

RADIATION IN ENCLOSURES WITH SOME SPECULARLY REFLECTING SURFACES

- Exchange Factor
- Net Radiation Method
- Curved Specularly Reflecting Surfaces

Scope

optical roughness

long wavelength (infrared): specular
fashion

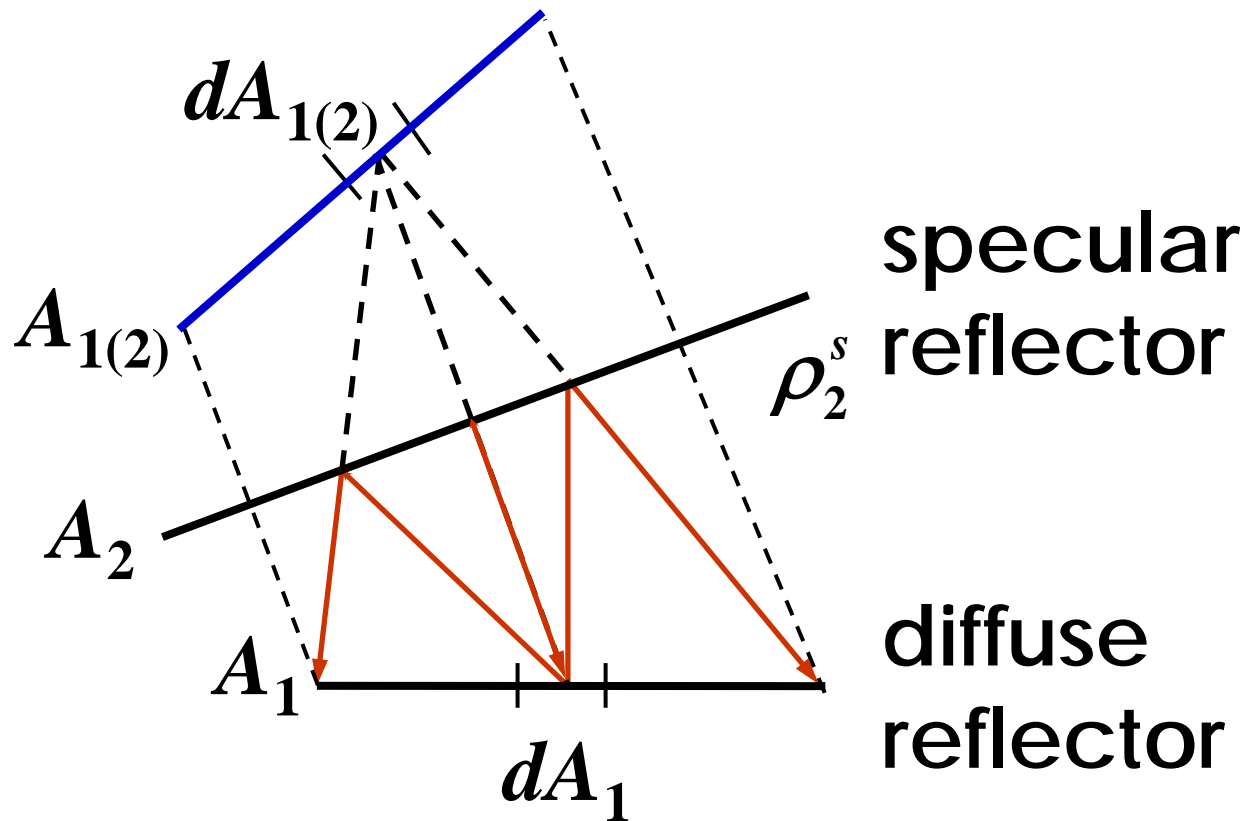
assumptions:

- 1) Specular reflectivity is independent of incident angle of radiation.
- 2) All surfaces are gray.

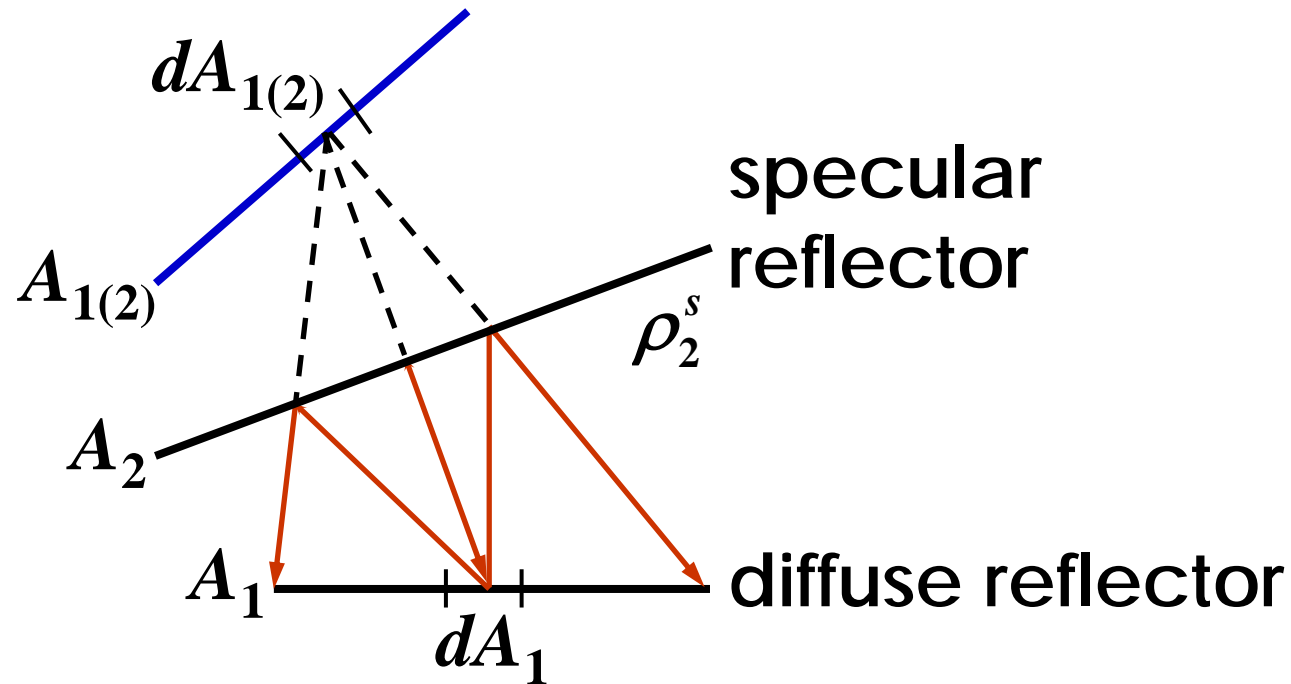
Exchange Factor

Specular view factor

Mirror-image method (Eckert & Sparrow 1965)



