

Report Title: **DEVELOPMENT OF IMPROVED CATALYSTS FOR THE SELECTIVE CATALYTIC REDUCTION OF NITROGEN OXIDES WITH HYDROCARBONS**

Report Type: **ANNUAL** | Reporting Period Start Date: **09/01/2001** End Date: **08/31/2001**

Principal Author(s): **Dr. Ates Akyurtlu**
Dr. Jale F. Akyurtlu

Report Issue Date: **10/05/2001** | DOE Award No.: **DE-FG26-99FT40617**

Submitting Organization: **Hampton University**
Chemical Engineering Department
Hampton, VA 23668

**DEVELOPMENT OF IMPROVED CATALYSTS FOR THE SELECTIVE
CATALYTIC REDUCTION OF NITROGEN OXIDES WITH
HYDROCARBONS**

GRANT AWARD NUMBER: DE-FG26-99FT40617
START DATE: September 1, 1999
EXPECTED COMPLETION DATE: August 31, 2002

PRINCIPAL INVESTIGATOR: Ates Akyurtlu
CO-INVESTIGATOR: Jale F. Akyurtlu

Department of Chemical Engineering
Hampton University
Hampton, VA 23668

Annual Technical
Progress Report
September 2001

DISCLAIMER

“This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.”

ABSTRACT

Significant work has been done by the investigators on the cerium oxide-copper oxide based sorbent/catalysts for the combined removal of sulfur and nitrogen oxides from the flue gases of stationary sources. A relatively wide temperature window was established for the use of alumina-supported cerium oxide-copper oxide mixtures as regenerable sorbents for SO₂ removal. Preliminary evaluation of these sorbents as catalysts for the selective reduction of NO_x gave promising results with ammonia, but indicated low selectivity when methane was used as the reductant. Since the replacement of ammonia by another reductant is commercially very attractive, in this project, four research components will be undertaken.

The investigation of the reaction mechanism, the first component, will help in the selection of promoters to improve the catalytic activity and selectivity of the sorbents in the SCR with methane. This will result in new catalyst formulations (second component). If this research is successful, the combined SO₂-NO_x removal process based on alumina-supported copper oxide-ceria sorbent/catalysts will become very attractive for commercial applications. The objective of the third component of the project is to develop an alternative SCR process using another inexpensive fuel, residual fuel oil, instead of natural gas. This innovative proposal is based on very scant evidence concerning the good performance of coked catalysts in the selective reduction of NO and if proven to work the process will certainly be commercially viable. The fourth component of the project involves our industrial partner TDA Research, and the objective is to evaluate long- term stability and durability of the prepared sorbent/catalysts.

In the second year of the project, the catalysts were investigated for their SCR activity with methane in a microreactor setup and also, by the temperature-programmed desorption (TPD) technique. The results from the SCR experiments indicated that manganese is a more effective promoter than rhodium on the supported copper oxide-ceria catalysts under study; the effectiveness of the promoter increases with the increase in Ce/Cu ratio. The TPD profiles of the unpromoted catalyst (Cu/Ce=3) is different than those promoted with 0.1% rhodium.

TABLE OF CONTENTS

	<u>Page</u>
Disclaimer	iii
Abstract	iii
Executive Summary	1
Work Done	3
I) Background Information	3
II) Experimental Work	5
III) Results and Discussion	9
IV) Conclusions	22
V) Additional Activities	23
Future Plans	23

EXECUTIVE SUMMARY

Significant work has been done by the investigators on the cerium oxide-copper oxide based sorbent/catalysts for the combined removal of sulfur and nitrogen oxides from the flue gases of stationary sources. A relatively wide temperature window was established for the use of alumina-supported cerium oxide-copper oxide mixtures as regenerable sorbents for SO₂ removal. Preliminary evaluation of these sorbents as catalysts for the selective reduction of NO_x gave promising results with ammonia, but indicated low selectivity when methane was used as the reductant. Since the replacement of ammonia by another reductant is commercially very attractive, in this project, four research components will be undertaken:

- Investigation of the adsorption-reaction mechanism for the reduction of NO_x by methane using temperature programmed desorption and temperature programmed reaction studies.
- Improvement of the activity and selectivity of alumina supported cerium oxide-copper oxide-based sorbent catalysts for the reduction of NO_x by methane by the addition of promoters to enhance NO chemisorption, NO oxidation, intermediate stabilization, or methane activation. Alternative catalyst preparation methods will also be tried to enhance metal aluminate formation over the formation of oxide crystals.
- Investigation of the possibility of using inexpensive and widely available residual fuel oils as an alternate reductant to replace ammonia in the SCR reaction.
- Long term testing of the sorbent catalysts in a pilot size setup by TDA Research, our industrial partner.

The investigation of the reaction mechanism will help in the selection of promoters to improve the catalytic activity and selectivity of the sorbents in the SCR with methane. If this research is successful, the combined SO₂-NO_x removal process based on alumina-supported copper oxide-ceria sorbent/catalysts will become very attractive for commercial applications. The objective of the third component of the project is to develop an alternative SCR process using another inexpensive fuel, residual fuel oil, instead of natural gas. This innovative proposal is based on very scant evidence concerning the good performance of coked catalysts in the selective reduction of NO and if proven to work the process will certainly be commercially viable. The fourth component of the project involves our industrial partner TDA Research, and the objective is to evaluate long- term stability and durability of the prepared sorbent/catalysts.

In the second year of the project, the catalysts were investigated for their SCR activity with methane in a microreactor setup and also, by the temperature-programmed desorption (TPD) technique. The results from the SCR experiments indicated that manganese is a more effective promoter than rhodium on the supported copper oxide-ceria catalysts under study; the effectiveness of the promoter increases with the increase in Ce/Cu ratio. The TPD profiles of the unpromoted catalyst (Cu/Ce=3) is different than those promoted with 0.1% rhodium.

WORK DONE

I. Background Information

The sorbents (Table 1) consisting of cerium oxide and copper oxide impregnated on alumina were prepared and characterized during a previous research project funded by DOE (DE-FG22-96PC96216). Their sulfation performance was investigated in a TGA setup, studying mainly the effects of temperature, sorbent composition, metal loading and support type. As a result of the sulfation experiments, a relatively wide temperature window was established for the use of alumina-supported cerium oxide-copper oxide as regenerable sorbents for sulfur dioxide removal. In the 723-823 K temperature range, cerium oxide-copper oxide sorbents have specific sorbent capacities (mass of sulfur removed per unit mass of metal sorbent) and sulfation rates significantly higher than those of cerium oxide and copper oxide sorbents used alone. Best sulfation performance was exhibited by the sorbent containing 1:1 molar ratio of cerium and copper. Specific sulfur capacities decreased as the coverage of the support surface by the metal oxides approached monolayer coverage. Sorbents appeared to be resistant to cycling. No loss of sulfation capacity was observed after the third cycle.

The evaluation of these sorbents for the selective reduction of NO_x gave promising results with ammonia, but indicated low selectivity when methane was used as a reductant. In the reduction of NO with NH_3 , the conversion passes through a maximum at 573 K. Selective catalytic reduction studies with methane indicated that NO conversions between 10% and 17% could be obtained in the temperature range 648-748 K on catalysts containing both copper and cerium oxides for the space velocity used in the experiments (13700/hr).

Since propylene is known to be a more active and selective reductant for NO with other SCR

catalysts and since hydrocarbons are much more desirable reductants for NO removal, the performance of Cu-Ce catalysts for SCR of NO with propylene was also investigated. Although propylene was found to be very active in the absence of oxygen, the NO conversions obtained in wet oxygen-containing gases was limited to the same range observed using methane. With propylene, the temperature for maximum NO conversion decreased as the Cu/Ce ratio increased. Maximum conversion obtained was 17.5 % at 713 K on the catalyst with Cu/Ce=3 (Cu_{7.5}Ce_{2.5}). For Cu₈Ce₂ and Cu₂Ce₆ catalysts, the NO conversions obtained in wet oxygen-containing gases were limited to about 12.5% and 10.5% respectively, for the space velocities employed in this research (about 13,700/hour). This was due to low selectivity at high temperatures and low activity at low temperatures. In fact, the NO conversion passes through a maximum at around 730 K and 740 K for Cu₈Ce₂ and Cu₂Ce₆ catalysts, respectively. It was observed that water has a negative effect on NO conversion for Cu-Ce catalysts; NO conversion reduces from 21% in the absence of water to 12.5% in the presence of 7% water on Cu₈Ce₂ catalyst.

