

This document was prepared in conjunction with work accomplished under Contract No.  
AT(07-2)-1 with the U.S. Department of Energy.

## **DISCLAIMER**

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

This report has been reproduced directly from the best available copy.

Available for sale to the public, in paper, from: U.S. Department of Commerce, National Technical Information Service, 5285 Port Royal Road, Springfield, VA 22161, phone: (800) 553-6847, fax: (703) 605-6900, email: [orders@ntis.fedworld.gov](mailto:orders@ntis.fedworld.gov) online ordering: <http://www.ntis.gov/ordering.htm>

Available electronically at <http://www.doe.gov/bridge>

Available for a processing fee to U.S. Department of Energy and its contractors, in paper, from: U.S. Department of Energy, Office of Scientific and Technical Information, P.O. Box 62, Oak Ridge, TN 37831-0062, phone: (865) 576-8401, fax: (865) 576-5728, email: [reports@adonis.osti.gov](mailto:reports@adonis.osti.gov)



RECORD COPY

ENDF/B THERMAL DATA TESTING

The thermal data testing group is concerned with establishing the merit of ENDF/B cross sections for the analysis of thermal systems. The integral experiments used in the testing are designed to analyze each of the phenomena identified in the familiar four-factor formula,  $k = \eta f p \epsilon$ . The experiments are simple, clean and well-documented to minimize the complexity of the analysis and provide the clearest test of the cross sections. Personnel from six organizations participated in Version III thermal data testing, thus blending a diversity of calculational methods: Floyd Wheeler (ANC); Jud Hardy (BAPL); D. S. Craig and M. Hughes (CRNL); Don Mathews (GGA); Lester Petrie (ORNL); and R. L. Reed and F. J. McCrosson (SRL).

For brevity, only the testing of the cross sections in uranium systems is described below. The results for plutonium systems are summarized in reference 1.

Uranyl Nitrate Spheres

CSEWG benchmark experiments ORNL-1, 2, 3, 4, and 10 in Table I refer to experiments by R. Gwin and D. W. Magnuson<sup>(2,3)</sup> in which critical compositions were determined for aqueous solutions of  $^{235}\text{U}$  in spherical geometry. These experiments are useful for testing  $\text{H}_2\text{O}$  fast scattering data, the  $^{235}\text{U}$  fission spectrum, thermal capture and fission of  $^{235}\text{U}$ , and thermal absorption of hydrogen.

There is no ready explanation why the GGA results in Table 1 are 0.2 to 0.3% higher than the BAPL and SRL results. The GGA and SRL calculations used  $S_n$  methods, whereas the BAPL calculations were  $P_3$  epithermally and double  $P_1$  thermally with Marshak boundary conditions. Taken collectively, the BAPL, GGA, and SRL results indicate ENDF/B-III underpredicts  $k_{eff}$  by about 0.4%. This underprediction has been attributed in part to an underestimation of  $\nu\sigma_f$  for  $^{235}U$  at thermal energies. Also shown in Table 1 are ENDF/B-IV data testing results obtained at SRL. These results indicate there is a small improvement in the prediction of criticality for the ORNL spheres in going from Version III to Version IV. The observed increase in  $k_{eff}$  is primarily the result of a 0.7% increase in the ENDF/B-IV  $^{235}U$  thermal values for  $\nu\sigma_f$ . Fast leakage is increased somewhat using ENDF/B-IV because the effective nuclear temperature for the  $^{235}U$  fission spectrum is 1.30 MeV in Version III and 1.323 MeV in Version IV.

#### Uranium Lattices

Benchmark experiments TRX-1 and 2 in Table 1 correspond to lattice measurements by J. Hardy, Jr., D. Klein and J. J. Volpe.<sup>(4)</sup> These lattices contain slightly enriched (1.3%) uranium rods with diameters of 0.4915 cm. Benchmarks MIT-1, 2, and 3 correspond to  $D_2O$ -moderated lattices of natural uranium rods with diameters of 2.565 cm.<sup>(5)</sup> In addition to material bucklings, the TRX and MIT series of experiments determined several important activation parameters:

$\rho^{238}$  = The ratio of epithermal-to-thermal  $^{238}\text{U}$  captures

$\delta^{235}$  = The ratio of epithermal-to-thermal  $^{235}\text{U}$  fissions

$\xi^{238}$  = The ratio of  $^{238}\text{U}$  fissions to  $^{235}\text{U}$  fissions

These benchmark experiments directly test the thermal and epithermal cross sections for  $^{238}\text{U}$  capture and  $^{235}\text{U}$  fissions and the  $^{238}\text{U}$  fast fission cross section. They are sensitive to  $^{238}\text{U}$  inelastic scattering, the  $^{235}\text{U}$  fission spectrum, and the moderator cross sections.

The calculated values of  $k_{\text{eff}}$  reported by the laboratories for the lattices differ by as much as 1%. Part of this large variation may be attributed to the multiplicity of calculational methods used. Some laboratories used Monte Carlo, others the  $S_n$  approximation, and others integral transport theory. All the laboratories used detailed resonance treatments to account for resonance self-shielding, but again, there were variations in the methods and approximations. Differences can arise in the initial step of processing the ENDF/B point-wise data to multigroup form, but some of the laboratories were able to compare multigroup edits to eliminate this possibility.