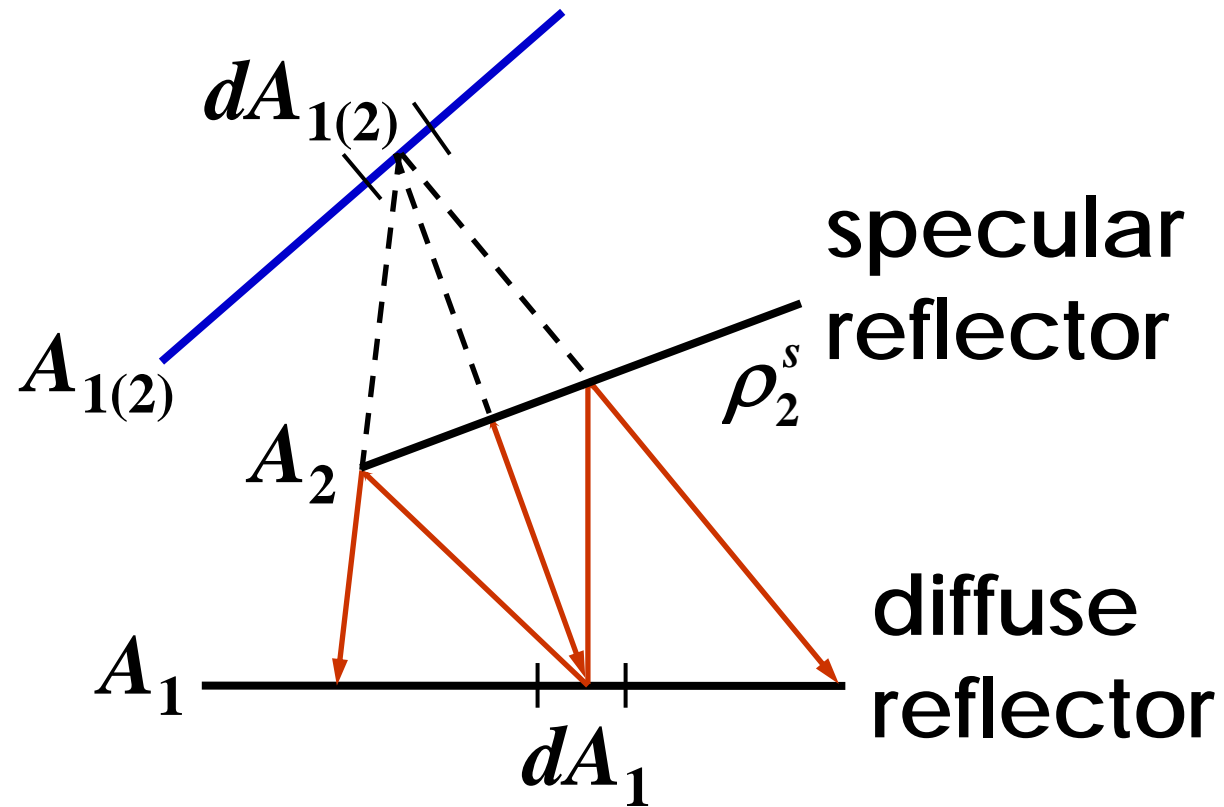
$dA_{1(2)}$: mirror image of dA_1 through A_2



When A_2 is a perfect specular reflector : $\rho_2^s = 1$

the fraction of radiation energy leaving dA_1
that strikes A_1 after one specular reflection
at A_2 : $F_{d1(2)-1}$

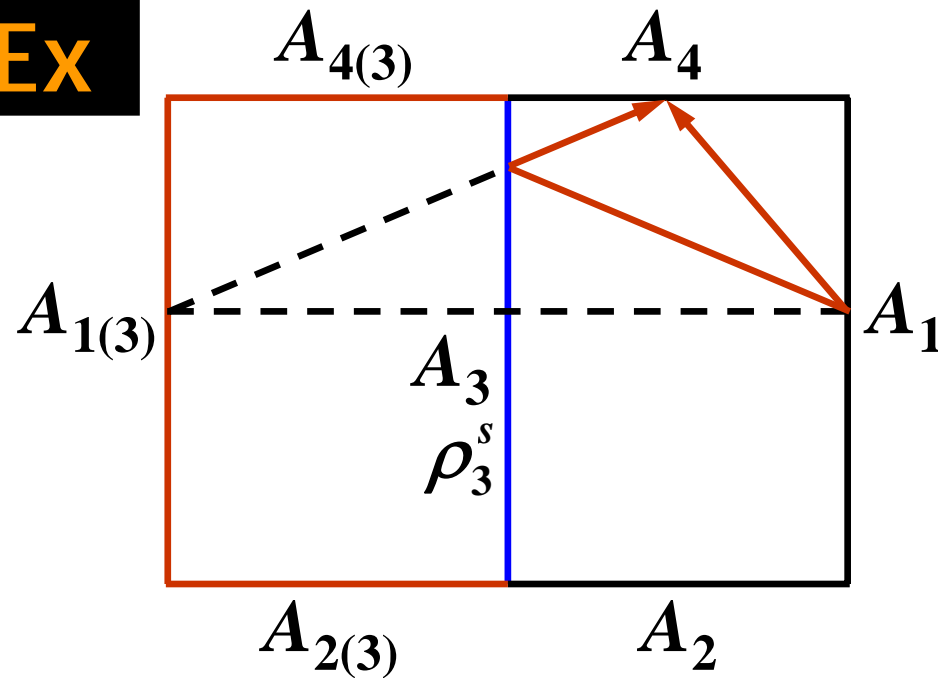
When $\rho_2^s \neq 1$: $\rho_2^s F_{d1(2)-1}$



