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In-Cell Gamma Count

## Caustic-Side Solvent Extraction Batch Distribution Measurements for SRS High Level Waste Samples and Dissolved Saltcake

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## **Caustic-Side Solvent Extraction Batch Distribution Measurements for SRS High Level Waste Samples and Dissolved Saltcake**

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### **Summary**

In 2001, the first measurements of cesium distribution behavior in actual waste samples during the Caustic-Side Solvent Extraction (CSSX) process were reported. These measurements showed acceptable behavior across the extraction, scrubbing and stripping stages of the CSSX process. However, extraction performance was not consistent with developed thermodynamic models. Therefore, additional batch tests were performed to measure the distribution coefficients with samples from F- and H-Area high level waste Tanks. The results of these tests provide the following conclusions.

- Extraction, scrubbing and stripping (ESS) behavior with actual tank waste including Tank 37H and Tank 41H dissolved saltcake and the newly optimized solvent system surpassed flowsheet requirements.
- Thermodynamic model predictions of extraction distribution coefficients agreed well with measured values in the optimized solvent system.
- The ESS distribution coefficients for a waste sample that had been processed using a permanganate treatment to remove transuranic components were acceptable compared to flowsheet requirements.
- The addition of sodium permanganate does not appear to adversely affect the CSSX process.
- Improved experimental techniques and counting methodologies greatly improved the ability to perform ESS testing with actual tank waste samples in the Shielded Cells.

### **Introduction**

High level wastes stored at the Savannah River Site (SRS) consist of insoluble metal hydroxides/oxy hydroxides (sludge) that were formed upon neutralization of acidic PUREX canyon wastes. Additionally concentrated supernate and crystallized saltcake, formed upon evaporation of the neutralized liquid waste, are stored in million gallon storage tanks. The Defense Waste Processing Facility (DWPF) is currently vitrifying the sludge component of the high level waste.

The supernate and saltcake streams required both cesium and actinide decontamination prior to disposal at the Saltstone Production Facility. The required decontamination factors for cesium can approach 40,000. For this reason, a caustic-side solvent extraction (CSSX) process<sup>1</sup> was developed by researchers at Oak Ridge National Laboratory. This cesium removal technology utilizes a 4 component solvent mixture comprised of a calixerene crown ether extractant (BOBCalixC6), an alcohol modifier (Cs-7SB), and an inhibitor (trioctylamine) dissolved in Isopar® L diluent.

The CSSX technology for cesium removal has received extensive study over the past several years. Included in this body of work has been several simulant studies,<sup>2</sup> chemical and radiolytic studies<sup>3,4</sup> of the solvent stability, and a demonstration of the CSSX process on a 100-L sample of actual SRS high level waste from tanks 44H and 37F.<sup>5</sup> The CSSX process was robust and successfully demonstrated cesium decontamination factors greater than 10<sup>6</sup>.

Testing experience with actual high level waste samples is limited. The initial batch testing<sup>6</sup> of actual tank supernate samples for the extraction, scrubbing and stripping (ESS) of cesium showed acceptable cesium behavior as compared to the proposed facility's flowsheet. However, this study suffered from poor cesium accountability related to possible dilution matrix effects. These dilutions were required to remove samples from the radiological shielded cells prior to gamma counting. Furthermore, Walker<sup>7</sup> examined the CSSX process for utility in removing cesium from dissolved saltcake samples from Tanks 38H and 46F. Difficulty was again experienced with initial cesium accountability, but good cesium accountability was eventually obtained and satisfactory CSSX performance was observed.

The purpose<sup>8</sup> of this study was to expand the CSSX performance database for actual tank wastes and to evaluate the adequacy of the newly optimized solvent composition. Additionally, CSSX performance models<sup>9,10</sup> have been under development at ORNL. The study compares actual CSSX performance with samples of supernate and dissolved saltcake to the CSSX prediction models.

## **Experimental Details**

### *Chemical Characterization of Tank Waste Samples*

High level waste samples<sup>11</sup> were obtained from several tanks in both the F- and H-Area tank farms. Previously, the 2F Evaporator system tanks (Tanks 26F and 46F) were tested through the ESS protocol with only limited success.<sup>6</sup> Therefore, additional samples were obtained from the feed tank (Tank 26F, samples labeled FTF-099 and FTF-100) and the drop tank (Tank 46F, samples labeled FTF-103 and FTF-104). The final samples from an F-Area tank were obtained from Tank 34F (FTF-109, FTF-110, and FTF-111). This tank represents a long-term inactive tank since no additions had been made to this tank for over 10 years. Additionally, samples were also obtained from on-going research<sup>12,13</sup> involving the 3H evaporator and samples from the feed tank (Tank 32H) and drop tank

