

## Pore Connectivity Effects on Solute Transport in Rocks

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### Abstract

Retardation of nuclear contaminants in rock matrices can lead to long retention times, allowing substantial radionuclide decay prior to eventual release. Imbibition and diffusion into the rock matrix can move contaminants away from an active fracture, thereby contributing to their retardation. However, diffusive transport in some rocks may behave anomalously because of their sparsely connected porespace, in contrast to diffusion in rocks with denser pore connections. We examined imbibition of weakly sorbing tracers into welded tuff and Indiana sandstone, and water imbibition into metagraywacke and Berea sandstone. Tuff samples were initially equilibrated to 12% and 76% water (v/v) within controlled humidity chambers, while the other rocks were air-dried. For imbibition, one face was exposed to water, with or without tracer, and uptake was measured over time. Following imbibition, tracer concentration measurements were made at fine (1 mm) increments. Three anomalous results were observed: (1) Indiana sandstone and metagraywacke showed mass of imbibed water scaling as  $\text{time}^{0.26}$ , while tuff and Berea sandstone showed the more classical scaling with  $\text{time}^{0.5}$ ; (2) tracer movement into dry (2% initial saturation) Indiana sandstone showed a dispersion pattern similar to that expected during tracer movement into moist (76% initial saturation) tuff; and (3) tracer concentrations at the inlet face of the tuff sample were approximately twice those deeper inside the sample. The experiment was then modeled using random walk methods on a 3-D lattice with different values of pore coordination. Network model simulations that used a pore coordination of 1.49 for Indiana sandstone and 1.56 for metagraywacke showed similar temporal scaling, a result of their porespace being close to the percolation threshold. Tracer concentration profiles in Indiana sandstone and tuff were closely matched by simulations that used pore coordinations of 1.49 and 1.68, respectively, because of how low connectivity alters the accessible porosity in the vicinity of the inlet face. The study supports pore connectivity as a coherent explanation for the observed anomalies and demonstrates the utility of pore-scale modeling in elucidating mechanisms critical to radionuclide retardation in geological repositories.

## 1 Introduction

2 Conservative assessment of the long-term fate of radioactive waste assumes that some leakage  
3 from the waste packages will occur. An appropriate design strategy is to assure that migration of  
4 leaking materials is slow enough that considerable radioactive decay will occur during the  
5 leakage and migration phase. To this end, waste may be confined in rock repositories, because  
6 diffusion into and through rock is relatively slow, thus assuring the needed time. Such a strategy  
7 is used in the potential high-level nuclear waste repository at Yucca Mountain, NV, USA.

8  
9 The picture at Yucca Mountain, and in rocks generally, is complicated by the presence of  
10 fractures. These fractures can function as high-velocity flow pathways, with solutes being both  
11 dispersed and retarded via diffusive exchange between the fracture and the rock matrix. If the  
12 matrix is even slightly below saturation, imbibition from active fractures will augment the  
13 diffusive movement of solutes from fracture to matrix. Accurate assessment of rock matrix  
14 imbibition and diffusion is therefore a key issue in evaluating an unsaturated repository site.

15  
16 It is well established that diffusion and dispersion are often scale-dependent (Tyler and  
17 Wheatcraft, 1988; Berkowitz and Scher, 1998). Most explanations of this phenomenon invoke  
18 increasing heterogeneity at increasing scales, but such heterogeneity is not always observed. A  
19 different explanation was recently advanced by Ewing and Horton (2002a,b), who showed  
20 through pore-scale diffusion modeling that low connectivity at the pore scale could lead to  
21 diffusivity decreasing with increasing time and/or distance. In essence, low connectivity can  
22 cause increasing heterogeneity of flowpaths at increasing scales, even though the connectivity  
23 itself, as well as macroscopic properties such as porosity, may be spatially homogeneous.