Table 1. Physical Properties of the Sorbent/Catalysts

Sorbent	Cerium Loading, mass %		Copper Loading, mass %		Surface Area, m ² /g
	Nominal	Actual	Nominal	Actual	
SOR10-II	5	4.58	5	5.54	122
SOR10-III	2.5	2.26	7.5	8.42	134
SOR10-IV	7.5	6.49	2.5	2.77	122
SOR10-V	2	1.90	8	8.76	130
SOR10-VI	0	0	10	10.36	105
SOR 10-VII	10		0	0	126

II. Experimental

(i) NO_x Removal

a) Catalysts

In the second year of the project, new catalysts were prepared in order to investigate their selective catalytic activity for the reduction of NO by methane by the promotion of some of the catalysts presented in Table 1. The catalysts were selected according to the observations summarized in Section I of this report.

As promoters, rhodium and manganese were used. The new catalysts are:

1. SOR10-III-0.1%RH
2. SOR10-III-1%Mn
3. SOR10-IV-0.1%RH
4. SOR10-IV-1%Mn

These catalysts are prepared by the incipient wetness technique, by impregnating the base catalysts (SOR10-III and SOR10-IV) by the appropriate metal salts, rhodium(III) chloride hydrate and manganese(II) nitrate hydrate, purchased from Sigma-Aldrich Co. (Milwaukee, WI).

b) Experimental Setup and Procedure

The experimental setup used for the selective catalytic reduction of NO is presented in Figure 1. For NO_x removal experiments, 2 grams of the catalyst/(sorbent) (particle size of 250 - 425 μm) is weighed and placed in the quartz microreactor. The reactant gas mixture is prepared from high purity bottled gases without further purification. Methane is used as the reductant.

The reactant gas composition for the standard SCR experiments is 650-900 ppm NO, which contains a maximum of 5 ppm NO₂, 1.5% O₂, 7% H₂O, CH₄/NO molar ratio of 1, and balance He.

Temperature range is 573 – 798 K.

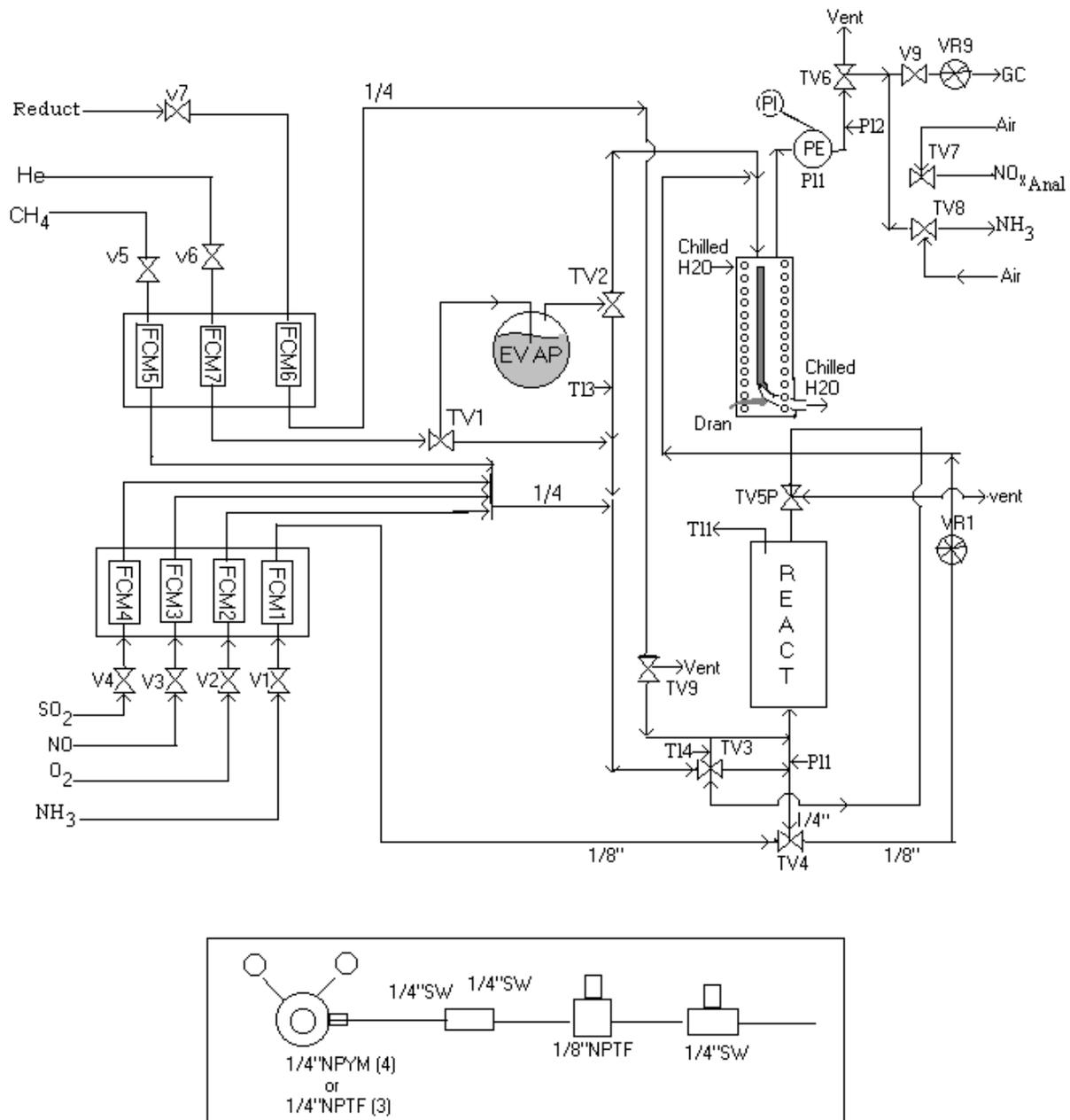


FIGURE 1. Experimental Setup for NO_x Removal Experiments

Gas samples were analyzed using a Varian 3400 Gas Chromatograph for CO, CO₂, N₂, O₂, CH₄ and C₃H₆. For the first five components, TCD detector with a 15' Carboxen 1000 column from Supelco was used. The column was temperature-programmed for the optimum resolution of the components; it was kept at 35°C for 5 minutes, then heated to 225°C at 20°C/minute and kept at that temperature for 10 minutes. Under these conditions, the retention times were 5.5 min for O₂, 6 min for N₂, 7.7 min for CO, 11.5 min for CH₄, and 13.8 min for CO₂.

A Thermo Environmental Instruments Model 42 H Chemiluminescence NO-NO₂-NO_x analyzer was employed for the quantitative analysis of NO₂ and NO. In the presence of a reductant, the high temperature (923 K) converter in the instrument leads to side reactions and gives erroneous NO₂ and NO_x readings. To overcome this shortcoming, the low temperature (623 K) Mo converter is utilized. With this converter reliable NO₂ measurements can be made.



The results from the NO_x removal experiments are interpreted by calculating the conversion of NO_x as:

$$\text{NO conversion } (X_{\text{NO}}) = [\text{NO in feed} - \text{NO in reactor effluent}] / [\text{NO in feed}]$$

(ii) Temperature-Programmed Desorption Experiments

In the investigation of the mechanism of selective catalytic reduction reaction, one approach is to use Temperature-Programmed Desorption (TPD) Experiments in order to evaluate the NO, NO₂, and O₂ chemisorption capacity of the catalysts and to identify the surface species and desorption species. For temperature-programmed experiments, a Micromeritics Pulse Chemisorb 2705 with TPD/TPR Option is used. A mass spectrometer-gas chromatograph system (SATURN 2000MS/3800GC) from Varian is used

for the identification of desorbed species and reaction products.

A typical TPD run is described below:

1. Pretreat all the samples in He (20 ml/min) at 323 K for 2 hours. This thermal treatment will prevent any appreciable oxygen uptake.
2. Carry out NO (NO_2 , $\text{NO}+\text{O}_2$, O_2 , CH_4 , or CH_4+O_2) adsorption at 323 K by flowing a NO/He mixture (or a similar mixture containing other adsorbents) containing 1.93 % NO in He, 3.6 % O_2 in He, 2.03 % CH_4 in He.
Flow rate: 40 ml/min
Temperature range: 35 °C – 700 °C
Temperature ramp: 3 °C/min
3. Flush the sample with a stream of dry helium at 323 K to eliminate gaseous NO and weakly adsorbed NO (or any other adsorbent).
4. When no NO (or any other adsorbent) is observed, heat the sample to 973 K in flowing He stream. Record the desorbed species.
5. The amount of NO adsorbed on the catalyst will be determined either from the NO adsorption measurement and the desorbed surface species from the TPD profile by integrating the desorption rate versus time data.
6. Repeat this procedure for two more cycles. Cool the sample to 323 K.
7. Adsorb methane at 323 K, then helium for 30 minutes.
8. Adsorb NOe at 323 K, then helium for 30 minutes.
9. Heat the sample up to 973 K in flowing helium stream for TPD. Cool the sample to 323 K.
10. Adsorb oxygen at 323 K, then helium for 30 minutes.
11. Adsorb methane at 323 K, then helium for 30 minutes.
12. Heat the sample up to 973 K in flowing helium stream for TPD.
13. Regeneration: a) Treat with oxygen at 923 K for two hours; cool to 323 K.
b) Treat with helium (saturated at 300 K) at 323 K for 15 minutes.

