

L.H. Q. S
MAY 15 2000

ENGINEERING DATA TRANSMITTAL

Page 1 of 1
1. EDT 623381

2. To: (Receiving Organization) Distribution		3. From: (Originating Organization) RPP Radiological Control		4. Related EDT No.: N/A	
5. Proj./Prog./Dept./Div.: Radiological Engineering		6. Design Authority/Design Agent/Cog. Engr.: D. J. Foust		7. Purchase Order No.: N/A	
8. Originator Remarks: "Radiological Design Review Screening - Saltwell Pumping at 241-U-106 Distributor Pit" is being issued as RPP-6307.				9. Equip./Component No.: N/A	
11. Receiver Remarks: 11A. Design Baseline Document? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No				10. System/Bldg./Facility: RPP/241-U-106	
				12. Major Assm. Dwg. No.: N/A	
				13. Permit/Permit Application No.: N/A	
				14. Required Response Date: N/A	

15. DATA TRANSMITTED					(F)	(G)	(H)	(I)
(A) Item No.	(B) Document/Drawing No.	(C) Sheet No.	(D) Rev. No.	(E) Title or Description of Data Transmitted	Approval Designator	Reason for Transmittal	Originator Disposition	Receiver Disposition
1	RPP-6307	N/A	0	Radiological Design Review	N/A	3	1	
				Screening - Saltwell				
				Pumping at 241-U-106				
				Distributor Pit				

16. KEY		
Approval Designator (F)	Reason for Transmittal (G)	Disposition (H) & (I)
E, S, Q, D OR N/A (See WHC-CM-3-5, Sec. 12.7)	1. Approval 2. Release 3. Information 4. Review 5. Post-Review 6. Dist. (Receipt Acknow. Required)	1. Approved 2. Approved w/comment 3. Disapproved w/comment 4. Reviewed no/comment 5. Reviewed w/comment 6. Receipt acknowledged

17. SIGNATURE/DISTRIBUTION (See Approval Designator for required signatures)											
(G) Reason	(H) Disp.	(J) Name	(K) Signature	(L) Date	(M) MSIN	(G) Reason	(H) Disp.	(J) Name	(K) Signature	(L) Date	(M) MSIN
		Design Authority	N/A								
		Design Agent	N/A								
1	1	Cog. Eng.	D. J. Foust	<i>David Foust</i>	5/8/00						
		Cog. Mgr.	N/A								
		QA	N/A								
		Safety	N/A								
		Env.	N/A								

18. <i>David Foust</i> D. J. Foust Signature of EDT Originator Date: 5/8/00		19. N/A Authorized Representative for Receiving Organization Date:		20. <i>W. Gray</i> W. Gray Design Authority/Cognizant Manager Date: 5/8/00		21. DOE APPROVAL (if required) Ctrl No. N/A <input type="checkbox"/> Approved <input type="checkbox"/> Approved w/comments <input type="checkbox"/> Disapproved w/comments	
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Radiological Design Review Screening - Saltwell Pumping at 241-U-106 Distributor Pit

D. J. Foust

CH2M Hill Hanford Group Inc.

Richland, WA 99352

U.S. Department of Energy Contract DE-AC06-99RL14047

EDT/ECN: EDT-623381

UC: 2080

Cost Center: 79700

Charge Code: 110641

B&R Code: N/A

Total Pages: 7

Key Words:

241-U-106; Saltwell; Radiological Design Review; Steel Cover Plate;
Cover Block; Distributor Pit

Abstract:

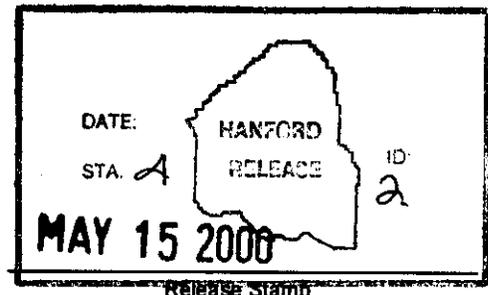
This document provides the radiological design review screening for the 241-U-106 distributor pit cover block replacement with a steel cover plate.

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5/11/00
Date

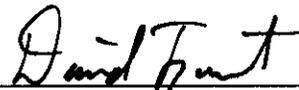


Approved For Public Release

RPP-6307
Revision 0

**Radiological Design Review Screening –
Saltwell Pumping at 241-U-106 Distributor Pit**

Prepared
by:

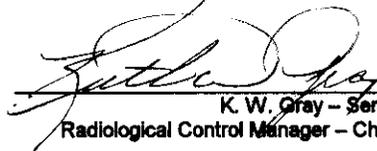


5/8/00

D. J. Foust – Senior Health Physicist
RPP Radiological Engineering & Technical Support

Date

Reviewed
by:



5/8/00

K. W. Gray – Senior Health Physicist
Radiological Control Manager – Characterization & Stabilization Projects

Date

CH2M Hill Hanford Group Incorporated

May 5, 2000

Scope

This document provides the calculated basis for the level of radiological design review¹ required for the replacement of the existing 241-U-106 distributor pit 61 cm (24 inch) concrete cover block with one of the following options in order of priority:

- 5.1 cm (2") steel plate
- 7.6 cm (3") steel plate

The determination of the expected dose rate over the 241-U-106 distributor pit after the installation of various options is described. The existing concrete cover block must be replaced to facilitate access to the pit for saltwell pumping operations.