24  
25 Imbibition of water from active fractures into an unsaturated matrix can be a critical contributor  
26 to solute exchange between fracture and matrix. Furthermore, imbibition is mathematically a  
27 diffusive process, so its behavior should be related to diffusive behavior. Hu et al. (2002 and  
28 unpublished results) examined imbibition of tracer-laced water into rocks, and observed three  
29 apparently anomalous results: first, while the imbibition front is generally expected to advance in  
30 proportion to the square root of time (Philip, 1957), in some rocks an advance approximately  
31 proportional to the fourth root of time is observed. Second, while a tracer concentration profile is  
32 expected to resemble the saturation profile during imbibition into initially dry media but show  
33 greater dispersion during imbibition into wet media, high apparent dispersion was observed  
34 during imbibition into initially air-dry Indiana sandstone. And third, an apparently anomalous  
35 increase in porosity was observed at the inlet face during imbibition into welded tuff, even

1 though this face was prepared from the inside of a solid sample rather than from a weathered  
2 fracture face.

3

4 The objective of this research was to investigate pore connectivity as a potential cause of these  
5 three anomalous observations, through comparison of laboratory imbibition experiments with  
6 pore-scale imbibition simulations.

7

#### 8 **Methods:**

9 Rocks used were welded tuff, Berea sandstone, Indiana sandstone, and metagraywacke. Rock  
10 properties are summarized in Table 1. The imbibition protocols are described by Hu et al.  
11 (2001). Briefly, cylindrical rock cores (2 cm length, 5 cm diameter) with epoxy-coated sides and  
12 exposed top and bottom faces are equilibrated in controlled humidity chambers to the desired  
13 water contents, approximately 2% (air-dry), 12.5%, and 76% saturation. They are then  
14 suspended, from an analytical balance, in a chamber with a water pan, such that the bottom face  
15 of the core contacts the free water surface. Balance readings are initially recorded at 3 s  
16 intervals, with time intervals increasing over the duration of the experiment. Imbibition is  
17 calculated from the cumulative change in suspended mass over time, with corrections for  
18 buoyancy resulting from changes in the water level caused by both imbibition and evaporative  
19 losses from the chamber (Hu et al., 2001). For welded tuff and Indiana sandstone, the procedure  
20 was modified by the addition of multiple tracers (bromide [nonsorbing], Sulpho-Rhodamine B  
21 [sorption coefficient 0.09 mL/g], and FD&C Blue #1 [sorption coefficient 0.06 mL/g]) to the  
22 water. Upon completion of the imbibition phase of the experiment, small holes were drilled into  
23 the cores from both the inlet and air-exit faces, with rock powder sampled at 1 mm depth  
24 intervals. Tracer concentrations in the rock powder were measured using an ion-specific  
25 electrode (bromide), a fluorometer (Sulpho-Rhodamine B), or a UV/Vis spectrophotometer  
26 (FD&C Blue #1). Further details concerning rock drilling and analysis of tuff can be found in Hu  
27 et al. (2002).

1 Table 1. Properties of the rocks used.

2	Rock	% Porosity	Permeability, m <sup>2</sup>	% Initial Saturation	Tracers	Source
4	Berea Sandstone	22.8	9.1 * 10 <sup>-13</sup>	Air-dry*	None	Berea Quarry, OH, USA
6	Indiana Sandstone	17.6	1.8 * 10 <sup>-13</sup>	Air-dry*	Bromide FD&C Blue #1 Sulpho- Rhodamine B	Gas Storage Formation, IN, USA
8	Welded Tuff	9.25	5.0 * 10 <sup>-19</sup>	12.5	Bromide FD&C Blue #1 Sulpho- Rhodamine B	Potential high-level nuclear waste repository, Yucca Mtn., NV, USA (Hu et al., 2002)
9				76.0		
10	Meta-graywacke	3.85	1.2 * 10 <sup>-17</sup>	Air-dry*	None	The Geysers, CA, USA (Persoff and Hulen, 2001)

