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# Neutron Screening Measurements of 110 gallon drums at T-Plant

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January 2011



**Pacific Northwest**  
NATIONAL LABORATORY

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# **Neutron Screening Measurements of 110 gallon drums at T-Plant**

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January 2011

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## Executive Summary

The Pacific Northwest National Laboratory (PNNL) Nondestructive Assay (NDA) Service Center was contracted to develop and demonstrate a simple and inexpensive method of assaying 110 gallon drums at the Hanford Site's T-Plant. The drums contained "pucks" of crushed old drums used for storage of transuranic (TRU) waste. The drums were to be assayed to determine if they meet the criteria for TRU or Low Level Waste (LLW).

Because of the dense matrix (crushed steel drums) gamma measurement techniques were excluded and a mobile, configurable neutron system, consisting of four sequentially connected slab detectors was chosen to be used for this application. An optimum measurement configuration was determined through multiple test measurements with a californium source. Based on these measurements the initial calibration of the system was performed applying the isotopic composition for aged weapon-grade plutonium. A series of background and blank "puck" drum measurements allowed estimating detection limits for both total (singles) and coincidence (doubles) counting techniques. It was found that even conservative estimates for minimum detection concentration using singles count rate were lower than the essential threshold of 100 nCi/g. Whereas the detection limit of coincidence counting appeared to be about as twice as high of the threshold.

A series of measurements intended to verify the technique and revise the initial calibration obtained were performed at the Waste Receiving and Processing (WRAP) facility with plutonium standards. Standards with a total mass of 0.3 g of plutonium (which is estimated to be equivalent of 100 nCi/g for net waste weight of 300 kg) loaded in the test "puck" drum were clearly detected. The ensuing measurements of higher plutonium loadings verified the calibration factors obtained in the initial exercise. The revised and established calibration factors were also confirmed within established uncertainties by additional measurements of plutonium standards in various locations in the test drum.

Due to necessity to dispense the blank "test" drum an alternative method of baseline determination was established during field measurements. Count rates of ambient background were corrected by the differences between observed background and blank "test" drum count rates which were previously determined over a series of measurements.

Only 31 drums out of 352 counted during the intensive measurement campaign at T-Plant were determined to be "Suspect TRU". 25 of these drums were re-measured at the WRAP facility using the SuperHENC. Of the 25 drums measured, 21 were confirmed to be TRU and the remaining four LLW.

## **Acronyms and Abbreviations**

AK	Accepted Knowledge
c/s	Counts per second
DE	Diatomaceous Earth
LLW	Low Level Waste
MDC	Minimal Detectable Concentration
MDL	Method Detection Limit
nCi	nanoCurie
NDA	Nondestructive Assay
NIST	National Institute of Standards and Technology
PNNL	Pacific Northwest National Laboratory
SuperHENC	Super High Efficiency Neutron Counter
TRU	Transuranic
WIPP	Waste Isolation Pilot Plant
WRAP	Waste Receiving and Processing Facility

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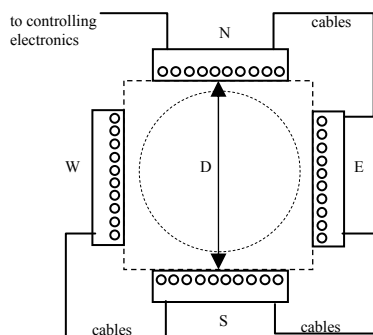
## 1.0 Introduction

T-Plant uses a compactor to crush used empty 55 and 85 gallon drums which previously contained waste categorized as Transuranic<sup>†</sup> (TRU) and are contaminated to an unknown extent. Once crushed, the drum “pucks” are placed in a 110 gallon over pack drum for final disposal. The drums are to be assayed to determine if they meet the criteria for TRU or Low Level Waste (LLW) as defined in document [1].

Once classified as LLW drums may be then sent to the Hanford disposal site whereas the others classified as “Suspect TRU” are to be shipped to Waste Receiving and Processing (WRAP) Facility for the official characterization. If confirmed as TRU they are sent to the National Repository at Waste Isolation Pilot Plant (WIPP) in Carlsbad, NM, for final disposal. Because sorting the non-TRU drums at WRAP is extremely inefficient it was determined to perform initial screening of the 110 gallon “puck” drums at T-Plant. Identification of the anticipated majority of non-TRU drums would reduce shipment evolutions and facility efforts.

The Pacific Northwest National Laboratory (PNNL) Nondestructive Assay (NDA) Service Center was contracted to develop and demonstrate a simple method of assaying the drums. Considering the bulk density of the “puck” drums, neutron measurements appeared to be the preferred counting method over any gamma assay techniques [2] for the given application. Although active interrogation neutron techniques [3,4] could be more sensitive and accurate in the application, the required equipment is more sophisticated and substantial (and hence expensive) than those utilized for passive neutron methods [5]. Thus passive neutron counting was selected to be the most appropriate measurement technique and easiest to implement for this task.

The mobile, configurable neutron system was chosen to be used for this application. The system consists of four sequentially connected slab detectors operated by a computer-controlled neutron coincidence analyzer based on a shift register. Each slab comprises ten 4-atm <sup>3</sup>He tubes embedded in a polyethylene block 32 inches tall and 25 inches wide. Depending on the size and shape of an object to be counted the slabs can be positioned in different configurations. The so called “square” configuration shown in Figure 1.1 is applied for measurements of drums and other relatively small objects. Distance between opposite banks of the slabs, “D”, is defined by the size of an object. The slabs can be elevated by lift jacks up to 14 inches high from the ground level to help with profile as well as potential scattering effects from the ground surface.



