

Calibration of Mobile Robotic Systems: A Pilot Study [†]

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[†] Presented at the 4th International Electronic Conference on Sensors and Applications, 15–30 November 2017; Available online: <http://sciforum.net/conference/ecsa-4>.

Published: 14 November 2017

Abstract: The type of wheeled mobile robots (WMRs) may affect the level of positional errors during motion. The errors are inevitable, as caused by imperfections in design to fabrication, and need to be rectified using calibration techniques. This paper uses the odometry method to provide improved short-term accuracy with high sampling rates. Odometry is economical and requires fewer landmarks and simpler sensory system to localize WMRs, compared to other existing techniques such as 3D camera error detection. The context introduces an odometry-based method to correct the motion of a WMR with two-wheeled mechanism. Experimental results showed that positional errors were significantly improved after applying outcome of the calibration.

Keywords: calibration; sensory system; positional error; performance analysis; wheeled mobile robot

1. Introduction

Wheeled mobile robots (WMRs) are employed in many areas such as logistics, inspection and maintenance, security and defense, agriculture, medical care, home care, urban transport, planetary exploration and surveillance operations. Due to the precision required during the performance of a WMR, the robot should properly be calibrated, and the positional error should be improved, before implementation in real field. Developing effective calibration techniques have recently been interested for robotic systems [1]. They include odometry, 3D camera error detection, active beacons, gyroscope and magnetic compasses [2–6]. Odometry uses the information of positional sensors attached to each actuator to estimate change in position over time. The odometry method is applied to correct errors of different types of WMRs [2,3].

The calibration of WMRs using odometry approach has been performed by researchers and engineers. Correcting systematic errors with localization based on magnetic fields has been discussed in [6]. University of Michigan Benchmark (UMBmark) method was introduced to measure odometry errors in differential drive mobile robots [7]. The UMBmark was then employed to reduce positional errors of several WMRs with differential drive mechanism. The author proposed a new technique to reduce both systematic [2,8] and non-systematic [3] errors. This context proposes a kinematic-based calibration method, which is simple to implement and applicable to all types of wheeled mobile robots including differential drive, omnidirectional and multi-degree of freedom (DOF) WMRs. The proposed technique is employed to correct the motion of a two-wheeled mobile robot.

The rest of this paper is organized as follows. Sources of positional errors are described in Section 2. Kinematic modeling of WMRs are presented in Section 3. Section 4 documents the development of the proposed calibration method. Section 5 describes the prototyped mobile robot, followed by experimental results in Section 6. Section 7 outlines the conclusions of this research.

2. Positional Errors

The accuracy of robot movement and the amount of positional errors depend on the sources causing both systematic and nonsystematic errors. Systematic errors originate from control and mechanical elements due to imperfections from design to fabrication. Non-systematic errors are independent of the robot structure and its characteristics, and are defined unwanted errors produced due to surface irregularities.

3. Kinematic Modeling

Figure 1 shows the structure of a typical two-wheeled WMR with a differential drive mechanism. In this schematic, the driving wheels are used to supply required power of the platform. Considering the fact that the two driving wheels roll and do not slip, we have:

$$\dot{x} \cos \theta + \dot{y} \sin \theta = 0.25 (D_L \dot{\theta}_L + D_R \dot{\theta}_R) \quad (1)$$

$$4l\dot{\theta} = D_R \dot{\theta}_R - D_L \dot{\theta}_L \quad (2)$$

where (x, y) is the coordinate of the robot center of mass, \dot{x} and \dot{y} are the velocities of this center along X and Y axes, respectively. θ denotes the orientation of the robot with respect to the initial position at the start point of the motion, and $\dot{\theta}$ is its derivatives with respect to time. D_R and D_L are the nominal diameters of the right and left wheels, respectively. Angular velocities of the right and left wheels are denoted by $\dot{\theta}_R$ and $\dot{\theta}_L$, respectively. The nominal distance between the two driving wheels is represented by l .