III. Results and Discussion

(i) Results and Discussion of NO_x Removal Experiments

In the previous project, it was observed that NO conversions showed a maximum with temperature due to the effect of temperature on the rates of reductant + NO and reductant + O₂ reactions, indicating that the reductant+ NO reaction has a smaller activation energy. It was also found that cerium oxide and copper oxide by themselves were not good catalysts for the reduction of NO with methane, especially at low temperatures. Maximum NO conversion at the space velocities used in the experiments (13700/hr) was 9 % at 475°C with cerium oxide and about 8 % at 450°C for copper oxide. Catalysts containing both copper and cerium oxides had better activities for NO reduction with methane, regardless of the Cu/Ce metal ratio. The maximum NO conversion at the space velocity used was about 17 % obtained at 425°C with both SOR10-III (Cu/Ce=3) and SOR10-IV (Cu/Ce=1/3) catalysts, being slightly lower for the former.

The effect of promoters, Mn and Rh, are investigated this year and the results of the NO reduction experiments on the promoted catalysts are presented in Figures 1-4. The conclusions that may be drawn from these figures are as follows:

1. With the SOR10-III (Cu/Ce=3), the activity remained the same with promotion by rhodium compared to the unpromoted catalyst. However, manganese was an effective promoter, increasing the activity to 21.8 % NO reduction compared to 16.5 % with the unpromoted SOR10-III catalyst.
2. With the SOR10-IV (Cu/Ce=1/3), the activity increased with promotion by both rhodium and manganese compared to the unpromoted catalyst, reaching to 20.7 % by rhodium and 23.6 % by manganese.

Effect of promoter on catalyst activity is more pronounced on catalysts with higher Ce/Cu ratio; this observation implies that the synergy is due to cerium rather than copper.

FIGURE 1. Reduction of NO by Methane on SOR10-III-0.1% Rh

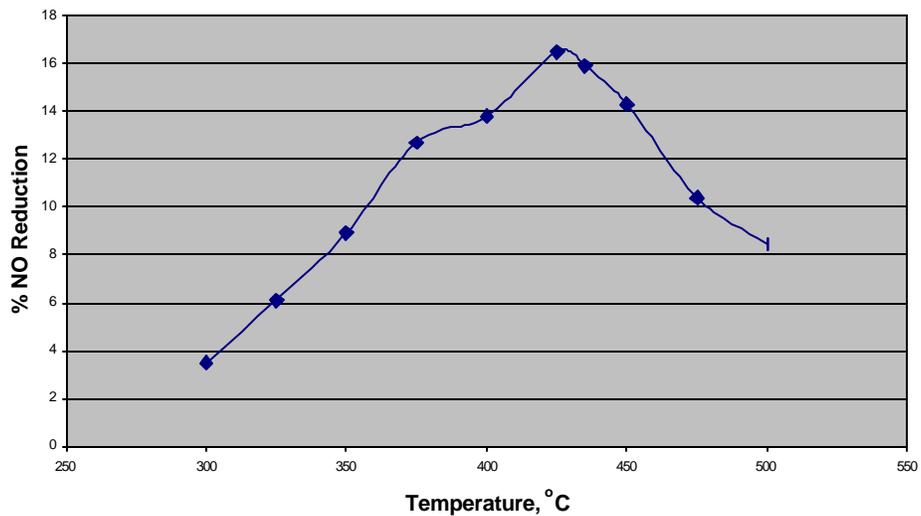


FIGURE 2. Reduction of NO by Methane on SOR10-III-1% Mn

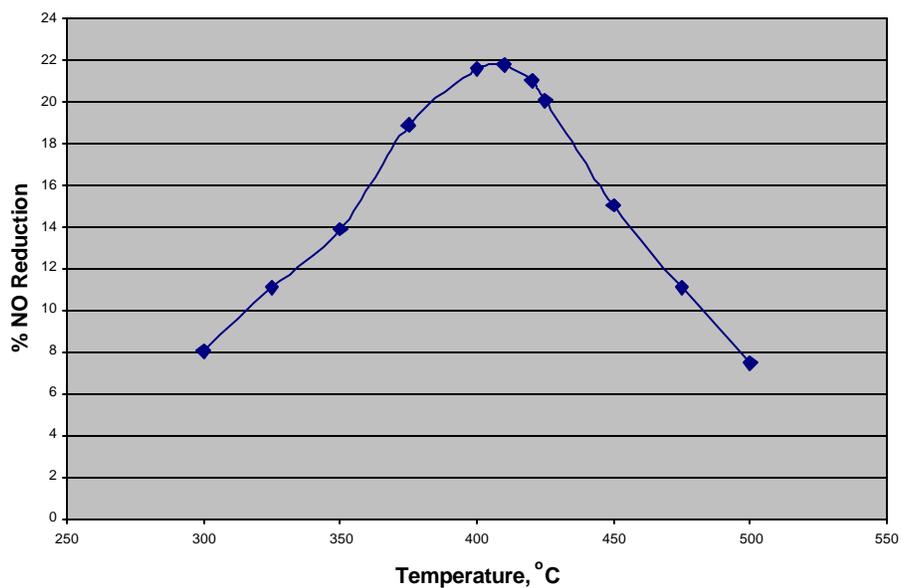


FIGURE 3. Reduction of NO by Methane on SOR10-IV-0.1% Rh

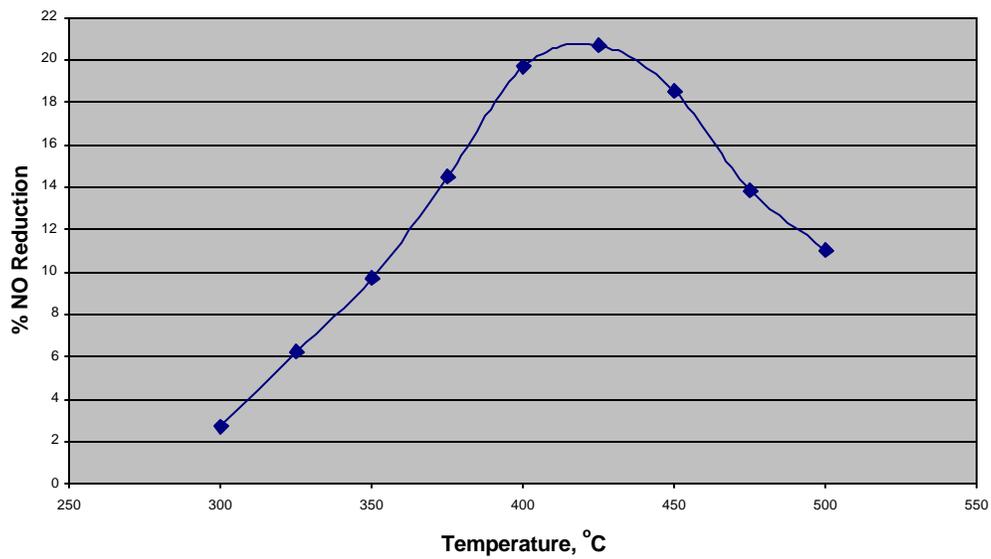
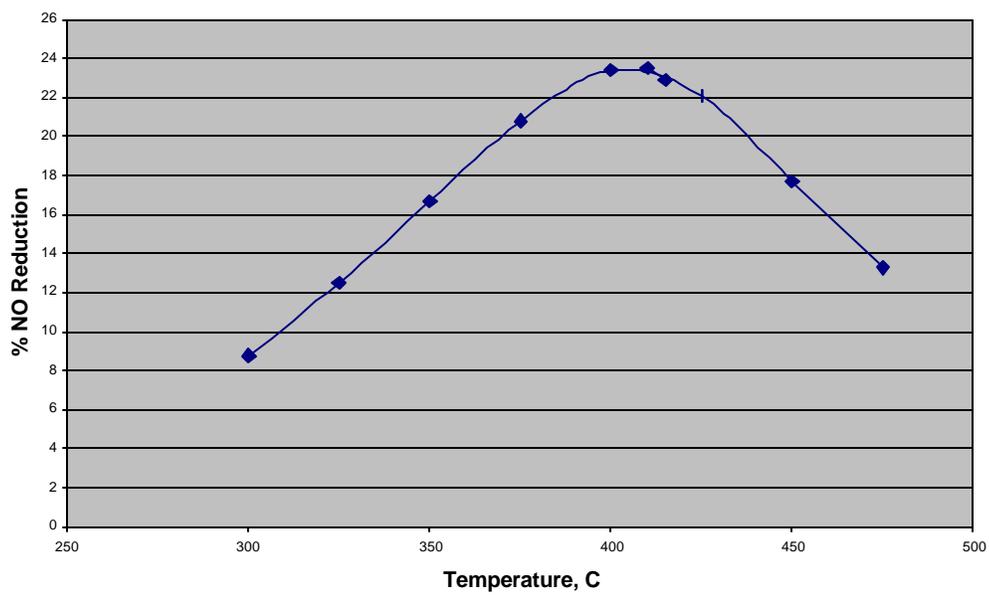


FIGURE 4. Reduction of NO by Methane on SOR10-IV-1% Mn



More promoted catalysts will be prepared to understand the reason for the different performance of promoters in the extent of NO reduction with catalysts with different Cu/Ce ratios. These catalysts will also be subjected to TPD-TPR analysis to investigate the effects of various promoters on the catalyst performance.