**Figure 1.1.** Slabs in “Square” configuration

<sup>†</sup> Waste containing more than 100 nCi of alpha-emitting isotopes with atomic number greater than 92 and with half-lives greater than 20 years per gram of waste.



An over pack 110 gallon drum filled with uncontaminated crushed drum pucks was specifically composed to simulate the matrix of the real drums and used for calibration and test exercises. Several source tubes were installed throughout the crushed drum pucks in the test drum to allow for the placement of radioactive sources at various heights and locations within the over pack.

A National Institute of Standards and Technology (NIST) traceable  $^{252}\text{Cf}$  neutron source (identified as Cf-2) was used for the initial calibration and testing exercises. A pallet with a turn table mounted on its top was manufactured to position the test drum during the exercises. Both total (singles) and coincidence (doubles) neutron counting techniques were tested.

Since a measured value of the isotopic distribution of material contained in a drum was impossible to obtain, the isotopic composition for aged weapon-grade plutonium was mutually agreed upon as accepted knowledge (AK) data (see Table 1.1) providing conservative estimates and were considered the “default” values unless the material isotopic composition could actually be measured and found to be different.

**Table 1.1.** Accepted Data of Plutonium Isotopic Composition

Nuclide	wt%
$^{238}\text{Pu}$	0.03 ( $\pm 10\%$ )
$^{239}\text{Pu}$	93.68 ( $\pm 1\%$ )
$^{240}\text{Pu}$	6.05 ( $\pm 5\%$ )
$^{241}\text{Pu}$	0.22 ( $\pm 3\%$ )
$^{242}\text{Pu}$	0.02 ( $\pm 30\%$ )
$^{241}\text{Am}$	0.50 ( $\pm 3\%$ )
$^{240}\text{Pu}_{\text{eff}}^{\dagger}$	$6.16 \pm 0.30$ (4.9%)
TRU Specific Activity [Ci/g]	$0.094 \pm 0.002$ (2.4%)

---

$^{\dagger} \text{}^{240}\text{Pu}_{\text{eff}}$  (effective) is the mass of  $^{240}\text{Pu}$  that would give the same neutron response as that obtained from all the even isotopes in the actual sample.

## 2.0 Description of Calculation Algorithm

The background-corrected neutron count rate is proportional to the  $^{240}\text{Pu}$  effective mass contained in an item under consideration. The relationship between count rate observed and  $^{240}\text{Pu}_{\text{eff}}$  quantity can be obtained through calibration of the measurement system with NIST traceable plutonium standards and/or spontaneous fission neutron sources. For waste applications where total plutonium mass ranges below 100 grams a linear function is most often applicable as a calibration curve:

$$CR = a + b \cdot {}^{240}m_{\text{eff}} \quad \text{or} \quad CR = b \cdot {}^{240}m_{\text{eff}} \quad (2.1)$$

where  $CR$  - count rate [1/s];  
 ${}^{240}m_{\text{eff}}$  -  $^{240}\text{Pu}_{\text{eff}}$  mass [g];  
 $a, b$  - intercept [1/s] and slope [1/(s·g)] of fitted function, respectively.

Thus using the calibration factors the count rate obtained on an assayed drum can be converted to  $^{240}\text{Pu}_{\text{eff}}$  mass as follows

$${}^{240}m_{\text{eff}} = (CR - a)/b \quad \text{or} \quad {}^{240}m_{\text{eff}} = CR/b \quad (2.2)$$

with its associated uncertainty:

$$\Delta({}^{240}m_{\text{eff}}) = {}^{240}m_{\text{eff}} \cdot \sqrt{\left(\frac{\sigma_m}{{}^{240}m_{\text{eff}}}\right)^2 + (\delta_s)^2} \quad (2.2A)$$

where  $\delta_s$  - relative systematic uncertainty of spatial detection efficiency;  
 $\sigma_m$  - combined uncertainty of calibration and counting components

$$\sigma_m = \sqrt{\frac{\sigma_{CR}^2 + \sigma_a^2 + ({}^{240}m_{\text{eff}})^2 \sigma_b^2 + 2({}^{240}m_{\text{eff}})\sigma_{ab}}{b^2}} \quad \text{or} \quad (2.2B)$$

$$\sigma_m = \sqrt{\frac{\sigma_{CR}^2 + ({}^{240}m_{\text{eff}})^2 \sigma_b^2}{b^2}}$$

$\sigma_{CR}$  - count rate uncertainty;  
 $\sigma_a; \sigma_b$  - errors of corresponding calibration factors;  
 $\sigma_{ab}$  - covariance of calibration factors.

Uncertainties associated with  $^{240}\text{Pu}_{\text{eff}}$  mass values of Pu standards are negligible comparing to others and therefore may be disregarded.

