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# Calculation of Demonstration Bulk Vitrification System Melter Inleakage And Off-Gas Generation Rate

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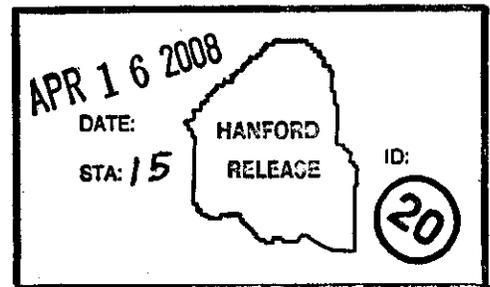
Key Words: DBVS, ICV inleakage, gas generation

**Abstract:** This calculation estimates the DBVS melter inleakage and gas generation rate based on test data. Inleakage is estimated before the melt was initiated, at one point during the melt, and at the end of the melt. Maximum gas generation rate is also estimated.

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**CALCULATION OF DEMONSTRATION BULK VITRIFICATION  
SYSTEM MELTER INLEAKAGE AND OFF-GAS GENERATION RATE**

**T. H. May**  
CH2M-HILL Hanford Group, Inc.

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**Calculation Review Checklist.**

Calculation Reviewed: DBVS Melter Inleakage and Off-Gas Generation Estimate

Scope of Review: Entire  
(e.g., document section or portion of calculation)

Engineer/Analyst: T.H. May *Thomas May* Date: 4/15/08

Organizational Manager: D.H. Shuford Date: \_\_\_\_\_

This document consists of \_\_\_\_\_ pages and the following attachments (if applicable):

- | Yes                                 | No                       | NA*                                 |  |
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| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/>            | 8. Calculations are sufficiently detailed such that a technically qualified person can understand the analysis without requiring outside information.  |
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| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/>            | 10. Limits/criteria/guidelines applied to the analysis results are appropriate and referenced. Limits/criteria/guidelines were checked against references.   |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/>            | 11. Conclusions are consistent with analytical results and applicable limits.  |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/>            | 12. Results and conclusions address all points in the purpose.   |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/>            | 13. Referenced documents are retrievable or otherwise available.   |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/>            | 14. The version or revision of each reference is cited.  |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/>            | 15. The document was prepared in accordance with Attachment A, "Calculation Format and Preparation Instructions."  |
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| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/>            | 17. All checker comments have been dispositioned and the design media matches the calculations.**  |

M.W. Leonard *M.W. Leonard* 4/15/08  
Checker (printed name and signature) Date

\* No software was used in this calculation

\*\* All checker comments have been dispositioned. The test data matches the calculations.

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**CONTENTS**

1.0 OBJECTIVE.....1

2.0 SUMMARY OF RESULTS AND CONCLUSIONS .....1

3.0 BACKGROUND.....1

4.0 INPUT DATA .....2

5.0 ASSUMPTIONS .....2

6.0 METHOD OF ANALYSIS .....2

    6.1 INLEAKAGE CALCULATION BEFORE THE MELT .....3

    6.2 INLEAKAGE CALCULATION AT ONE POINT DURING THE MELT .....3

    6.3 INLEAKAGE CALCULATION AT THE END OF THE MELT .....6

    6.4 CALCULATE MAXIMUM OFF-GAS GENERATION RATE .....7

7.0 USE OF COMPUTER SOFTWARE.....9

8.0 RESULTS.....9

9.0 CONCLUSIONS.....10

10.0 REFERENCES.....10

**TABLE OF FIGURES**

6-1 SIMPLIFIED IDMT ICV OGTS FLOWSHEET ..... 3

6-2 ICV INLET AND MELT GAS PLUS INLEAKAGE FLOW 8/14/07 ..... 5

6-3 ICV INLET AND MELT GAS PLUS INLEAKAGE FLOW 8/17/07 ..... 7

6-4 ICV INLET AND MELT GAS PLUS INLEAKAGE FLOW 8/8/07 ..... 9

**APPENDIX**

ICV FLOW AND TEMPERATURE DATA

**LIST OF TERMS**

ACFM	Actual Cubic Feet per Minute
DBVS	Demonstration Bulk Vitrification System
ICV	In-Container Vitrification
OGTS	Off-Gas Treatment System
RPP	River Protection Project
SCFM	Standard Cubic Feet per Minute
SVF	Spreadsheet Verification Form