fraction : $\rho_2^s F_{d1(2)-1}^*$

partial diffuse view factor

Ex



A_1, A_2, A_4 : diffuse

A_3 : specular

$$1 \rightarrow 4: E_{14} = F_{14} + \rho_3^s F_{1(3)-4}$$

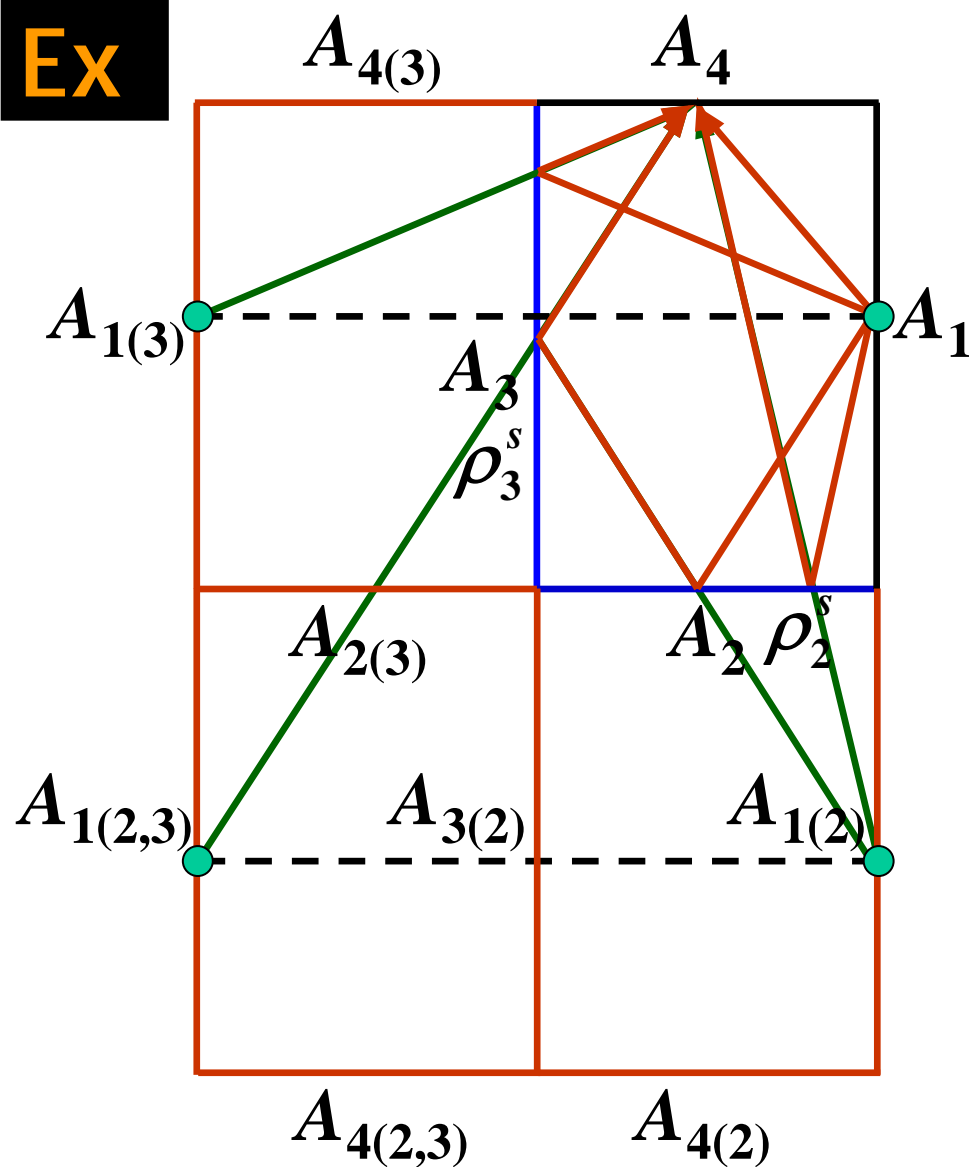
$$2 \rightarrow 4: E_{24} = F_{24} + \rho_3^s F_{2(3)-4}$$

$$1 \rightarrow 1: E_{11} = \rho_3^s F_{1(3)-1}$$

$$1 \rightarrow 2: E_{12} = F_{12} + \rho_3^s F_{1(3)-2}$$

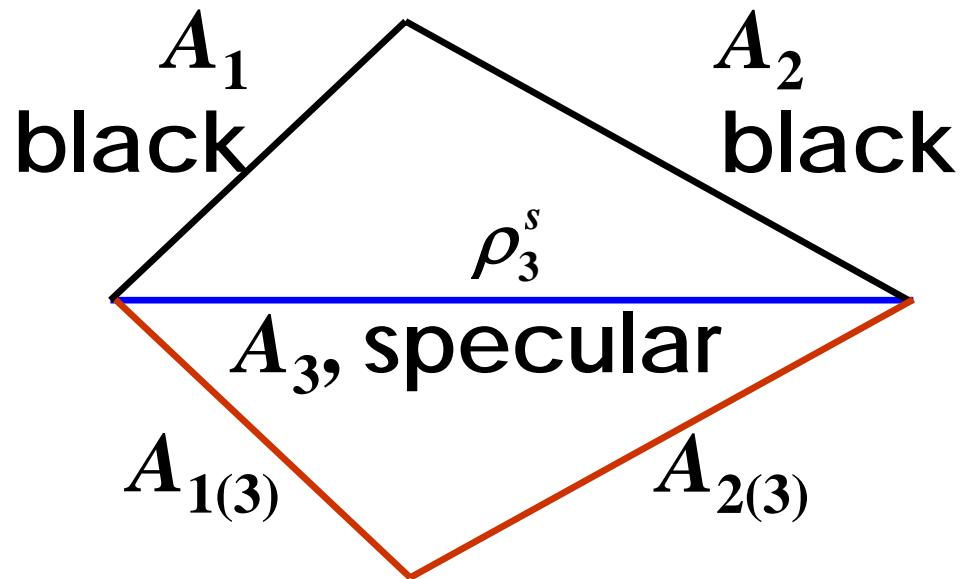
$$2 \rightarrow 1: E_{21} = F_{21} + \rho_3^s F_{2(3)-1}$$