(ii) Results and Discussion of Temperature-Programmed Desorption Experiments

The results from the TPD Experiments are presented in Figures 5-22.

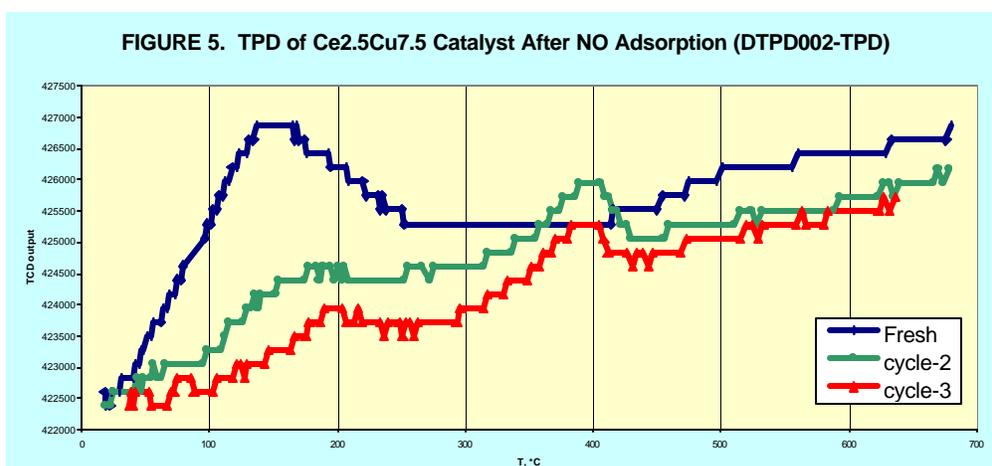


FIGURE 6. Evolved Species During TPD of Fresh Ce_{2.5}Cu_{7.5} Catalyst After NO Adsorption. (DTPD002A)

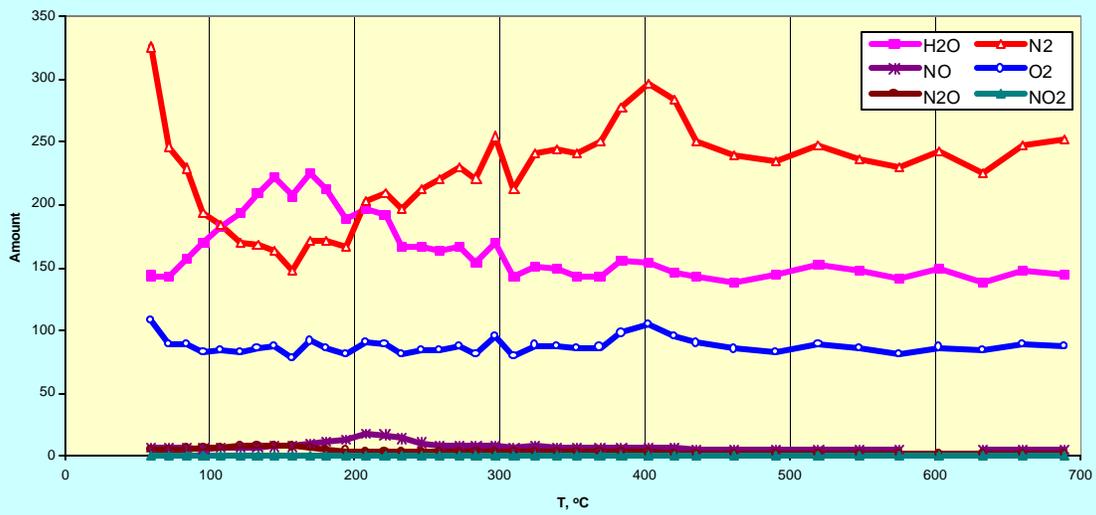


FIGURE 7. Evolved Species During TPD of Ce_{2.5}Cu_{7.5} Catalyst After NO Adsorption. Cycle-2 (DTPD002C)

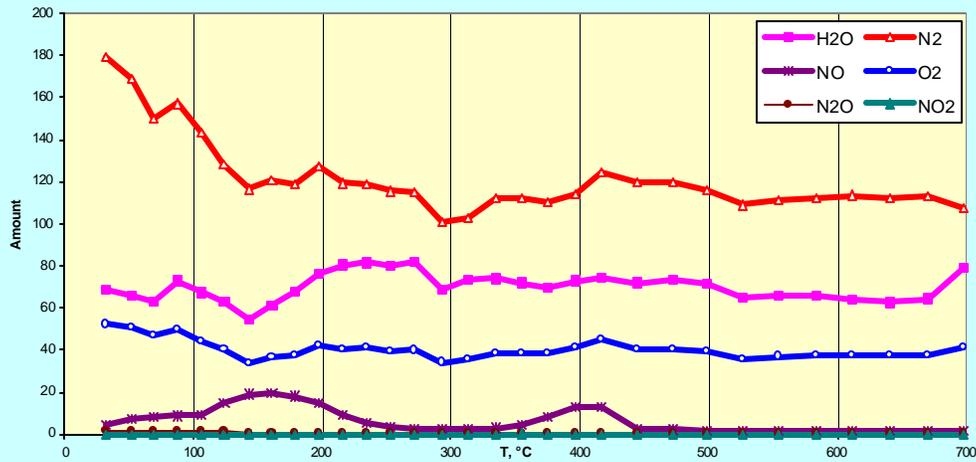


FIGURE 8. Evolved Species During TPD of Ce_{2.5}Cu_{7.5} Catalyst After NO Adsorption. Cycle-3 (DTPD002D)

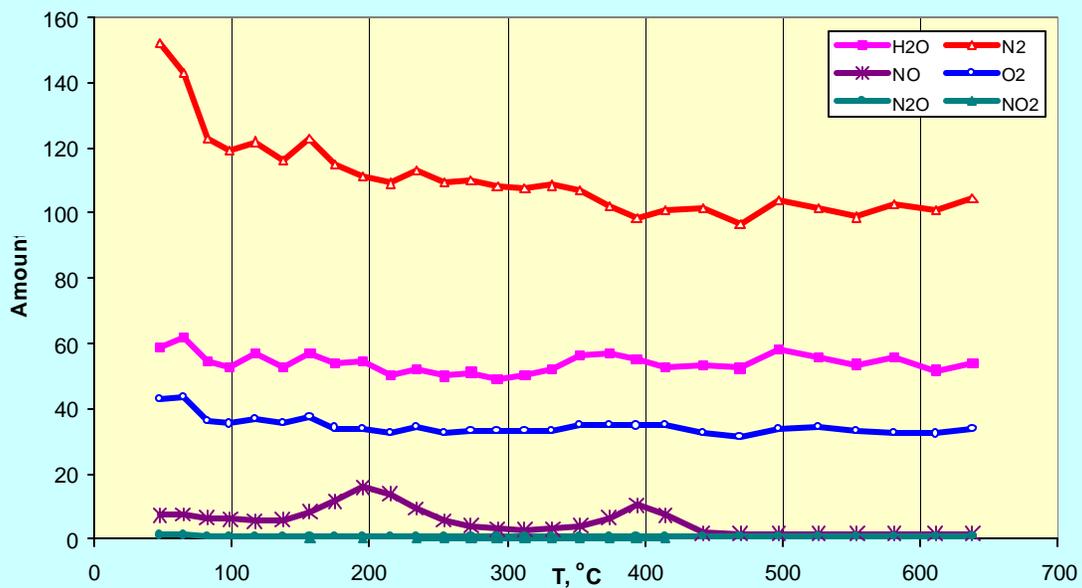


FIGURE 9. TPD of Ce_{2.5}Cu_{7.5} Catalyst with 0.1 % Rh After NO Adsorption (DTPD001-TPD)

