensile modulus were determined as a function of GnPs contents [vol%] within the composites. The stress-strain curves of all the composites are described in Figure 5 with extracted parameters detailed in Table 5. Overall, tensile strength and modulus were consistently enhanced as the amount of GnPs incorporated increased except for the composites processed with H100. For the PP/H100 composites, the tensile modulus was significantly enhanced while the tensile stress failed to show a considerable improvement. However, both tensile strength and tensile moduli were improved for all the composites incorporated with M25, M5, and C300, respectively. The failure of increasing tensile strength with H100 can be attributed to inferior interfacial



**Figure 5.** The representative stress-strain curves of PP composites incorporated with (a) H100, (b) M25, (c) M5, and (d) C300, respectively.



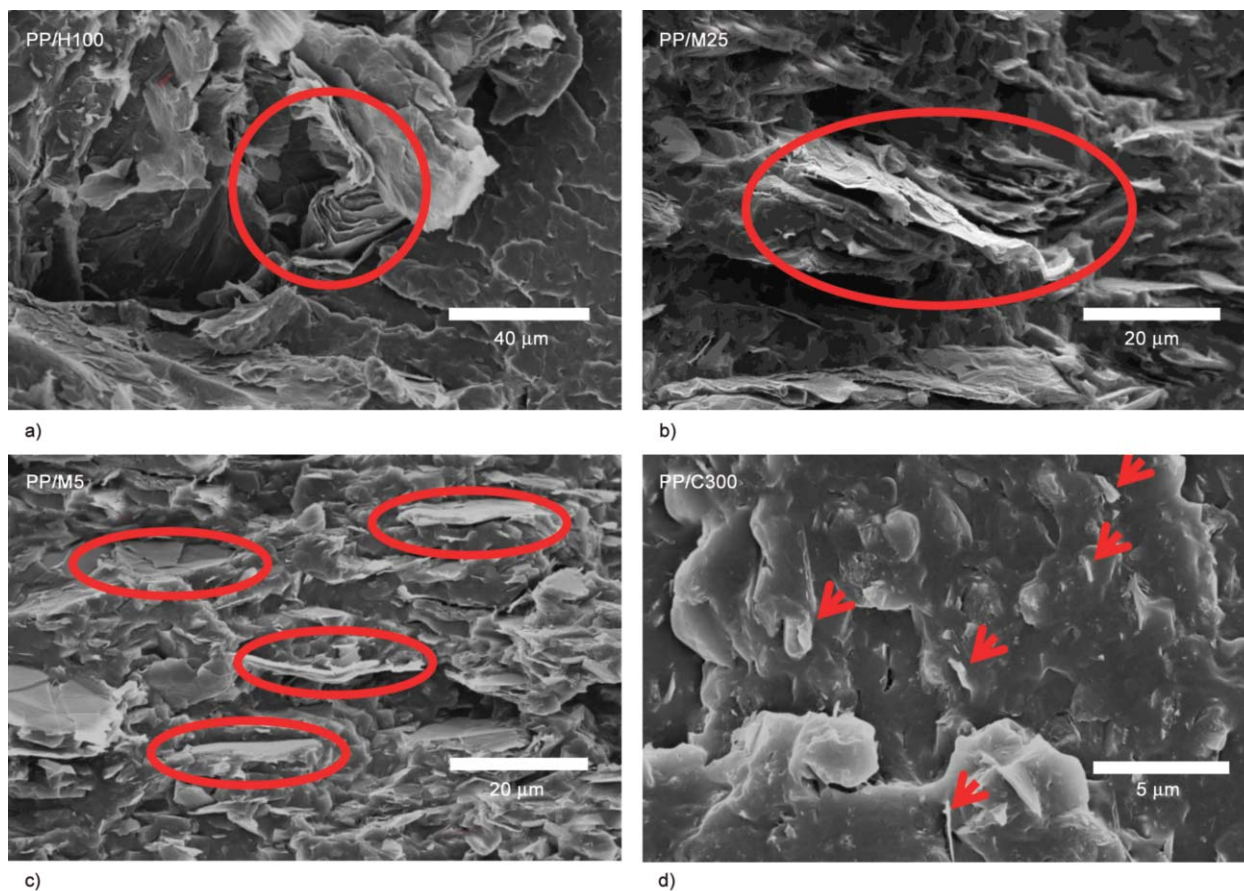
**Table 5.** Tensile parameters extracted from the stress-strain curve with respect to GnPs grades and their contents in the composites.