12 \*: Air-dry was assumed to be 2% saturation

14 The pore-scale modeling conceptualizes the rock matrix as an assemblage of pore bodies  
 15 connected by pore throats. Rocks with well-interconnected porespace, such as non-cemented  
 16 sandstones, have coordination (mean number of pore bodies to which each body is connected) in  
 17 the range of  $z = 4-8$  (Lin and Cohen, 1982; Yanuka et al., 1984). Note that the coordination  
 18 number given applies to the entire network: even at the percolation threshold, pores that are part  
 19 of the “infinite cluster” have on average a coordination number no less than 2.0 (Ewing and  
 20 Horton, 2002a). We used a cubic lattice ( $z = 6$ ) and pruned connections at random to arrive at  
 21 the desired coordination. Because our interest was in exploring the effects of pore connectivity,  
 22 in this study we ignore issues such as pore size. Related stochastic process models that focus on  
 23 medium properties other than the pore size distribution have been described by Flury and Flüher  
 24 (1995), Trantham and Durnford (1999), and Ewing and Horton (2002a,b).

26 The stochastic process model anti-DLA (anti-Diffusion-Limited Aggregation; also called internal  
 27 DLA; see Paterson, 1984; Meakin and Deutch, 1986) has been identified as an analog for stable  
 28 displacement during imbibition (Lenormand, 1990). The choice of anti-DLA as the underlying  
 29 imbibition model in this research is justified by the observations that imbibition upward is  
 30 gravity-stabilized, the viscosity ratio is positive, and imbibition into low aspect ratio media  
 31 generally shows a stable front at almost any capillary number (Lenormand, 1990). In anti-DLA,

1 a random walker starts at a source location within phase A and diffuses until it reaches a phase B  
2 point, whereupon it stops, converting that point to A. As applied to our physical situation, free  
3 water at the inlet face of the core is the source point, and a random walker diffuses through  
4 water-filled pores into the core. Upon reaching a pore that is not occupied by water, it fills the  
5 pore, and a new walker is initiated. The anti-DLA model is diffusion based, so (for example)  
6 scaling of cumulative imbibed mass with the square root of time is an expected macroscopic  
7 behavior, although it is not explicitly programmed to occur.

8

9 In this model, random walkers cannot move across connections that have been pruned.  
10 Antecedent saturation is included simply by marking some proportion of the matrix pores as  
11 water-filled at the outset. Progress of the imbibition process is recorded whenever 100 particles  
12 have imbibed, and a saturation profile is written when the wetting front first touches the far end  
13 of the lattice. Modeling the placement of retarding tracers takes into account both the retardation  
14 factor and the antecedent saturation. Specifically, tracers were emplaced as the average of (1) the  
15 final position of a water molecule divided by the retardation factor, weighted by antecedent  
16 unsaturation, and (2) the  $(\text{total time}/\text{retardation}^2)^{\text{th}}$  position of a diffusing water molecule,  
17 weighted by antecedent saturation. We used a 100 x 50 x 50 site lattice, emplacing 10,000 tracer  
18 molecules per realization and averaging results over five realizations.

19

## 20 **Results and Discussion**

### 21 1. Temporal Behavior of Imbibition

22 The absolute rates of imbibition are functions of the pore size distribution and porosity, and do  
23 not concern us here. Imbibition into Berea sandstone and welded tuff scaled with the square root  
24 of time (Figure 1), as is generally expected (Philip, 1957). However, imbibition into  
25 metagraywacke (early time only) and Indiana sandstone scaled approximately with  $\text{time}^{0.26}$ . This  
26 scaling result matches predictions of percolation theory (Stauffer and Aharony, 1992) for 3-D  
27 diffusion at the percolation threshold, the coordination at which a sparsely connected porespace  
28 is only just connected.