Having determined  $^{240}\text{Pu}_{\text{eff}}$  mass the total mass of plutonium can be found as

$$m_{\text{Pu}} = {}^{240}m_{\text{eff}} / {}^{240}C_{\text{eff}} \quad (2.3)$$

and its associated uncertainty

$$\Delta m_{\text{Pu}} = m_{\text{Pu}} \cdot \sqrt{\left( \frac{\Delta({}^{240}m_{\text{eff}})}{m_{\text{eff}}} \right)^2 + \left( \frac{\Delta({}^{240}C_{\text{eff}})}{{}^{240}C_{\text{eff}}} \right)^2} \quad (2.3A)$$

where  ${}^{240}C_{\text{eff}}$  -  $^{240}\text{Pu}_{\text{eff}}$  content [wt%]

$\Delta({}^{240}C_{\text{eff}})$  -  $^{240}\text{Pu}_{\text{eff}}$  content uncertainty [wt%];

Then, TRU activity value is determined

$$A_{\text{TRU}} = m_{\text{Pu}} \cdot a_{\text{TRU}} \quad (2.4)$$

and its uncertainty

$$\Delta A_{\text{TRU}} = A_{\text{TRU}} \cdot \sqrt{\left( \frac{\Delta m_{\text{Pu}}}{m_{\text{Pu}}} \right)^2 + \left( \frac{\Delta a_{\text{TRU}}}{a_{\text{TRU}}} \right)^2} \quad (2.4A)$$

where  $a_{\text{TRU}}$  - specific TRU activity [Ci/(g of Pu)]

$\Delta a_{\text{TRU}}$  - specific TRU activity uncertainty [Ci/(g of Pu)].

Finally, TRU concentration is calculated based on net weight of the waste

$$x_{\text{TRU}} = A_{\text{TRU}} / W_{\text{NET}} \quad (2.5)$$

and its uncertainty

$$\Delta x_{\text{TRU}} = \Delta A_{\text{TRU}} / W_{\text{NET}} \quad (2.5A)$$

where  $W_{\text{NET}}$  - net weight of the waste

The weight uncertainty is considered negligible (<0.5%) comparing to that of TRU activity value and hence may be disregarded in this calculation.

The method detection limit is calculated based on the uncertainty of baseline count rate using the following simplified<sup>‡</sup> version of formula from HASQARD document [6]

$$MDL = 4.65 \cdot \Delta CR_{bgrd} / b \quad (2.6)$$

where  $\Delta CR_{bgrd}$  – standard deviation of background count rate obtained with a blank “puck” drum in place;

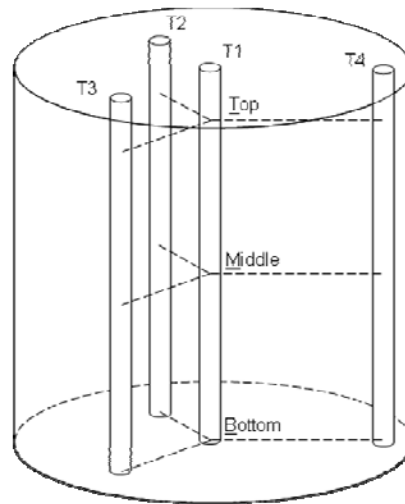
$b$  – calibration function slope.

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<sup>‡</sup> Original formula is  $MDL = (2.71/T_{bgrd} + 4.65 \cdot \Delta CR_{bgrd})/b$ . As T gets longer the former fraction becomes insignificantly small and may be omitted.

### 3.0 Initial Test Measurements with Cf Source

Multiple test measurements using the NIST-traceable  $^{252}\text{Cf}$  neutron source “Cf-2” were performed with the test drum at varying standoff distances of the slabs ranging from 36 to 48 inches, and the slabs at various elevations ranging from 8 – 14 inches in order to determine the optimum measurement configuration. The source was placed at three height levels (top, middle and bottom) in four tubes (T1, T2, T3 and T4) of the drum (see Figure 3.1). The source height is about one inch, thus measurements on the chosen vertical positions provided extreme minimum and maximum responses. As a result of these tests the final configuration with the slabs elevated at 11 inches from the ground and spread 43 inches apart (see Figure 3.2) was found as a compromise between variations in axial and azimuthal response profiles and absolute detection efficiency. The data obtained in several measurement sessions are summarized in Tables 3.1. and 3.2.



**Figure 3.1.** Source positions in the test drum



**Figure 3.2.** Measurements of the test drum with  $^{252}\text{Cf}$  source inside

**Table 3.1.** Spatial responses for chosen 43" x 43" configuration

Tube	Singles [1/s]				Doubles [1/s]			
	T1	T2	T3	T4	T1	T2	T3	T4
Top	1357.048	1311.278	1467.376	1581.011	54.567	49.976	64.040	74.242
	1328.512	1363.897	1561.600	1585.940	51.772	53.996	73.643	75.361
	1254.745	1369.463		1769.775	46.243	54.146		91.914
				1428.808				61.363
				1543.138				69.477
				1376.526				56.831
Middle	2070.309	2177.711	2274.363	2400.351	126.715	141.069	151.791	175.373
	2064.863	2190.586	2337.323	2332.709	127.459	141.264	161.540	162.428
	2055.830	2200.258		2134.450	124.776	148.183		136.359
				2519.435				188.348
				2703.778				218.683
Bottom	1438.232	1463.612	1388.624	1410.477	61.188	64.159	55.970	59.937
	1465.354	1448.052	1391.699	1350.099	62.382	60.999	56.890	55.297
	1435.751	1422.041		1443.849	58.731	59.676		58.788
				1496.883				64.020

**Table 3.2.** Averaged spatial responses for chosen 43'' x 43'' configuration

Averaged for each position								
Top	1313	1348	1515	1548	51	53	69	72
Middle	2064	2190	2306	2418	126	144	157	176
Bottom	1446	1445	1390	1425	61	62	56	60
Averaged for each level								
Top	1431				61			
Middle	2244				151			
Bottom	1427				60			
Overall average and standard uncertainty calculated using formulae (3.1) and (3.1A)								
Overall	1866 ± 319 (17.1%)				114 ± 36 (31.9%)			