**TITLE: CALCULATION OF DEMONSTRATION BULK VITRIFICATION SYSTEM MELTER INLEAKAGE AND OFF-GAS GENERATION RATE****ORIGINATOR: T.H. MAY****T.H.M.****DATE: 4/15/08****CHECKER: M.W. LEONARD****M.W.L.****DATE: 4/15/08****ORGANIZATIONAL MANAGER: D.H. SHUFORD****DATE: 4/15/08****1.0 OBJECTIVE**

The River Protection Project (RPP) mission is to safely store, retrieve, treat, immobilize, and dispose of the Hanford Site tank waste. The Demonstration Bulk Vitrification System (DBVS) is a research and development project whose objective is to demonstrate the suitability of Bulk Vitrification treatment technology waste form for disposing of low-activity waste from the Tank Farms.

The objective of this calculation is to determine the DBVS melter inleakage and off-gas generation rate based on full scale testing data from 38D.

**2.0 SUMMARY OF RESULTS AND CONCLUSIONS**

	=	scfm	@	inches water
ICV inleakage before melt	=	250	@	-2.9
ICV inleakage during melt	=	150	@	-1.5
ICV inleakage post melt	=	140	@	-2.0
ICV peak off-gas generation rate	=	290	@	-3.0

**3.0 BACKGROUND**

The Demonstration Bulk Vitrification System is a treatment technology that is currently being used domestically and internationally for radioactive, hazardous, and mixed waste treatment. Bulk Vitrification can be conducted in large containers (e.g., 20 to 30 cubic meters) resulting in waste forms with small surface area to volume ratio, and thereby minimizing the potential for waste form leaching. The melter used to vitrify the waste is also the waste container and is, therefore, disposed with the waste upon completion of treatment.

Bulk Vitrification is performed by mixing the waste with glass-forming materials of appropriate chemical composition in the process vessel. Vitrification is achieved by inserting electrodes into the process vessel and applying electrical power. Additional waste handling considerations are obviated by using the process vessel as the immobilized waste form disposal container.

Full scale testing was performed in 2007 to demonstrate the technology and to determine design inputs such as melter inleakage and off-gas generation rate.

**TITLE: CALCULATION OF DEMONSTRATION BULK VITRIFICATION SYSTEM MELTER  
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Input data used in the calculation was collected during a full scale test called the Integrated Dryer Melt Test also called the 38D test. Off-gas data was recorded by a subcontractor and quoted in the calculation below. Excerpts from the data are attached in Appendix A.

Flow, temperature, and pressure data collected early in the melt is considered to be valid. Later in the melt, instrumentation down stream of the ICV was exposed to dirty and corrosive gases which may have compromised data quality. To ensure validity of the data, where possible, different instrument readings were correlated such as box ICV vacuum and ICV inleakage.

The following input data was used in the calculations.

One 60% dryer batch (initial charge to ICV) = 9776 pounds	SVF-1319
One 20% dryer batch = 3331 pounds	SVF-1319
One 20% dryer batched contains 231 pounds cellulose	SVF-1319
One 20% dryer batch contains 1135# dry simulant	SVF-1319
0.85 # nitrates/nitrites / # dry simulant	SVF-1319
Sufficient cellulose added to react with 75% of the nitrates/nitrites	SVF-1319
1 pound mole of gas at Standard Pressure and Temperature = 378 standard ft <sup>3</sup> at 60 °F	

**5.0 ASSUMPTIONS**

Cellulose reaction:  $2C_6H_{10}O_5 + 8NO_3 \implies 4N_2 + 12 CO_2 + 10 H_2O$

Moles of gas generated per mole of cellulose =  $26 / 2 = 13$  moles

**6.0 METHOD OF ANALYSIS**

Hand calculations were performed to estimate ICV inleakage and off-gas generation rates. Inleakage was estimated before the melt was initiated, at one point during the melt,

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and at the end of the melt. Maximum off-gas generation rates were calculated during the initial phases of the melt when there was the greatest quantity of reactant in the ICV.