Ex



$$\begin{aligned}
 E_{14} &= F_{14} + \rho_2^2 F_{1(2)-4} \\
 &\quad + \rho_3^2 F_{1(3)-4} \\
 &\quad + \rho_2^2 \rho_3^2 F_{1(2,3)-4}
 \end{aligned}$$

Reciprocity for specular surfaces



$$q_{1 \rightarrow 2} : 1) A_1 \rightarrow A_2,$$

$$2) A_1 \rightarrow A_3 \rightarrow A_2$$

$$q_{2 \rightarrow 1} : 1) A_2 \rightarrow A_1,$$

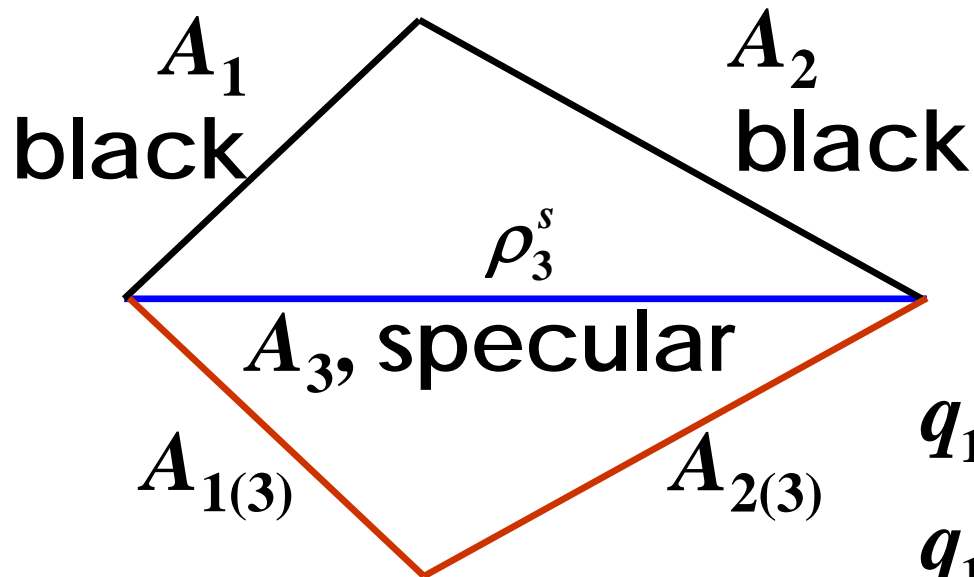
$$2) A_2 \rightarrow A_3 \rightarrow A_1$$

$$q_{1 \rightarrow 2} = \sigma T_1^4 A_1 \left(F_{12} + \rho_3^s F_{1(3)-2} \right)$$

$$q_{2 \rightarrow 1} = \sigma T_2^4 A_2 \left(F_{21} + \rho_3^s F_{2(3)-1} \right)$$

isothermal enclosure $q_{1 \rightarrow 2} = q_{2 \rightarrow 1}$

since $A_1 F_{12} = A_2 F_{21} \rightarrow A_1 F_{1(3)-2} = A_2 F_{2(3)-1}$



$$q_{1 \rightarrow 2} + q_{3 \rightarrow 2} = q_{2 \rightarrow 1} + q_{2 \rightarrow 3}$$

$$q_{1 \rightarrow 2} - q_{2 \rightarrow 1} = q_{2 \rightarrow 3} - q_{3 \rightarrow 2}$$

$$q_{2 \rightarrow 3} = \varepsilon_3 \sigma T_2^4 A_2 F_{23}$$

$$q_{3 \rightarrow 2} = \varepsilon_3 \sigma T_3^4 A_3 F_{32}$$

isothermal enclosure

$$q_{2 \rightarrow 3} = \varepsilon_3 \sigma T^4 A_2 F_{23}$$

$$q_{1 \rightarrow 2} = q_{2 \rightarrow 1}$$

$$q_{3 \rightarrow 2} = \varepsilon_3 \sigma T^4 A_2 F_{23}$$

Net Radiation Method

enclosure with n plane surfaces

d : diffuse reflecting surfaces

$n - d$: specularly reflecting surfaces

for diffuse surfaces: $1 \leq k \leq d$

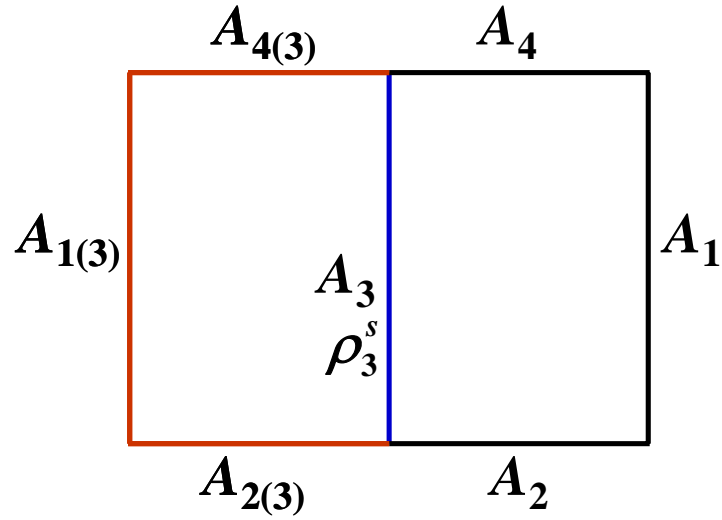
$$q_k'' = J_k - G_k \quad \text{or} \quad q_k'' = \frac{\varepsilon_k}{1 - \varepsilon_k} (\sigma T_k^4 - J_k)$$

$$J_k = \varepsilon_k \sigma T_k^4 + (1 - \varepsilon_k) G_k$$

for specular surfaces: $d + 1 \leq k \leq n$

$$q_k'' = \varepsilon_k (\sigma T_k^4 - G_k)$$

irradiation $G_k = \sum_{i=1}^d J_i E_{ki} + \sigma \sum_{i=d+1}^n \varepsilon_i T_i^4 E_{ki}$