	Neat PP	H100				M25				M5				C300			
Contents of GnPs [vol%]	0.0	1.3	3.2	4.4	9.3	2.1	4.4	6.7	9.3	2.1	4.4	6.7	9.3	2.1	4.4	6.7	9.3
Tensile strength    [MPa]	34.8±0.4	34.4±0.4	32.5±0.6	34.5±0.9	34.3±1.4	35.7±0.7	35.3±0.6	37.7±1.8	41.6±1.9	37.5±0.4	39.6±1.1	40.2±1.0	43.6±1.7	40.9±1.7	43.8±1.0	45.2±1.6	46.3±0.8
Tensile modulus    [MPa]	514±17	540±17	567±49	610±53	660±35	574±82	563±102	628±145	785±46	615±38	698±32	719±56	817±54	659±35	727±14	742±29	775±18
Elongation at break   [%]	908	17	15	12	7	13	10	9	7	18	10	9	8	21	14	9	8

bonding between the polymer matrix and filler, largely caused by agglomeration, and thereby preventing the composites from achieving high degree of dispersion. Further, the morphology of H100 has been changed from platelets to spherical shapes as seen in Figure 6a, which can also cause adverse influences on reinforcement.

The improvement of tensile strength was most effective with the use of C300 grade of GnPs (Table 6). The smaller the size of the GnPs, the greater the efficiency of reinforcement was obtained. The addition of only 2.1 vol% of C300 resulted in the obtainment

of a tensile strength greater than 40 MPa, which is a 17.5% of improvement from neat PP. Also, a 28.3% enhancement for tensile modulus was observed with the incorporation of 2.1 vol% of C300 (Table 6). It has been reported that a more significant reinforcement can be achieved with a reduced size of GnPs [15], and the mechanical property enhancement is inversely proportional to the size of the filler in many studies [36, 37]. This could be due to increased surface areas that expedite efficient stress transfer between polymer matrix and fillers [38]. An increased surface area of fillers also provides a

**Figure 6.** The SEM images for PP/GnPs composites with (a) H100, (b) M25, (c) M5, and (d) C300, respectively. GnPs are indicated by circles or arrows in red.



**Table 6.** Percentage improvement [%] of tensile strength and tensile modulus of PP/GnPs composites.

GnPs [vol%]	Tensile strength [% improvement]				Tensile modulus [% improvement]			
	H100	M25	M5	C300	H100	M25	M5	C300
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.3	-1.1	—	—	—	5.1	—	—	—
2.1	—	2.6	7.8	17.5	—	11.7	19.6	28.3
3.2	-6.6	—	—	—	10.4	—	—	—
4.4	-0.9	1.4	13.8	25.9	18.7	9.5	35.9	41.5
6.7	—	8.3	15.5	29.9	—	22.2	40.0	44.4
9.3	-1.4	19.5	25.3	33.0	28.4	52.9	59.1	50.9

greater hindrance to crack propagation leading to an improved strength [15]. Moreover, the largest elongation at break for the loading of 2.1 vol% of GnPs was also interestingly obtained with C300. This could be indicative of a greater degree of dispersion and less agglomeration of C300 within the matrix, since affinity between PP and GnPs does not change with GnPs size. In addition, C300 and other grades of GnPs with a small sheet size did not suffer from bending or buckling as seen from Figure 6, which helps boost the reinforcement effects. Therefore, the efficient reinforcement with small-sized fillers can be attributed to the combined effects of better dispersion, less agglomeration, and retention of the original filler morphology within the polymer matrix.

### 3.4. Electrical conductivity

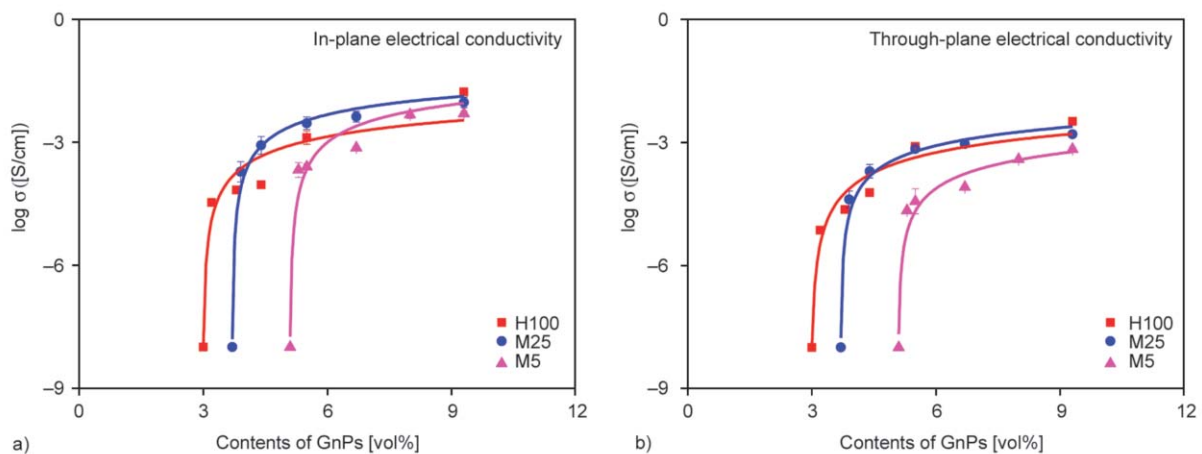
In-plane and through-plane electrical conductivities of each composite were measured and described in Figure 7 and 8. As the amount of GnPs fillers in the composite increases, the composite undergoes an abrupt insulator-conductor transition, and there exists a particular concentration where