**6.1 INLEAKAGE CALCULATION BEFORE THE MELT**

Input data from AMEC log book data from 8/7/07 (see Appendix):

ICV Off-Gas Treatment System (OGTS) was balanced at 10:30

Inlet valve (V-029) was 40% open

S1 (ICV inlet air flow) = 180 acfm

ICV Vacuum was -2.9" water

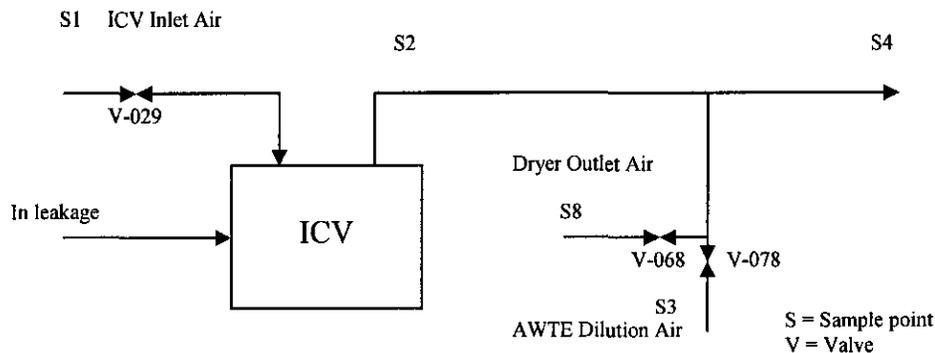
S2 (ICV outlet air flow) = 430 acfm

S3 (see below) = 500 acfm

Inlet valve (V-068) was 20% open

Inlet valve (V-078) was 20% open

S4 (see Figure 6-1 below) = 1280 acfm

**6-1 SIMPLIFIED IDMT ICV OGTS FLOWSHEET****Calculate Inleakage**

$$S2 - S1 = 430 - 180 = 250 \text{ scfm (acfm and scfm are equal at time of balancing)}$$

**6.2 INLEAKAGE CALCULATION AT ONE POINT DURING THE MELT****IDMT Data:**

From 8:09 to 8:39 on 8/14/07 1838# dried product was transferred to the melter at 3% moisture

**TRC Data (see Appendix):**

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From 8:40 to 8:50 on 8/14/07 S1 (ICV Inlet air) = 11 acfm  
 From 8:40 to 8:50 on 8/14/07 S2 (ICV Outlet air) = 300 acfm at 183 °F  
 At 9:11 on 8/14/07 S2 (ICV Outlet air) = 358 acfm at 209 °F (peak)  
 From 8:40 to 8:50 on 8/14/07 S3 (AWTE dilution air) = 340 acfm at 72 °F  
 From 8:40 to 8:50 on 8/14/07, the flow at S8 was 0 acfm.  
 From 8:40 to 8:50 on 8/14/07 S4 (ICV Outlet plus AWTE Dilution air) = 670 acfm  
 ICV Outlet plus AWTE dilution air temperature is not available but is calculated as a mass weighted temperature average as follows:

$$\frac{((358 \times (60 + 459) / (209 + 459)) \times 209 + 340 \times 72) / ((358 \times (60 + 459) / (209 + 459)) + 340)}{= 134 \text{ °F}}$$

**Check flow sum for S2, S3, S8, and S4 to Validate Flow Measurement**

S2 300 acfm X (60 + 459) / (183 + 459) = 240 scfm  
 S3 340 acfm X (60 + 459) / (72 + 459) = 330 scfm  
 S8 0 acfm = 0  
 Sum = 570 scfm  
 S4 670 acfm X (60 + 459) / (134 + 459) = 590 scfm  
 This is a good match and indicates valid flow measurement

**Calculate Steam generation:**

1838 # dried product X 3 wt% moisture = 55 # water

55 # water / 18 #/mole X 378 scf/mole = 1160 scf

**Calculate theoretical gas evolution:**

1838 # dried product X 231 # cellulose per 20% batch / 3331 # dried product per 20% batch = 127 # cellulose (see table "IDMT DRYER TO ICV TRANSFER DATA" contained in appendix)

127 #cellulose / 162#/mole X 13 #moles gas/mole X 378 ft<sup>3</sup>/mole gas = 3870 scf

1838# dried product X (1135 # simulant solids / 3331 # dried product) X 0.85 # nitrates/nitrites per # simulant solids X 0.25 fraction unreacted nitrates/nitrites / 46 #/mole X 378 scf/mole = 1090 scf from unreacted nitrates/nitrites.