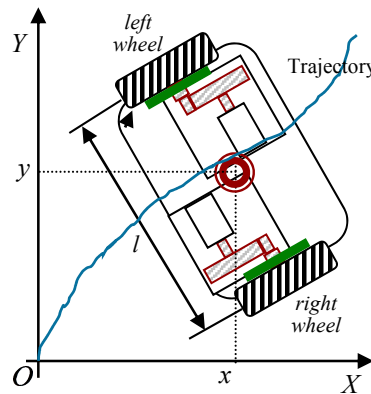


Figure 1. Reference frame of a two-wheeled mobile robot (revised from [2]).

In addition, considering the fact that the mobile robot cannot move in the lateral direction, the third equation is obtained as follows:

$$\dot{x} \sin \theta - \dot{y} \cos \theta = 0 \quad (3)$$

4. Proposed Odometry Technique

Figure 2 shows the test trajectory and needed parameters. As observed, the robot is programmed to travel along the path A, while regardless of the error sources, the robot follows path B [2,3]. The positional error has two components: lateral error and longitudinal error. Therefore, two corrective indices are defined to correct these two errors: lateral corrective factor and longitudinal corrective factor. The lateral corrective factor (F_{lat}) is applied to kinematic equations of robot to ensure that the robot stays along the desired trajectory. This factor presents the ratio of two angular velocities read from the encoders (the displacement over time) and is defined as below [2]:

$$F_{lat} = \frac{D_L}{D_R} + \frac{4l\lambda}{D_R \theta_L} \quad (4)$$

where,

$$\lambda = (D_R \theta_R - D_L \theta_L) / 4l \quad (5)$$

To compensate the longitudinal position error, the longitudinal corrective factor (F_{lon}) is defined as follows [2]:

$$F_{lon} = \frac{L}{\sqrt{(L - \delta x)^2 + (\delta y)^2}} \quad (6)$$

where L is the length of trajectory A. $\delta x = \sum_{j=1}^N x_{e,i}$ and $\delta y = \sum_{j=1}^N y_{e,i}$ are averages of the robot longitudinal and lateral errors over N number of trial runs [6].

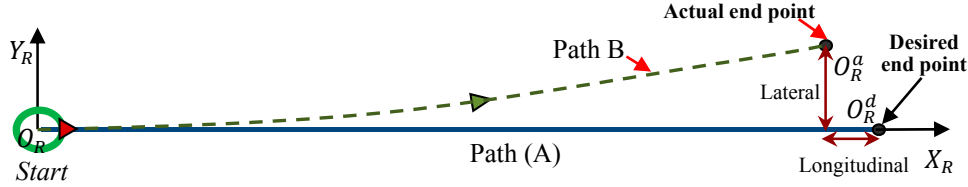
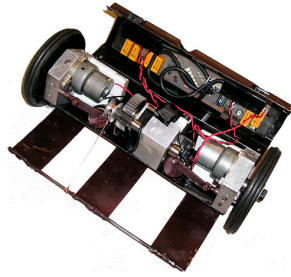


Figure 2. Trajectory taken by the differential drive WMR in the proposed technique.

5. Prototype WMR

This section describes a prototype mobile robots with a variety of components to examine the performance of the described benchmark techniques. Detailed description of the robot are given in [2]. The Jumper (two-wheeled) consists of two driving wheels, two stepping motors with gear boxes, two ultrasonic sensors and a wireless camera to detect the obstacles (Figure 3). Specifications of the robot are also shown in Figure 3.



Specifications	
Dimension (L × W × H) (cm)	10 × 10 × 22.5
Weight (kg)	0.880
Stall torque of motor (Nm)	0.2
Maximum linear speed (m/min)	0.115
Wheel radius (cm)	5.0
Wheelbase (cm)	10.5
Encoder resolution (pulse/rev)	48

Figure 3. Prototype two-wheeled mobile robot.