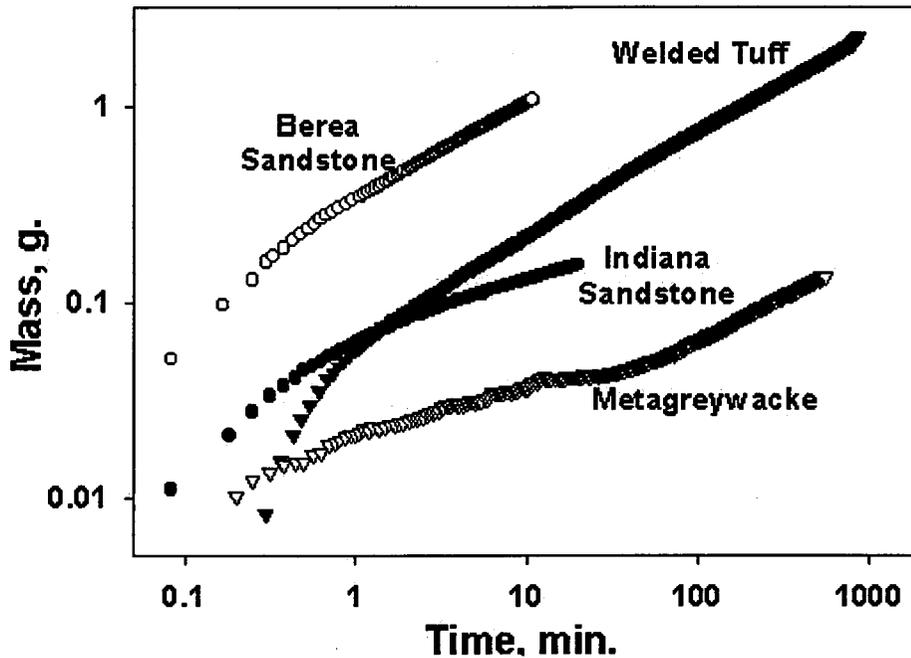


Figure 1. Experimental results showing cumulative imbibition into Berea sandstone, Indiana sandstone, welded tuff, and metagraywacke.

Simulations of imbibition match the experimental data well, showing an initially steep period (rapid wetting of the inlet face) followed by a fairly straight section (Figure 2). The slope of the straight section is 0.5 at high ( $z > 1.68$ ) connectivities. Progressively lower pore coordination results in a lower imbibition rate, and eventually a change in the temporal scaling. Notice that at low but noncritical values of connectivity ( $z = 1.56$ ), the slope soon stabilizes at a slope of 0.26, then eventually reverts to 0.5. Likewise, the imbibition plot of metagraywacke (Fig. 1) suggests that around 50 minutes, it undergoes a gradual transition from short term, 0.26-slope behavior to longer-term, 0.5-slope behavior. A similar transition, from 0.26-slope at early times to 0.50-slope at later times, was observed by Ewing and Horton (2002a) for diffusion in lattices slightly above criticality. Pore connectivity therefore provides a simple, unified explanation for the observed anomaly.