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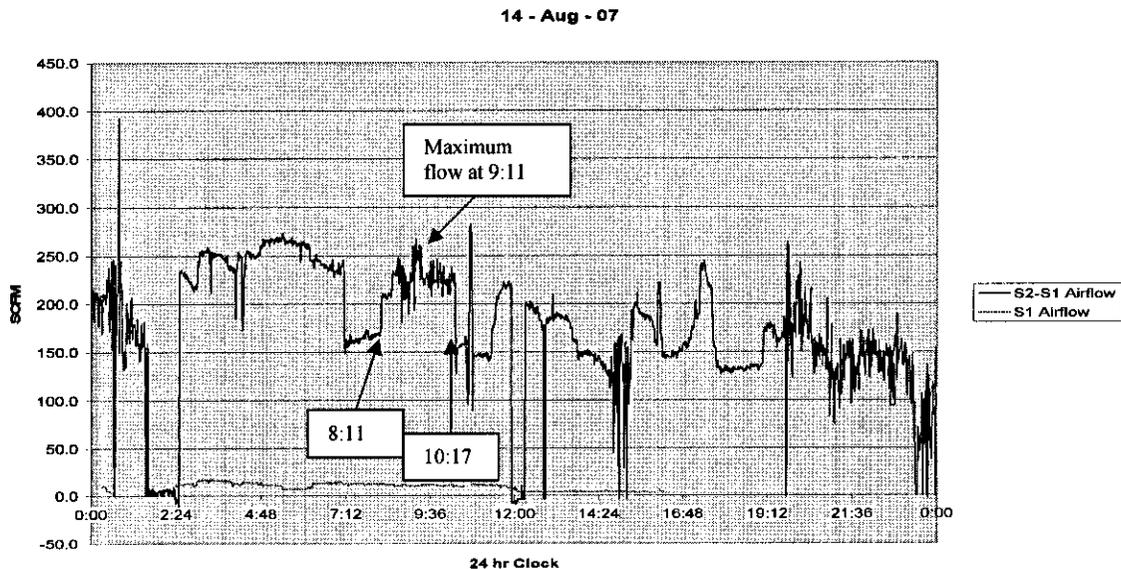
**Total Off-Gas Volume**

1160 scf + 3870 scf + 1090 = 6120 scf

**Off-Gas Evolution Duration**

At 8:40 on 8/14/07, 3525 # dried product was added to melt. Assume that gas evolution begins at 8:40 and continues until ICV outlet flow (minus ICV inlet flow) drops back to the same flow rate as the flow rate at 8:40. From Figure 6-2 below, the flow rate drops back to the same flow at 10:17. This duration is 1 hour and 37 minutes.

**6-2 ICV INLET AND MELT GAS PLUS INLEAKAGE FLOW 8/14/07**



**Calculate Off-Gas Evolution Rate on 8/14/07**

6120 scf X (3525 # dried product / 1838 # dried product) / 97 min = 121 scfm

**Calculate Nominal Difference between ICV inlet flow and outlet flow**

S2 - S1 = 240 scfm - 11 scfm = 230 scfm

**Calculate Nominal Inleakage**

230 scfm - 121 scfm = 109 scfm  $\implies$  round up to 110 scfm nominal

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DATE: 4/15/08  
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**Calculate Peak Difference between ICV inlet flow and outlet flow**

$$S2 - S1 = 358 \text{ acfm} \times (60 + 459) / (209 + 459) - 11 \text{ scfm} = 270 \text{ scfm}$$

**Calculate Peak Inleakage**

$$270 \text{ scfm} - 121 \text{ scfm} = 150 \text{ scfm} @ -1.5 \text{ "water}$$

Peak inleakage on 8/14/07 is lower than that measured during the pre-melt HVAC balancing because the vacuum is only -1.5 "water versus the pre-melt vacuum of -2.9" water.

**6.3 INLEAKAGE CALCULATION AT THE END OF THE MELT**

Feed while melt was terminated at 4:16 and power was turned off to the melt at 6:17 on 8/17/07. Four hours later, the melt gas generation rate is near zero. TRC data available at 10:37 on 8/17/07 indicates an S2 flow rate of 311.9 acfm at 444.7 °F and an S1 flow rate of 38 acfm at 76.2 °F.