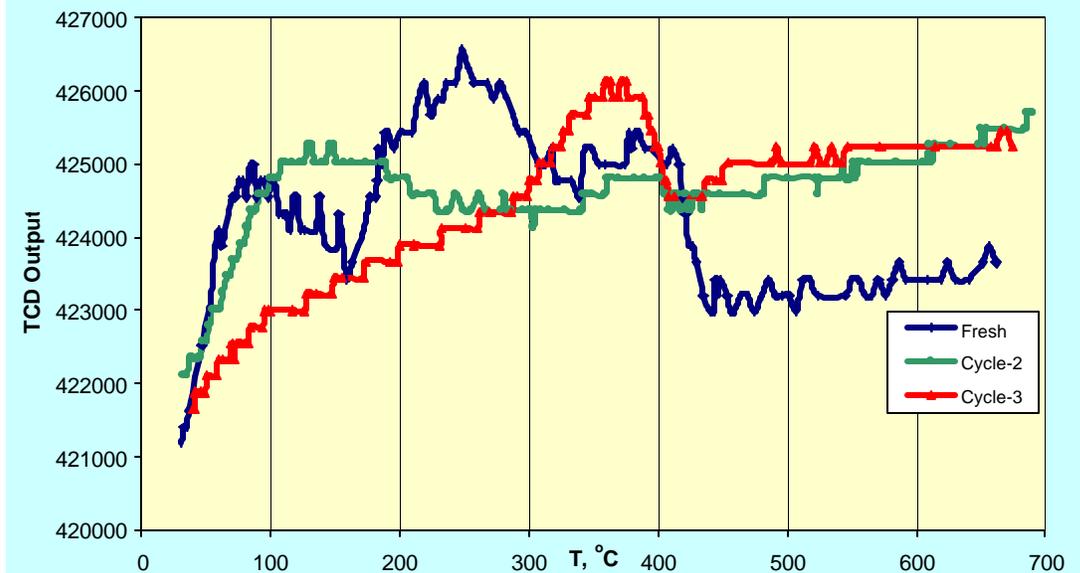


FIGURE 10. Evolved Species During TPD of Fresh Ce_{2.5}Cu_{7.5} Catalyst with 0.1 % Rh After NO Adsorption. (DTPD001A)

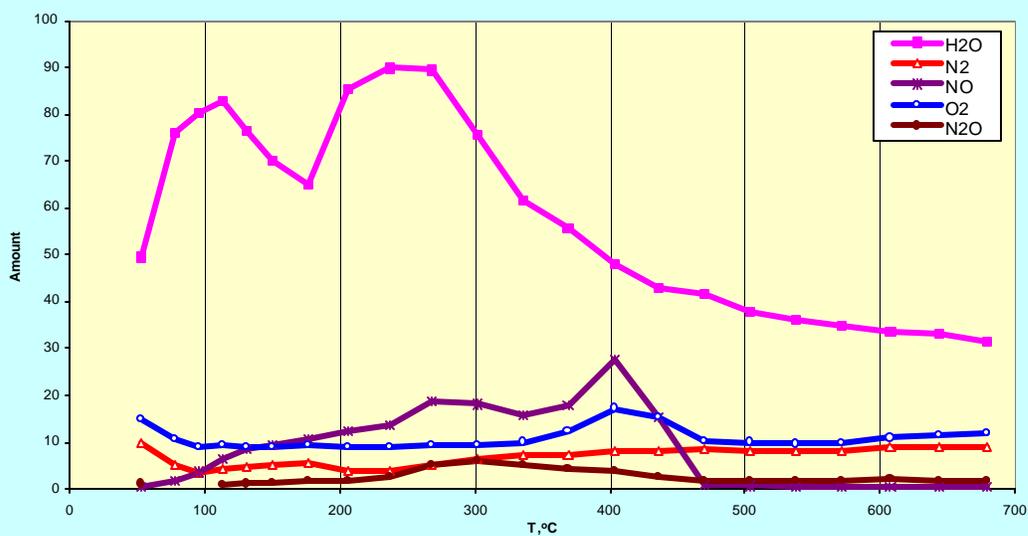


FIGURE 11. Evolved Species During TPD of Ce_{2.5}Cu_{7.5} Catalyst with 0.1 % Rh After NO Adsorption. Cycle-2 (DTPD001C)

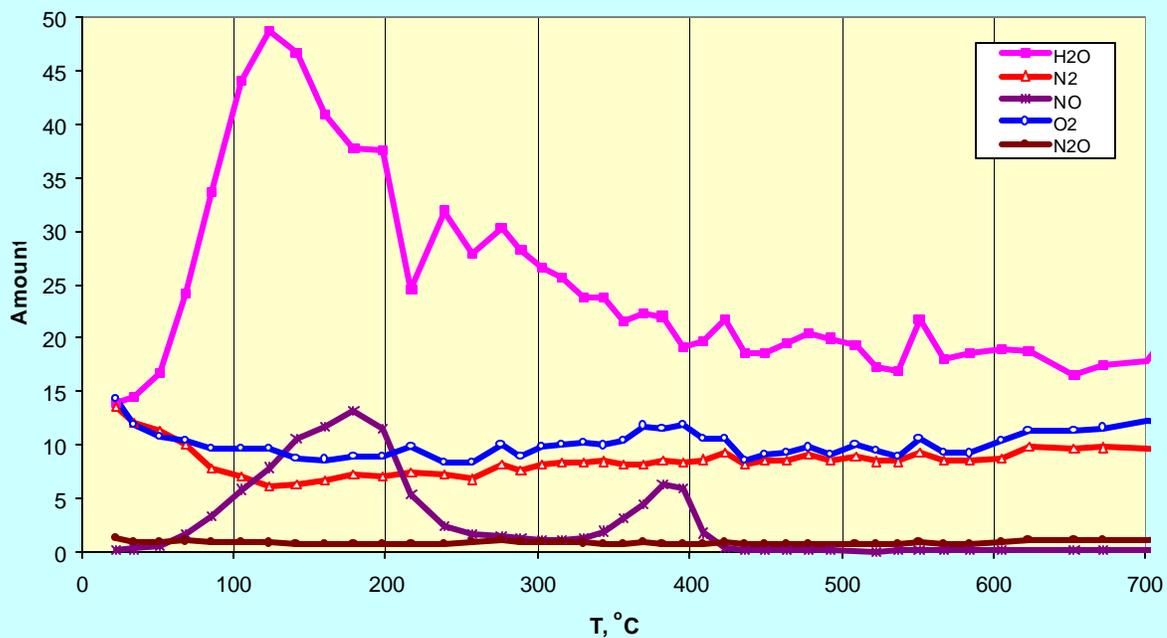


FIGURE 12. Evolved Species During TPD of Ce_{2.5}Cu_{7.5} Catalyst with 0.1 % Rh After NO Adsorption. Cycle-3 (DTPD001D)

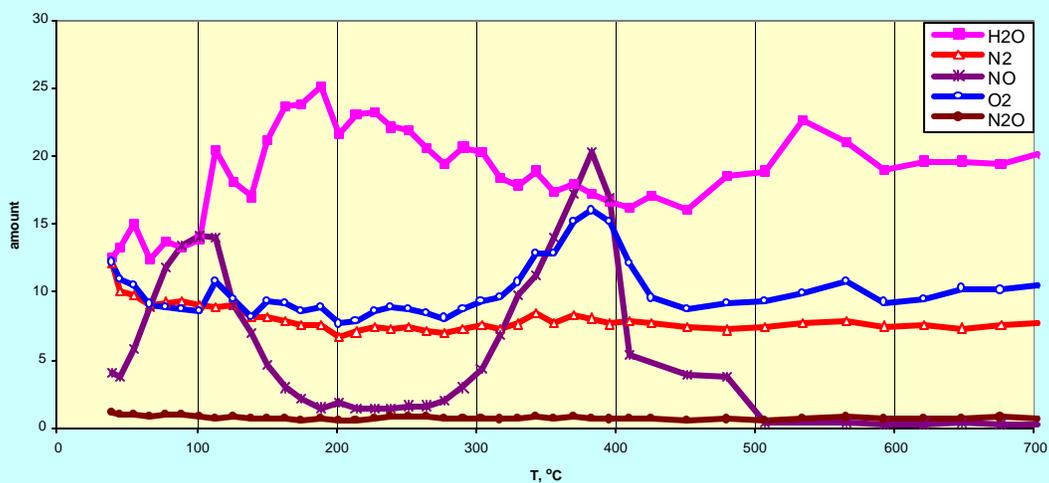


FIGURE 13. TPD of Ce_{2.5}Cu_{7.5} Catalyst After NO and CH₄ Adsorption (DTPD002F)