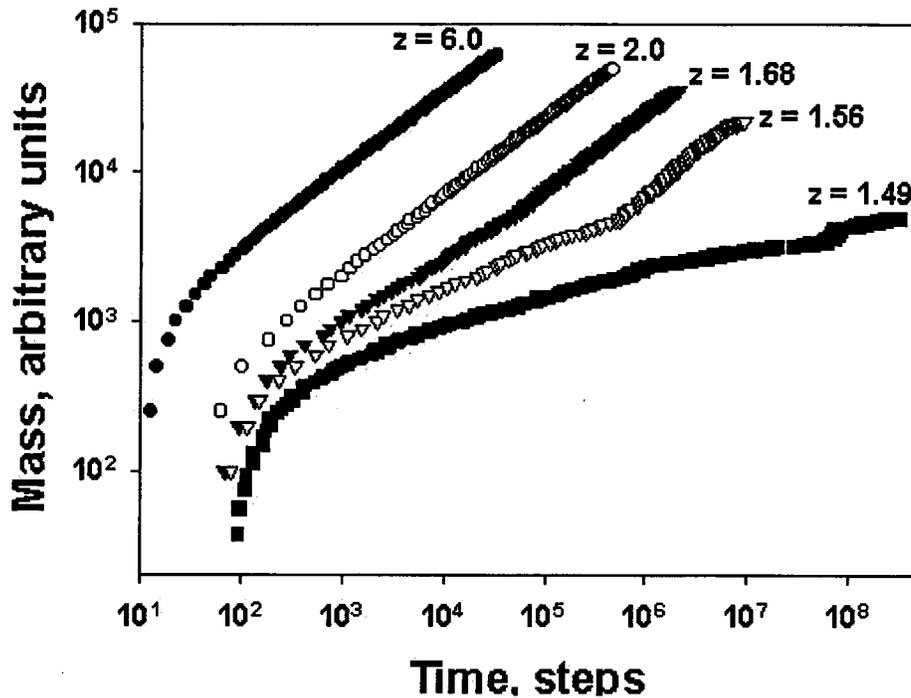


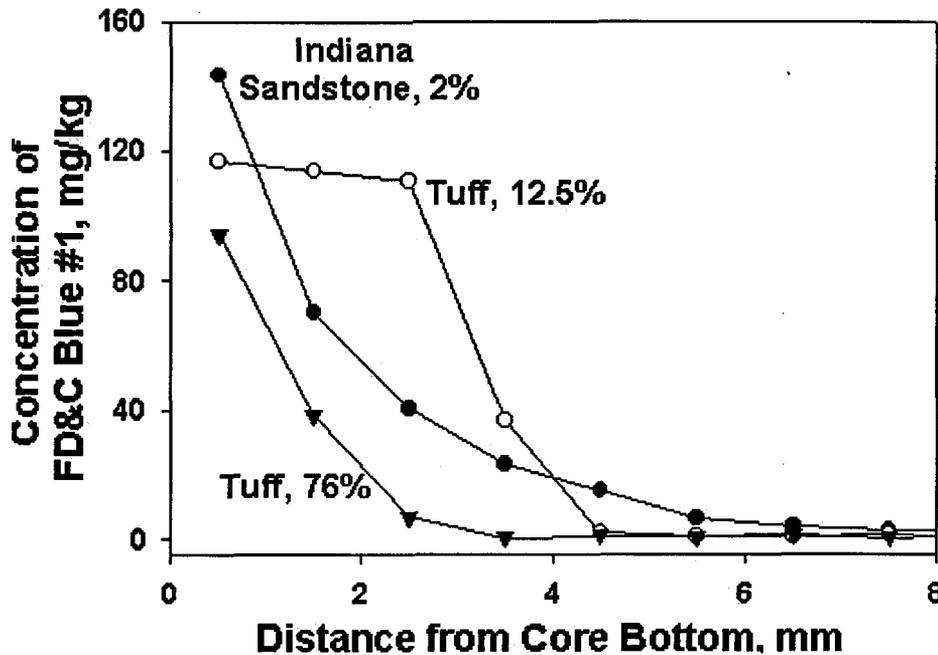
Figure 2. Simulation of cumulative imbibition over a range of pore coordinations.

## 2. Tracer Dispersion with Initial Saturation

During imbibition into a dry medium, a solute concentration profile typically will resemble the saturation profile, with retardation changing the position but not the shape of the profile. In contrast, during imbibition into a moist medium, solutes will disperse by mixing with “old” water, and so a less sharp profile would generally be observed. These trends are illustrated for the case of dye imbibition into welded tuff, where a more dispersed distribution is observed 76% than at 12.5% initial saturation (Figure 3). However, against usual expectations, tracer concentration profiles for dye imbibition into air-dry Indiana sandstone show the high-dispersion pattern seen with imbibition into moist (76% initial saturation) tuff.