$$S2 \text{ flow} = 311.9 \times (60 + 459) / (444.7 + 459) = 179 \text{ scfm}$$

$$S1 \text{ flow} = 38 \times (60 + 459) / (76.2 + 459) = 37 \text{ scfm}$$

$$\text{Difference (inleakage)} = 140 \text{ scfm} @ -2.0 \text{ "water}$$

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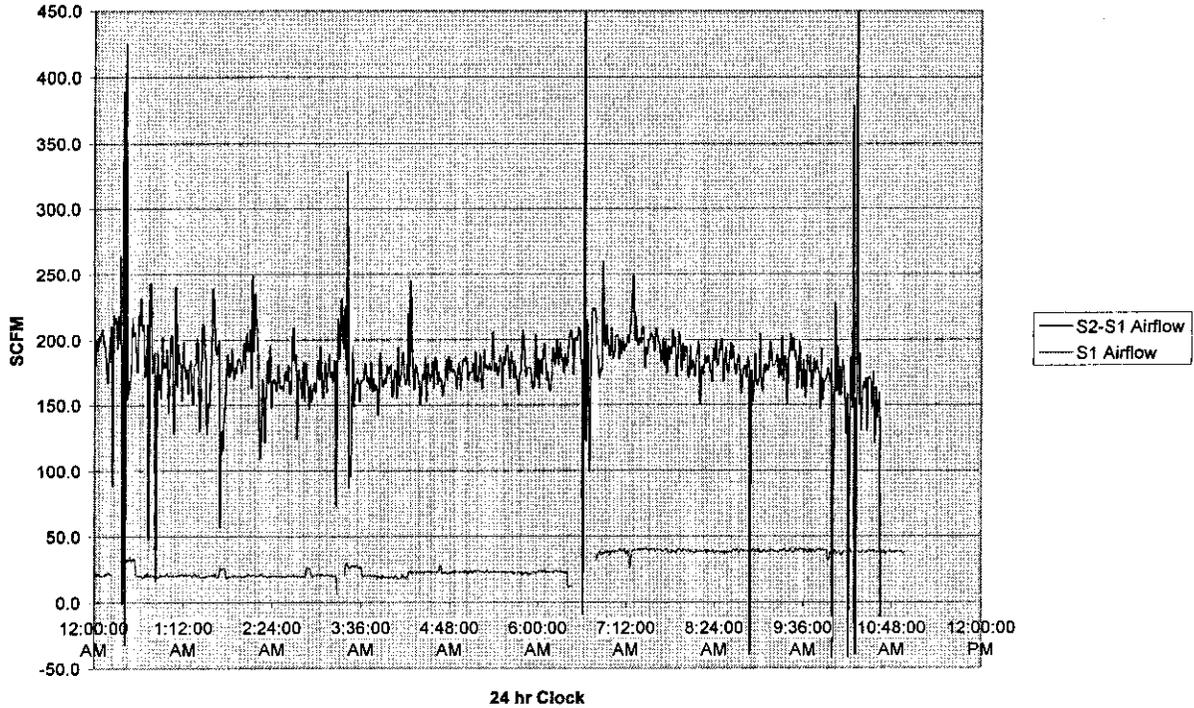
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**6-3 ICV INLET AND MELT GAS PLUS INLEAKAGE FLOW 8/17/07**

17 - Aug - 07



**6.4 CALCULATE MAXIMUM OFF-GAS GENERATION RATE**

The maximum off-gas generation rate occurred during startup of the melt when 9776 # of dried product was contained in the ICV (SVF-1319). As melt off-gas generation rate increased, the box negative pressure decayed to less than -1" water gage at 18:06. As can be seen from the graph of 8/8/07 data below, at 18:06 the ICV air inlet dropped to 0 acfm. This may have been caused by an instrument failure or if the ICV inlet air valve was closed in order to preserve vacuum during the peak generation rate. The ICV off-gas exhaust line was not occluded at this time. Off-Gas generation rates are calculated below for three time periods.

The ICV outlet flow rate (S2) peaked at approximately 16:37 at 847 acfm at 235 °F. S1 flow rate at 16:37 was reported as 160 acfm. Hood vacuum at 16:37 was -2.2" water which is assumed to result in 250 scfm air inleakage similar to the value calculated in section 6.1.

The ICV outlet flow rate (S2) at approximately 22:47 was 823 acfm at 248 °F. S1 flow rate at 22:47 was reported as 0 acfm but this appears to be an instrument problem. It was

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DATE: 4/15/08  
 DATE: 4/15/08  
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assumed that the S1 flow rate was actually 70 cfm. Hood vacuum at 22:47 was -3.0" water which is assumed to result in 250 scfm air inleakage similar to the value calculated in section 6.1.

The ICV outlet flow rate (S2) at approximately 22:14 was 790 acfm at 216 °F. S1 flow rate at 22:14 was reported as 0 acfm but this appears to be an instrument problem. It was assumed that the S1 flow rate was actually 70 cfm. Hood vacuum at 22:14 was -3.0" water which is assumed to result in 250 scfm air inleakage similar to the value calculated in section 6.1.