Also determined is the lifecycle dose differential due to this facility modification.

1. Calculations:

1.1. Baseline Dose Rate Determination

Based on current radiological survey report², without the saltwell screen installed, the maximum unshielded penetrating whole body dose rate over the distributor pit is 200 mrem/hr. Installation of the saltwell screen will reduce this dose rate to approximately 13 mR/hr as calculated by MicroShield³ (Attachment 1), and installation of the saltwell pump will further reduce this dose rate primarily due to shielding provided by the 2.5 cm (1 inch) steel base plate of the pump. The dose rate with the pump installed is determined as follows:

- The majority of the penetrating radiation from the distributor pit is due the 0.662 Mev gamma emitted by the ^{137m}Ba daughter of ¹³⁷Cs.⁴
- The half-value layer for ¹³⁷Cs in iron is approximately 1.9 cm (0.75 inch).⁵

$Dose\ Rate_{max\ shielded} = Dose\ Rate_{max\ unshielded} \times (.5)^n$ where n = number of half-value layers

$$n = \frac{2.5\ cm}{1.9\ cm} = 1.3$$

$$Dose\ Rate_{max\ pump\ installed} = \frac{13\ mrem}{hr} \times (.5)^{1.3} = \frac{5\ mrem}{hr}$$

Initiation of pumping activities will increase this dose rate. Previous experience with pumping activities indicates that dose rates may increase by as much as 300 mrem

¹ RPP-MD-010, Rev. 0, December 22, 1999

² IS001842, page 1, Item No. 1

³ MicroShield is a registered trademark of Grove Engineering Inc.

⁴ HNF-SD-WM-ER-636

⁵ Shleien, page192

per hour⁶ with the commencement of pumping. Because the specific activity of ¹³⁷Cs is lower in U-106 than in the typical tank, pumping is estimated to increase the dose rate in the pit by no more than 200 mrem/hr. This would make the dose rate in the pump pit 205 mrem per hour during pumping operations.

The estimated calculated dose rate over a 5.1 cm (2") steel cover plate when the pump is not in operation is as follows:

$$Dose\ Rate_{max\ pump\ not\ in\ operation} = \frac{5\ mrem}{hr} \times (.5)^{\frac{5.1}{1.9}} = \frac{1\ mrem}{hr}$$

The estimated calculated dose rate over the pit with a total of 7.6 cm (3") of steel cover plate when the pump is not in operation is as follows:

$$Dose\ Rate_{max\ pump\ not\ in\ operation} = \frac{5\ mrem}{hr} \times (.5)^{\frac{7.6}{1.9}} = \frac{.3\ mrem}{hr}$$

The estimated calculated dose rate over the 5.1 cm (2") steel cover plate during pumping operations is as follows:

$$Dose\ Rate_{max\ pump\ in\ operation} = \frac{205\ mrem}{hr} \times (.5)^{\frac{5.1}{1.9}} = \frac{32\ mrem}{hr}$$

The calculated dose rate over the pit with a total of 7.6 cm (3") of steel cover plate during pumping operations is as follows:

$$Dose\ Rate_{max\ pump\ in\ operation} = \frac{205\ mrem}{hr} \times (.5)^{\frac{7.6}{1.9}} = \frac{13\ mrem}{hr}$$

1.2. Life Cycle Exposure Differential

- Maximum personnel occupancy over the pump pit cover is estimated to be 5 minutes (0.08 hr) per week while pumping is in progress and 25 minutes (0.4 hr) per week when the pump is not in operation.⁷
- U-106 pumping schedule is 9 mo.⁸ (39 weeks)
- Half-value layer for ¹³⁷Cs of concrete cover block to be replaced by the carbon steel plates is 7.0 cm⁹.
- Thickness of concrete cover block to be replaced is 61 cm (24").¹⁰

$$n = \frac{61\ cm}{7.0\ cm} = 8.7$$

The calculated dose rate over the existing 61 cm (24") concrete cover block while the pump is not in operation would be as follows:

⁶ Craft, September 1998

⁷ McVey, January 1999

⁸ Jaka, April 6, 2000

⁹ Shleien, page 192

¹⁰ Jaka, April 6, 2000

$$Dose\ Rate_{ConcreteShielded} = \frac{5\ mrem}{hr} \times (.5)^{8.7} = \frac{0\ mrem}{hr}$$

The calculated dose rate over the existing 61 cm (24") concrete cover block while the pump is operating would be as follows:

$$Dose\ Rate_{ConcreteShielded} = \frac{205\ mrem}{hr} \times (.5)^{8.7} = \frac{0.5\ mrem}{hr}$$