$$G_k = \sum_{i=1}^d J_i E_{ki} + \sigma \sum_{i=d+1}^n \varepsilon_i T_i^4 E_{ki}$$

$$G_1 = J_1 E_{11} + J_2 E_{12} + J_4 E_{14} + \varepsilon_3 \sigma T_3^4 E_{13}$$

$$G_1 A_1 = J_1 A_1 \rho_3^s F_{1(3)-1}$$

$$+ J_2 A_2 \left(F_{21} + \rho_3^s F_{2(3)-1} \right)$$

$$+ J_4 A_4 \left(F_{41} + \rho_3^s F_{4(3)-1} \right)$$

$$+ \varepsilon_3 \sigma T_3^4 A_3 F_{31}$$

$$A_2 F_{21} = A_1 F_{12},$$

$$A_2 F_{2(3)-1} = A_1 F_{1(3)-2},$$

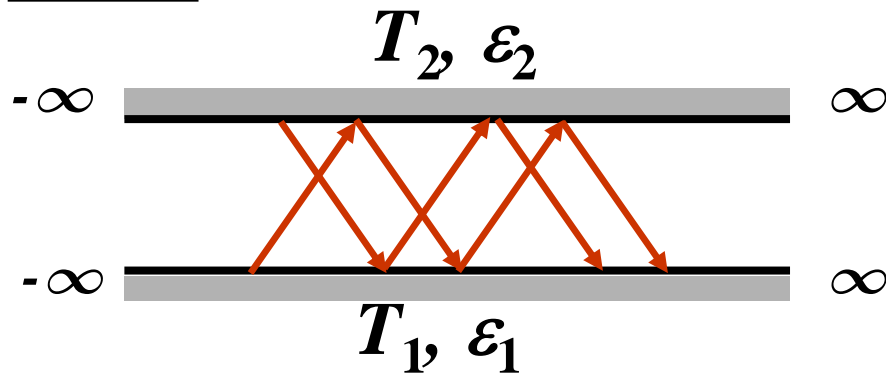
$$A_4 F_{4(3)-1} = A_1 F_{1(3)-4}, A_4 F_{41} = A_1 F_{14}, A_3 F_{31} = A_1 F_{13}$$

$$G_1 = J_1 \rho_3^s F_{1(3)-1} + J_2 \left(F_{12} + \rho_3^s F_{1(3)-2} \right)$$

$$+ J_4 \left(F_{14} + \rho_3^s F_{1(3)-4} \right) + \varepsilon_3 \sigma T_3^4 F_{13}$$

$$= J_1 E_{11} + J_2 E_{12} + J_4 E_{14} + \varepsilon_3 \sigma T_3^4 E_{13}$$

Ex parallel plates (both specular)



$$q_k'' = \varepsilon_k (\sigma T_k^4 - G_k)$$

$$G_k = \sum_{i=1}^d J_i E_{ki} + \sigma \sum_{i=d+1}^n \varepsilon_i T_i^4 E_{ki}$$

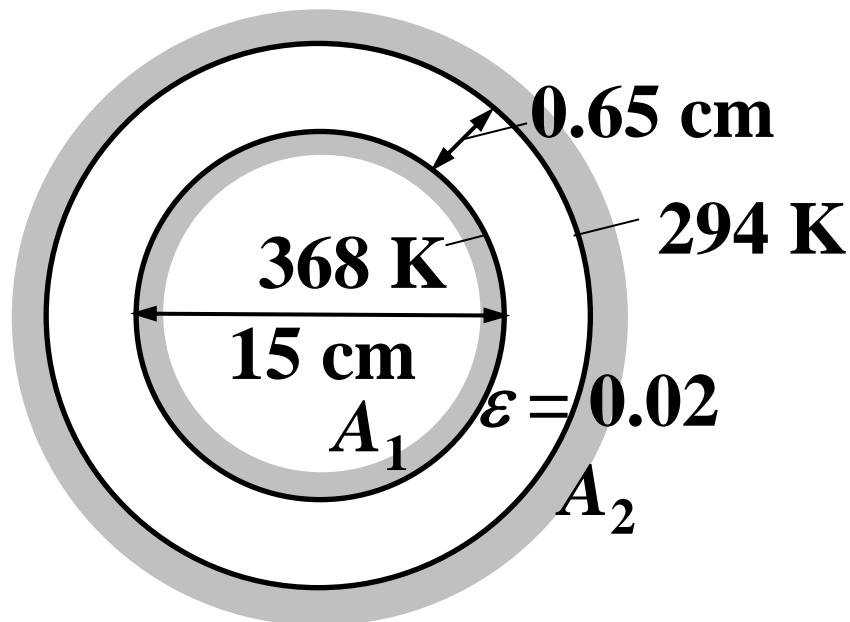
$$q_1'' = \varepsilon_1 (\sigma T_1^4 - G_1), \quad G_1 = \sigma [\varepsilon_1 T_1^4 E_{11} + \varepsilon_2 T_2^4 E_{12}]$$

$$E_{11} = \rho_2^s F_{1(2)-1} + (\rho_2^s)^2 (\rho_1^s) F_{1(2,1,2)-1} + (\rho_2^s)^3 (\rho_1^s)^2 F_{1(2,1,2,1,2)-1} + \dots = \frac{\rho_2^s}{1 - \rho_1^s \rho_2^s}$$

$$E_{12} = F_{12} + \rho_1^s \rho_2^s F_{1(1,2)-2} + (\rho_1^s)^2 (\rho_2^s)^2 F_{1(1,2,1,2)-2} + \dots$$

$$= \frac{1}{1 - \rho_1^s \rho_2^s}$$

$$q_1'' = \frac{\sigma (T_1^4 - T_2^4)}{\frac{1}{\varepsilon_1} + \frac{1}{\varepsilon_2} - 1}$$

Ex 9-1**spherical vacuum bottle**

specular: $q_1 = \frac{A_1 \sigma (T_1^4 - T_2^4)}{\frac{1}{\varepsilon_1} + \frac{1}{\varepsilon_2} - 1}$