(Tank 30H) were allocated to CSSX ESS testing. The samples were composited by tank and gravimetrically diluted by weight with 0.2 M nitric acid. Diluted samples were removed from the cell and analyzed by Inductively Coupled Plasma-Emission Spectroscopy (ICP-ES) for sodium ion concentration. Subsequently, an aliquot of 1.6 M sodium hydroxide solution was added to each tank composite to reduce the sodium ion concentration to a target value of 5.6 M. The entire tank composite adjusted to 5.6M sodium ion concentration was then passed through a 0.45  $\mu\text{m}$  filter and samples were gravimetrically diluted in dilute nitric acid for elemental concentrations and radionuclide content and by weight with water for anion analysis. Table 1 shows the analytes measured in the tank waste samples after dilution to 5.6 M sodium ion concentration.

Two additional samples were obtained from other programs supporting the Salt Waste Processing Facility. The first of these was a sample from the filtrate of a Cells Unit Filter (CUF) test involving the addition of sodium permanganate<sup>14</sup> to remove transuranic species. This filtrate was tested without additional dilution; however, it was passed through a 0.45  $\mu\text{m}$  filter. Additionally, a sample of the Tank 37H dissolved saltcake was obtained prior to the centrifugal contactor run and was tested without alteration or sampling because it had already been filtered and characterized. This report contains characterization data for these waste samples and references to their origin.

Additional funding was obtained that allowed testing with samples of the identical waste composite prior to the permanganate treatment. Analysis of this testing will allow for direct comparison as to the effect of permanganate. This supernate was obtained from the stock solution used in the permanganate testing and was not altered prior to use. Likewise, another sample of dissolved saltcake was obtained from Tank 41H.<sup>15</sup> The composition of this sample agreed with expected saltcake chemistry. Table 2 contains the chemical characterization for these samples.

#### *Extraction, Scrubbing and Stripping Protocol*

The ESS protocol was slightly adapted from that previously performed on the actual tank waste samples.<sup>6</sup> Walker<sup>7</sup> altered the protocol to include a second scrub step and this second scrub was included in the current step regiment. However, during the testing with samples of dissolved saltcake, Walker found that the centrifuge currently installed increased the temperature by  $\sim 5\text{ }^{\circ}\text{C}$  and could affect the measurement. Therefore, several changes were made to the ESS protocol to ensure accurate measurement in the SRTC Shielded Cells. First, the sample size of actual waste was increased to 90 ml and separatory funnels replaced the centrifuge tubes used previously. Campbell<sup>5</sup> and Spence<sup>4</sup> had previous success using this methodology. The standard organic-to-aqueous ratios were used and were 0.33 for the extraction and 5 for the scrubbing and stripping. Phase separation was accomplished by allowing the mixture to stand for 24 hours. The second change was to utilize the new optimized<sup>16</sup> solvent composition shown in Table 3.

**Table 1. Analyte Measurements for Tank Waste Samples**

Analyte	Units	Tank 26F	Tank 34F	Tank 46F	Tank 30H	Tank 32H	Permanganate Treated Waste Composite	Tank 37H Saltcake
Fluoride	mg/L	249		76				
Formate	mg/L	970	101	680				
Chloride	mg/L	224	197	201	152	50	293	320
Nitrite	M	0.46	0.42	0.49	0.53	0.78	0.47	0.88
Nitrate	M	1.17	0.97	0.38	0.51	1.31	0.48	0.73
Phosphate	mg/L	373	269	327	482	298	587	1900
Sulfate	M	0.03	0.01	0.01	0.004	0.02	0.004	< 0.006
Hydroxide	M	3.68	3.49	3.23	3.86	3.05	3.47	3.7
Carbonate	M	0.08	0.07	0.08	0.07	0.07	0.07	< 0.22
Aluminate	M	0.25	0.28	0.28	0.37	0.46	0.30	0.54
Sodium	M	5.53	5.94	5.77	5.75	6.02	5.50	6.22