Simulations using a pore coordination of  $z = 1.49$  (at the percolation threshold) for “Indiana sandstone” and  $z = 1.68$  for “welded tuff” (Figure 4) show a pattern similar to those observed experimentally (Figure 3). The tracer concentration profile following simulated imbibition into the dry “tuff” is similar to the wetting front after adjustment for retardation (not shown), while that following simulated imbibition into the moister “tuff” shows more retardation and dispersion. This indicates that the particle emplacement algorithm gives the correct behavior with

1 respect to antecedent saturation. Of greater interest is that the tracer profile in the simulated  
 2 Indiana sandstone also matches the experimental data fairly well. The explanation for this tracer  
 3 profile in the "Indiana sandstone" lies not in dispersion mechanisms, but in the spatial  
 4 distribution of accessible porosity in a low-coordination porous medium.



26 Figure 3. Concentration profiles of a weakly sorbing dye following imbibition into welded tuff  
 27 (12.55 and 76% initial saturation) and air-dry Indiana sandstone. Data for Bromide and Sulpho-  
 28 Rhodamine B (not shown) exhibit similar behavior.

30 Recall that the Indiana sandstone core showed an imbibition plot slope of 0.26, in contrast to the  
 31 more classical 0.5; an explanation can therefore be based on Indiana sandstone being at the  
 32 percolation threshold. Near and at the percolation threshold, the porosity accessible from one  
 33 end varies as a function of distance from the exposed face (Ewing and Horton, 2002b). This  
 34 phenomenon is illustrated by the dotted lines in Figure 5, showing accessible porosity from 5  
 35 realizations on a cubic lattice at two different coordinations, scaled to match the Indiana  
 36 sandstone bromide curve. The agreement between the two curves supports low pore connectivity  
 37 as a reasonable explanation. In other words, the tracer profile in the Indiana sandstone is caused  
 38 not by dispersion, but rather by the accessible porosity.

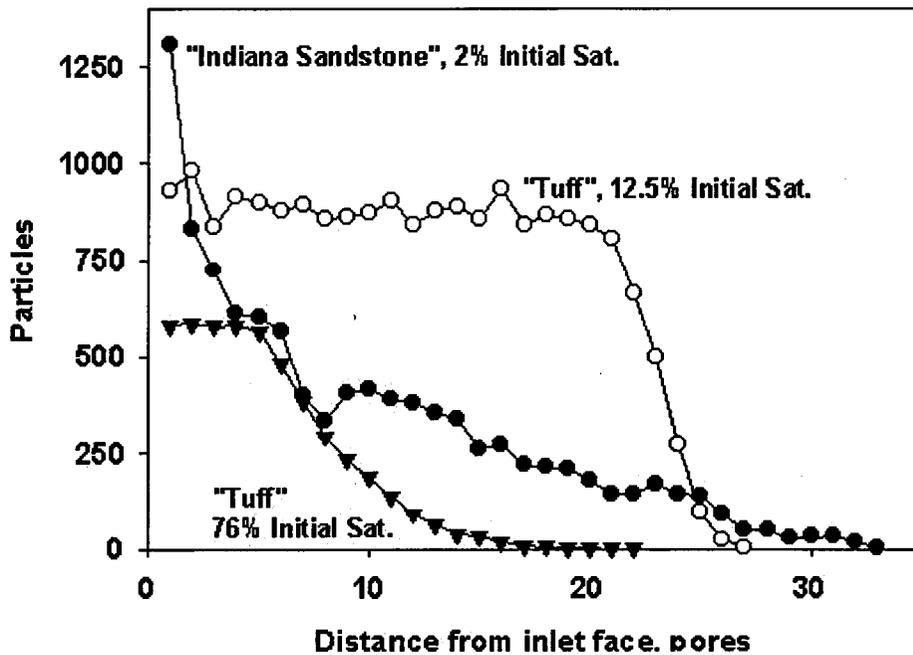


Figure 4. Simulated concentration profiles of dyes following imbibition.