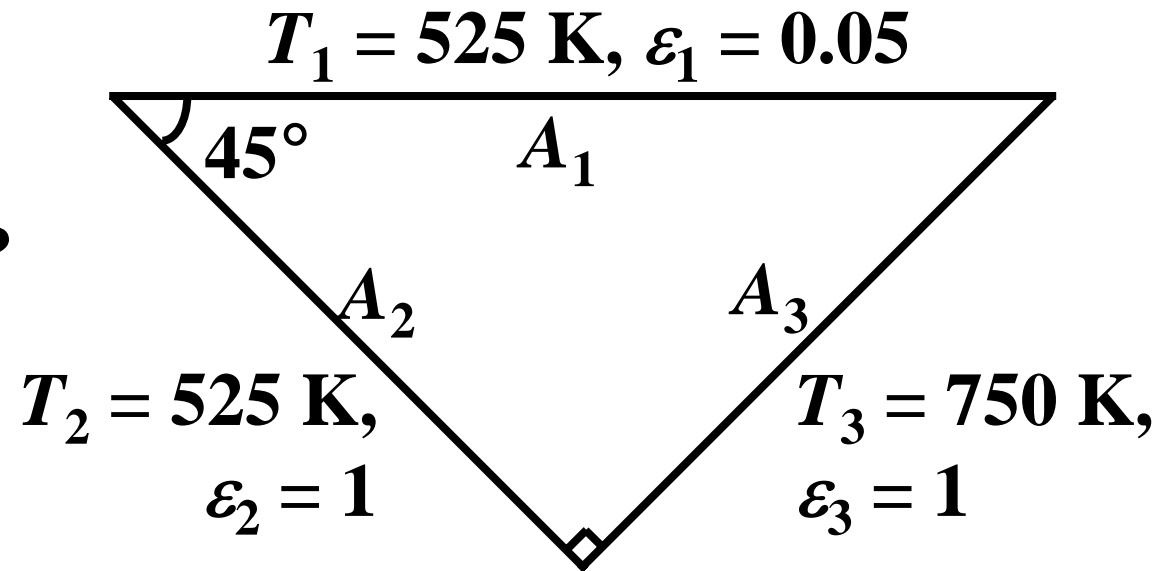
diffuse: $q_1 = \frac{A_1 \sigma (T_1^4 - T_2^4)}{\frac{1}{\varepsilon_1} + \frac{A_1}{A_2} \left(\frac{1}{\varepsilon_2} - 1 \right)}$

specular: $q_1 = \frac{\pi (0.15)^2 \times 5.671 \times 10^{-8} (368^4 - 294^4)}{\frac{1}{0.02} + \frac{1}{0.02} - 1} = 0.440 \text{ W}$

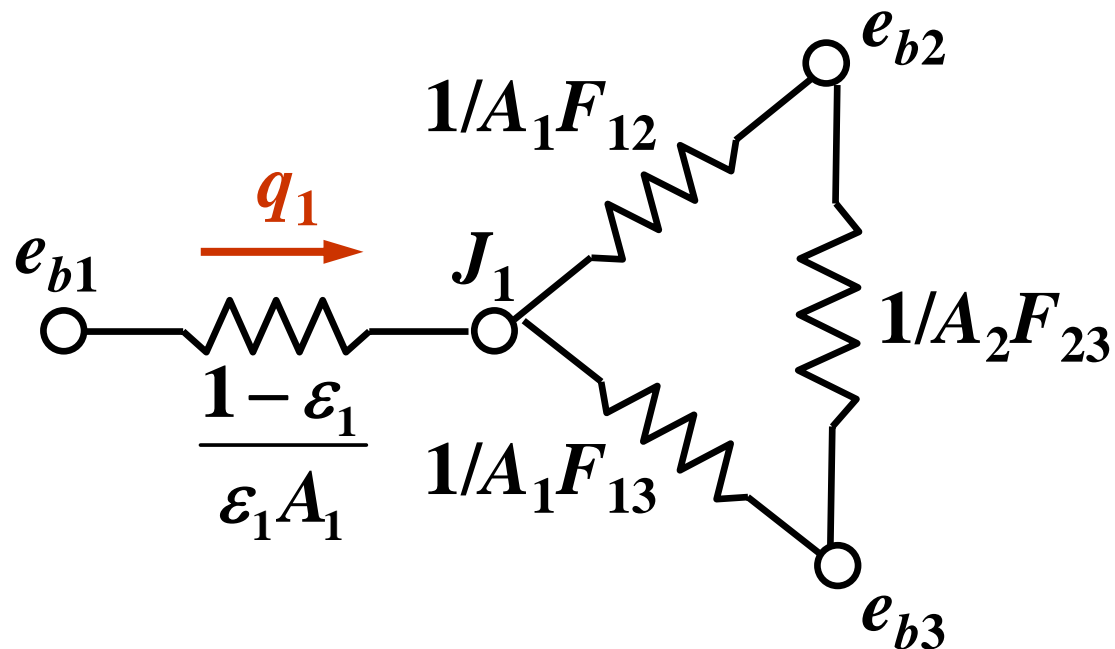
diffuse: $q_1 = \frac{\pi (0.15)^2 \times 5.671 \times 10^{-8} (368^4 - 294^4)}{\frac{1}{0.02} + \left(\frac{15}{16.3} \right)^3 \left(\frac{1}{0.02} - 1 \right)} = 0.476 \text{ W}$