Analyte	Units	Tank 26F	Tank 34F	Tank 46F	Tank 30H	Tank 32H	Permanganate Treated Waste Composite	Tank 37H Saltcake
Al	M	0.25	0.28	0.28	0.37	0.46	0.29	0.56
B	mg/L	154	130	156	107	83	87.50	96
Ba	mg/L	0.00	0.15	0.24	1.32	0.00	0.00	3.8
Ca	mg/L	2.31	2.57	2.06	0.70	2.78	2.25	< 0.1
Cd	mg/L	0.42	0.59	0.55	0.00	0.71	0.73	1.1
Co	mg/L	0.08	0.13	0.11			0.00	< 0.3
Cr	mg/L	124	143	143	189	208	86.53	167
Cu	mg/L	1.71	1.94	1.90	3.02	2.40	1.47	2.4
Fe	mg/L	12.18	14.34	17.11	11.29	9.32	5.52	9.9
La	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	< 1
Li	mg/L	0.45	0.00	0.52	0.00	0.00	0.34	0.8
Mg	mg/L	0.43	0.59	0.57	0.00	0.45	0.44	0.2
Mn	mg/L	0.24	0.20	1.38	0.00	0.30	0.10	1.9
Mo	mg/L	35.9	30.5	42.4	98.5	68.2	65	155
Na	M	5.53	5.94	5.77	5.75	6.02	5.50	6.22
Ni	mg/L	0.90	0.87	1.00	0.00	0.71	0.00	< 1
P	mg/L	137	135	153	152	133	149	
Pb	mg/L	3.77	5.24	5.36	0.00	10.63	4.45	9.4
Si	mg/L	18.55	25.17	20.95	11.99	11.93	25	19
Sn	mg/L	5.86	6.66	7.28	7.44	12.99	6.9	12
Sr	mg/L	0.34	0.38	0.44	1.27	0.40	0.34	< 0.1
Ti	mg/L	0.00	0.00	0.00	0.00	0.00	0.00	1.6
U	mg/L	16.01	11.42	32.17	0.00	9.40	6.50	15
V	mg/L	1.69	2.09	2.09	0.00	1.95	2.15	3.6
Zn	mg/L	8.47	13.12	9.83	6.20	4.88	9.83	5.2
Zr	mg/L	0.12	0.10	0.11	0.00	0.35	0.06	1.1
K	mg/L	1176	1469	1336	1520	1264	1436	1525
Cs	mg/L	3.9	3.9	3.9	16.1	17.5	4.2	45.2

**Table 2. Analyte Measurements for Waste Composite Prior to Permanganate Treatment and Saltcake Sample from Tank 41H**

<u>Analyte</u>	<u>Units</u>	<u>Tank 41H Saltcake</u>	<u>Waste Composite Prior to Permanganate</u>
Al	M	0.16	0.47
B	mg/L	70.56	4.75
Ca	mg/L	1.83	2.68
Cr	M	0.00	0.00
Cu	mg/L	2.06	1.54
Fe	mg/L	3.65	7.38
La	mg/L	0.69	0.82
Mo	mg/L	57.11	18.53
Na	M	6.56	5.20
P	M	0.002	0.002
Si	mg/L	17.36	34.04
Sn	mg/L	8.83	31.69
Sr	mg/L	0.66	15.26
Zn	mg/L	8.25	1.43
K	M	0.04	0.005
Cs	mM	0.17	0.04
Anions			
Nitrite	M	0.13	0.39
Nitrate	M	3.28	0.46
Sulfate	M	0.04	0.00
Hydroxide	M	0.66	3.29
Carbonate	M	0.41	0.15

**Table 3. Optimized Solvent Composition**

Extractant	BOBCalixC6	0.007 M
Modifier	Cs-7SB	0.75 M
Inhibitor	Trioctylamine	0.003 M
Diluent	Isopar® L	

The last change was to avoid dilution issues and count each phase neat. Therefore, the In-Cell Gamma Monitor (IGM) was used. The IGM is a 9" by 5" by 6" tungsten block into which a miniaturized NaI gamma detector has been inserted. The detector views samples in one of three positions and was designed to measure Cs-137 activities over a dynamic range of  $10^5$  to  $10^{10}$  dpm/ml in the high background environment of the SRTC Shielded Cells. The initial position is in close contact with the sample container, further