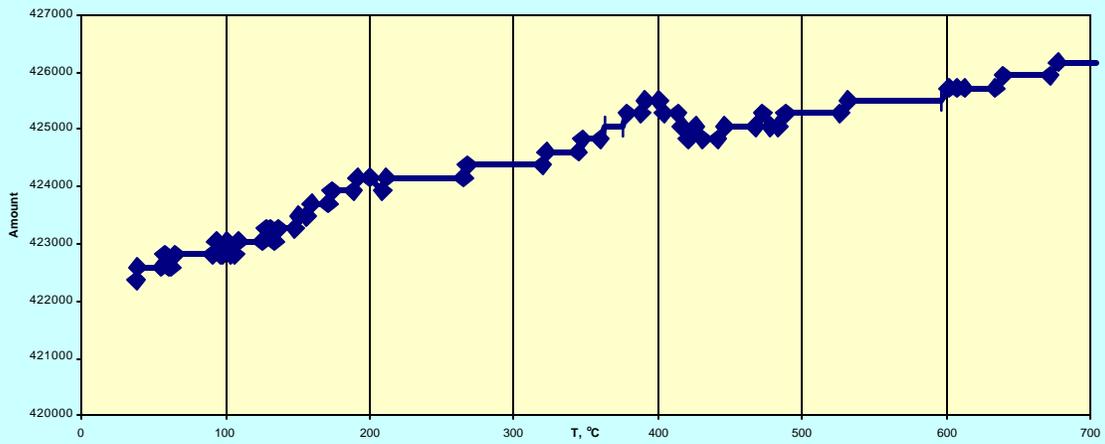


FIGURE 14. Evolved Species During TPD of Ce_{2.5}Cu_{7.5} Catalyst After Successive CH₄ and NO Adsorption (DTPD002F)

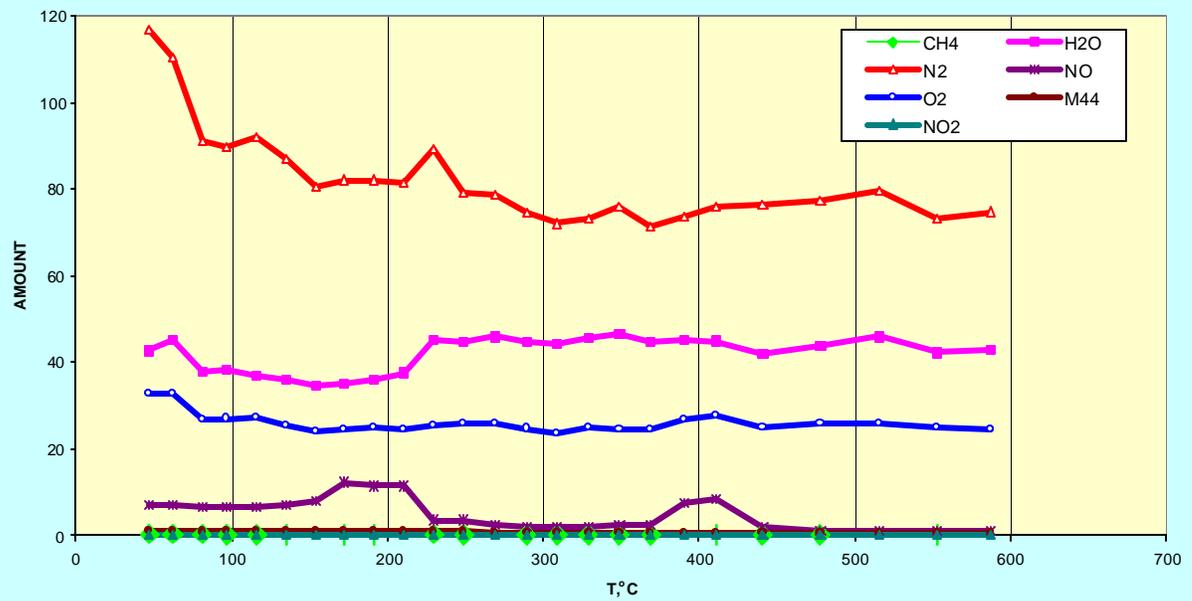


FIGURE 15. TPD of Ce_{2.5}Cu_{7.5} Catalyst After Successive O₂, NO, and CH₄ Adsorption (DTPD002H)

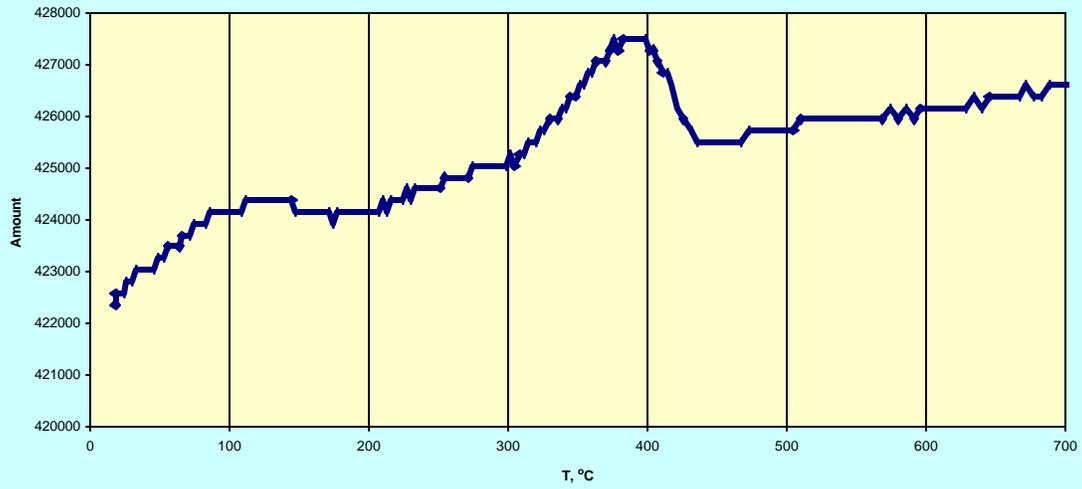


FIGURE 16. Evolved Species During TPD of Ce_{2.5}Cu_{7.5} Catalyst After Successive O₂, NO, and CH₄ Adsorption (DTPD002H)

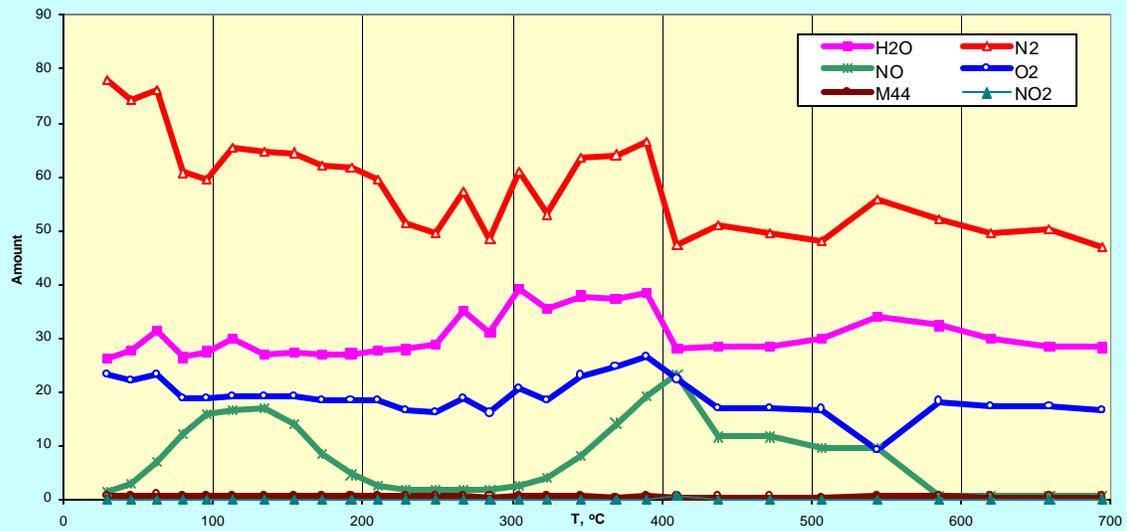


FIGURE 17. TPD OF Ce_{2.5}Cu_{7.5} Catalyst with 0.1 % Rh After Successive CH₄ and NO Adsorption (DTPD001h-TPD)