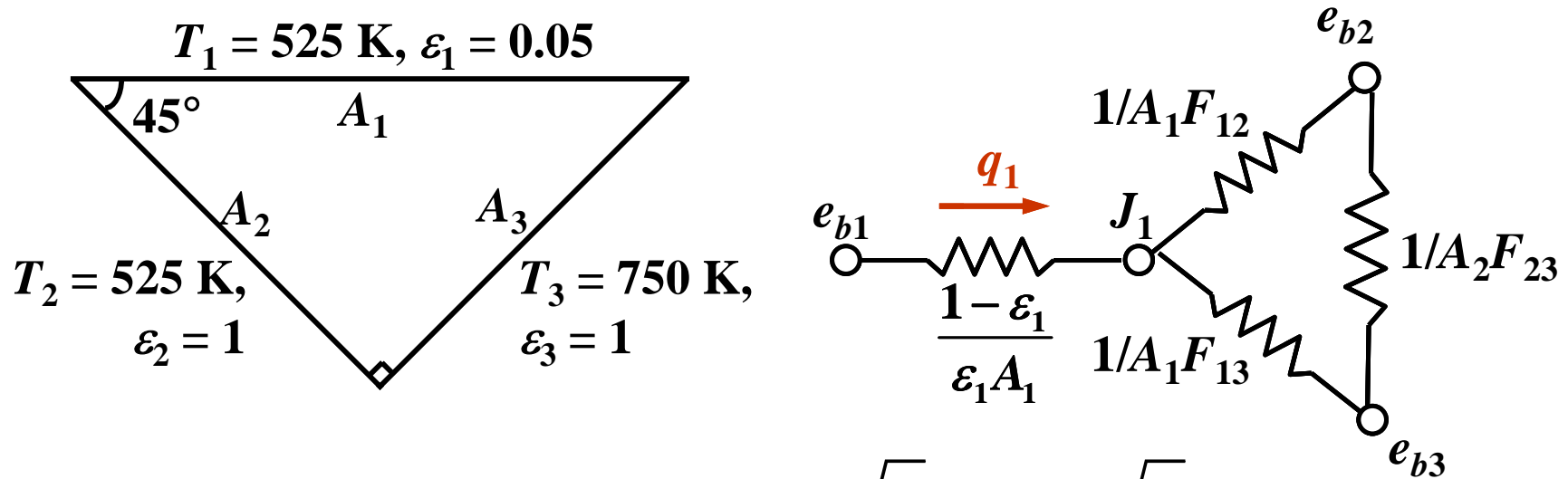
Ex 9-6

$$q_1, q_2, q_3 = ?$$



a) surface 1 : diffuse reflector





$$F_{12} = F_{13} = \frac{1}{2}, \quad F_{23} = \frac{1+1-\sqrt{2}}{2} = \frac{2-\sqrt{2}}{2}$$

$$q_1 = \frac{\sigma T_1^4 - J_1}{\frac{1-\varepsilon_1}{\varepsilon_1 A_1}} = \frac{J_1 - \sigma T_2^4}{\frac{1}{A_1 F_{12}}} + \frac{J_1 - \sigma T_1^4}{\frac{1}{A_1 F_{13}}}$$

$$q_1 = -144.6 \text{ W}, \quad q_2 = -2571.8 \text{ W}, \quad q_3 = 2716.4 \text{ W}$$

b) surface 1 : specular

$$q_1 = \varepsilon_1 A_1 (\sigma T_1^4 - G_1)$$

$$G_1 = J_2 E_{12} + J_3 E_{13} + \varepsilon_1 \sigma T_1^4 E_{11}$$

$$E_{12} = F_{12}, \quad E_{13} = F_{13}, \quad E_{11} = 0$$

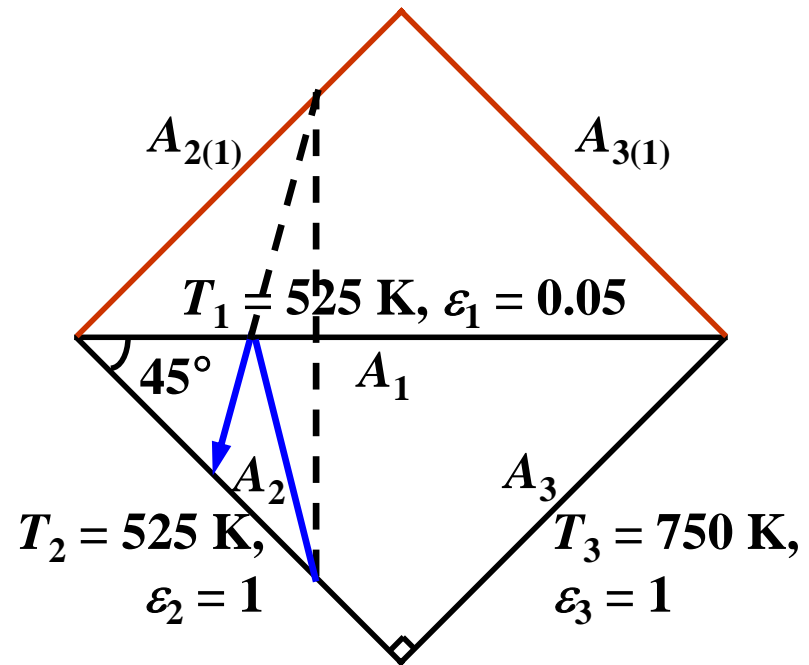
$$J_2 = \sigma T_2^4, \quad J_3 = \sigma T_3^4$$

$$q_1 = \varepsilon_1 A_1 (\sigma T_1^4 - \sigma T_2^4 F_{12} - \sigma T_3^4 F_{13}) = -144.6 \text{ W}$$

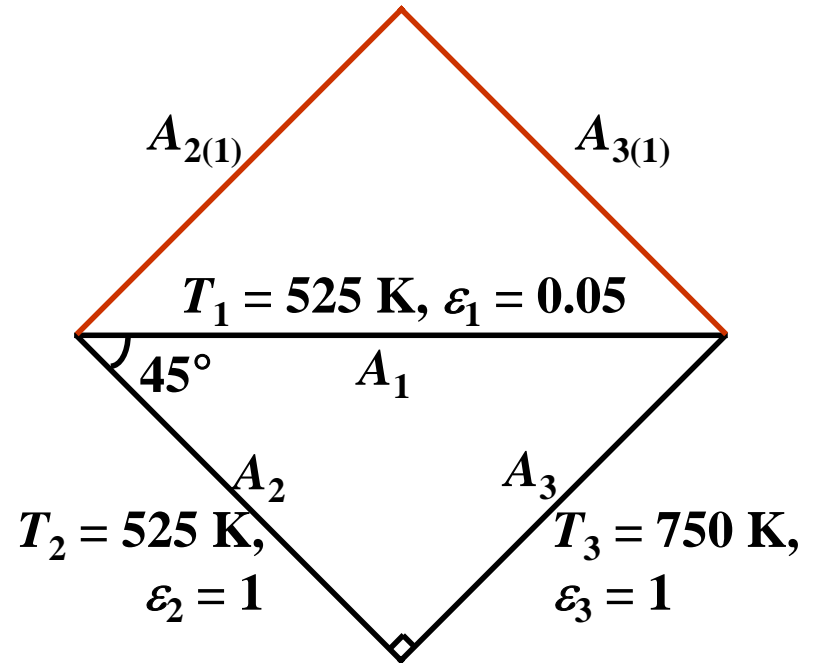
$$q_2 = A_2 (\sigma T_2^4 - G_2)$$

$$G_2 = J_2 E_{22} + J_3 E_{23} + \varepsilon_1 \sigma T_1^4 E_{21}$$

$$E_{22} = \rho_1^s F_{2(1)-2}, \quad E_{23} = F_{23} + \rho_1^s F_{2(1)-3}, \quad E_{21} = F_{21}$$