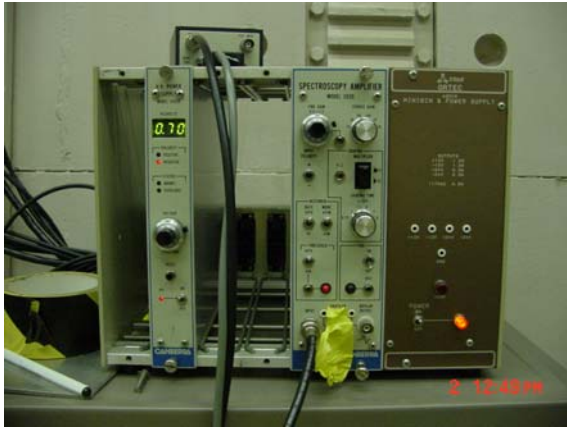
positions are viewed through a 0.25-inch diameter collimator. The block was coated with a plastic layer, and each sample port was designed with numerous layers of containers in the event decontamination became necessary. The gamma spectra are acquired using a Canberra Genie2k Gamma Acquisition System. Peak energy calibration was performed prior to commencement of testing and intensity calibration was performed during testing. An aliquot of 3 mL was pipetted to the counting tube and counted for 300 s. If the dead time was higher than 5 %, an alternate sample position is selected. Occasionally, there was insufficient sample to obtain 3 mL for counting. In those instances the liquid phase was gravimetrically diluted to 3 mL with the fresh liquid phase. Figure 1 shows photographs of the In-Cell Gamma Monitor. The distribution coefficients were calculated based on the activity in the organic phase divided by the activity in the aqueous phase. Temperature corrections were performed using enthalpy values previously reported.<sup>5</sup> All distribution coefficients are reported as corrected to 25 °C.

## **Results and Discussion**

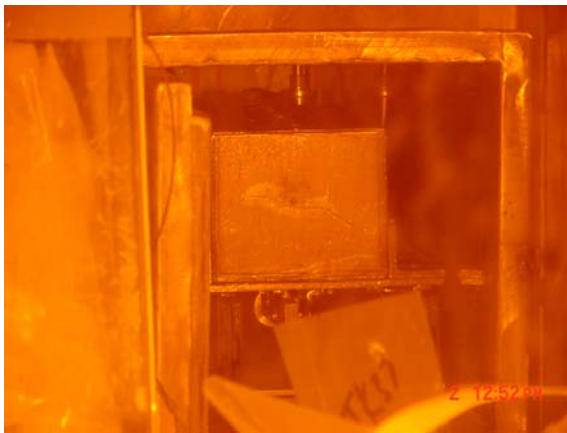
### *ESS Behavior of 2F Evaporator Samples and Tank 34F*

During testing in FY01, samples from the 2F Evaporator system were examined for their behavior in the ESS batch protocol.<sup>6</sup> The batch equilibrium distribution coefficient,  $D_{Cs}$ , for the waste from Tank 26F measured  $7.7 \pm 1.9$  while the measured values for Tank 46F was  $13.8 \pm 2.8$ . These values for extraction coefficients had a much larger difference than the ORNL predicted extraction coefficients that were 14.95 and 16.55 for Tank 26F and Tank 46F, respectively. In addition, the averaged extraction coefficient for Tank 26F was below the facility flowsheet criteria of a  $D_{Cs}$  of 8. The scrubbing and strip performance in the previous testing was acceptable but had high cesium uncertainties.

In testing with the current samples in the shielded cells and utilizing the In-Cell Gamma Monitor, the data for the cesium behavior during the ESS testing are shown in Table 4 for the wastes collected from F-Area tanks (Tanks 26F, 46F and 34F). The extraction  $D_{Cs}$ 's for the tanks were  $12.7 \pm 0.14$ ,  $12.4 \pm 0.57$ , and  $11.3 \pm 0.14$  for Tank 26F (evaporator feed tank), Tank 46F (evaporator drop tank), and Tank 34F (concentrate storage). Additionally, the cesium accountability was much improved and was within 10 %.



Electronic Components located  
external to the Shielded Cell



Tungsten counting block  
located inside shielded transfer  
port within the Shielded Cells

**Figure 1. Photographs of In-Cell Gamma Monitor**

The scrubbing behavior was very repeatable for each of the batch tests for the two consecutive scrub steps. The distribution coefficient for the first scrub was between 1.64 and 1.86. Good agreement was obtained for each of the duplicate scrub tests for each of the tanks with the exception of Tank 34F where the difference for the averaged  $D_{Cs}$  value was high at 1.19. The value for the second scrub was always below 1 and ranged from 0.71 to 0.84. These distribution coefficients for scrubbing exceed the flowsheet basis of a value of greater than 0.6. This behavior, however, does not match with the simulant data of Klatt<sup>16</sup> where the second scrub results ranged between 1.16 and 1.91. The reduced scrub distribution coefficient will effectively lead to higher cesium concentrations in the extraction bank. In each of the scrubs the cesium accountability was within 5 %.