The SRL results in Table 1 indicate that ENDF/B-IV yields a 1.0% increase in  $k_{\text{eff}}$  for the TRX lattices and a 1.4% increase for the MIT lattices. These increases significantly improve the prediction of  $k_{\text{eff}}$ , particularly when they are applied to the ~~ENDF~~-average ENDF/B-III  $k_{\text{eff}}$  as determined by all the participating laboratories.

The calculated values of  $\rho^{238}$  in Table 2 correspond to a thermal cutoff energy 0.625 eV. The ENDF/B-III values are about 10% higher

than experiment. This suggests epithermal  $^{238}\text{U}$  neutron capture is being overpredicted by about 10%. This overprediction of epithermal  $^{238}\text{U}$  capture largely accounts for the 1.5 to 2.0% underprediction of  $K_{\text{eff}}$  for the benchmark lattices. The ENDF/B-IV results for  $\rho^{23}$  are about 3% lower than the ENDF/B-III results obtained at SRL.

In concluding this section on thermal data testing, it will only be noted that the results for  $\delta^{25}$  and  $\delta^{23}$  for the lattices did not reveal any deficiencies in the ENDF/B-III or ENDF/B-IV data. The first of these parameters tests the epithermal  $^{235}\text{U}$  fission cross section, while the second tests not only the  $^{238}\text{U}$  fast fission cross section, but also the  $^{238}\text{U}$  inelastic cross section and the  $^{235}\text{U}$  and  $^{238}\text{U}$  fission neutron spectra.

REFERENCES

1. F. J. McCrosson. "Thermal Data Testing of ENDF/B-III and Prognosis for ENDF/B-IV." Trans. Amer. Nucl. Soc. 18, 352 (1974).
2. R. Gwin and D. W. Magneson. "The Measurement of Beta and Other Nuclear Properties of  $^{233}\text{U}$  and  $^{235}\text{U}$  in Critical Aqueous Solutions." Nucl. Sci. Eng. 12, 364 (1962).
3. A. Staub, D. R. Harris, and M. Goldsmith. "Analysis of a Set of Critical Homogeneous U-H-H<sub>2</sub>O Spheres." Nucl. Sci. Eng. 34, 263 (1968).
4. J. Hardy, Jr., D. Klein, and J. J. Volpe. "A Study of Physics Parameters in Several H<sub>2</sub>O-Moderated Lattices of Slightly Enriched and Natural Uranium." Nucl. Sci. Eng. 40, 101 (1970).
5. T. J. Thompson, et al. Heavy Water Lattice Project Final Report. MIT-2344-12 (1967).

TABLE 1

Criticality

CRITICALITY	DESCRIPTION	$K_{eff}$ (ENDF/B-III)						$K_{eff}$ (ENDF/B-IV) SRL
		ANC	BAPL	CRNL	GGA	ORNL	SRL	
-1	Unref. spheres of uranyl nitrate sol.							0.9973
-2	H/U-235=1378; R=34.595 cm	0.9965						0.9975
-3	H/U-235=1177; R=34.595 cm	0.9963						0.9975
-3	H/U-235=1033; R=34.595 cm	0.9933						0.9975
-4	H/U-235=971; R=34.595 cm	0.9947						0.9975
-10	H/U-235=1835; R=61.011 cm	0.9931						0.9975
-1	$H_2O$ moderated U lattices							0.9975
-2	Mod/fuel = 2.35 Mod-Fuel = 4.02	0.9741	0.9872	0.9808	0.9791	0.995	0.9766	0.9975
-2		0.9823	0.9913	0.9376	0.9924	0.988	0.9859	0.9941
-1	$D_2O$ moderated U lattices							0.9983
-2	Mod/fuel = 20.74 Mod/fuel = 25.82 Mod/fuel = 34.59	0.9801	0.9888	0.994	0.9735	0.9983	0.9988	0.9911
-2		0.9804	0.9925	0.974	0.974	0.9983	0.9975	0.9911
-2		0.9326	0.9996	0.975	0.975	0.9983	0.9975	0.9911

TABLE 2

Ratio of Epithermal-to-Thermal  $^{238}\text{U}$  Captures\*

<u>BENCH-MARK</u>	$\rho^{28}$ (ENDF/B-III)							$\rho^{28}$ (ENDF/B-IV) SRL
	<u>EXP</u>	<u>ANC</u>	<u>BAPL</u>	<u>CRNL</u>	<u>GCA</u>	<u>GRNL</u>	<u>SRL</u>	
TRK-1	1.311	1.438	1.422	1.419	1.416	1.41	1.454	1.417
				$\pm 0.020$				
TRK-2	0.830	0.906	0.899	0.874	0.877	0.91	0.890	0.868
				$\pm 0.015$				
MIT-1	0.498			0.5319	0.53 <sup>b</sup>	.535	0.5683	0.5464
				$\pm 0.008$				
MIT-2	0.394			0.4365	0.435	.430	0.4659	0.4483
				$\pm 0.002$				
MIT-3	0.305			0.3400	0.33 <sup>b</sup>	.346	0.3624	0.3490
				$\pm 0.004$				

\* Thermal cutoff energy = 0.625 eV