**Calculate Off-Gas Generation Rate for 16:37**

$$847 \text{ acfm} \times (60 + 459) / (235 + 459) = 633 \text{ scfm S2 flow}$$

$$633 \text{ scfm S2 flow} - 160 \text{ scfm S1 flow} = 473 \text{ scfm S2-S1 flow}$$

$$473 \text{ scfm} - 250 \text{ scfm air inleakage} = 223 \text{ scfm off-gas generation rate}$$

**Calculate Off-Gas Generation Rate for 22:47**

$$823 \text{ acfm} \times (60 + 459) / (248 + 459) = 604 \text{ scfm S2 flow}$$

$$604 \text{ scfm S2 flow} - 70 \text{ scfm S1 flow} = 534 \text{ scfm S2-S1 flow}$$

$$534 \text{ scfm} - 250 \text{ scfm air inleakage} = 284 \text{ scfm off-gas generation rate}$$

**Calculate Off-Gas Generation Rate for 22:14**

$$790 \text{ acfm} \times (60 + 459) / (215 + 459) = 607 \text{ scfm S2 flow}$$

$$607 \text{ scfm S2 flow} - 70 \text{ scfm S1 flow} = 537 \text{ scfm S2-S1 flow}$$

$$537 \text{ scfm} - 250 \text{ scfm air inleakage} = 287 \text{ scfm off-gas generation rate}$$

**Maximum Off-Gas Generation Rate**

Round 287 scfm up to 290 scfm

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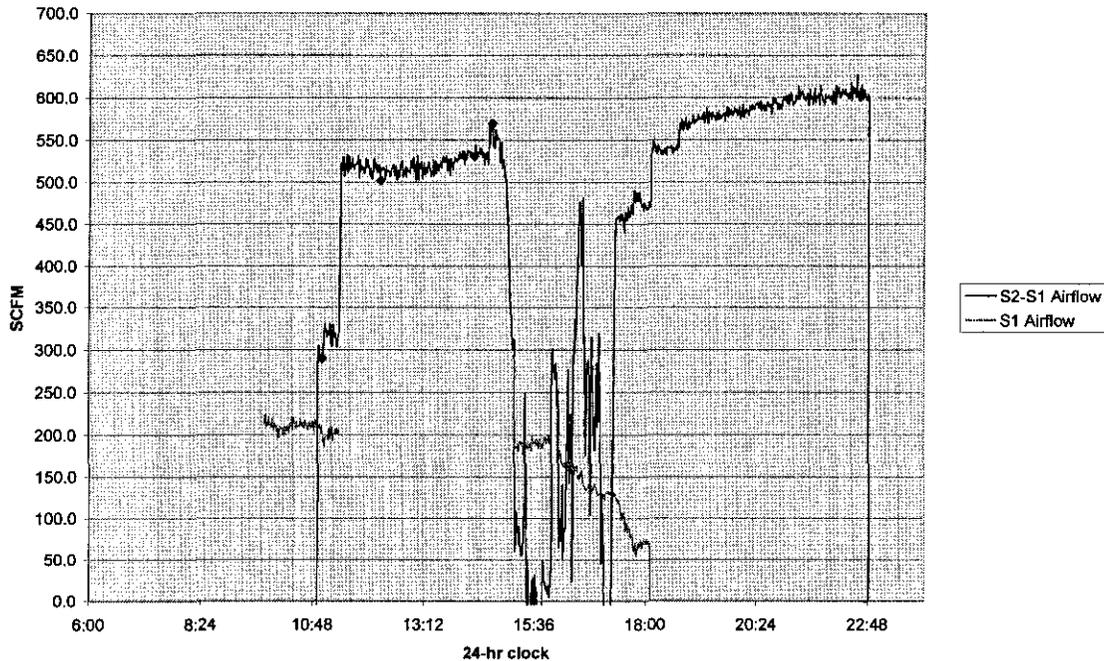
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**6-4 ICV INLET AND MELT GAS PLUS INLEAKAGE FLOW 8/8/07**

8 - Aug - 07



**7.0 USE OF COMPUTER SOFTWARE**

No computer software was used in this calculation.

**8.0 RESULTS**

ICV inleakage before melt	=	scfm		inches water
		250	@	-2.9
ICV inleakage during melt	=	150	@	-1.5
ICV inleakage post melt	=	140	@	-2.0
ICV peak off-gas generation rate	=	290	@	-3.0

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**ORGANIZATIONAL MANAGER: D.H. SHUFORD**DATE: 4/15/08  
DATE: 4/15/08  
DATE: 4/15/08**9.0 CONCLUSIONS**

These results will provide input to DBVS design calculations. There are no conclusions from this calculation.