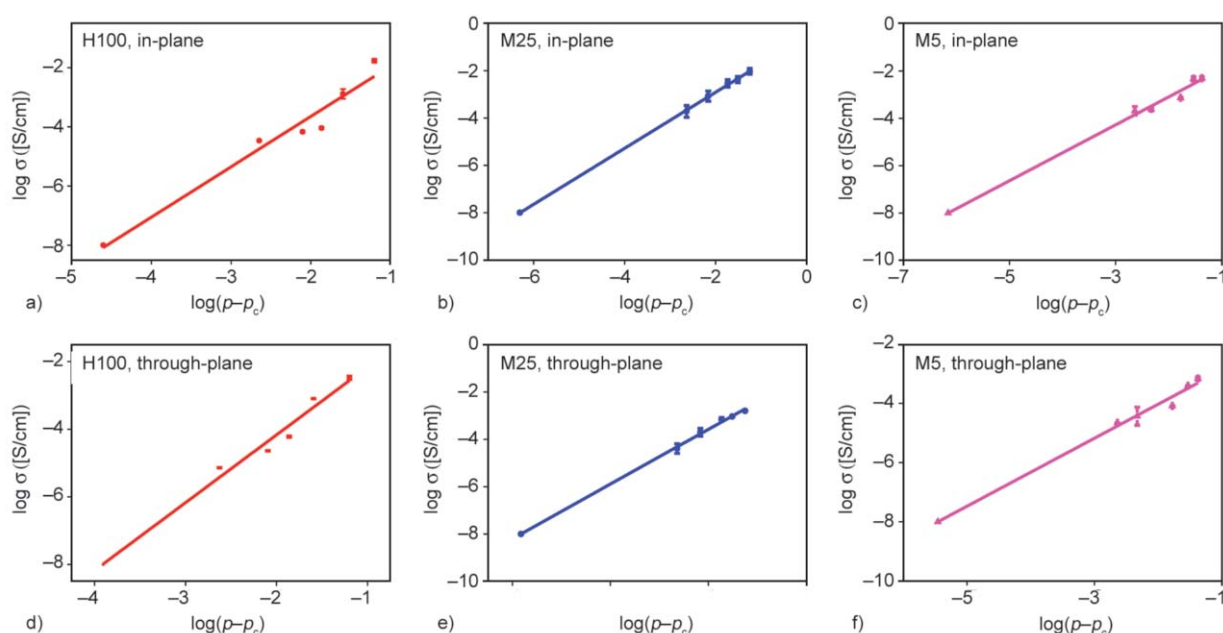
electrical conductivity exhibits a sudden increase. This specific concentration is commonly referred to as the percolation threshold [39]. The percolation threshold can be determined by fitting experimentally observed values to the power law as Equation (3):

$$\sigma \sim (p - p_c)^s \quad (3)$$

where  $\sigma$  is the electrical conductivity of the composite,  $p$  is the volumetric content of filler within composite,  $p_c$  is the particular percolation content, and  $s$  is the critical exponent [39].

The estimated percolation thresholds for the composites with each GnPs grade are detailed in Table 7. It should be noted that the percolation threshold was not determined for the composites with C300 because the C300 composite was still insulating even with 9.29 vol% of loading. A very low percolation threshold is achieved with the use of H100 when compared to other studies where GnPs were used as fillers and processed by conventional melt compounding as shown in Table 7. H100 exhibited the percolation thresholds of 2.99 vol% for in-plane and 2.98 vol% for through-plane conductivity, respectively. In fact, the percolation threshold from H100 was expected to be even lower, but the compromised morphology of fillers may have led to an increased percolation threshold. The percolation threshold for M25 and M5 was 3.66 and 5.05 vol%, respectively. It is clearly observed that the percolation threshold increases as the sheet size of the GnPs reduces, and this trend confirms the well-known relationship between the aspect ratio of fillers and percolation threshold [40]. For the composites to become electrically conductive, the incorporated conducting fillers should

**Figure 7.** The (a) in-plane and (b) through-plane electrical conductivity of PP/GnPs composites with each grade of GnPs as a function of volume concentration of GnPs.