6. Results

The metric used to facilitate the comparison is the radial error (δr) as [2]:

$$\delta r = \sqrt{(\delta x)^2 + (\delta y)^2} \quad (7)$$

where δx and δy are the longitudinal and lateral errors (x_e and y_e in Figure 2). Effectiveness of each method is then measured by comparing the mean error improvement index (δr_m):

$$\delta r_m = \frac{\delta r_{m,b} - \delta r_{m,a}}{\delta r_{m,b}} (100\%) \quad (8)$$

In (8), $\delta r_{m,b}$ and $\delta r_{m,a}$ are the mean values of radial errors before and after calibration, respectively.

Figure 4 shows the position errors before and after calibration using the proposed method for the jumper robot. As seen, the motions of the robot were corrected with the method, i.e., the errors converged to the center of coordinate system (zero positional error). Statistical measures, to show the performance of the robot motion, are also reported in Figure 4.

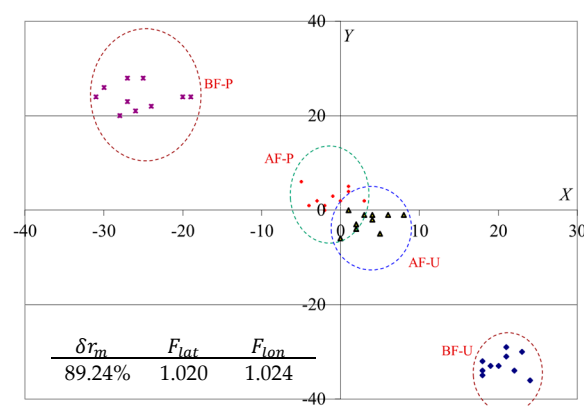


Figure 4. Radial systematic error of (left) jumper robot before and after calibration. BF and AF shows the locations of the robot stop point before and after calibration, respectively. The improvement measures are also shown in the figure.

7. Conclusions

Odometry errors in WMRs with differential drives are inevitable as they originates from hard to completely avoid imperfections such as unequal wheels diameters, misalignment at joints, backlash, slippage in encoder pulses and much more. The focus of this study was on introducing an odometry-based technique to correct the systematic errors of WMRs. A prototype differential drive mobile robot was constructed to evaluate the effectiveness of the developed method. Experimental results showed that the method was able to reduce the systematic errors by at least 83%.

Conflicts of Interest: The authors declare no conflict of interest.

References

1. Maddahi, Y.; Maddahi, A. Mobile robots experimental analysis based on kinematics. *WSEAS Trans. Circuits Syst.* **2004**, *3*, 1662–1667.
2. Maddahi, Y.; Sepehri, N.; Maddahi, A.; Abdolmohammadi, M. Calibration of wheeled mobile robots with differential drive mechanisms: an experimental approach. *J. Robot.* **2012**, *30*, 1029–1039.
3. Maddahi, Y.; Maddahi, A.; Sepehri, N. Calibration of omnidirectional wheeled mobile robots: Method and experiments. *J. Robot.* **2013**, *31*, 969–980.
4. Piaggio, M.; Sgorbissa, A.; Zaccaria, R. Navigation and localization for service mobile robots based on active beacons. *J. Syst. Sci.* **2001**, *27*, 71–83.
5. Rahok, S.A.; Koichi, O. Odometry correction with localization based on landmarkless magnetic map for navigation system of indoor mobile robot. In Proceedings of the 4th International Conference on Autonomous Robots and Agents, Wellington, New Zealand, 10–12 February 2009; pp. 572–577.
6. Nistér, D.; Naroditsky, O.; Bergen, J. Visual odometry for ground vehicle applications. *J. Field Robot.* **2006**, *23*, 3–20.
7. Borenstein, J.; Feng, L. Measurement and correction of systematic odometry errors in mobile robots. *IEEE Trans. Intell. Robot. Syst.* **1996**, *12*, 869–880.
8. Maddahi, Y.; Seddigh, M.; Pour, M.M.; Maleki, M. Simulation study and laboratory results of two-wheeled mobile robot. *WSEAS Trans. Syst.* **2004**, *3*, 2807–2812.



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