**10.0 REFERENCES**

SVF-1319, "DBVS 38D Recipe", Rev. 0, CH2M HILL Hanford Group, Inc., Richland, Washington

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**APPENDIX A**

**ICV FLOW AND TEMPERATURE DATA**



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TRC DATA												
Unit 38D - Site 1				Unit 38D - Site 2			Unit 38D - Site 3			Unit 38D - Site 4		
Stack Temp	Stack Gas Velocity	Stack Gas Airflow	Time	Stack Temp	Stack Gas Velocity	Stack Gas Airflow	Inlet Gas Temp	Airflow	Airflow	Inlet Gas Temp	Airflow	
August 14, 2007												
(° F)	(fm)	(acfm)	time	(° F)	(ft/sec)	(acfm)	(° F)	(fpm)	(acfm)	(° F)	(acfm)	time
75.8	53.63	10.5	8:40	181.40	38.84	317.77	71	1240.0	243.5		561.2	8:40
75.4	53.63	10.5	8:41	181.70	38.98	318.87	71	2238.0	439.4		758.3	8:41
75.5	52.09	10.2	8:42	181.84	34.90	285.53	71.36	2252.0	442.2		727.7	8:42
76.0	51.32	10.1	8:43	182.11	38.62	315.93	71	2201.0	432.2		748.1	8:43
76.2	52.09	10.2	8:44	182.51	36.00	294.52	71.36	2130.0	418.2		712.7	8:44
76.0	51.7	10.2	8:45	182.75	35.85	293.34	72.08	2242.0	440.2		733.6	8:45
76.3	50.93	10.0	8:46	182.94	37.55	307.18	71		0.0		307.2	8:46
76.2	50.93	10.0	8:47	183.37	28.88	236.24	72.08	2130.0	418.2		654.5	8:47
76.3	59.42	11.7	8:48	183.81	33.82	276.68	71.72	2163.0	424.7		701.4	8:48
76.5	60.58	11.9	8:49	184.53	38.07	311.49	72.8	2157.0	423.5		735.0	8:49
76.7	59.8	11.7	8:50	185.27	35.23	288.24	72.8	2285.0	448.7		736.9	8:50
76.9	59.42	11.7	8:51	186.25	37.58	307.46	72.8	2157.0	423.5		731.0	8:51
77.1	59.03	11.6	8:52	187.22	32.80	268.32	73.5	2075.0	407.4		675.7	8:52
77.3	57.1	11.2	8:53	188.01	36.72	300.41	73.5	2023.0	397.2		697.6	8:53
77.7	55.95	11.0	8:54	188.87	34.43	281.72	72.8	2141.0	420.4		702.1	8:54
77.8	54.79	10.8	8:55	189.84	33.10	270.82	72.44	2185.0	429.0		699.8	8:55
77.8	53.24	10.5	8:56	190.89	35.29	288.68	73.14	2315.0	454.5		743.2	8:56
77.9	51.7	10.2	8:57	192.05	35.70	292.07	73.5	1913.0	375.6		667.7	8:57
78.1	51.7	10.2	8:58	193.58	31.28	255.92	72.8	1925.0	378.0		633.9	8:58
78.6	51.7	10.2	8:59	194.85	30.78	251.78	73.86	1941.0	381.1		632.9	8:59
78.9	48.61	9.5	9:00	196.00	35.38	289.44	73.5	1799.0	353.2		642.7	9:00
79.4	48.61	9.5	9:01	197.63	37.48	306.66	73.14	1805.0	354.4		661.1	9:01
79.2	54.02	10.6	9:02	199.07	36.16	295.82	74.22	1958.0	384.5		680.3	9:02