**Table 4. ESS Batch Distribution Data for the F-Area Waste Samples at 25 °C**

Tank 26F	Dcs	Std Dev	Cs Recovery	Std Dev
Extraction	12.7	0.14	105%	16
Scrub 1	1.83	0.33	101%	0.5
Scrub 2	0.79	0.02	104%	0.7
Strip 1	0.10	0.01	98%	1.1
Strip 2	0.094	0.01	97%	3.9
Strip 3	0.077	0.010	101%	1.1
Tank 46F	Dcs	Std Dev	Cs Recovery	Std Dev
Extraction	12.4	0.57	90%	0.21
Scrub 1	1.64	0.19	101%	1.5
Scrub 2	0.71	0.01	103%	1.1
Strip 1	0.10	0.023	99%	1.3
Strip 2	0.082	0.008	93%	3.2
Strip 3	0.073		102%	4.8
Tank 34F	Dcs	Std Dev	Cs Recovery	Std Dev
Extraction	11.3	0.14	94%	0.78
Scrub 1	1.86	1.19	101%	1.8
Scrub 2	0.84	0.06	102%	1.1
Strip 1	0.13	0.005	90%	0.5
Strip 2	0.07	0.001	98%	2.6
Strip 3	0.04	0.002	121%	10.8

The stripping distribution coefficients were acceptably low and well below the flowsheet requirement of less than 0.2. Previous testing had shown slightly higher values and it appears that the second scrub of the solvent neutralized the remaining caustic entrained in the solvent and allowed for efficient cesium stripping behavior. The first strip distribution coefficients were very low and near a value of 0.1. Again, with the exception of the third strip on the Tank 34F solvent samples the cesium radioactivity balance was very good.

#### *ESS Behavior of 3H Evaporator Sample*

On-going research programs in evaporator chemistry provided samples of supernate from the 3H Evaporator system (Tank 32H, feed tank and Tank 30H, drop tank). Only a limited quantity of material was obtained and this material had been passed through a 0.02  $\mu\text{m}$  filter prior to the ESS testing. Unfortunately, there was insufficient sample to proceed past the second scrub test with the Tank 30H sample. Additionally, the Tank 32H composite was not counted prior to allocating the sample for the extraction tests. Therefore cesium accountability could not be completed.

The extraction distribution coefficients (Table 4) exhibited some variance and measured 9.7 and 11.1 for feed tank (32H) and the drop tank (30H), respectively. This result is a little surprising considering the amount of recycle between tanks that occurs when the 3H Evaporator operates.<sup>17</sup> However, the extraction distribution coefficients are well above the flowsheet minimum of 8. The behavior during scrubbing also varied between the tanks. The scrubbing behavior for the Tank 32H sample was similar to the F-Area waste behavior previously discussed where the first scrub was near 1 and the second scrub value was below 1. In the data from the Tank 30H waste sample, both scrub measurements were above 1 and more in line with simulant measurements. The performance during stripping was acceptable for the sample from Tank 32H.

**Table 5. Batch Distribution Data for 3H Evaporator Tanks at 25 °C**

Tank 32H	Dcs	Std Dev	Cs Recovery	Std Dev
Extraction	9.7	0.00	*	*
Scrub 1	1.00	0.13	100%	0.4
Scrub 2	0.86	0.01	99%	0.6
Strip 1	0.17	0.018	97%	0.1
Strip 2	0.12	0.014	101%	3.9
Strip 3	0.068	0.001	94%	0.1
Tank 30H	Dcs	Std Dev	Cs Recovery	Std Dev
Extraction	11.1	0.00	103%	0.42
Scrub 1	1.48	0.00	101%	1.0
Scrub 2	1.7	0.01	101%	0.2
**				

\*Cs recovery not measured

\*\*Insufficient sample to continue testing

### *ESS Behavior of Dissolved Saltcake*

Cesium is stored in two forms, supernate and saltcake, in SRS high level waste tanks. Previous ESS testing<sup>6</sup> looked only at supernate and the discussion above has described additional results with supernate. Initial investigation by Walker<sup>7</sup> examined two samples of dissolved saltcake. In this work, two additional samples were obtained for testing. The first waste was a dissolved saltcake sample from Tank 37H that was processed through the 2-cm centrifugal contactor assembly in the Shielded Cells.<sup>18</sup> The second

sample<sup>15</sup> was from Tank 41H that was obtained after initial characterization supporting the Low Curie Salt process.<sup>19</sup>

The data shown in Table 6 for the ESS testing with the Tank 37H dissolved saltcake proved successful when compared to the flowsheet requirements of distribution coefficients of 8 for extraction, 0.6 for scrubbing and 0.2 for stripping. The extraction distribution coefficient was, however, lower than the values Walker<sup>7</sup> measured in saltcake samples from Tanks 38H and 46F. This may be an artifact of their solution chemistries. The chemistry of the Tank 37H saltcake showed higher levels of hydroxide than expected and higher than the samples tested by Walker.