**Figure 8.** The log-log plot of electrical conductivity ( $\sigma$ ) versus  $(p-p_c)$  of in-plane conductivity for (a) H100, (b) M25, and through-plane for (d) H100, (e) M25, (f) M5, respectively.

make contact with one another and construct an interconnected pathway for electrons to travel. Using fillers with a large-sized sheet size, this conductive pathway will be readily formed with low concentration [41]. This is highly beneficial because a great processability and mechanical property can be retained. In order to further reduce percolation threshold, it is desired that the compromising of fillers be minimized by optimizing processing conditions or by employing other techniques that improve dispersion of fillers and introduce less shear force to compounding, such as solid state ball milling as seen in Table 7. Interestingly, while it is usual that a higher conductivity be observed with a large sheet size of fillers at the same loading of fillers, the composites with M25 exhibited higher conductivity at the GnPs loadings

at around 4~5 vol% for both in-plane and through-plane. This could be due to the inferior state of dispersion caused by agglomeration of H100. As it was seen from Figure 6, H100 GnPs are considerably agglomerated, leading to reduction in lateral sheet size and a reduced number of dispersed particles per unit volume. This is very likely to produce a negative influence on the electrical conductivity. Nevertheless, the use of H100 is still beneficial for achieving a low percolation threshold which provides significant advantages for obtaining a great processability from a manufacturing point of view.

#### 4. Conclusions

Four classes of GnPs (H100, M25, M5, and C300) with different physical properties were incorporated

**Table 7.** Comparison of reported percolation thresholds between this study and the literature.

Ref.	Polymer matrix	Filler (diameter in $\mu\text{m}$ )	Percolation threshold		Processing
[26]	Polypropylene	xGnP-5 (5) xGnP-10 (10)	6 vol%	4 vol%	Two roller mixing chamber
[25]	Polypropylene	xGnP-1 (1)	15 wt%		Twin screw extrusion
[42]	PE-LLD	xGnP-15	12 wt%		Solution compounding
[43]	PE-HD	xGnP-15	10–15 vol%	3–5 vol%	Twin screw extrusion Solid State Ball Milling
This study	Polypropylene	xGnP H100 (~150) xGnP M25 (~25) xGnP M5 (~5) xGnP C300 (~2)	<b>In-plane</b> 2.99 vol% 3.66 vol% 5.05 vol% >9.29 vol%	<b>Through-plane</b> 2.98 vol% 3.66 vol% 5.05 vol% >9.29 vol%	Twin screw extrusion

into PP to produce PP/GnPs composites. The composites' thermal stability, the effect of GnPs on the crystallization behaviour of PP, tensile strength, and electrical conductivity were thoroughly studied. The PP composites incorporated with GnPs smaller than 25  $\mu\text{m}$  in diameter exhibited an improved thermal stability as indicated by  $T_{5\%}$  and  $T_{\text{max}}$ . The addition of H100 into PP did not result in an enhanced thermal stability, especially at the initial stages of decomposition. This could be due to ultra large-sized GnPs with a high thermal conductivity that transfers heat across the composite, boosting the thermal decomposition throughout the entire composite simultaneously. The GnPs exert a considerable nucleating effect on the crystallization of PP by increasing  $T_c$  and by inducing particular planes, such as (300), (040), (060), which can be formulated by the epitaxial growth of polymer chains on the GnPs. The  $X_c$  was not significantly increased, however. The greatest efficiency in tensile strength reinforcement was achieved with the use of C300 due to the retention of original morphology and a high degree of dispersion with less agglomeration within the composite. The lowest percolation threshold was obtained when the GnPs with the largest sheet size (H100) was incorporated into a polymer matrix. It was shown from this study that a physical property of GnPs has a significant influence on the performance of the final composites. The GnPs with a smaller sheet size is recommended for the purpose of increasing thermal stability and mechanical strength while high electrical conductivity is readily achieved with large-sized GnPs. To achieve a composite with all-around performances, high dispersion of large-sized GnPs with retained original morphology should be accomplished with improved interfacial interactions.

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