Since count rates obtained in the middle plane gave the maximum and those on the top and bottom the lowest, the overall average values and their uncertainties were determined based on the range of the data from the “averaged for each position” section of the table. For a random source position the probability distribution of the data is considered to be rectangular. Therefore, the overall average value and its standard uncertainty<sup>†</sup> [7] are calculated using the formulae below.

$$\langle CR \rangle = (CR_{MAX} + CR_{MIN}) / 2 \quad (3.1)$$

$$\Delta \langle CR \rangle = [(CR_{MAX} - CR_{MIN}) / 2] / \sqrt{3} \quad (3.1A)$$

Note that ratio ( $\Delta \langle CR \rangle / \langle CR \rangle$ ) represents relative systematic uncertainty of spatial detection efficiency,  $\delta_s$ , identified in equation (2.2A)

The neutron yield of Cf-2 Source on September 30, 2007 was  $3.6 \cdot 10^4$  neutrons per second. Using the decay-corrected yield of the source and the foregoing singles count rate the detection efficiency of the measurement system for the chosen configuration was determined to be 5.3%.

---

<sup>†</sup> The standard uncertainty is equivalent to one standard deviation and is a key quantity in the combination of uncertainties.

## 4.0 Method Demonstration

### 4.1 Initial Cf source based calibration

According to equations of the point model in neutron coincidence counting [8] the observed doubles count rate from a  $^{252}\text{Cf}$  source (no multiplication and (alpha,n) production) can be expressed as follows:

$$D^{Cf} = F^{Cf} \cdot \varepsilon^2 \cdot f_d \cdot \frac{\nu_{S2}^{Cf}}{2} \quad (4.1.1)$$

where  $F^{Cf}$  – fission rate of a  $^{252}\text{Cf}$  source, in turn

$$F^{Cf} = \frac{Y}{\nu_{S1}^{Cf}},$$

$Y$  – yield of the source and

$\nu_{S1}$  – the first factorial moment of multiplicity distribution of spontaneous fission

$$(\nu_{S1}^{Cf-252} = 3.757; \nu_{S1}^{Pu-240} = 2.156) [9]$$

$\varepsilon$  – detection efficiency

$f_d$  – doubles gate fraction

$\nu_{S2}$  – the second factorial moment of multiplicity distribution of spontaneous fission

$$(\nu_{S2}^{Cf-252} = 11.962; \nu_{S2}^{Pu-240} = 3.825) [9]$$

Then  $F^{Pu}$  – fission rate of  $^{240}\text{Pu}$  equivalent to  $D^{Cf}$  may be expressed as

$$F^{Pu} = \frac{2 \cdot D^{Cf}}{\varepsilon^2 \cdot f_d \cdot \nu_{S2}^{Pu}} = \frac{Y \cdot \nu_{S2}^{Cf} \cdot 2}{\nu_{S1}^{Cf} \cdot 2 \cdot \nu_{S2}^{Pu}} \cdot \frac{[f_d \cdot \varepsilon^2]^{Cf}}{[f_d \cdot \varepsilon^2]^{Pu}} \quad (4.1.2)$$

If effective mass of  $^{240}\text{Pu}$  can be determined as  $^{240}m_{eff} = F^{Pu} / g$ ,

where  $g$  – specific fission rate of  $^{240}\text{Pu}$  {473.5 fissions/s/g}

Then

$$^{240}m_{eff} = \frac{1}{g} \cdot \frac{Y \cdot \nu_{S2}^{Cf}}{\nu_{S1}^{Cf} \cdot \nu_{S2}^{Pu}} \cdot \frac{[f_d \cdot \varepsilon^2]^{Cf}}{[f_d \cdot \varepsilon^2]^{Pu}} \quad (4.1.3)$$



On the other hand, a calibration factor for a neutron coincidence system is  $D/^{240}\text{m}_{\text{eff}}$ . Hence, assuming that the ratio of brackets in equations (4.1.2) and (4.1.3) is approximately unity the calibration factor can be estimated as

$$b_D = \frac{g \cdot D^{Cf}}{Y} \cdot \frac{\nu_{S1}^{Cf} \cdot \nu_{S2}^{Pu}}{\nu_{S2}^{Cf}} \quad (4.1.4)$$

Estimation of the calibration factor for singles count rate can be done even simpler using the following equation:

$$b_S = \varepsilon g \cdot \nu_{S1} (1 + \alpha) \quad (4.1.5)$$

where  $\alpha$  – alpha parameter which is the ratio between neutron production rate due to (alpha,n) reaction(s) in a sample and that from spontaneous fission.

However, the calibration factor accuracy depends on correctness of assumed alpha parameter of plutonium-bearing material.

The source equivalent  $^{240}\text{Pu}$  mass calibration factors determined through equations (4.1.3), (4.1.4), (4.1.5) are presented in Table 4.1.1.