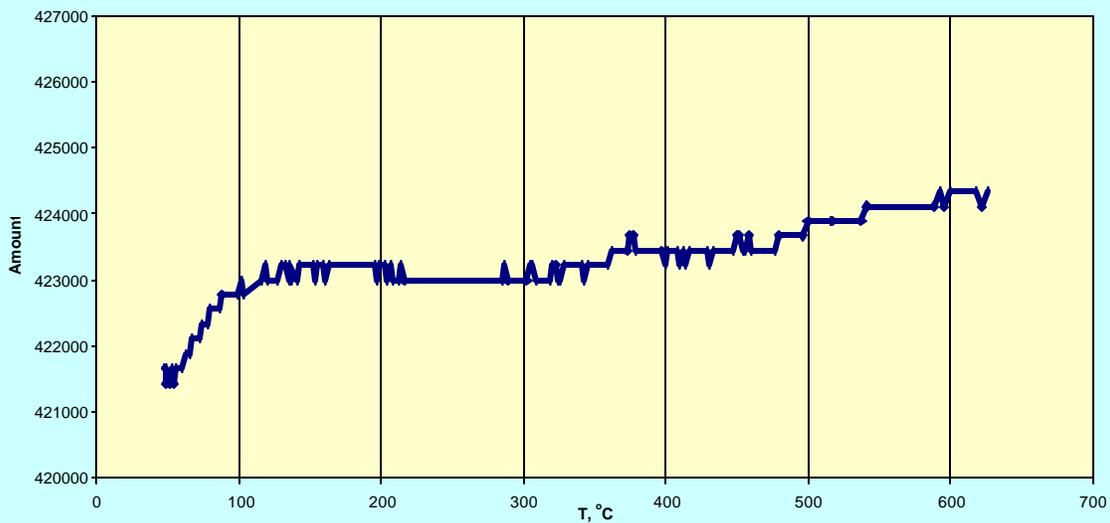


FIGURE 18. Evolved Species During TPD of Ce_{2.5}Cu_{7.5} Catalyst with 0.1 % Rh After Successive NO, and CH₄ Adsorptions (DTPD001H)

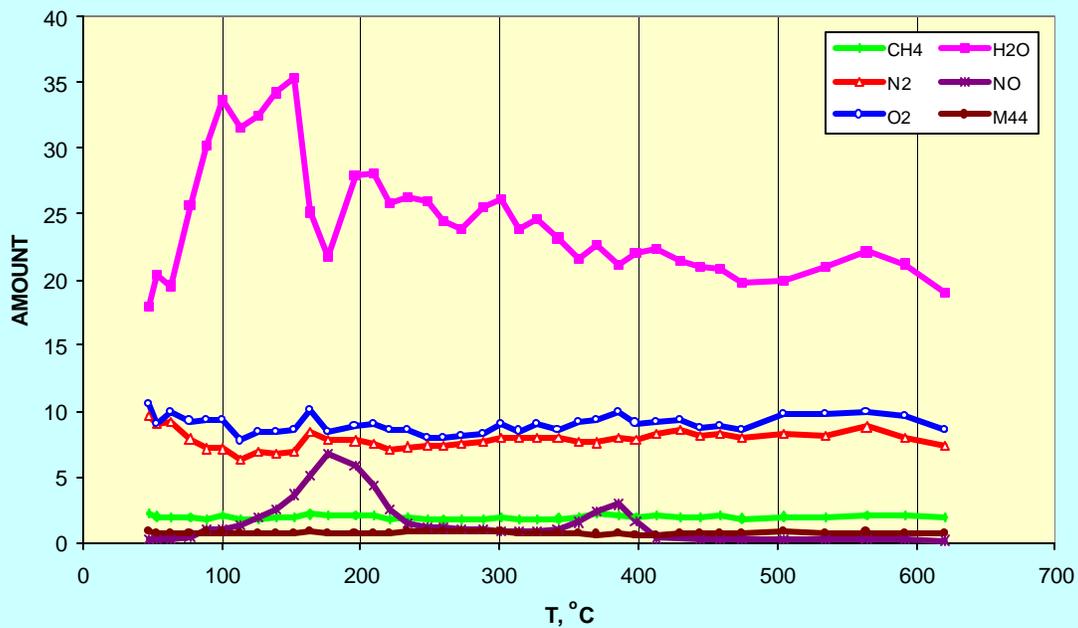


FIGURE 19. TPD of Ce_{2.5}Cu_{7.5} Catalyst with 0.1 % Rh After Successive O₂, NO, and CH₄ Adsorption (DTPD001L-TPD)

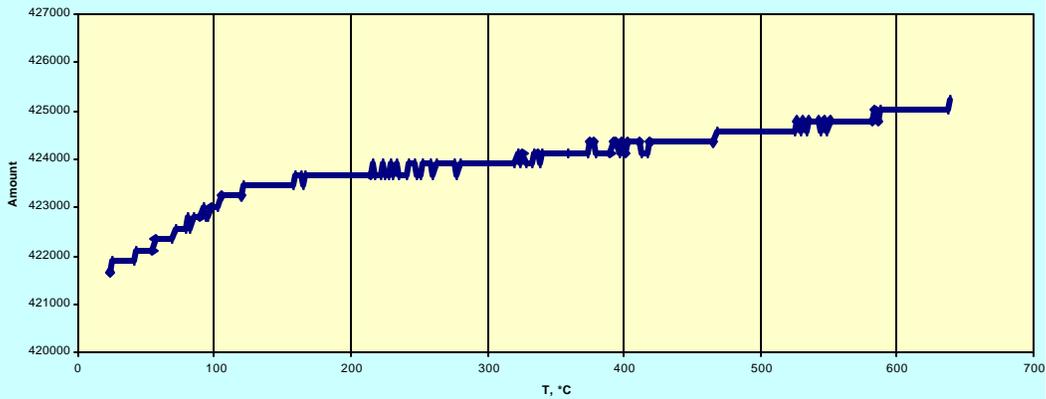


FIGURE 20. Evolved Species During TPD of Ce_{2.5}Cu_{7.5} Catalyst with 0.1 % Rh After Successive O₂, NO, and CH₄ Adsorptions (DTPD001L)

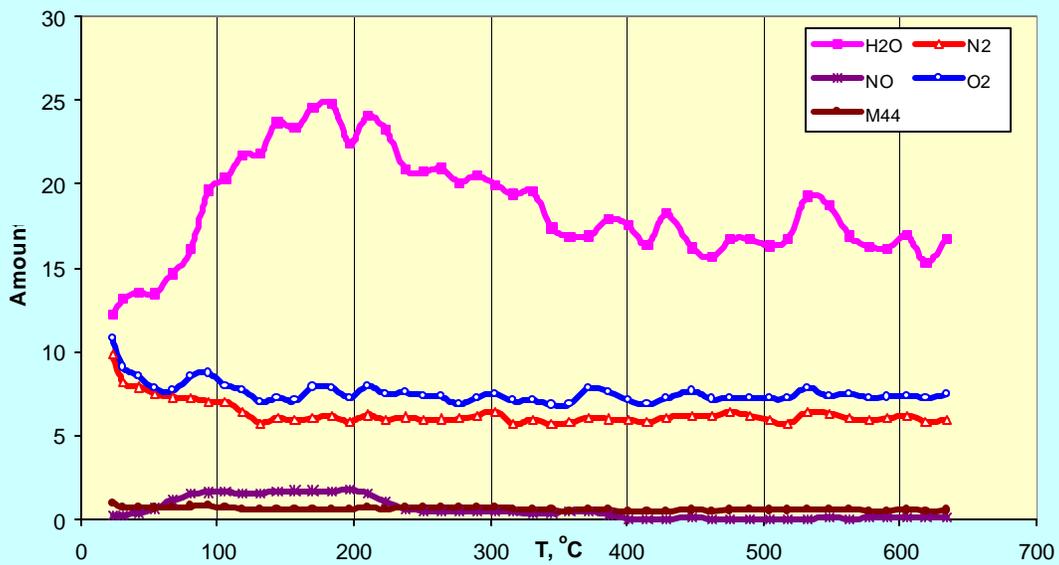


FIGURE 21. TPD of Fresh and Regenerated Ce_{2.5}Cu_{7.5} Catalyst with 0.1 % Rh After NO Adsorption