Likewise, the ESS data for dissolved saltcake from Tank 41H was acceptable. The extraction distribution coefficient was slightly higher with an average value of 10.2. The values for the  $D_{Cs}$  for the scrub steps were above 1 and the sequential strip values were near 0.1 and below.

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**Table 6. ESS Data from Testing with Dissolved Saltcake**

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Tank 37H Saltcake	Dcs	Std Dev	Cs Recovery	Std Dev
Extraction	9.0		107%	0.28
Scrub 1	0.94	0.08	100%	0.1
Scrub 2	0.735	0.01	95%	3.9
Strip 1	0.1035	0.005	102%	0.3
Strip 2	0.075	0.003	89%	1.1
Strip 3	0.051	0.001	100%	5.3

Tank 41H Saltcake	Dcs	Std Dev	Cs Recovery	Std Dev
Extraction	10.2	0.28	78%	7.42
Scrub 1	1.065	0.19	98%	3.5
Scrub 2	1.215	0.01	100%	0.6
Strip 1	0.1055	0.008	99%	2.3
Strip 2	0.1095	0.018	103%	5.0
Strip 3	0.078	0.016	111%	3.6

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### *The Effect of Permanganate Addition on the ESS Behavior of Waste Supernate*

Two additional ESS tests were performed to ascertain if the addition of the oxidant sodium permanganate would have an effect during the downstream process of cesium removal by the CSSX process. The first waste type was a filtrate from a Cells Unit Filter (CUF) demonstration run of a permanganate process. The permanganate process is an alternative strontium and actinide removal flowsheet under consideration as a replacement of the baseline monosodium titanate (MST) adsorption process. It had been previously shown<sup>5</sup> that the MST process did not affect the cesium behavior during the

CSSX process. Therefore, an ESS test was conducted on a filtrate sample from a composite tank sample that received the permanganate treatment.<sup>14</sup> The second sample was from the same stock supernate prior to the addition of permanganate.

The behavior during the ESS testing for the permanganate-treated supernate (comprised of samples from Tanks 37H, 44F, 26F, and 46F) aligned well with the Tank 32H analysis results where the extraction distribution coefficient was near 9, as shown in Table 7. The value of the first scrub distribution coefficient was above 1 with the second value slightly below 1. The stripping performance was again very successful. Prior to the permanganate addition, the ESS performance was essentially the same with the exception of the extraction. Prior to permanganate addition, the extraction distribution coefficient was 10.2. Statistically, the extraction coefficients are different at 95 % confidence. However, there are several reasons that may explain this difference including the sodium ion concentration. Further discussion will be included in the next section of this report.

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**Table 7. ESS Data from Testing on the Effect of Permanganate Addition**

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Permanganate Filtrate	Dcs	Std Dev	Cs Recovery	Std Dev
Extraction	8.6	0.14	91%	0.78
Scrub 1	1.33	0.10	101%	0.3
Scrub 2	0.93	0.01	98%	0.0
Strip 1	0.14	0.04	102%	1.2
Strip 2	0.09		95%	4.9
Strip 3	0.065	0.003	113%	20
Before Permanganate	Dcs	Std Dev	Cs Recovery	Std Dev
Extraction	10.9	0.14	75%	6.36
Scrub 1	1.27	0.06	99%	1.1
Scrub 2	0.925	0.02	100%	1.1
Strip 1	0.12	0.01	98%	1.3
Strip 2	0.08	0.01	100%	3.0
Strip 3	0.0635	0.004	100%	0

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### *ESS Model Comparisons*

Delmau and coworkers<sup>9</sup> at Oak Ridge National Laboratory developed a multivariate thermodynamic model for predicting extraction behavior of cesium from solutions comprised of a number of species present in SRS waste. In 2002, the model<sup>10</sup> was extended to include behavior with the newly optimized solvent system and included additional species. The improved model was used to estimate the predicted extraction distribution coefficients for the wastes involved in this study. The data shown in Table 1

and Table 2 served as the basis for the chemical composition of the wastes. However, charge balance between the sum of cations and sum of anions was not satisfied. Therefore, slight changes in analyte concentrations were made prior to inputting the data into the thermodynamic model. Table 8 and Table 9 shows these chemical compositions.