**Table 4.1.1.** Calibration factors for singles and doubles based on  $^{252}\text{Cf}$  measurements

Parameter/Factor	Singles ( $b_S$ )		Doubles ( $b_D$ )
Alpha Ratio (assumption)	~0.8 (pure $\text{PuO}_2$ ) <u>conservative</u>	~2.4 ( $\text{PuO}_2$ with DE <sup>§</sup> ) <u>likely</u>	N/A
Equivalent $^{240}\text{Pu}$ mass [g]	62.24		
Calibration factor value ± 1 standard deviation [counts/s/g of $^{240}\text{Pu}$ ]	$96.8 \pm 16.5$	$182.8 \pm 31.2$	$1.83 \pm 0.53$

Thus using the foregoing calibration factors the obtained singles and doubles count rates can be converted to mass of  $^{240}\text{Pu}_{\text{eff}}$  as follows:

$$^{240}\text{m}_{\text{eff}(S)} = S/b_S \quad \text{and} \quad ^{240}\text{m}_{\text{eff}(D)} = D/b_D, \quad \text{respectively.} \quad (4.1.6)$$

---

<sup>§</sup> Diatomaceous earth

Their corresponding uncertainties are then:

$$\Delta(^{240}m_{eff})_{(S)} = ^{240}m_{eff(S)} \cdot \sqrt{\left(\frac{\sigma S}{S}\right)^2 + \left(\frac{\delta b_S}{b_S}\right)^2} \quad \text{and}$$

$$\Delta(^{240}m_{eff(D)}) = m_{eff(D)} \cdot \sqrt{\left(\frac{\sigma D}{D}\right)^2 + \left(\frac{\delta b_D}{b_D}\right)^2} \quad (4.1.7)$$

where S – singles count rate;  
D – doubles count rate.

Equations (4.1.6) and (4.1.7) resemble those (2.2) and (2.2A). Subsequent calculations to obtain total mass of plutonium and hence TRU concentration are identical for both singles and doubles and are performed per equations in section 2.

## 4.2 Method Detection Limit

Counting times of background measurements ranged from 600 to 1800 seconds. Background measurements repeated several times over the testing period showed good reproducibility. Although the counting uncertainty of singles of an individual measurement was about 0.12 c/s the uncertainty calculation based on multiple measurements almost doubled. For doubles the opposite behavior was observed; counting uncertainty of an individual measurement was about 0.016 c/s and that calculated based on multiple measurements was half of that value. Several measurements were also performed with the blank test drum (with no sources) in order to check for possible effects of the drum volume and matrix on the background count rates. The summarized data are shown in Table 4.2.1. The obvious difference in the countrates with and without the drum can be attributed to increased scattering and spallation effects in the drum matrix. Thus the detection limits were calculated based on the “baseline” countrates obtained with the blank drum in place.

**Table 4.2.1.** Background/Baseline measurements at T-Plant

Parameter	Singles [c/s]	Doubles [c/s]
Averaged over testing exercise (multiple measurements on several days)		
With the blank test drum in place (no sources)	$15.18 \pm 0.22$	$0.094 \pm 0.006$
Without the drum	$14.55 \pm 0.42$	$0.014 \pm 0.006$
Difference	$0.63 \pm 0.48$	$0.080 \pm 0.008$

Taking the highest values of uncertainty for singles and doubles, 0.22 c/s and 0.016 c/s, respectively, one can estimate MDL for the count rates (“drum background” corrected ) using formula (2.6) and then using formulae (4.1.6) (or (2.2)) and (2.3):

Singles:	1.02 c/s	→	0.17 g of weapon-grade Pu ( <u>conservative</u> )
		or	0.09 g of weapon-grade Pu ( <u>likely</u> )
Doubles:	0.074 c/s	→	0.66 g of weapon-grade Pu

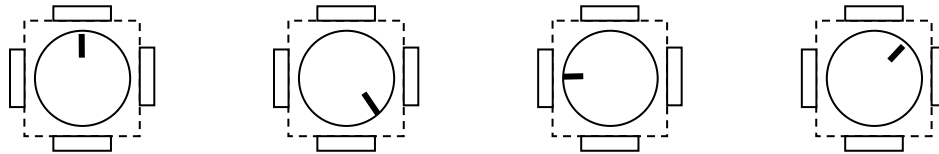
The net weight of the majority (>95%) of these 110 gallon “puck” drums exceeded 300 kilograms with about 350 kilograms as the average. Thus the conservative estimates (from the Pu mass values above and for net weight of 300 kg ) of the minimum detectable concentration (MDC) would be obtained using equations (2.4) and (2.5):

Singles: 54 nCi/g (conservative)  
or 28 nCi/g (likely)  
Doubles: 207 nCi/g

Even the conservative estimate of an MDC using a singles count rate will meet the criteria to distinguish the drums between LLW and TRU.

### 4.3 Routine Measurement Approach

Each drum measurement combined four separate 10-minute long counts; thus the total measurement time was 40 minutes. A measured drum was rotated on a turntable by 135 degrees between the separate counts (see Figure 4.3.1). Measurement results were obtained as an average of the values from all counts with the counting uncertainty calculated as a standard deviation. Total measurement uncertainty was calculated according to the algorithm described in Section 2.



**Figure 4.3.1.** Drum Counting Positions

After successful completion of a daily performance check measurement, the current baseline (with blank “puck” drum in place) countrate value and its uncertainty was obtained before measurements of real “puck” drums.

The result obtained from counting a drum was compared against the detection limit values (derived from blank “puck” drum measurements) as follows:

- If the singles count rate was less than the corresponding detection limit, then the singles detection limit value was assigned to the drum content and used for the concentration calculation.
- If the singles count rate was higher than the corresponding detection limit, but the calculated TRU concentration was less than 100nCi/g for the net waste weight of the drum then the drum was classified as “LLW”.
- If the TRU concentration calculated based on the singles count rate was higher than 100nCi/g for the net waste weight of the drum then the drum was considered “Suspect TRU” waste. If doubles count rates were below the corresponding detection limit then the doubles detection limit was used to assign the upper bounding value for the content and concentration.
- If doubles count rates were higher than the corresponding detection limit then the drum content and concentration was assigned based on this value.