The net change in dose rate due to the installation of the 5.1 cm (2") steel cover plate while the pump is not in operation is as follows:

$$\frac{1\ mrem}{hr} - \frac{0\ mrem}{hr} = \frac{1\ mrem}{hr}$$

The net change in dose rate due to the installation of the 5.1 cm (2") steel cover plate while the pump is in operation is as follows:

$$\frac{32\ mrem}{hr} - \frac{0.5\ mrem}{hr} = \frac{31.5\ mrem}{hr}$$

The net change in dose rate due to the installation of the 7.6 cm (3") steel cover plate while the pump is not in operation is as follows:

$$\frac{0.3\ mrem}{hr} - \frac{0\ mrem}{hr} = \frac{0.3\ mrem}{hr}$$

The net change in dose rate due to the installation of the 7.6 cm (3") steel cover plate while the pump is in operation is as follows:

$$\frac{13\ mrem}{hr} - \frac{0.5\ mrem}{hr} = \frac{12.5\ mrem}{hr}$$

The total change in dose due to the replacement of the concrete cover blocks with the 5.1 cm (2") steel cover plate would be as follows:

$$\left[\left(\frac{31.5\ mrem}{hr} \times \frac{0.08\ hr}{week} \right) + \left(\frac{1\ mrem}{hr} \times \frac{0.4\ hr}{week} \right) \right] \times 39\ weeks = 114\ person - mrem$$

The total change in dose due to the replacement of the concrete cover blocks with the 7.6 cm (3") steel cover plate would be as follows:

$$\left[\left(\frac{12.5\ mrem}{hr} \times \frac{0.08\ hr}{week} \right) + \left(\frac{0.3\ mrem}{hr} \times \frac{0.4\ hr}{week} \right) \right] \times 39\ weeks = 44\ person - mrem$$

Since the pit cover must be removed and replaced as a normal part of saltwell pump installation, no additional exposure will be incurred as a result of installation and removal of the steel cover plate.

2. Conclusion

The calculated exposure increase due to the proposed installation of the 5.1 cm (2") carbon steel cover plate is 114 person-mrem for the life cycle of the project. The calculated exposure increase due to the proposed installation of the 7.6 cm (3") carbon steel cover plate is 44 person-mrem for the life cycle of the project. For these options, the calculated lifecycle exposure change is less than ±one person-rem. This calculated exposure is based on several conservative assumptions. Actual dose rates should be verified by field measurements after installation of the cover plate. Exposure may be further reduced by administratively limiting personnel occupancy over the cover plate.

3. References

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- HNF-SD-WM-ER-636, Rev. 0, Brown, T. M., Tank Characterization Report for Single Shell Tank 241-U-106, April, 1997
- IS-001842, Holland, R. A., Project Hanford Radiological Survey Report, April 12, 2000
- Jaka, O. M., Electronic Communication, April 6, 2000
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- RPP-MD-010, Rev. 0, Implementation of RPP-PRO-1622, Radiological Design Review Process, December 22, 1999
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- Shleien, Bernard, The Health Physics and Radiological Health Handbook, Revised Edition, 1992

Page : 1
 DOS File: U-106.MS5
 Run Date: May 3, 2000
 Run Time: 6:28:36 AM
 Duration: 00:00:00

Attachment 1

File Ref: _____
 Date: _____
 By: _____
 Checked: _____

Case Title: U-106SS
 Description: Dose @ U-106 Heel Jet Pit w/Saltwell Screen
 Geometry: 8 - Cylinder Volume - End Shields



Height
 Radius

Source Dimensions

213.36 cm 7 ft 0.0 in
 12.7 cm 5.0 in

Dose Points

#	X	Y	Z
# 1	0 cm 0.0 in	1097.28 cm 36 ft	0 cm 0.0 in

Shields

Shield Name	Dimension	Material	Density
Source	6597.345 in ³	Water	1.2
Air Gap		Air	0.00122

Source Input

Grouping Method : Actual Photon Energies

Nuclide	curies	becquerels	μCi/cm ³	Bq/cm ³
Ba-137m	2.5773e+001	9.5359e+011	2.3839e+002	8.8205e+006
Cs-137	2.7244e+001	1.0080e+012	2.5200e+002	9.3240e+006

Buildup

The material reference is : Source

Integration Parameters

Radial	20
Circumferential	10
Y Direction (axial)	10

Results

Energy MeV	Activity photons/sec	Fluence Rate MeV/cm ² /sec		Exposure Rate mR/hr	
		No Buildup	With Buildup	No Buildup	With Buildup
0.0318	1.974e+10	5.674e-01	1.641e+00	4.727e-03	1.367e-02
0.0322	3.642e+10	1.081e+00	3.187e+00	8.699e-03	2.564e-02
0.0364	1.325e+10	5.339e-01	1.930e+00	3.033e-03	1.097e-02
0.6616	8.580e+11	2.378e+03	6.448e+03	4.609e+00	1.250e+01
TOTALS:	9.275e+11	2.380e+03	6.455e+03	4.626e+00	1.255e+01