**Table 8. Modified Tank Waste Chemical Compositions used for Thermodynamic Modeling**

Analyte	Units	Tank 26F	Tank 34F	Tank 46F	Tank 30H	Tank 32H	Permanganate Treated Waste Composite	Tank 37H Saltcake
Fluoride	mg/L	249		76				
Formate	mg/L	970	101	680				
Chloride	mg/L	224	197	201	152	50	293	320
Nitrite	M	0.44	0.64	0.62	0.65	0.80	0.70	0.82
Nitrate	M	1.00	1.14	1.12	0.65	1.40	0.87	0.8
Phosphate	mg/L	373	269	327	482	298	587	1900
Sulfate	M	0.03	0.01	0.01	0.004	0.02	0.004	0.005
Hydroxide	M	3.68	3.60	3.60	3.90	3.05	3.60	3.9
Carbonate	M	0.08	0.07	0.08	0.07	0.07	0.07	0.06
Potassium	M	0.030	0.038	0.034	0.039	0.032	0.037	0.039
Cesium	mM	0.029	0.029	0.029	0.120	0.132	0.032	0.34
Aluminate	M	0.25	0.28	0.28	0.40	0.50	0.30	0.54
Sodium	M	5.60	5.80	5.79	5.73	5.90	5.60	6.2

**Table 9. Modified Tank Waste Chemical Compositions from Tank 41H and Supernate Prior to Permanganate Treatment used for Thermodynamic Modeling**

Analyte	Units	Tank 41H Saltcake	Waste Composite Prior to Permanganate
Al	M	0.16	0.47
B	mg/L	70.56	4.75
Ca	mg/L	1.83	2.68
Cr	M	0.00	0.00
Cu	mg/L	2.06	1.54
Fe	mg/L	3.65	7.38
La	mg/L	0.69	0.82
Mo	mg/L	57.11	18.53
Na	M	5.13	5.20
P	M	0.002	0.002
Si	mg/L	17.36	34.04
Sn	mg/L	8.83	31.69
Sr	mg/L	0.66	15.26
Zn	mg/L	8.25	1.43
K	M	0.04	0.005
Cs	mM	0.17	0.04
Anions			
Nitrite	M	0.17	0.51
Nitrate	M	3.28	0.61
Sulfate	M	0.04	0.01
Hydroxide	M	0.66	3.29
Carbonate	M	0.41	0.15

The results of the modeling for the extraction distribution coefficients are shown in Table 10 and displayed in Figure 2. For four of the nine actual waste matrices the model prediction and the experimental measurement agree within ~ 10 %. The waste matrices are from Tanks 26F, 34F, 46F, and Tank 30H. For three waste matrices (Tank 32H, the permanganate-treated waste composite, and the dissolved saltcake from Tank 37H) the model prediction is higher by ~ 20 –30 %. The Tank 41H saltcake the model under predicts the cesium extraction behavior by 33%. The authors reviewed the waste compositional changes performed as discussed above for their impact, i.e., a sensitivity analysis, and the resultant variance remained. There are no obvious compositional aspects that lead to the observed variance.

However, in one instance (the supernate prior to permanganate treatment) the model and experiment differ substantially. The model prediction for the cesium extraction distribution coefficient was 25.1 and the measured value was 10.9. Examination of the chemical composition both measured and modeled indicated a very low potassium concentration in this waste (5 mM) as compared to the after treated supernate (~ 35 mM). As well documented, the potassium concentration in the waste can drive the model prediction for the extraction behavior. In this instance, the measured potassium level appears low even though measured in duplicate. This statement concerning the potassium concentration is made based on the general agreement of the model and experiment within  $\pm 30$  % for other samples tested herein.

Therefore, in order to determine if the addition of sodium permanganate to the waste adversely impacts the CSSX process, the cesium extraction behavior was modeled on a more consistent potassium level. The modeled chemical compositions for the supernate after permanganate addition showed that the model prediction was ~ 25 % higher than measurement. Prior to permanganate treatment, if one further modified the chemical composition to include potassium ion at a concentration of 30 mM, a direct comparison can be made. Table 10 includes this prediction for the extraction distribution coefficient,  $D_{Cs}$ , for the supernate composite prior to permanganate addition with the K level at 30 mM and the value is 13.8. The difference between the predicted and measured  $D_{Cs}$  is ~ 20%. Although this comparison is not perfect, one would come to the conclusion that the permanganate treatment did not have a very large impact on the cesium extraction in the CSSX process.