**TITLE: CALCULATION OF DEMONSTRATION BULK VITRIFICATION SYSTEM MELTER INLEAKAGE AND OFF-GAS GENERATION RATE**

**ORIGINATOR: T.H. MAY** THM  
**CHECKER: M.W. LEONARD** MWL  
**ORGANIZATIONAL MANAGER: D.H. SHUFORD**

**DATE: 4/15/08**  
**DATE: 4/15/08**  
**DATE: 4/15/08**

TRC DATA												
Unit 38D - Site 1				Unit 38D - Site 2			Unit 38D - Site 3			Unit 38D - Site 4		
Stack Temp	Stack Gas Velocity	Stack Gas Airflow	Time	Stack Temp	Stack Gas Velocity	Stack Gas Airflow	Inlet Gas Temp	Airflow	Airflow	Inlet Gas Temp	Airflow	
August 8, 2007												
Unit 38D - Site 1				Unit 38D - Site 2								
	753.9	148.0	16:31	228.2	90.8	742.7						
	778.5	152.9	16:32	229.5	99.0	809.7						
	744.7	146.2	16:33	230.8	101.1	827.3						
	784.6	154.1	16:34	229.4	100.7	823.8						
	766.2	150.4	16:35	230.4	94.8	775.6						
	803	157.7	16:36	233.8	91.3	747.3						
	773.9	152.0	16:37	235.1	103.5	846.5						
	715.5	140.5	16:38	237.6	86.9	711.1						
	706.3	138.7	16:39	235.5	73.2	598.7						
	698.6	137.2	16:40	235.6	73.7	602.7						
			22:13	214.4	96.9	792.5						
			22:14	215.5	96.6	790.2						
			22:15	216.8	96.3	788.1						
			22:16	218.8	96.5	789.2						
			22:17	219.0	97.5	797.9						
			22:18	220.6	96.6	790.3						
			22:19	220.8	97.0	793.3						
			22:20	221.1	95.9	784.9						
			22:21	221.1	97.0	793.5						
			22:22	220.9	95.9	784.7						
			22:39	236.2	100.8	825.0						
			22:40	238.6	98.2	803.6						

**TITLE: CALCULATION OF DEMONSTRATION BULK VITRIFICATION SYSTEM MELTER INLEAKAGE AND OFF-GAS GENERATION RATE**

ORIGINATOR: T.H. MAY *TMM*  
 CHECKER: M.W. LEONARD *MWL*  
 ORGANIZATIONAL MANAGER: D.H. SHUFORD

DATE: 4/15/08  
 DATE: 4/15/08  
 DATE: 4/15/08

TRC DATA												
Unit 38D - Site 1				Unit 38D - Site 2			Unit 38D - Site 3			Unit 38D - Site 4		
Stack Temp	Stack Gas Velocity	Stack Gas Airflow	Time	Stack Temp	Stack Gas Velocity	Stack Gas Airflow	Inlet Gas Temp	Airflow	Airflow	Inlet Gas Temp	Airflow	
			22:41	241.0	99.5	813.7						
			22:42	241.5	100.5	822.5						
			22:43	241.4	100.2	819.6						
			22:44	241.8	98.8	808.4						
			22:45	242.7	98.9	808.9						
			22:46	244.5	99.0	810.0						
			22:47	247.8	100.6	823.3						
			22:48	248.3	98.9	809.2						

**IDMT DRYER TO ICV TRANSFER DATA**

DATE/TIME	DRYER LOAD CELL WEIGHT	UNITS	NOTES	DRYER RPM	ROTARY VALVE RPM
	58370	#	end simulant feed		
8/14/07 4:09	60900	#	open AOV-013	30	15
8/14/07 4:19	60200	#	close AOV-013		
delta	700	#			
divided by .8	875	#			
		#	end simulant feed		
8/14/07 4:25	60100	#	open AOV-013	30	15
8/14/07 4:35	59450	#	close AOV-013		
delta	650	#			

**TITLE: CALCULATION OF DEMONSTRATION BULK VITRIFICATION SYSTEM MELTER INLEAKAGE AND OFF-GAS GENERATION RATE**

ORIGINATOR: T.H. MAY *THM*  
 CHECKER: M.W. LEONARD *MWL*  
 ORGANIZATIONAL MANAGER: D.H. SHUFORD

DATE: 4/15/08  
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divided by .8	813	#			
		#	end simulant feed		
8/14/07 8:09	58770	#	open AOV-013	30	14
8/14/07 8:21	58000	#	close AOV-013		
delta	770	#			
divided by .8	963	#			
		#	end simulant feed		
8/14/07 8:25	57950	#	open AOV-013	30	13
8/14/07 8:38	57250	#	close AOV-013		
delta	700	#			
divided by .8	875	#			
Total #	3525	#			
Added batch 6-2 to melter					

TITLE: CALCULATION OF DEMONSTRATION BULK VITRIFICATION SYSTEM MELTER INLEAKAGE AND OFF-GAS GENERATION RATE

ORIGINATOR: T.H. MAY TAM

DATE: 4/15/08

CHECKER: M.W. LEONARD MWL

DATE: 4/15/08

ORGANIZATIONAL MANAGER: D.H. SHUFORD

DATE: 4/15/08

Test 38D  
ICV™ Hood Vacuum