## 5.0 Verification Measurements With Pu Standards

### 5.1 Pu Standards Data

A series of measurements intended to verify the measurement method and revise the initial calibration were performed at the WRAP facility with the test “puck” drum and NIST-traceable plutonium standards. Isotopic and mass values for Pu standards used in this exercise are presented in tables 5.1.1 and 5.1.2.

**Table 5.1.1.** Isotopic Content of Pu standards

Nuclide	Content [wt%] on date	
	09/21/1999	12/08/2007
$^{238}\text{Pu}$	0.014± 0.005	0.013± 0.005
$^{239}\text{Pu}$	93.808± 0.015	93.873± 0.015
$^{240}\text{Pu}$	5.939± 0.007	5.939± 0.007
$^{241}\text{Pu}$	0.185± 0.009	0.121± 0.006
$^{242}\text{Pu}$	0.054± 0.003	0.054± 0.003
$^{241}\text{Am}$	0.11289± 0.00003	0.1755± 0.00005
$^{240}\text{Pu}_{\text{eff}}$	6.07±0.02	6.06± 0.02

**Table 5.1.2.** Mass values of Pu standards

On date	09/21/1999	12/08/2007	
	Total Pu [g]	Total Pu [g]	$^{240}\text{Pu}_{\text{eff}}$ [g]
Pu Standard #1	0.09710± 0.00011	0.09701± 0.00011	0.00588± 0.00002
Pu Standard #2	0.20038± 0.00021	0.20020± 0.00021	0.01214± 0.00005
Pu Standard #3	0.50831± 0.00051	0.50785± 0.00051	0.03079± 0.00013
Pu Standard #4	0.51523± 0.00051	0.51477± 0.00051	0.03121± 0.00013
Pu Standard #5	1.01534± 0.00098	1.01443± 0.00098	0.06151± 0.00025
Pu Standard #6	5.04299± 0.00474	5.03845± 0.00474	0.30550± 0.00124
Pu Standard #7	5.01168± 0.00472	5.00717± 0.00472	0.30360± 0.00123

## 5.2 Baseline Measurements at WRAP

The first day at WRAP was spent finding an appropriate measurement location. Very high background values (over ten times higher than those obtained at T-Plant) were observed at the initially planned measurement location. This forced relocation to an alternative place. Satisfactory count rates of ambient background were obtained on a side of the parking lot by building 2720W, although the choice of measurement location (being outside of the controlled area and at a distance from the material storage) impacted practicality of the test measurements for WRAP operations staff.

Multiple measurements of ambient background and the blank “puck” drum were conducted to establish the baseline value for the test measurements. The data obtained on all three days are summarized in Table 5.2.1. As it can be seen from the table, the data obtained on different dates are in good agreement. The negative difference in the singles count rate between ambient background and the blank “puck” drum may be attributed to, so called, background suppression effect.

**Table 5.2.1.** Baseline count rates observed at WRAP during the test measurements

	Date	Ambient Background [c/s]	Blank “puck” drum [c/s]	Difference [c/s]
Singles	12/5/07	$32.922 \pm 0.154$	$31.940 \pm 0.152$	$-0.982 \pm 0.216$
	12/7/07	$32.753 \pm 0.207$	$31.581 \pm 0.259$	$-1.172 \pm 0.332$
	12/11/07	$30.847 \pm 0.256$	$29.873 \pm 0.173$	$-0.974 \pm 0.309$
	Averaged:			$-1.043 \pm 0.112$
Doubles	12/5/07	$0.018 \pm 0.011$	$0.131 \pm 0.013$	$0.113 \pm 0.016$
	12/7/07	$0.020 \pm 0.017$	$0.123 \pm 0.030$	$0.104 \pm 0.035$
	12/11/07	$0.027 \pm 0.024$	$0.123 \pm 0.030$	$0.097 \pm 0.039$
	Averaged:			$0.104 \pm 0.009$

### 5.3 Measurements with Pu Standards

The primary purpose of the measurements with Pu standards was to verify if the detection limit identified was below 100 nCi/g; which was equivalent to about 0.3 g of weapon-grade plutonium for selected net waste weight of 300 kg. For this measurement the plutonium standards of 0.1 g and 0.2 g were loaded at the top of T1 tube and at the middle of T3 tube, respectively. The observed singles countrate was  $2.404 \pm 0.327$  c/s which was almost twice as high as the determined detection limit of 1.301 c/s. The doubles count rate of  $0.047 \pm 0.009$  c/s was less than half of the corresponding detection limit of 0.112 c/s. Both results were in good agreement with predicted values for detection limits.

The next activity – measurements with a higher mass of plutonium – was intended to revise calibration factors obtained in the initial exercise with the californium source. The summarized measurement results (with blank “puck” drum count rates subtracted) are presented in Table 5.3.1 and plotted in Figures 5.3.1 and 5.3.2. The highest mass point was used to fit a linear function through the origin point. This equation has been used as a new calibration curve. The medium mass points were used as confirmation data.