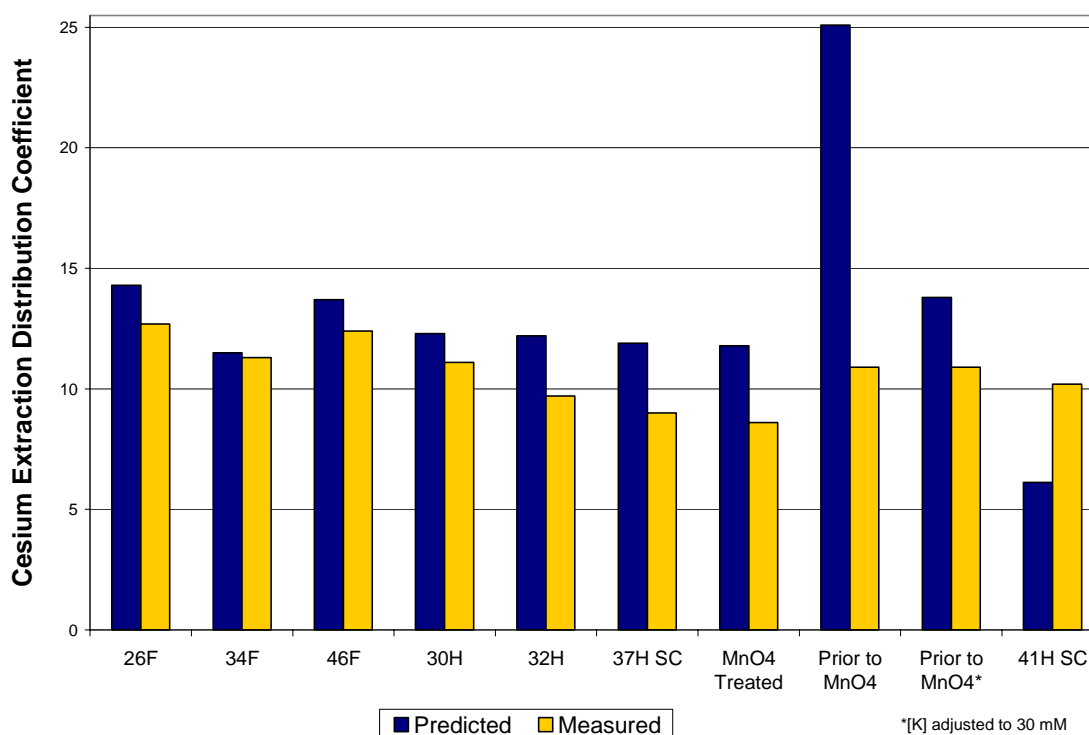


**Table 10. Comparison of Predicted and Measured Extraction  $D_{Cs}$**

	Predicted	Measured
26F	14.3	12.7
34F	11.5	11.3
46F	13.7	12.4
30H	12.3	11.1
32H	12.2	9.7
37H SC	11.9	9
41H SC	6.12	10.2
MnO <sub>4</sub> Treated	11.8	8.6
Prior to MnO <sub>4</sub>	25.1	10.9
Prior to MnO <sub>4</sub> *	13.8	10.9

SC = Saltcake

\* K concentration set at 30 mM



**Figure 2. Graphical Representation of Modeled and Measured Extraction Distribution Coefficients**

## **Conclusions**

The CSSX process has been shown to effectively remove cesium for SRS high level wastes and provide the vitrification facility with a concentrated stream for coupled operations. Technical uncertainty exists due to the limited testing of the proposed flowsheet with actual waste. Therefore, an additional set of batch distribution tests of the CSSX process was performed with samples of supernate from the F- and H-Area tanks. Additionally, tests were performed with dissolved saltcake from Tank 37H and Tank 41H. Furthermore, tests examining the effect of the permanganate treatment for removing the actinide components were conducted and indicate little effect of the addition of permanganate.

Changes were executed in the experimental methodology used in the batch testing to improve experimental precision, reduce sample removal and lower cost. These changes produced an ESS protocol that reproducibly gave good cesium accountability. The measured performance for cesium using the newly optimized solvent system showed acceptable cesium behavior during the extraction, scrubbing and stripping steps in the CSSX processing. This indicates that the CSSX process will effectively decontaminate the high level waste and provide an adequately concentrated stream to DWPF.

The results also showed that the improved thermodynamic model predicts the cesium behavior during extraction. Moreover, the testing showed acceptable cesium behavior for two other actual tank waste matrices. These matrices included dissolved saltcake and permanganate-treated supernate. These results continue to show the need for accurate measurement of the soluble cesium and potassium concentrations to allow for direct comparisons to the thermodynamic model.

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