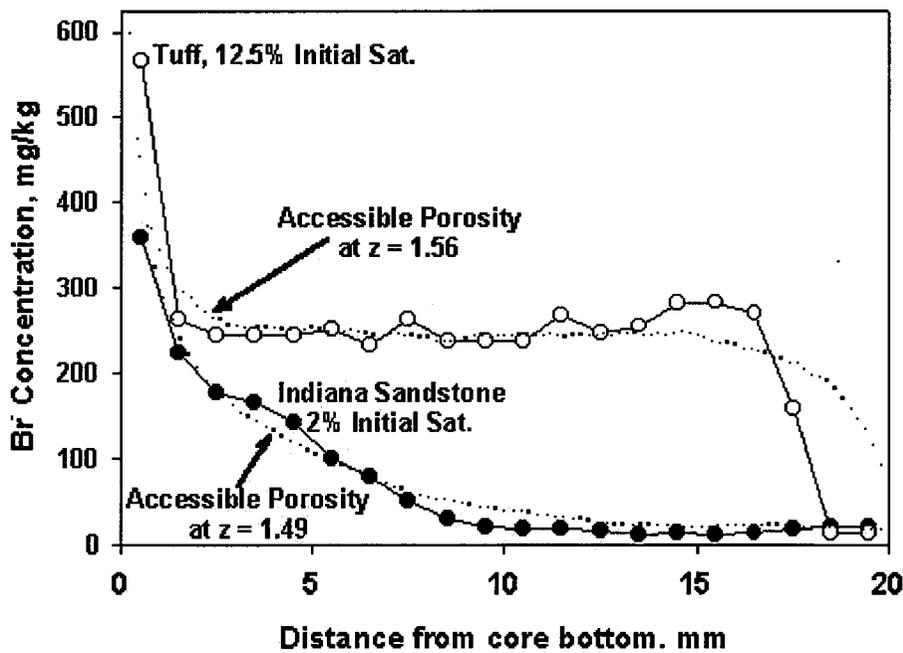


Figure 5. Concentration profiles of bromide following imbibition into welded tuff (12.5% initial

1 saturation) and air-dry Indiana sandstone. Dotted lines show theoretical predictions of accessible  
2 porosity (normalized to the bromide concentrations) at coordination numbers of 1.49 (for Indiana  
3 sandstone) and 1.56 (for tuff).  
4

### 5 3. Tracer Concentrations at the Fracture Face

6 In several of the welded tuff cores with initial saturation of 12.5%, bromide concentration in the  
7 millimeter closest to the inlet end was approximately twice the concentration through the rest of  
8 the core (Figure 5). This might initially have been thought a measurement error had it not been  
9 observed in multiple cores, with proportions of edge to plateau concentration ranging from 1.45  
10 to 2.17. Again, pore connectivity considerations can explain the disparity. As with the tracer  
11 concentration profile in Indiana sandstone, it appears that the apparently anomalous reading at  
12 the inlet end is an artifact of differences in accessible porosity with position. The difference  
13 between coordination numbers of 1.56 and 1.49 appears quite small, but the difference in the  
14 corresponding accessible porosity profiles is dramatic (Fig. 5). Again, pore connectivity  
15 provided a simple and coherent explanation for the observed anomalies.  
16

### 17 **Conclusions**

18 We examined imbibition and/or tracer concentration profiles in four rocks, and simulated several  
19 of the tracer imbibition experiments to more closely examine results that appeared anomalous.  
20 Pore connectivity near or at the percolation threshold appeared to be the root cause in all cases,  
21 explaining the anomalous temporal scaling of cumulative imbibition in Indiana sandstone and  
22 metagraywacke, the apparent dispersion during imbibition into air-dry Indiana sandstone, and the  
23 high tracer concentrations at the inlet edge of welded tuff. The anti-DLA-based imbibition  
24 model matched experimental results quite well, giving us a useful new simulation tool and  
25 helping to evaluate a simple and consistent explanation for the observed anomalies.  
26

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