**Table 5.3.1.** Results of measurements with Pu standards

Pu mass g	$^{240}\text{Pu}_{\text{eff}}$ g	Loading Location Sensitivity*	Singles		Doubles	
			$\text{s}^{-1}$	$(\text{s} \cdot \text{g}^{240}\text{Pu}_{\text{eff}})^{-1}$	$\text{s}^{-1}$	$(\text{s} \cdot \text{g}^{240}\text{Pu}_{\text{eff}})^{-1}$
0.30	0.018	average	$2.40 \pm 0.33$	133.5	$0.05 \pm 0.01$	2.58
10.05	0.609	average	$88.58 \pm 0.63$	147.6	$1.29 \pm 0.06$	2.15
6.06	0.367	above average	$57.73 \pm 0.65$	160.4	$0.89 \pm 0.05$	2.46
2.04	0.124	below average	$16.10 \pm 0.22$	134.2	$0.21 \pm 0.02$	1.78
2.04	0.124	above average	$19.68 \pm 0.48$	164.0	$0.20 \pm 0.02$	1.65
Average:			$143.9 \pm 12.7$		Average:	$2.2 \pm 0.4$

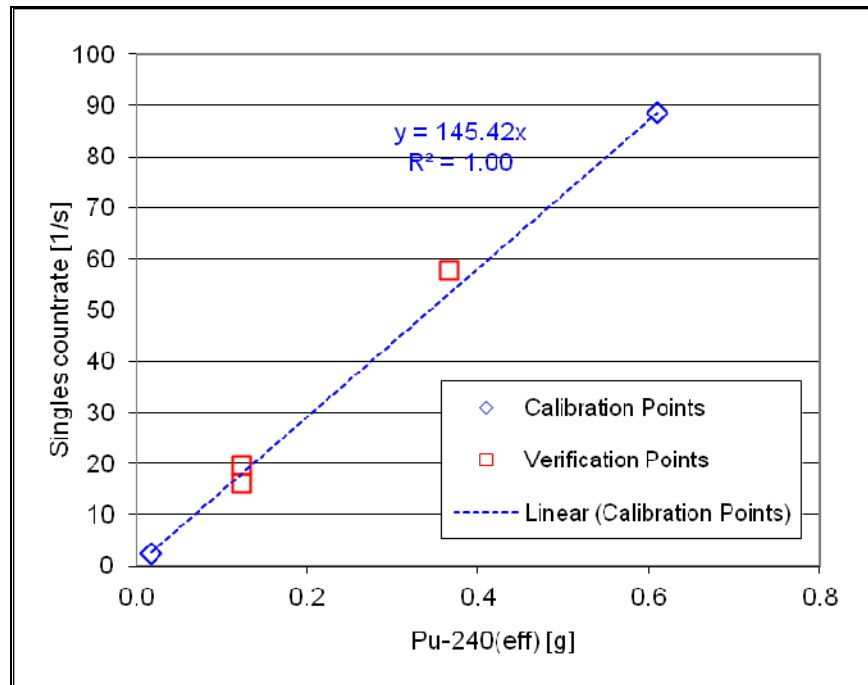
\* - based on results of the initial testing (see table 3.1)

The newly obtained (revised) calibration functions were

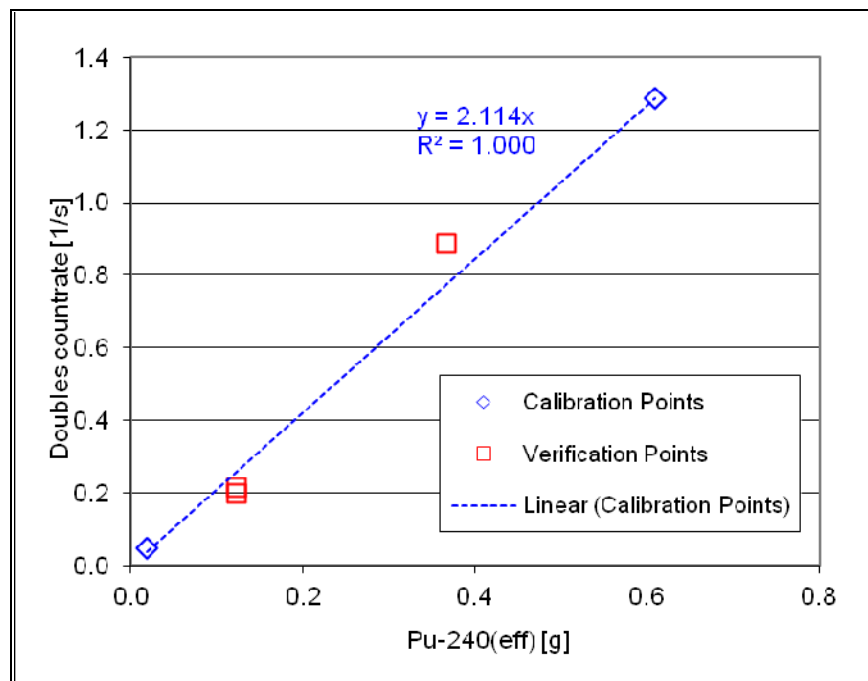
a) Singles  $[\text{c/s}] = 145.42 (\pm 0.36) \cdot [^{240}\text{Pu}_{\text{eff}} \text{ grams}]$

and

b) Doubles  $[\text{c/s}] = 2.114 (\pm 0.014) \cdot [^{240}\text{Pu}_{\text{eff}} \text{ grams}]$ .