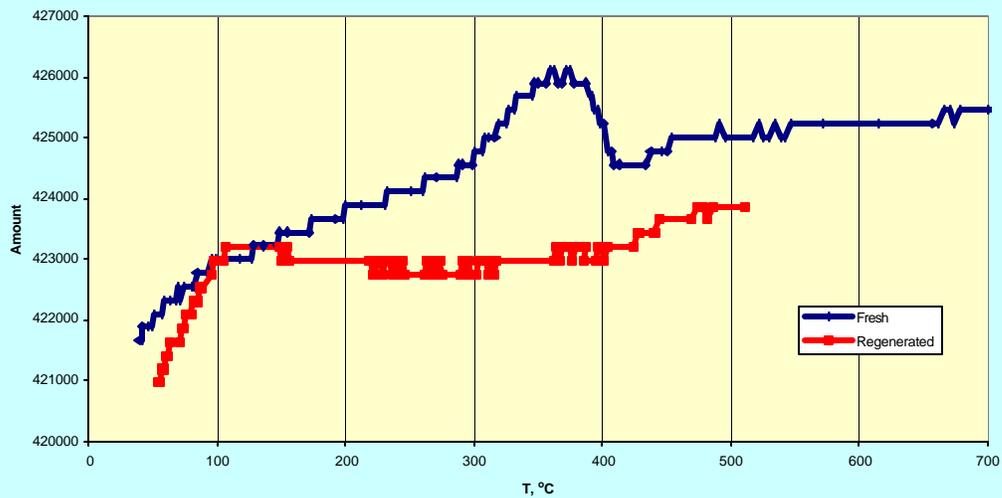
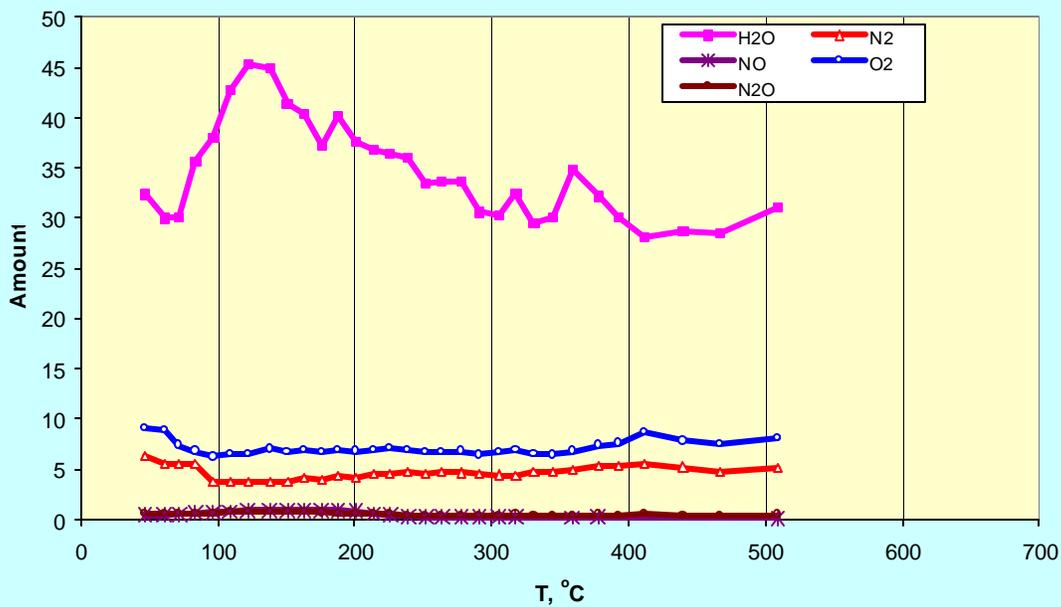


FIGURE 22. Evolved Species During TPD of Regenerated Ce_{2.5}Cu_{7.5} Catalyst with 0.1 % Rh After NO Adsorption (DTPD001N)



Figures 5-22 exhibit the effect of repeated NO adsorption-TPD to 923 K on catalyst performance; TPD after successive CH₄ and NO adsorptions; TPD after successive O₂, NO, and CH₄ adsorptions; and the possibility of regeneration by oxidation at 873 K and subsequent treatment with moist He at 323 K.

When repeated NO adsorption followed by TPD is performed on the fresh unmodified catalyst (SOR10-III; Cu/Ce=3), the main desorption peak is at 423 K (Figures 5-8). This peak is the result of desorption of water. NO desorption peak appears at 493 K. N₂O desorption is limited to temperatures less than 473 K. Significant N₂ desorption occurs above 473 K with the peak at 673 K. For the second and third TPD cycles, the main desorption peak is observed at 673 K and corresponds to the second NO desorption peak. This peak is not observed on the fresh catalyst. This may imply that the fresh catalyst is more active for NO dissociation. The first NO desorption peaks appears at 433 K for cycle 2 and 473 K for cycle 3. No N₂O desorption is observed.

The fresh catalyst (SOR10-III) containing 0.1 % Rh exhibit three desorption peaks at 373, 523, and 673 K (Figures 9-12). The first two peaks appear to be the result of water desorption and the third peak corresponds to NO desorption. N₂O desorption peak is at 573 K. For the second TPD cycle, the second peak disappears. In the third TPD cycle, only the third peak remains. Two distinct NO desorption peaks appear (at 453 and 653 K for cycle 2, and 393 and 653 K for cycle 3). The relative height of the second peak increases with cycling. There is an oxygen desorption peak corresponding to the second NO desorption peak in all cycles. No N₂O peak is observed in cycle 2 and 3. Low N₂ desorption suggests lower activity for NO dissociation.

The TPD after successive NO and CH₄ adsorptions on the fresh unmodified catalyst (SOR10-III; Cu/Ce=3) shows two peaks at 473 K and 673 K corresponding to the two NO desorption peaks (Figures 13-14). There is also a uniform N₂ desorption, either due to NO dissociation or reduction by methane or both. The TPD after successive O₂, NO, and CH₄ adsorptions also shows two peaks at 403 K and 673 K corresponding to the two NO desorption peaks (Figures 15-16). The uniform N₂ desorption is also observed.

The TPD after successive NO and CH₄ adsorptions on the catalyst (SOR10-III) modified with 0.1 % Rh does not show any distinct peaks because the two NO peaks at 463 K and 663 K appear to be

masked by the uniform water desorption (Figures 17-18). The TPD after successive O₂, NO, and CH₄ adsorptions also do not show any distinct peaks (Figures 19-20). There is a single broad NO peak between 353 and 493 K. The significant uniform water desorption is also observed. There is CO₂ formation, too, corresponding to CH₄ oxidation. This result reinforces the results from the NO-SCR experiments, which revealed that catalysts promoted with rhodium did not have enhanced SCR activities.

Figures 21 and 22 indicate that treatment with oxygen reduces NO adsorption.

IV. CONCLUSIONS

The NO reduction activity of the catalysts with higher Cu/Ce ratio (Cu/Ce=3) remained the same when promoted by rhodium compared to the activity of the unpromoted catalyst. However, manganese was an effective promoter, increasing the activity of these catalysts to 21.8% NO reduction compared to 16.5% with the unpromoted catalyst.

Promotion with both rhodium and manganese increased the activity of the catalysts having lower Cu/Ce ratio (Cu/Ce=1/3), reaching 20.7% by rhodium and 23.6% by manganese. These observations imply that the synergy is due to cerium rather than copper.

NO-TPD on fresh unpromoted catalyst (Cu/Ce=3) exhibited a single NO desorption peak at 493 K; N₂O desorption was limited to temperatures lower than 473 K; N₂ desorption increased after 473 K and showed a peak at 673 K. For the second and third cycles, two NO peaks at 473 and 673 K were observed. There was no N₂O desorption during these cycles; and N₂ desorption does not increase after 473 K. On this catalyst, the behavior with successive (NO+CH₄) and (NO+CH₄+O₂) adsorptions was similar to the NO adsorption case.

The fresh catalyst (Cu/Ce=3) promoted with 0.1% Rh exhibited an NO desorption peak at 673 K, an N₂O desorption peak at 573 K and low nitrogen desorption with no peaks. For the second and third cycles, two distinct NO desorption peaks were observed at 453 and 653 K for the second cycle and at 393 and 653 K for the third cycle. This indicates lower NO dissociation, this fact being reiterated by low nitrogen desorption. There was no N₂O peak in the second and third cycles. The TPD with NO+CH₄ was similar to TPD with NO. However, with NO+CH₄+O₂, there is a single NO desorption peak between 353 and 493 K. Thus, the TPD behavior of the unpromoted SOR10-III catalyst was observed to be different

from that promoted with 0.1% rhodium with various adsorbents; it is hypothesized that this variance accounts for the lack of enhancement of SCR activity of this catalyst with promotion by rhodium. The TPD behavior of this catalyst with manganese as the promotor will be performed to interpret the source of activity and the effect of promoters on it for SCR reaction with these catalysts.

V. Additional Activities

Several students (Randolph Ashton, Anthony Samuels, Lashonda Martin, and Amy Gay) were employed as undergraduate research students. They were trained in the laboratory to use the TPR/TPD equipment and the reactor setup for the SCR experiments. They have learnt how to use the gas chromatograph and the NO_x Chemiluminescence equipment.

A poster paper, entitled “Selective Catalytic Reduction of NO_x by Hydrocarbons on Supported Copper Oxide-Cerium Catalysts” was presented at the 17th North American Catalysis Society Meeting at Toronto, Canada on June 3-8, 2001. A paper entitled “Investigation of Mixed Oxide Catalysts for the Selective Catalytic Reduction of NO by Methane and Propylene” has been accepted for presentation at the AIChE 2001 Annual Meeting at Reno, Nevada on November 4-8, 2001.

FUTURE PLANS

During next year, it is planned:

1. to do TPD and TPR_xN experiments with promoted catalysts;
2. to prepare more promoted catalysts;
3. to perform the selective catalytic reduction (SCR) of NO with methane on promoted catalysts in the microreactor;
4. to do SCR with fuel oil as reductant.