$$F_{2(1)-2} = \frac{2 - \sqrt{2}}{2}, \quad F_{2(1)-3} = \sqrt{2} - 1$$



$$q_2 = A_2 \left[\sigma T_2^4 - \sigma T_2^4 \rho_1^S F_{2(1)-2} \right.$$

$$\left. - \sigma T_3^4 (F_{23} + \rho_1^S F_{2(1)-3}) - \varepsilon_1 \sigma T_1^4 F_{21} \right] = -2807.5 \text{ W}$$

$$q_1 + q_2 + q_3 = 0 \rightarrow q_3 = 2952.1 \text{ W}$$

$$q_1 = -144.6 \text{ W}, \quad q_2 = -2807.5 \text{ W}, \quad q_3 = 2952.1 \text{ W}$$

$$q_1 = -144.6 \text{ W}, \quad q_2 = -2571.8 \text{ W}, \quad q_3 = 2716.4 \text{ W}$$

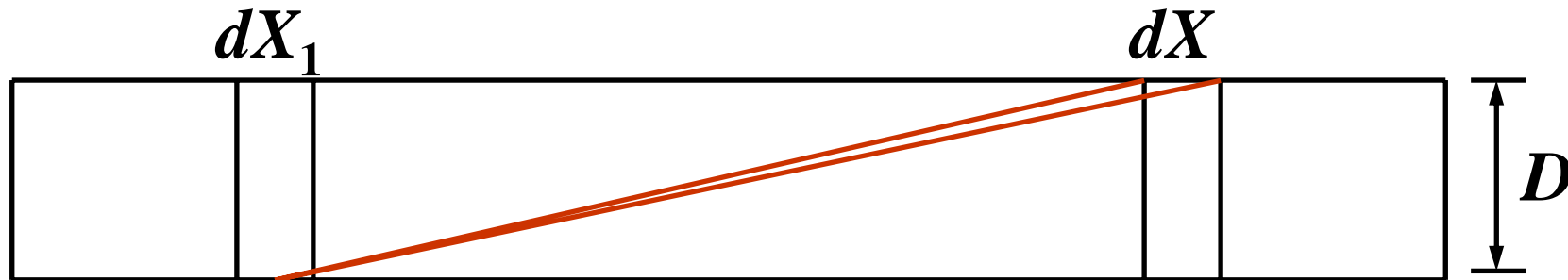
Curved Specularly Reflecting Surface

Ex specular tube

$$K(\xi, \eta) = 1 - \frac{|\eta - \xi|^3 + \frac{3}{2}|\eta - \xi|}{\left[(\eta - \xi)^2 + 1\right]^{3/2}}$$

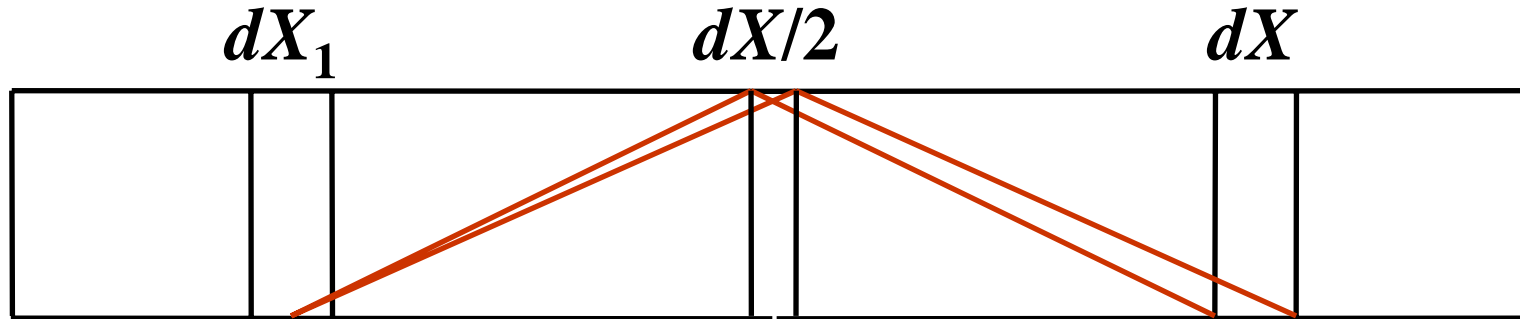
Let $X/D = |\eta - \xi|$

1) direct:



$$dF_{dX_1-dX} = \left\{ 1 - \frac{(X/D)^3 + 3X/2D}{\left[(X/D)^2 + 1\right]^{3/2}} \right\} dX$$

2) one-reflection:



$$dF_{dX_1 - \frac{dX}{2}} = \left\{ 1 - \frac{\left(\frac{X}{2D} \right)^3 + 3X / 4D}{\left[\left(\frac{X}{2D} \right)^2 + 1 \right]^{3/2}} \right\} \frac{dX}{2}$$

3) n reflection:

$$dF_{dX_1 - \frac{dX}{n+1}} = \left\{ 1 - \frac{\left[\frac{X}{(n+1)D} \right]^3 + 3X / 2(n+1)D}{\left\{ \left(\frac{X}{(n+1)D} \right)^2 + 1 \right\}^{3/2}} \right\} \frac{dX}{n+1}$$

$$dE_{dX_1 - dX} = \sum_{n=0}^{\infty} (\rho^s)^n dF_{dX_1 - dX / (n+1)}$$