**Figure 5.3.1.** Singles Count Rate results



**Figure 5.3.2.** Doubles Count Rate results



Using the revised calibration factors, the medium mass results were analyzed and compared to the acceptance criteria: the results should have been within  $\pm 30\%$  of the known or accepted Pu mass value. The results with associated uncertainties are presented in Table 5.3.2. As it can be seen from the table, all calibration confirmation measurements were within  $\pm 30\%$  of corresponding accepted values (and within  $\pm 1$  standard deviation).

**Table 5.3.2.** Confirmation of Calibration factors revised

Known $^{240}\text{Pu}_{\text{eff}}$	Singles		Doubles	
	Assayed $^{240}\text{Pu}_{\text{eff}}$	Difference	Assayed $^{240}\text{Pu}_{\text{eff}}$	Difference
g	g	%	g	%
0.367	0.397 $\pm$ 0.068 (17.1%)	8.2%	0.419 $\pm$ 0.136 (32.3%)	14.3%
0.124	0.111 $\pm$ 0.019 (17.2%)	-10.3%	0.101 $\pm$ 0.034 (33.5%)	-18.3%
0.124	0.135 $\pm$ 0.023 (17.3%)	9.6%	0.093 $\pm$ 0.032 (33.8%)	-24.4%

## 6.0 Field Measurements

### 6.1 Alternative for Baseline Determination

Once the measurement method had been demonstrated to meet requirements for distinguishing between LLW and TRU “puck” drums, the neutron slab system was promptly deployed at T-Plant to count hundreds of “puck” drums already accumulated. However, at the very beginning of the measurement campaign it became necessary to find an alternative for the baseline count rate measurements because the blank test “puck” drum was to be transferred to WRAP for SuperHENC calibration and baseline measurements.

The series of ambient background and the blank “puck” drum measurements were performed in order to determine an average difference between the count rate values. The data are shown in Table 6.1.1. Then the difference value was applied to correct a current ambient background value – to estimate the baseline value. On one hand, this “maneuver” allowed dispensing the need to have the blank test “puck” drum for baseline measurements, but on the other hand, propagated uncertainty of the background value elevated the detection limit from 25 – 35 up to 70 - 80 nCi/g.

**Table 6.1.1.** Difference between blank test drum and ambient background counts

Assay Date	Singles	S Sigma	Doubles	D Sigma
	c/s	c/s	c/s	c/s
11/13/2007	0.628	0.476	0.080	0.008
2/6/2008	1.013	0.329	0.076	0.021
1/16/2008	0.393	0.168	0.069	0.015
1/22/2008	0.608	0.258	0.069	0.006
1/23/2008	0.763	0.207	0.063	0.022
1/24/2008	1.019	0.189	0.094	0.016
2/5/2008	1.163	0.221	0.085	0.021
2/11/2008	0.853	0.136	0.082	0.014
2/12/2008	1.340	0.663	0.093	0.025
2/14/2008	-0.282	0.217	0.058	0.031
2/15/2008	0.346	0.274	0.079	0.021
Average	0.713	0.452	0.077	0.012

## 6.2 Performance Evaluation

A year after the beginning of the measurement campaign at T-Plant the mobile neutron slab system was brought to the WRAP facility in order to verify the calibration factors established for assaying of 110 gallon puck drums. The system performance was verified by measurements of the test drum loaded with Pu standards. The measurement results are summarized in Table 6.2.1. As it can be seen the differences between assayed and declared values of Pu mass for both singles and doubles were less than one standard deviation of measurement uncertainty.

**Table 6.2.1.** Results of verification measurements with Pu standards

##	Declared Pu mass [g]	Assayed Pu mass $\pm$ 1 std. dev. [g]		Recovery [A/D] [%]	
		Singles	Doubles	Singles	Doubles
1	1.02	$1.05 \pm 0.19$	$1.02 \pm 0.35$	103%	100%
2	10.04	$9.71 \pm 1.73$	$9.25 \pm 3.05$	97%	92%

Out of 352 drums assayed during the measurement campaign at T-Plant, only 31 were found to be “Suspect TRU” (two of them due to low net weight). Twenty five of these “Suspect TRU” drums were shipped to WRAP and assayed at the SuperHENC (stationary trailer-based, high efficiency neutron counter) [10]. 21 out of these 25 were confirmed to be TRU [Brian Anderson, Personal Communication, January 5, 2011]. Thus the immediate sorting of the “puck” drums at T-Plant had provided just about 1% of “false positive” results.

Net counting time of a drum at the mobile neutron slab system was 40 minutes versus that of 30 minutes at the SuperHENC. However, taking into account process of drum loading/unloading the gross counting times of the measurement systems were comparable.

Overall, the performance of the mobile neutron slab system and measurement approach may be considered outstanding.

## **7.0 Conclusions**

The PNNL NDA Service Center developed and demonstrated a simple and relatively inexpensive method of assaying 110 gallon “puck” drums. The configurable neutron slab system was calibrated to distinguish between TRU and LLW drums. Sorting drums at T-Plant considerably reduced efforts associated with drum handling and shipping. The suggested measurement method proved to be reliable and very cost-effective.

Over a year-long period of time the mobile neutron system demonstrated impeccable and steady performance sorting out over 350 “puck” drums. Just four drums out of the assessed inventory were over classified which in turn provided additional evidence of the measurement method efficiency.

Even with such outstanding performance of the system additional improvements of the measurement process are believed to be possible and should be further investigated. Potential reduction of counting time would result in increased drum throughput and hence lower costs of the measurements.

## 8.0 References

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